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P U F F 2

Determination of Multigroup Covariance Matrices
from ENDF/B-V Uncertainty Files

Contributed by
Oak Ridge National Laboratory
Oak Ridge, Tennessee 37830

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MULTIGROUP COVARIANCE MATRICES FOR
FAST REACTOR STUDIES

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ABSTRACT

This report presents the multigroup covariance matrices based on the ENDF/B-V nuclear data evaluations. The materials and reactions have been chosen according to the specifications of ORNL-5517. Several cross section covariances, other than those specified by that report, are included due to the derived nature of the uncertainty files in ENDF/B-V.

The materials represented are Ni, Cr, O-16, C-12, Fe, Na, U-235, U-238, Pu-239, Pu-240, Pu-241, and B-10 (present due to its correlation to U-238). The data have been originally processed into a 52-group energy structure by PUFF-II and subsequently collapsed to smaller subgroup structures. The results are illustrated in 52-group correlation matrix plots and tabulated into thirteen groups for convenience.

The multigroup covariance files are available from the Engineering Physics Information Center (EPIC) in a COVERX format. A service module to the COVERX format is also available.

Although ENDF/B-V uncertainty information represents much more material than the previous version, some valuable covariances may not be present. To fill this void, internally generated uncertainty information from ORNL may yet be added to the covariance library in order to satisfy the requirements of the cross section adjustment specifications of ORNL-5517.

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1. DESCRIPTION OF COVARIANCE MATRIX GENERATION

Standard formats and procedures have been established within the ENDF/B system^{1,2} for the processing of evaluated and correlated energy-dependent uncertainty information into a multigroup covariance matrix formulation. These covariance matrices were established to be used in conjunction with sensitivity studies to: (1) propagate uncertainties to final calculated results, (2) adjust data sets by incorporating information from some integral measurements, and (3) determine data accuracies needed to meet targeted uncertainties in results taking into account the correlations in uncertainties in the present data sets.²

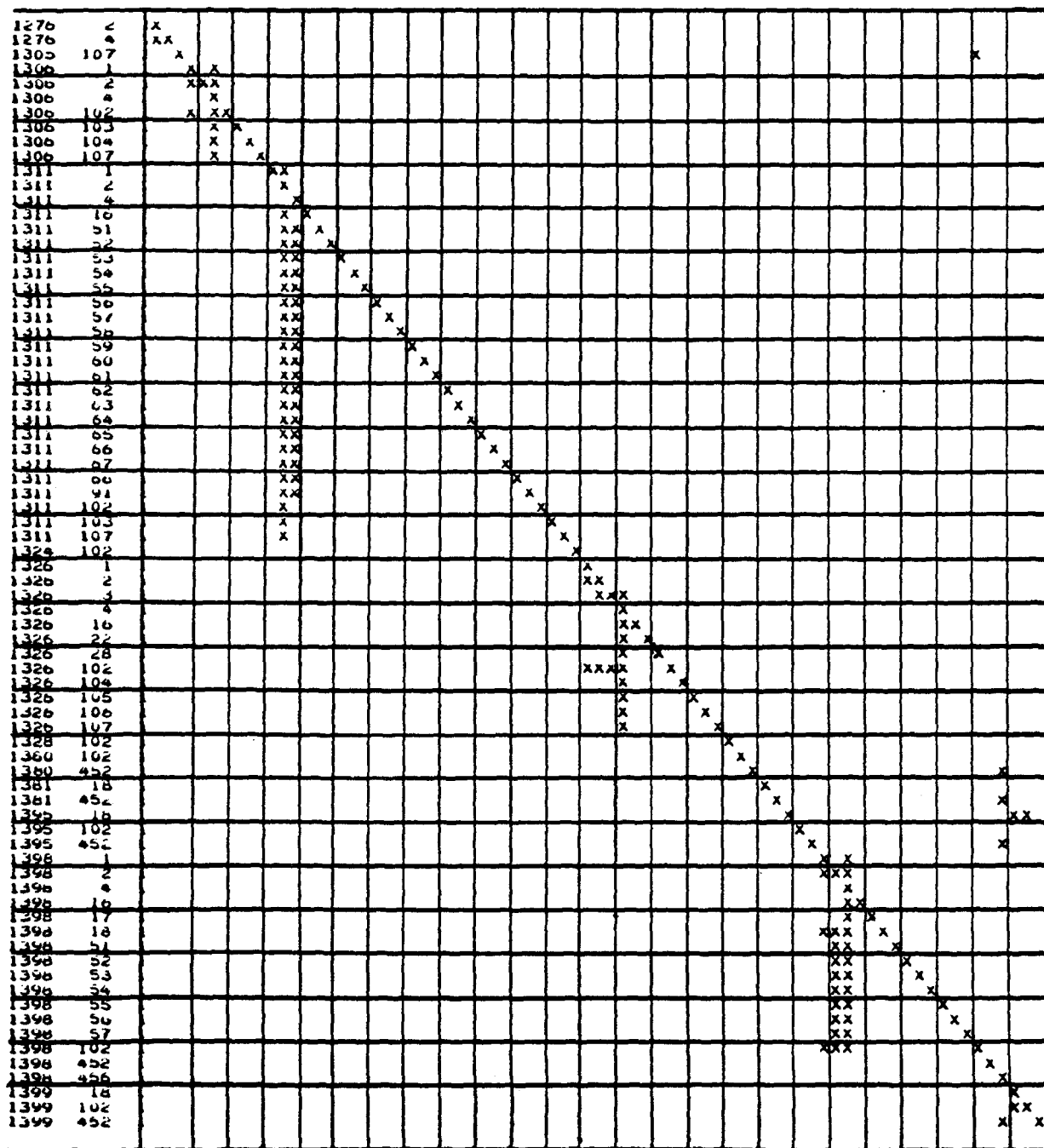
ENDF/B-IV contained uncertainties for N, O, and C only. Uncertainties for several other materials were generated for in-house use at ORNL.³ ENDF/B-V (see Table 1) contains uncertainties for many more materials and also includes uncertainties in $\bar{\nu}(E)$ and in resolved resonance parameters.

This report contains uncertainties and correlations for materials needed as specified in ORNL/TM-5517⁴ for cross section adjustment. These materials are Ni, Cr, O-16, C-12, Fe, Na, Pu-239, Pu-240, Pu-241, U-235, U-238 and B-10 (needed for correlation to U-238 (n, γ)). The covariance matrices that have been produced are summarized in Fig 1 by MAT-MT numbers with MAT and MT designations keyed in Tables 1 and 2.

The data have been processed into a 52-group energy structure by PUFF-II⁵. PUFF-II, which processes uncertainty data in ENDF/B-V formats, is the sequel to the ORNL uncertainty processor PUFF, which processes uncertainty data in ENDF/B-IV formats. The 52-group energies are a subset of the VITAMIN-E-174-group energies.⁶ The 52-group structure was chosen to be large enough that little information currently present in ENDF/B-V would be lost yet small enough to not be cumbersome to handle. The 52-group energy structure is shown in Table 3.

PUFF-II (unlike PUFF) is not an integral part of the multigroup cross section processor MINX. Thus, an additional input of multigroup reactions is required (see Section III). The multigroup cross sections used in producing this multigroup covariance library were taken from a 100-group

MAT MT



(Note that the horizontal order of MAT-MT number pairs is the same as in the vertical listing)

Fig. 1. Covariance Matrices for Fast Reactor Studies

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Table 1. Materials Present in
Multigroup Covariance Library

Material	MAT, MOD	Authors	Institution
0-16	1276, 0	Young, P. Foster, D. Jr., Hale, G. Identical to Version IV except error files to ENDF-V form Eval - 8/73, Rev 0 - 6/75, Dist 12/78	LASL
B-10	1305, 0	Hale, G, Stewart, L., Young, P Eval - 12/76, Rev 1 - 1/77, Dist - 5/79	LASL
C-12	1306, 1	Fu, C. Y., Perey, F. G. Eval - 12/73, Rev 1 - 1/77, Dist - 5/79	ORNL
Na	1311, 0	Larson, D. C. Eval - 12/77, Dist - 12/78	ORNL
Cr	1324,	Prince, A., Burrows, T. W. Eval - 12/77, Dist - 1/79	BNL
Fe	1326, 1	Fu, C. Y., Perey, F. G. Eval - 10/77, Rev 1 - 10/77, Dist - 4/79	ORNL
Ni	1328, 0	Divadeenam, M. Eval - 3/77, Dist - 1/79	BNL
Pu-240	1380, 0	Weston, L. W. Eval - 4/77, Dist - 5/79	ORNL
Pu-241	1381, 0	Weston, L. W., Wright, R. Q. Howerton, R. Eval - 10/77, Dist - 5/79	ORNL
U-235	1395, 1	Bhat, M. R. Eval - 4/77, Rev 1 - 11/77, Dist - 5/79	BNL
U-238	1398,	Howerton, R (LLL) Gamma Prod. Files Pennington, E., Smith, A., Poenitz, H. Eval - 6/77, Rev 3 - 3/79, Dist - 5/79	ANL
Pu-239	1399,	Kujawski, E., Stewart, L. (LASL) Eval - 10/76, Rev 0 - 10/76, Dist - 5/79	GE-FBRD

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Table 2. Reactions Present in Multigroup Covariance Library

MT	Description
1	Total cross section (total)
2	Elastic scattering cross section (elastic)
3	Nonelastic cross section (nonelastic)
4	Total inelastic cross section (n,n')
16	Direct (n,2n) cross section
17	(n,3n) cross section
18	Total fission cross section (n,f)
22	(n,n' α) cross section
28	(n,n'p) cross section
51	(n,n') to the first excited state (n,n', 1st)
52	(n,n') to the second excited state (n,n', 2nd)
•	
•	
•	
68	(n,n') to the 18th excited state (n,n, 18th)
91	(n,n') to the continuum. (n,n', cont.)
102	(n, γ) radiative capture cross section
103	(n,p) cross section
104	(n,d) cross section
105	(n,t) cross section
106	(n, ^3He) cross section
107	(n, α) cross section
452	$\bar{\nu}$, average total (prompt plus delayed) number of neutrons released per fission event ($\bar{\nu}$)
456	prompt neutrons from fission ($\bar{\nu}_p$)

Table 3. The 52-energy group structure on which the covariance matrices were produced. Also shown is the 13-group structure proposed by ORNL-5517 (where the highest energy boundary was changed to agree with VITAMIN-E).

Group	Upper Energy	Group	Upper Energy
1	1.9640E+07 *	27	2.4788E+04 *
2	1.3499E+07	28	2.3579E+04
3	1.0000E+07 *	29	1.5034E+04
4	7.7880E+06	30	1.1709E+04
5	6.0653E+06	31	9.1188E+03 *
6	4.7237E+06	32	7.1017E+03
7	3.6788E+06 *	33	5.5308E+03
8	2.8650E+06	34	4.3074E+03
9	2.2313E+06	35	3.3546E+03 *
10	1.6530E+06	36	2.6126E+03
11	1.3534E+06 *	37	2.0347E+03
12	1.0026E+06	38	1.5846E+03
13	8.2085E+05	39	1.2341E+03 *
14	6.0810E+05	40	9.6112E+02
15	4.9787E+05 *	41	7.4852E+02
16	3.8774E+05	42	5.8295E+02
17	3.0197E+05	43	4.5400E+02 *
18	2.3518E+05	44	3.5358E+02
19	1.8316E+05 *	45	2.7536E+02
20	1.4264E+05	46	1.6702E+02
21	1.1109E+05 *	47	1.0130E+02
22	8.6517E+04	48	6.1442E+01
23	6.7379E+04 *	49	3.7267E+01
24	5.2475E+04	50	2.2603E+01
25	4.0868E+04	51	1.3710E+01
26	3.1828E+04	52	8.3153E+00
		thermal	1.0000E-05 *

* indicates 13-group energy boundaries

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fast reactor data testing library, requested by GE, appropriate for analysis of fast reactor benchmarks.⁷ The 100-group energies are a subset of the VITAMINE-E 174-group energies (and the 52-group energies are a subset of the 100-group energies). The VITAMIN-E weighting function collapsed to 100 group was used as the weighting spectrum input to PUFF-II. The 100-group energy structure and weighting function can be seen in Table 4. The VITAMIN-E weighting function is shown in Table 5.

The multigroup covariance matrices have been processed into a COVERX⁸ format for easy use and manageability. The COVERX format is the format for multigroup covariance matrices used in the FORSS⁹ system. COVERX has been proposed to the CCCC for acceptance and is described in Appendix A. A sample COVERX data file is tabulated in Appendix B. Auxiliary routines for reading, writing, editing and collapsing these data are available in a COVERX service module.¹⁰

References to the uncertainty and cross section data used in production of this multigroup covariance library are given in Appendices C, D, and E. All calculations were performed using a PDP-10 computer at the Oak Ridge National Laboratory. The PUFF-II code is also operational on IBM computers. The necessary user input to the IBM version is contained in Appendix F. The multigroup covariance library and IBM version of PUFF-II are available through the Radiation Shielding Information Center (RSIC) at ORNL.

1). EVALUATED COVARIANCE FORMULATION

The covariance representations permitted by ENDF/B-V formats:²

LB = 0 Absolute components only correlated within each E_k interval

$$\text{COV}(X_i, Y_j) = \sum_k p_{j;k}^{i;k} F_{xy,k} \quad (1)$$

LB = 1 Fractional components only correlated within each E_k interval

$$\text{COV}(X_i, Y_j) = \sum_k p_{j;k}^{i;k} F_{xy,k} X_i Y_j \quad (2)$$

Table 4. 100-Energy Group Structure and Corresponding Weighting Function

	Upper Energy	Weighting Function		Upper Energy	Weighting Function
1	1.964032E+07	2.199371E+01	36	2.984913E+05	4.299000E-03
2	1.349858E+07	1.417282E+00	37	2.972105E+05	9.098999E-03
3	1.000000E+07	1.842999E-02	38	2.945181E+05	2.500000E-02
4	7.788007E+06	4.979799E-02	39	2.872466E+05	5.000000E-02
5	6.065306E+06	1.000399E-01	40	2.732374E+05	9.999996E-02
6	4.723665E+06	1.529229E-01	41	2.472353E+05	5.000000E-02
7	3.678794E+06	2.109699E-01	42	2.351774E+05	5.000000E-02
8	2.865048E+06	1.431599E-01	43	2.237079E+05	9.999996E-02
9	2.465970E+06	3.276000E-02	44	2.024192E+05	9.999996E-02
10	2.385207E+06	8.305999E-03	45	1.831564E+05	9.999996E-02
11	2.365253E+06	8.214999E-03	46	1.657268E+05	9.999996E-02
12	2.345703E+06	4.972000E-02	47	1.499558E+05	5.000000E-02
13	2.231301E+06	9.993994E-02	48	1.426423E+05	5.000000E-02
14	2.018966E+06	9.999996E-02	49	1.356857E+05	9.999996E-02
15	1.826835E+06	9.999996E-02	50	1.227734E+05	9.999996E-02
16	1.652989E+06	9.999996E-02	51	1.110899E+05	2.500000E-01
17	1.495686E+06	9.999996E-02	52	8.651694E+04	4.750000E-02
18	1.353352E+06	9.999996E-02	53	8.250344E+04	3.710000E-02
19	1.224564E+06	9.999996E-02	54	7.949869E+04	9.909999E-02
20	1.108031E+06	9.999996E-02	55	7.199813E+04	6.629997E-02
21	1.002589E+06	4.170000E-02	56	6.737944E+04	2.499999E-01
22	9.616404E+05	5.830000E-02	57	5.247518E+04	2.500000E-01
23	9.071797E+05	9.999996E-02	58	4.086770E+04	2.499999E-01
24	8.208501E+05	9.999996E-02	59	3.182780E+04	1.104000E-01
25	7.427364E+05	9.999996E-02	60	2.850105E+04	5.410000E-02
26	6.720554E+05	9.999996E-02	61	2.700011E+04	3.550000E-02
27	6.081011E+05	9.999996E-02	62	2.605841E+04	5.000000E-02
28	5.502324E+05	9.999996E-02	63	2.478752E+04	2.500000E-02
29	4.978706E+05	9.999996E-02	64	2.417552E+04	2.500000E-02
30	4.504923E+05	9.999996E-02	65	2.357864E+04	2.000000E-01
31	4.076221E+05	5.000000E-02	66	1.930454E+04	2.500000E-01
32	3.877421E+05	5.000000E-02	67	1.503439E+04	2.500000E-01
33	3.688319E+05	9.999996E-02	68	1.170880E+04	2.500000E-01
34	3.337328E+05	9.999996E-02	69	9.118816E+03	2.500000E-01
35	3.019738E+05	1.160000E-02	70	7.101742E+03	2.500000E-01

(continued)

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Table 4 (Cont'd)

	Upper Energy	Weighting Function
71	5.530840E+03	2.500000E-01
72	4.307422E+03	1.500000E-01
73	3.707437E+03	9.999996E-02
74	3.354626E+03	9.998996E-02
75	3.035392E+03	9.999996E-02
76	2.746535E+03	5.000000E-02
77	2.612535E+03	5.000000E-02
78	2.485169E+03	9.999996E-02
79	2.248674E+03	9.999996E-02
80	2.034684E+03	2.500000E-01
81	1.584613E+03	2.500000E-01
82	1.234098E+03	2.500000E-01
83	9.611165E+02	2.500000E-01
84	7.485183E+02	2.500000E-01
85	5.829465E+02	2.500000E-01
86	4.539990E+02	2.500000E-01
87	3.535750E+02	2.500000E-01
88	2.753643E+02	5.000000E-01
89	1.670170E+02	5.000000E-01
90	1.013009E+02	5.000000E-01
91	6.144212E+01	5.000000E-01
92	3.726653E+01	5.000000E-01
93	2.260329E+01	5.000000E-01
94	1.370959E+01	5.000000E-01
95	8.315287E+00	5.000000E-01
96	5.043476E+00	5.000000E-01
97	3.059023E+00	5.000000E-01
98	1.855391E+00	5.000000E-01
99	1.125351E+00	5.000000E-01
100	6.825604E-01	3.518850E+04
Thermal	1.000000E-05	

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Table 5. Weighting Function Used for Processing
VITAMIN-E Cross Sections

Functional Form	Energy Limits
1) Maxwellian Thermal Spectrum $W_1(E) = C_1 E e^{-E/kT}$	10^{-5} eV to 0.414 eV
2) "1/E" Slowing-Down Spectrum $W_2(E) = C_2/E$	0.414 eV to 2.12 MeV
3) Fission Spectrum ($\theta = 1.415$ MeV) $W_3(E) = C_3 E^{1/2} e^{-E\theta}$	2.12 MeV to 10.0 MeV
4) "1/E" Spectrum $W_4(E) = C_4/E$	10.0 MeV to 12.52 MeV
5) Velocity Exponential Fusion Peak ($E_p = 14.07$ MeV) ($kT = 0.025$ MeV) $W_5(E) = C_5 \exp \left\{ -\frac{5}{kT} (E^{1/2} - E_p^{1/2})^2 \right\}$	12.52 MeV to 15.68 MeV
6) "1/E" Spectrum $W_6(E) = C_6/E$	15.68 MeV to 19.64 MeV

LB = 2 Fractional components correlated over all E_k intervals

$$\text{COV}(X_i, Y_j) = \sum_{k, k'} p_{j; k'}^{i; k} F_{xy, k} F_{xy, k'} X_i Y_j \quad (3)$$

LB = 3 Fractional components correlated over E_k and E_l intervals

$$\text{COV}(X_i, Y_j) = \sum_{k, l} p_{j; l}^{i; k} F_{x, k} F_{y, l} X_i Y_j \quad (4)$$

LB = 4 Fractional components correlated over all E_l intervals
within each E_k interval

$$\text{COV}(X_i, Y_j) = \sum_{k, l, l'} p_{j, k, l'}^{i; k, l} F_{xy, l'} X_i Y_j \quad (5)$$

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LB = 5 Relative covariance matrix components

$$\text{COV}(X_i, Y_j) = \sum_{k, k'} p_{j; k'}^{i; k} F_{xy; k, k'}^{X_i Y_j} \quad (6)$$

where X_i and Y_j represent reactions X and Y evaluated at energies i and j , respectively, and the F 's ($F_{xy, k}$, $F_{x, k}$, etc.) represent uncertainty components, taken directly from the ENDF/B file describing the covariance of reactions X and/or Y for specific energy intervals. The dimensionless operators p in the above definitions are defined in terms of the operator s as follows:

$$p_{j; m, n, \dots}^{i; k, l, \dots} \equiv S_i^k S_i^l \dots S_j^m S_j^n \dots, \quad (7)$$

where

$S_i^k \equiv 1$ when the energy E_i is in the interval E_k to E_{k+1} of an E_k table (energy structure),

$S_k^k \equiv 0$ when the energy E_i is outside the range E_k to E_{k+1} of an E_k table.

In addition to these explicit relationships (the LB's), derived relationships are flagged in the ENDF/B file for the uncertainty processor. The relationships for the evaluated and multigroup results are essentially the same and will be described in the next section. Uncertainties for the resolved resonance parameters are also given in ENDF/B-V. The processing procedure for these data will be outlined in the next section.

III. COMPUTATION OF MULTIGROUP COVARIANCE MATRICES

The type of formulation described in the previous section (sums of quantities separable in X and Y) has the very desirable characteristic that, if one assumes a model in which the weighting function is uncorrelated to the cross section of interest, the multigroup covariance matrices are reduced to combinations of single integrals of the weighted cross sections which can be calculated easily.³ In particular, for

$$\text{LB} = 0, \quad \text{COV}(X_G, Y_H) = \frac{\sum_{k \in G, H} F_{xy, k} \phi_{G, k} \phi_{H, k}}{\phi_G \phi_H} \quad (8)$$

$$\text{LB} = 1, \quad \text{COV}(X_G, Y_H) = \frac{\sum_{k \in G, H} F_{xy, k} \phi_{G, k} X_{G, k} \phi_{H, k} Y_{H, k}}{\phi_G \phi_H} \quad (9)$$

$$\text{LB} = 2, \quad \text{COV}(X_G, Y_H) = \frac{(\sum_{k \in G} F_{xy, k} \phi_{G, k} X_{H, k}) (\sum_{k' \in H} F_{xy, k'} \phi_{H, k'} Y_{H, k'})}{\phi_G \phi_H} \quad (10)$$

$$\text{LB} = 3, \quad \text{COV}(X_G, Y_H) = \frac{(\sum_{k \in G} F_{x, k} \phi_{G, k} X_{G, k}) (\sum_{l \in H} F_{y, l} \phi_{H, l} Y_{H, l})}{\phi_G \phi_H} \quad (11)$$

$$\text{LB} = 4, \quad \text{COV}(X_G, Y_H) = \frac{\sum_{k \in G, H} F_k (\sum_{l \in G} F_{xy, l} \phi_{G, l} X_{G, l}) (\sum_{l' \in H} F_{xy, l'} \phi_{H, l'} Y_{H, l'})}{\phi_G \phi_H} \quad (12)$$

and

$$\text{LB} = 5, \quad \text{COV}(X_G, Y_H) = \frac{\sum_{k \in G, k' \in H} F_{xy; k, k'} \phi_{G, k} X_{G, k} \phi_{H, k'} Y_{H, k'}}{\phi_G \phi_H} \quad (13)$$

In general, the covariance matrix will be a sum of terms from any of the LB descriptions. The derivation of Eqs. (8-12) has been described previously,¹ while Eq. (13) can be derived directly from Eq. (6). The notation used here is:

$COV(X_G, Y_H)$ = multigroup covariance between reaction x, group G and reaction, Y, group H;

ϕ_G = weight for group G;

$X_{G,k}$ = multigroup cross section for reaction X for a supergrid (i,k) constructed from the union of energy boundaries of the uncertainty file and those from the user (e.g., 52-group) energy grid. $\phi_{G,k}$ is the weight for this group; and

F's = components of covariance taken directly from the uncertainty file.

The group G (or H) is appropriate to the type derived files to be processed and is explained in Ref. 5.

These explicitly given relationships (actually the multigroup covariance matrices formed from the LB's) form the basis for the derived uncertainties flagged in the ENDF/B file. Derived uncertainty is used here in one of two senses, either the cross section has been evaluated as a linear combination of other reactions or the cross section has been derived via a ratio measurement to some known reaction.

The "derived redundant cross section" covariances, for those cross sections evaluated as a linear combination of other reactions may be expressed as

$$COV(X_G, X_H) = \sum_{m=1}^n \sum_{m'=1}^n K_m K_{m'} COV(Y_{m,G}, Y_{m',H}) \quad , \quad (14)$$

where K_m are constants relating reaction X to reaction(s) Y_m and where m may range up to n such reactions. This relationship is specified over a certain energy range, that is, the covariance matrix is bounded by energies E_1 and E_2 specified in the ENDF/B file.

Equation (14) implies that many other covariance relationships exist. These other relationships have been called off-diagonal sub-matrices and may be defined as

$$\text{COV}(X_G, Y_{m,H}) = \sum_{m'=1}^n K_{m'} \text{COV}(Y_{m';H}, Y_{m,G}) \quad m=1,2,\dots,n. \quad (15)$$

Equation (15) is the defining expression for the covariance between the derived reaction X and each of the reactions from which it is evaluated, Y_m . This covariance matrix is also bounded by the specified energy ranges, E_1 and E_2 .

The second type of derived uncertainties is for a reaction which may have been wholly or partially derived from another reaction by a ratio measurement. The covariance matrix for the desired reaction, X is given in general as

$$\text{Rel. COV}(X_G, X_H) = \text{Rel. COV}(R_G, R_H) + \text{Rel. COV}(Z_G, Z_H) \quad (16)$$

where covariances are now given in terms of relative covariance matrices (see Section IV). R_G is the measured ratio of reaction X_G to the known reaction Z_G for group G .^{2,5}

A covariance between reaction X and Z may also exist and is given as

$$\text{Rel. COV}(X_G, Z_H) = \text{Rel. COV}(Z_G, Z_H) \quad (17)$$

Equations (16) and (17) assume that the measured ratio, R , is uncorrelated to the reaction Z .^{2,5}

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Equations (8-17) illustrate the relationships used in processing ENDF/B-V uncertainty data from files 31 and 33. However, the uncertainties in the resolved resonance parameters in file 32 are given a somewhat limited treatment. The resolved resonance parameters uncertainties have been propagated through to uncertainties in the infinitely dilute resonance cross section using a Breit-Wigner formalism.⁵ Uncertainties due to self-shielding effects have not been taken into account. In effect the resolved resonance parameter uncertainties have been propagated to infinitely dilute cross section uncertainties and summed to the previous results of file 33 of ENDF/B-V. Only three materials of the covariance library contain uncertainties due to the resolved resonance parameters; Fe, Na and Pu-240.

IV. RESULTS FOR PROCESSED UNCERTAINTY FILES

Several quantities related to uncertainties in multigroup cross sections are processed from the pointwise ENDF/B data covariance file using the PUFF-II covariance file processing code.⁵ Clearly, of interest is the covariance matrix

$$\text{Cov}(X_G, Y_H) = \langle (X_G - \bar{X}_G) (Y_H - \bar{Y}_H) \rangle \quad (18)$$

the covariance of reaction X , group G , and reaction Y , group H . (Angle brackets represent expectation values in this section.) The associated quantity, the relative covariance matrix, is defined:

$$\text{Rel Cov}(X_G, Y_H) = \text{Cov}(X_G, Y_H) / X_G Y_H \quad (19)$$

In this notation, the standard deviation is given by

$$\text{Std. Dev}(X_G) = \sqrt{\text{Cov}(X_G, X_G)} \quad (20)$$

and the analogous relative quantity, the relative standard deviation is

$$\text{Rel Std. Dev}(X_G) = \frac{\text{Std. Dev}(X_G)}{X_G} \quad (21)$$

It is reasonable to expect that in many cases the covariance matrix of energy-dependent cross sections is almost diagonal; i.e., the magnitude of the matrix element corresponding to distinct groups G and H tend to be small if groups G and H are widely displaced from each other in energy.

The correlation matrix is a quantity constructed by dividing the covariance matrix for X_G and Y_H by the respective standard deviations:

$$\text{Corr}(X_G, Y_H) = \frac{\langle (X_G - \bar{X}_G) (Y_H - \bar{Y}_H) \rangle}{\sqrt{\langle (X_G - \bar{X}_G)^2 \rangle \langle (Y_H - \bar{Y}_H)^2 \rangle}} \quad (22)$$

The correlation matrix is bounded by unity, i.e.,

$$|\text{Corr}(X_G, Y_H)| \leq 1 \quad (23)$$

When $\text{Corr}(X_G, Y_H) = 0$, the group cross sections are said to be totally uncorrelated; when $|\text{Corr}(X_G, Y_H)| = 1$, the group cross sections are termed fully correlated (or anticorrelated).

V. SPECIAL CASES

The B-10(n, α) (MT = 107) covariance matrix was produced from an explicit uncertainty file. Although the B-10(n, α) uncertainty file is given in ENDF/B-V as a derived file, an explicit file was needed by the uncertainty processor, PUFF-II, in order to process the U-238(n, γ) uncertainty data. This action is explained in a letter in Appendix D.

Also concerning U-238, an estimate of the uncertainty in the capture cross section from 1 eV to 4 keV was included in the uncertainty file. This estimate was provided by G. de Saussure under the limiting conditions explained in the letter in Appendix D, (also see comments in Appendix E). Estimates for the fission and total elastic reactions were also provided, but are not yet included in the covariance file. These estimates are not believed to be of great importance to fast reactor applications, where as the capture uncertainty estimate is believed to be needed.

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In an effort to cut down on the amount of preprocessed data needed to produce this multigroup covariance library, the total $\bar{\nu}(E)$ for U-238 was used as the prompt $\nu(E)$ of U-238 in processing the uncertainty file. The prompt $\bar{\nu}(E)$ ranged from 98.2% to 99.5% (low to high energy) of the total $\bar{\nu}(E)$ for U-238 in ENDF/B-V file 1. This means that neither the covariance matrices of U-238 total $\bar{\nu}(E)$ or U-238 prompt $\bar{\nu}(E)$ and its correlation are necessarily correct. The covariance matrix for the total $\bar{\nu}$ is the same as the prompt $\bar{\nu}$ covariance matrix with the MT value switched from 456 to 452.

VI. CONCLUSIONS

This report describes the covariance files created as a part of the ORNL effort to provide important group-structure uncertainty information for use in fast reactor sensitivity and uncertainty analysis. In particular, these data represent the uncertainties and correlations in the multigroup cross sections based on the uncertainty information estimated by the evaluators and expressed in ENDF/B-V.

This report presents the multigroup covariance matrices for many of the important reactions of B-10, C-12, O-16, Na, Cr, Fe, Ni, U-235, U-238, Pu-239, Pu-240, and Pu-241. Except for the special cases mentioned in the previous section, the uncertainty data has come wholly from ENDF/B-V uncertainty files.

Although the Version-V uncertainty files are the most complete ENDF/B effort to document the uncertainty information to date, some important covariances may be missing. Thus, additional covariance matrices may be added to the library as needed. This additional information may come from either ORNL internal generations or from ENDF/B-V modifications.

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VII. 52-GROUP STANDARD DEVIATION AND CORRELATION MATRIX PLOTS

The following section contains correlation matrices illustrated in a 3-dimension plot with corresponding standard deviations in a 2-dimension plot. The cross material and/or cross reactions contain no standard deviation plot since they can be found elsewhere for each of the individual material and/or reaction. For such a cross-correlation plot the 'for' material corresponds to the front-to-back axis and the 'to' material corresponds to the left to right axis. For example, in Fig. 175 the ^{239}Pu (n,f) axis is front to back and the ^{235}U (n,f) axis is left to right.

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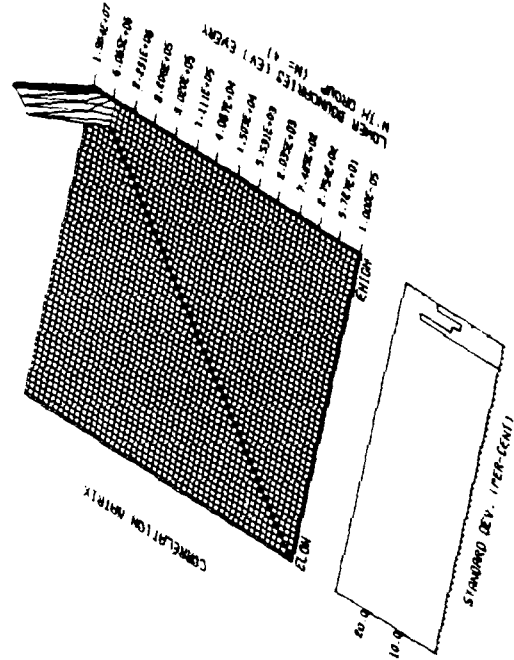


Fig. 3. Standard Deviation and Correlation Matrix for 0 Inelastic Cross Sections.

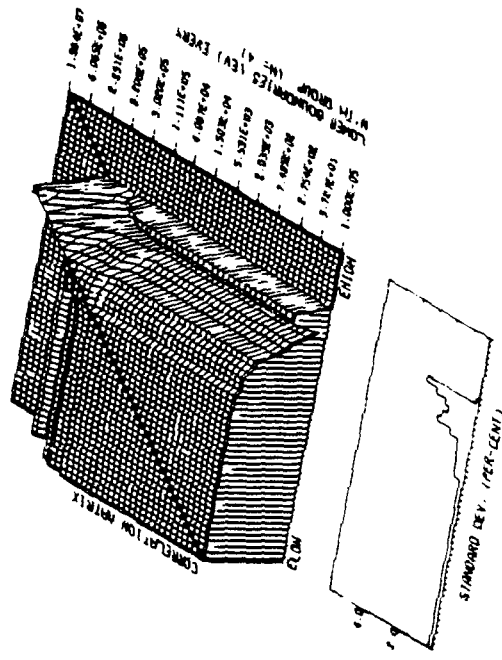


Fig. 5. Standard Deviation and Correlation Matrix for log(n, alpha) Cross Sections.

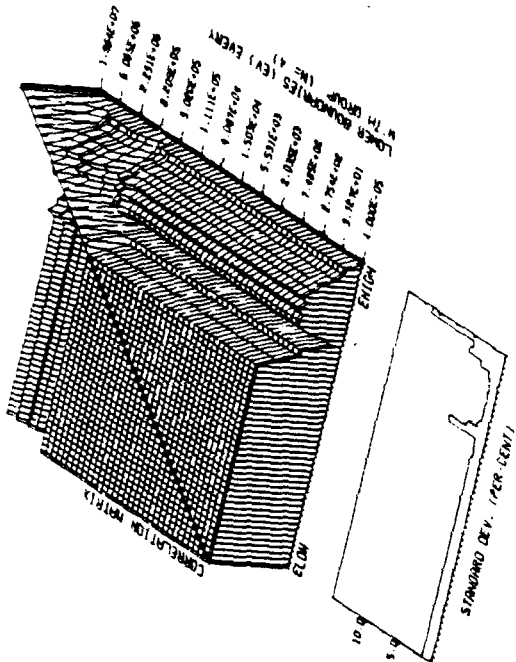


Fig. 2. Standard Deviation and Correlation Matrix for 0 Elastic Cross Sections.

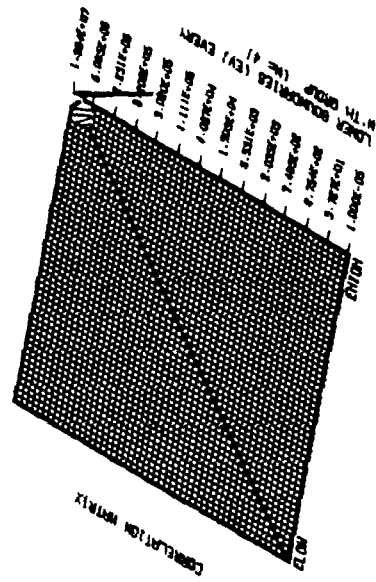


Fig. 4. Cross Correlation Matrix for 0 Elastic to 0 Inelastic Cross Sections.

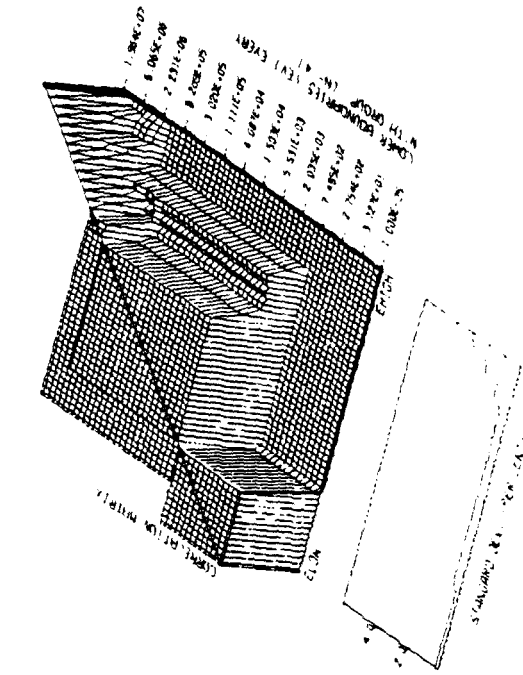


Fig. 7. Standard Deviation and Correlation Matrix for C Elastic Cross Sections.

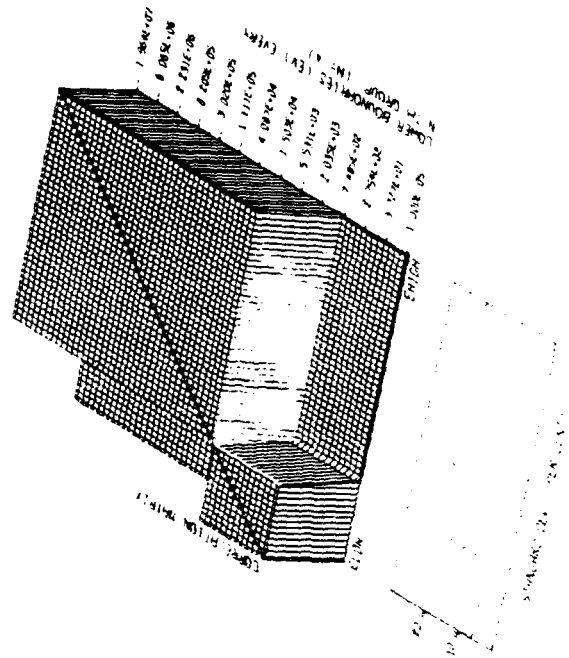


Fig. 9. Standard Deviation and Correlation Matrix for C(n,y) Cross Sections.

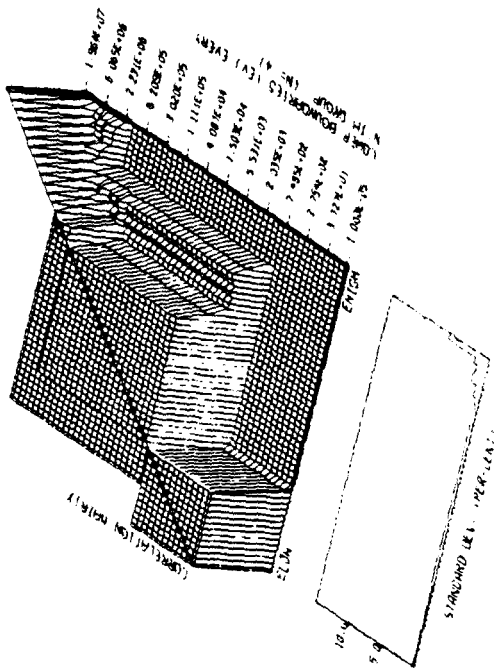


Fig. 6. Standard Deviation and Correlation Matrix for C Total Cross Sections.

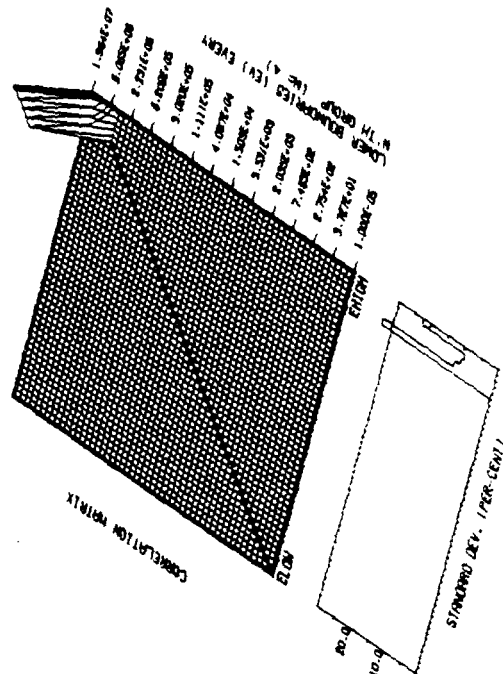


Fig. 8. Standard Deviation and Correlation Matrix for C Inelastic Cross Sections.

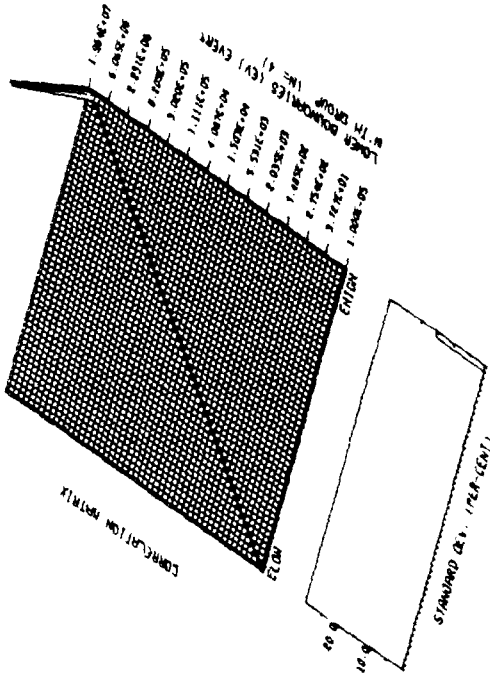


Fig. 11. Standard Deviation and Correlation Matrix for C(n,d) Cross Sections.

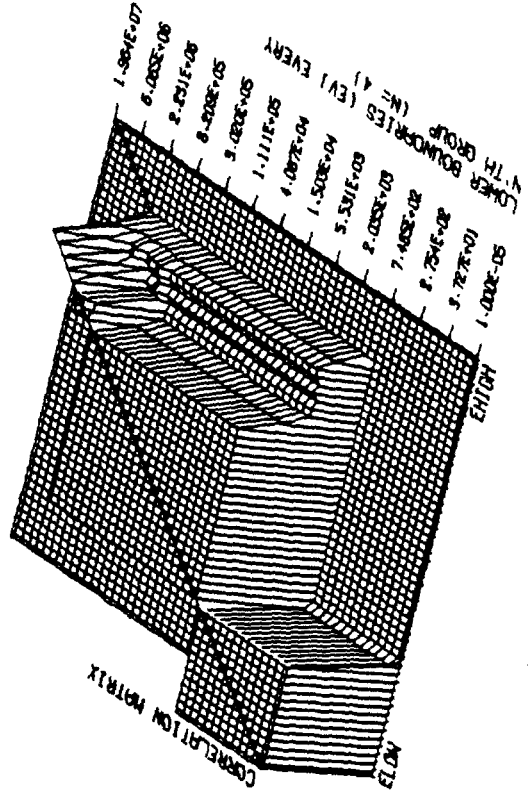


Fig. 13. Cross Correlation Matrix for C Total to C Elastic Cross Sections.

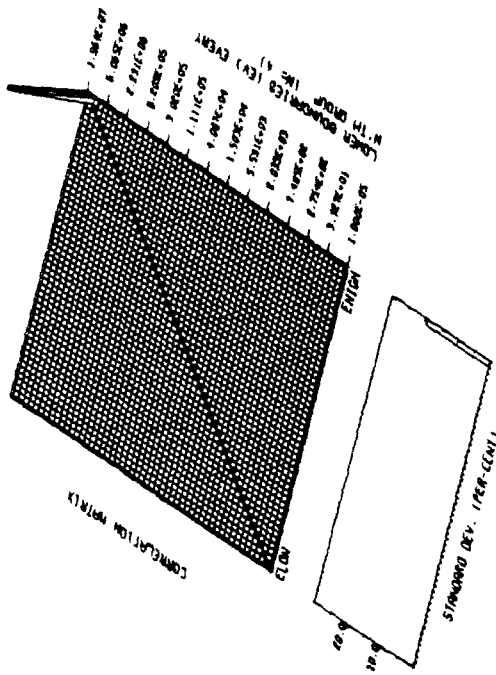


Fig. 10. Standard Deviation and Correlation Matrix for C(n,p) Cross Sections.

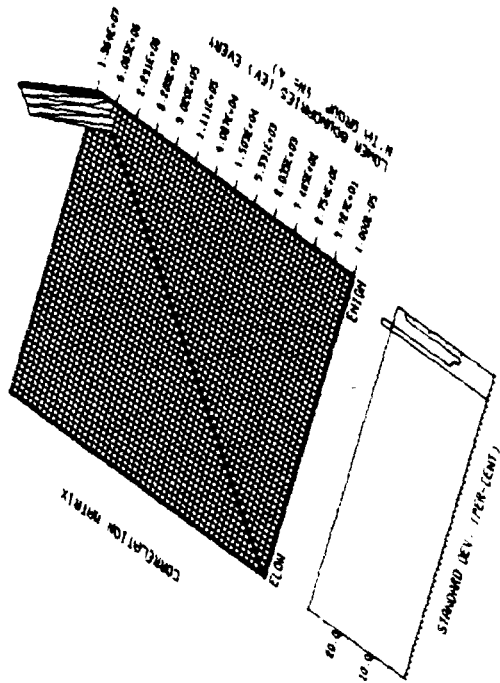


Fig. 12. Standard Deviation and Correlation Matrix for C(n,a) Cross Sections.

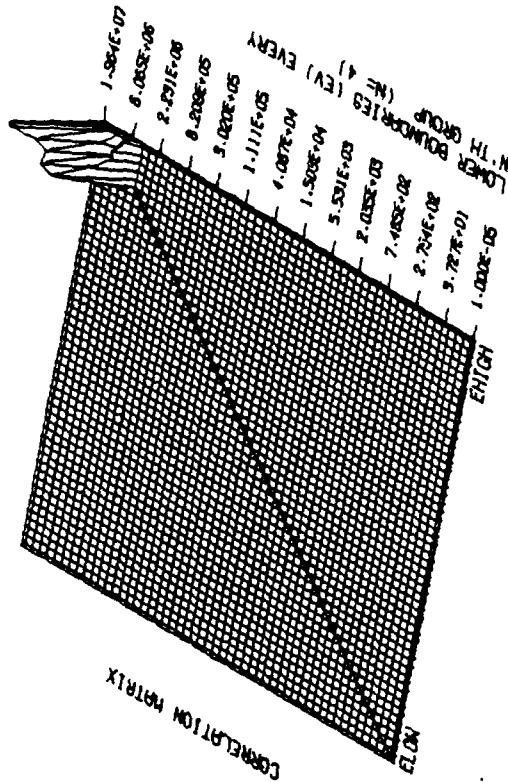


Fig. 15. Cross Correlation Matrix for C Inelastic to C Total Cross Sections.

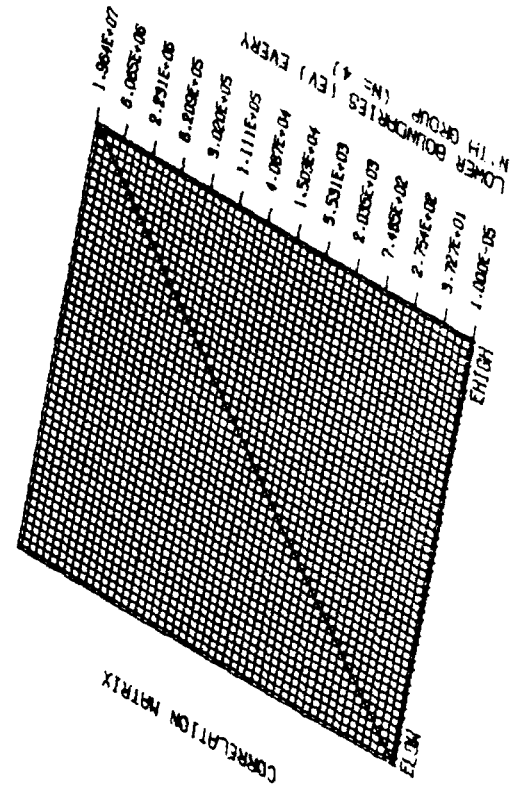


Fig. 17. Cross Correlation Matrix for C Inelastic to C(n,y) Cross Sections.

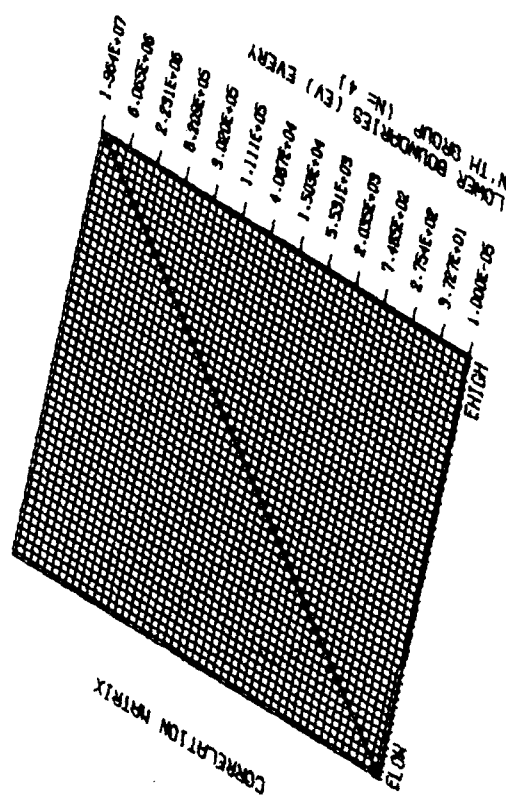


Fig. 14. Cross Correlation Matrix for C Total to C(n,y) Cross Sections.

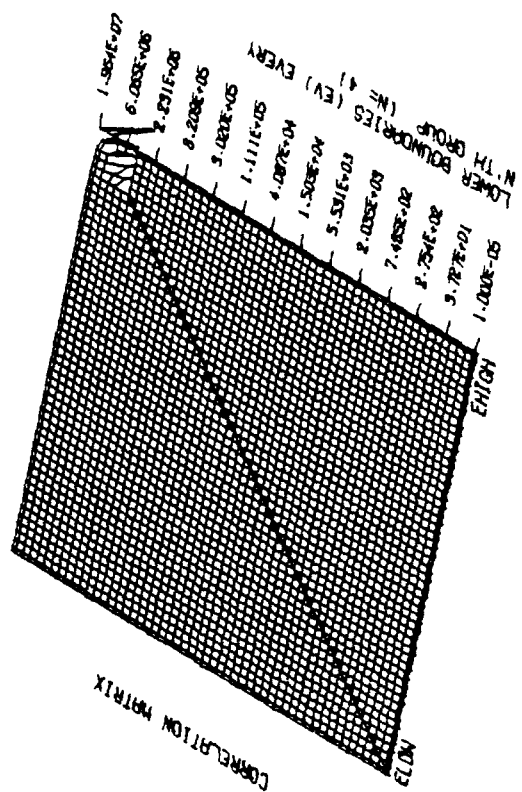


Fig. 16. Cross Correlation Matrix for C Inelastic to C Elastic Cross Sections.

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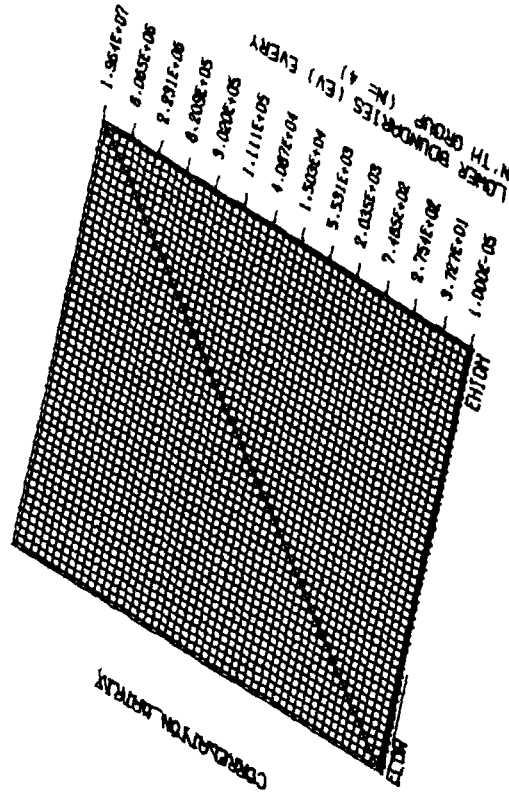


Fig. 19. Cross Correlation Matrix for C Inelastic to C(n,d) Cross Sections.

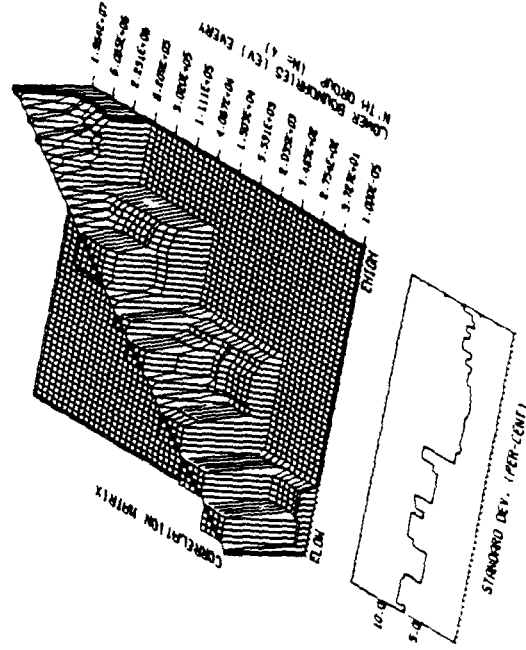


Fig. 21. Standard Deviation and Correlation Matrix for Na Total Cross Sections.

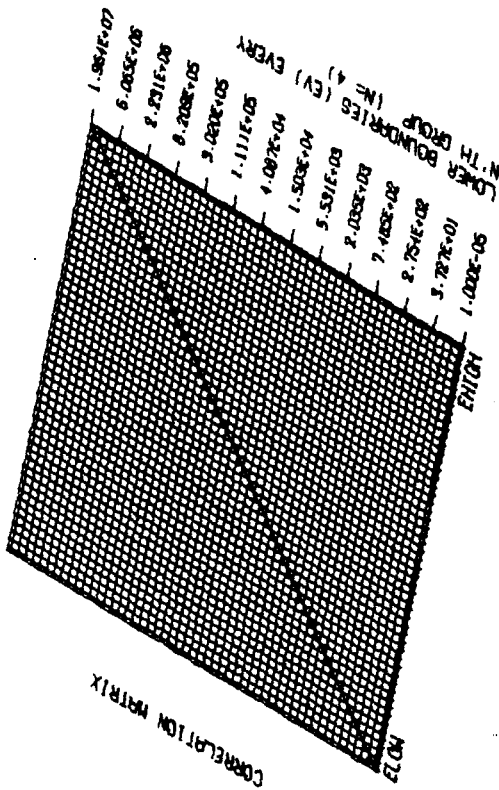


Fig. 18. Cross Correlation Matrix for C Inelastic to C(n,p) Cross Sections.

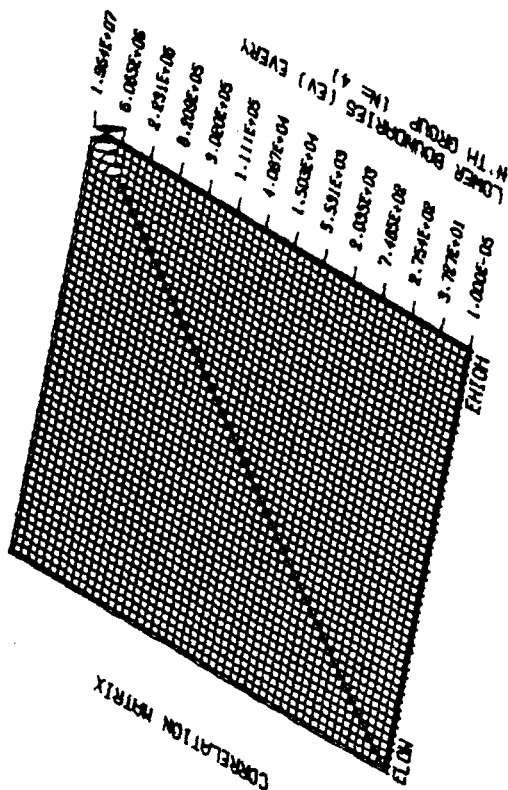


Fig. 20. Cross Correlation Matrix for C Inelastic to C(,a) Cross Sections.

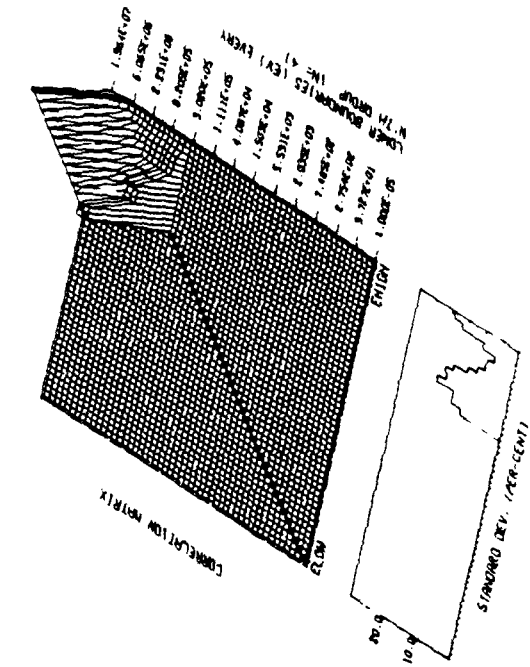


Fig. 23. Standard Deviation and Correlation Matrix for Na Inelastic Cross Sections.

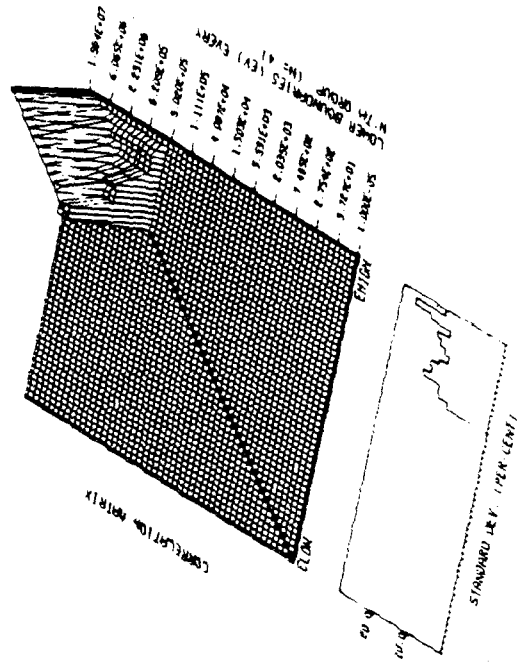


Fig. 25. Standard Deviation and Correlation Matrix for Na(n,n') Level 1 Cross Sections.

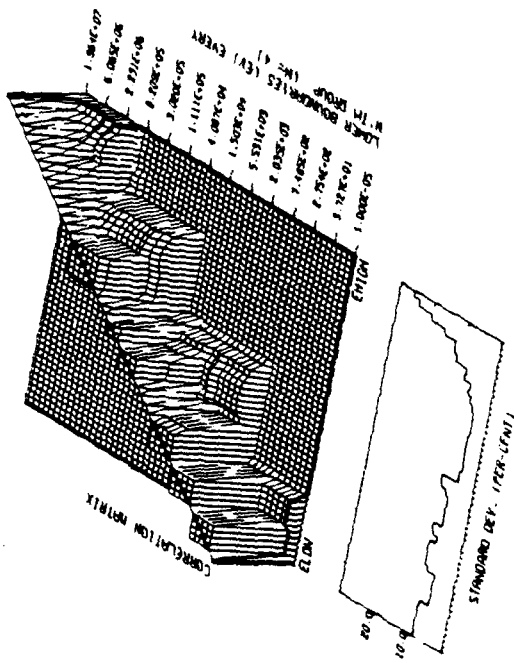


Fig. 22. Standard Deviation and Correlation Matrix for Na Elastic Cross Sections.

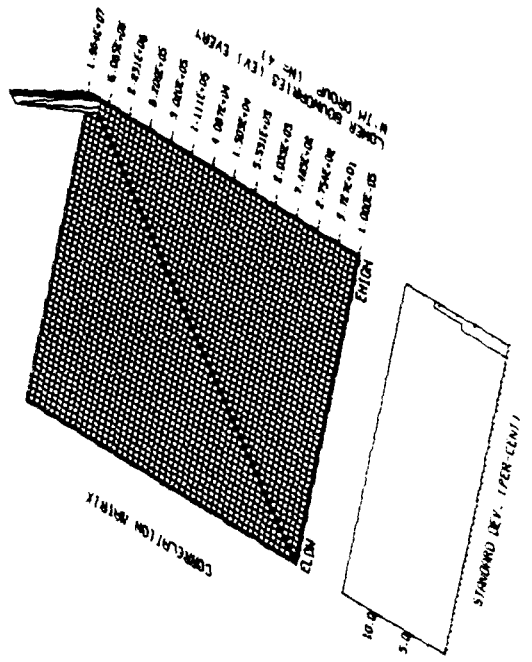


Fig. 24. Standard Deviation and Correlation Matrix for Na(n,n') Level 2 Cross Sections.

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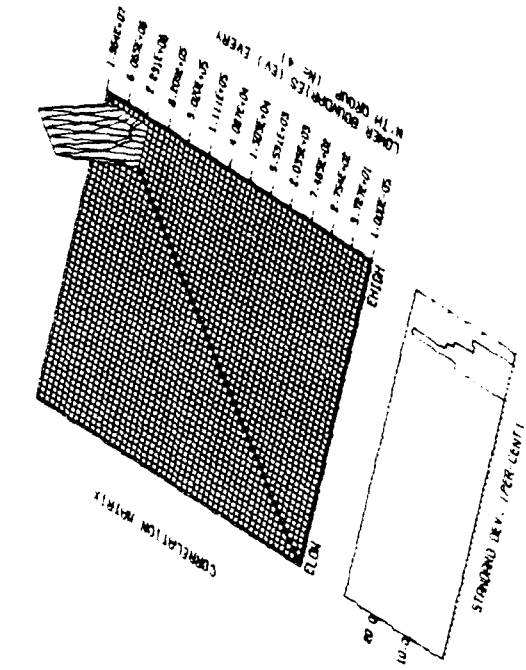


Fig. 27. Standard Deviation and Correlation Matrix for Na(n,n') Level 3 Cross Sections.

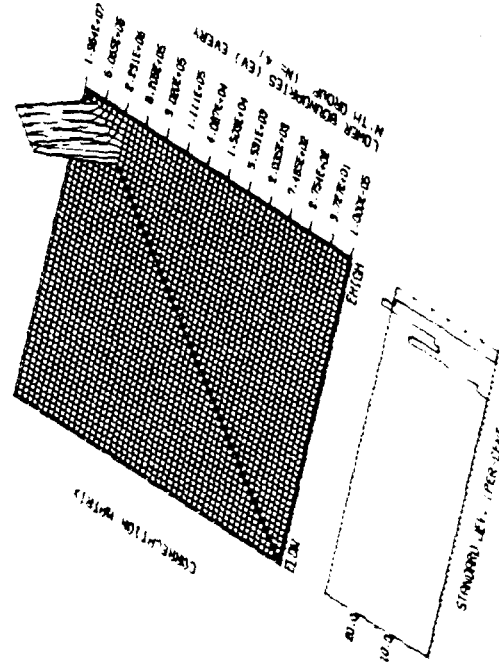


Fig. 29. Standard Deviation and Correlation Matrix for Na(n,n') Level 5 Cross Sections.

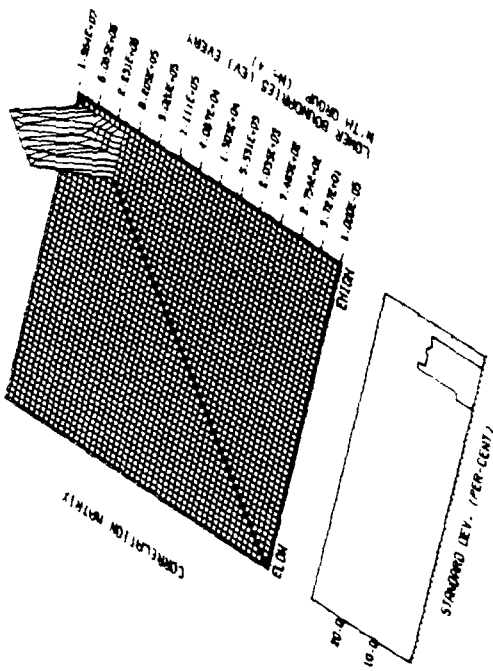


Fig. 26. Standard Deviation and Correlation Matrix for Na(n,n') Level 2 Cross Sections.

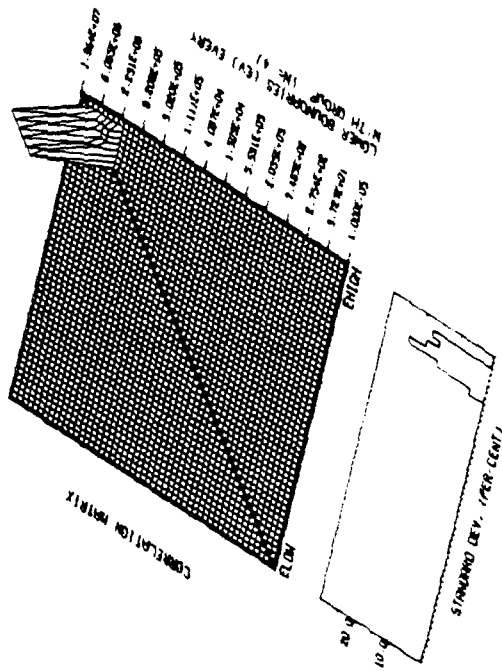


Fig. 28. Standard Deviation and Correlation Matrix for Na(n,n') Level 4 Cross Sections.

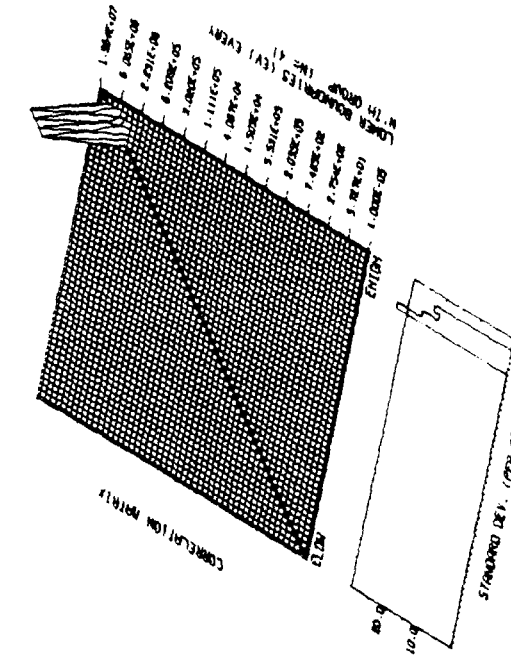


Fig. 31. Standard Deviation and Correlation Matrix for Na(n,n') Level 7 Cross Sections.

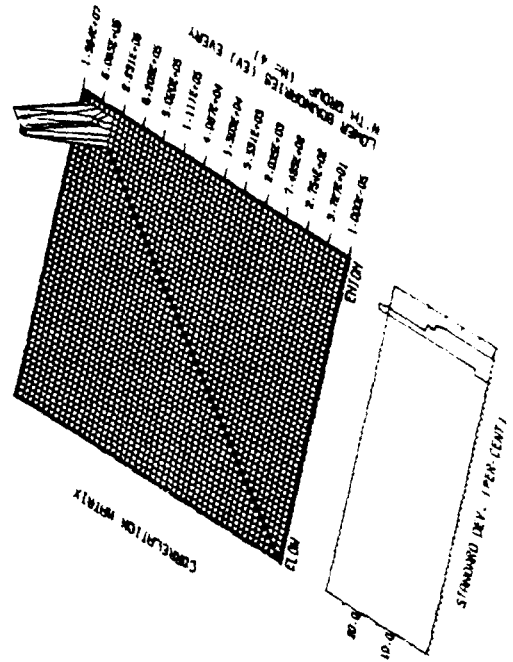


Fig. 33. Standard Deviation and Correlation Matrix for Na(n,n') Level 9 Cross Sections.

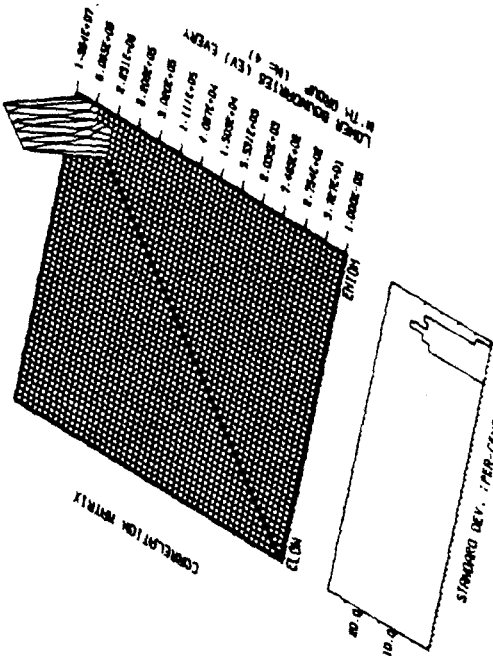


Fig. 30. Standard Deviation and Correlation Matrix for Na(n,n') Level 6 Cross Sections.

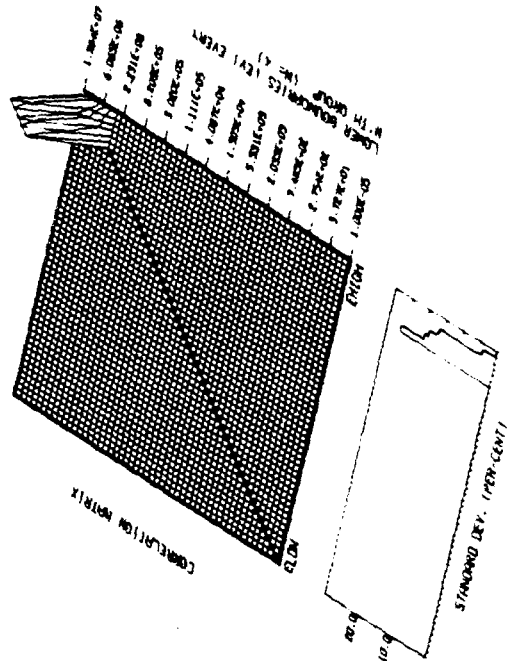


Fig. 32. Standard Deviation and Correlation Matrix for Na(n,n') Level 8 Cross Sections.

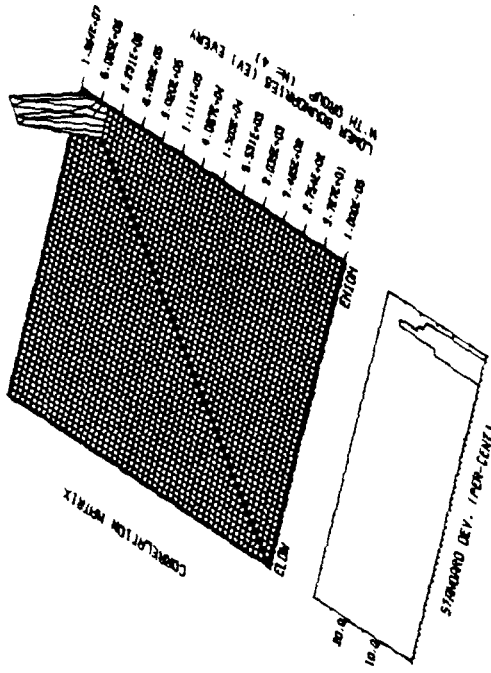


Fig. 35. Standard Deviation and Correlation Matrix for Na(n,n') Level 11 Cross Sections.

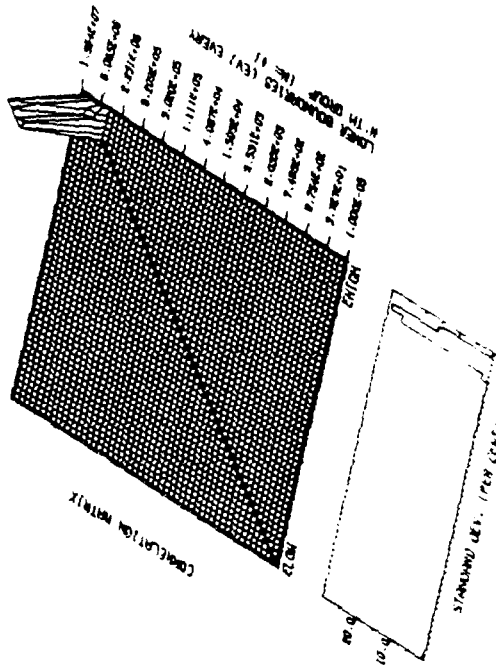


Fig. 37. Standard Deviation and Correlation Matrix for Na(n,n') Level 13 Cross Sections.

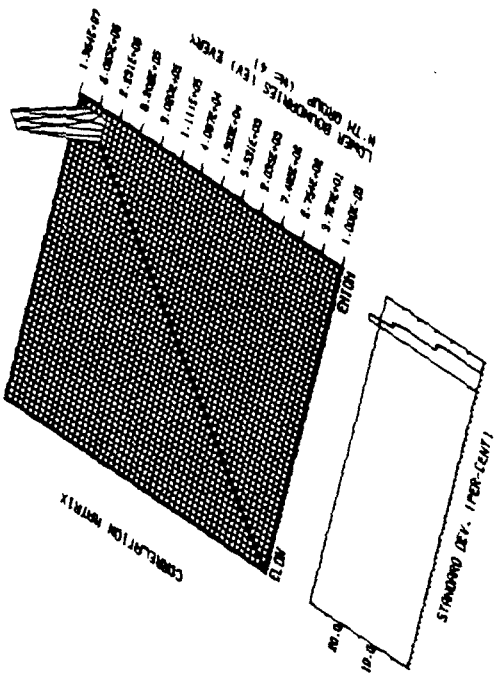


Fig. 34. Standard Deviation and Correlation Matrix for Na(n,n') Level 10 Cross Sections.

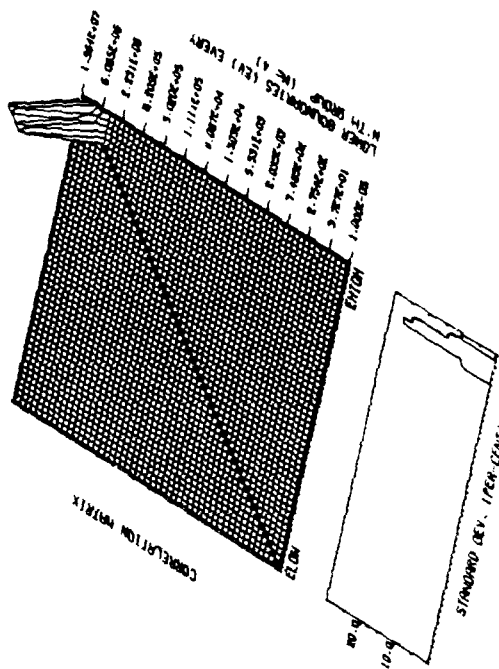


Fig. 36. Standard Deviation and Correlation Matrix for Na(n,n') Level 12 Cross Sections.

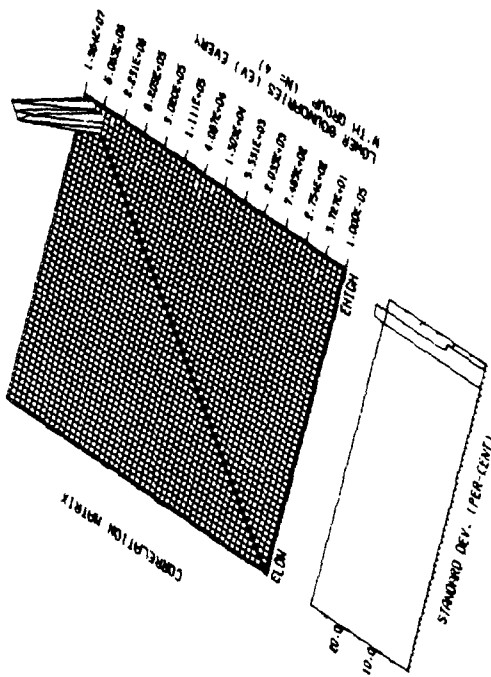


Fig. 38. Standard Deviation and Correlation Matrix for Na(n,n') Level 14 Cross Sections.

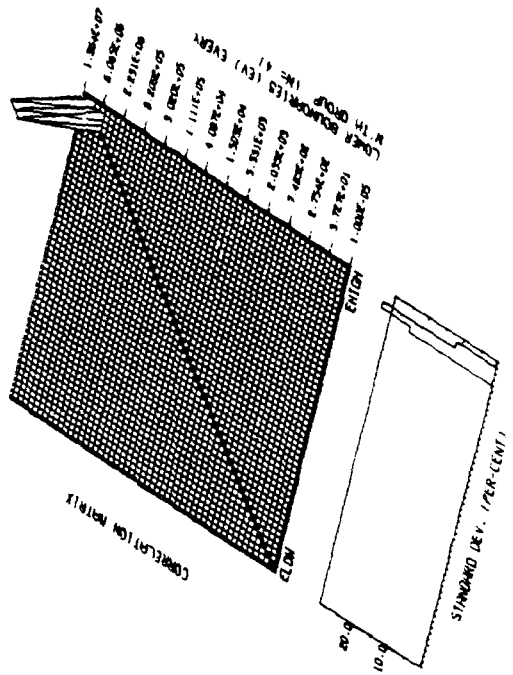


Fig. 40. Standard Deviation and Correlation Matrix for Na(n,n') Level 16 Cross Sections

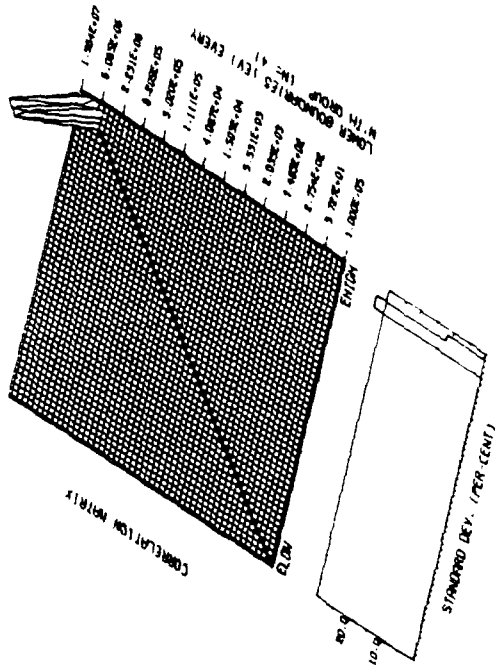


Fig. 39. Standard Deviation and Correlation Matrix for Na(n,n') Level 15 Cross Sections.

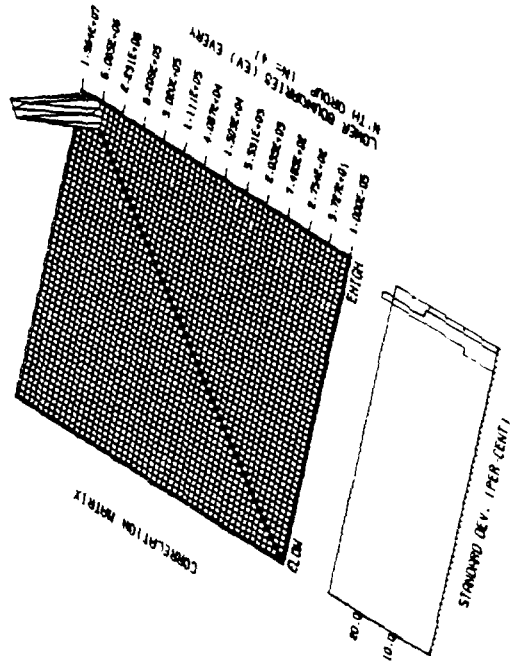


Fig. 41. Standard Deviation and Correlation Matrix for Na(n,n') Level 17 Cross Sections.

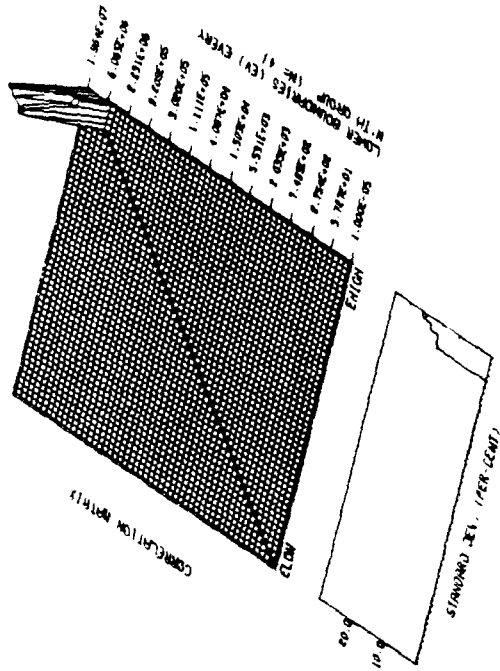


Fig. 43. Standard Deviation and Correlation Matrix for $Na(n,n')$ Continuum Cross Sections.

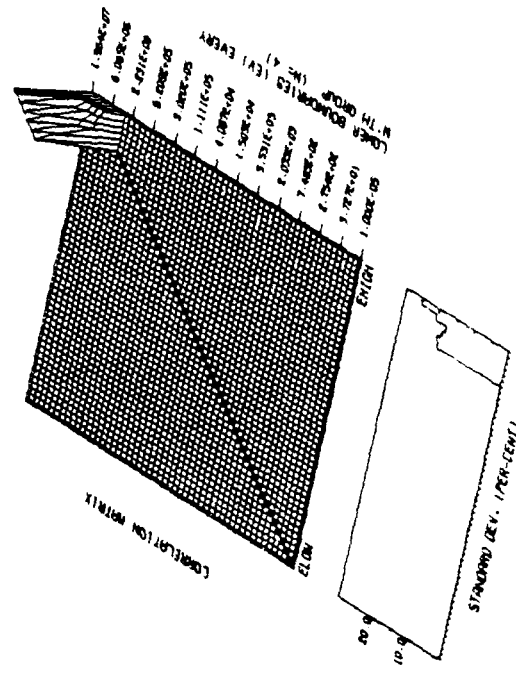


Fig. 45. Standard Deviation and Correlation Matrix for $Na(n,p)$ Cross Sections.

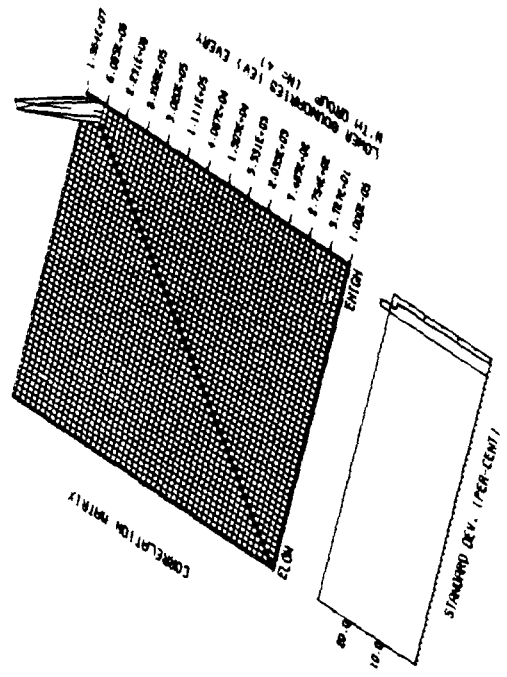


Fig. 42. Standard Deviation and Correlation Matrix for $Na(n,n')$ Level 18 Cross Sections.

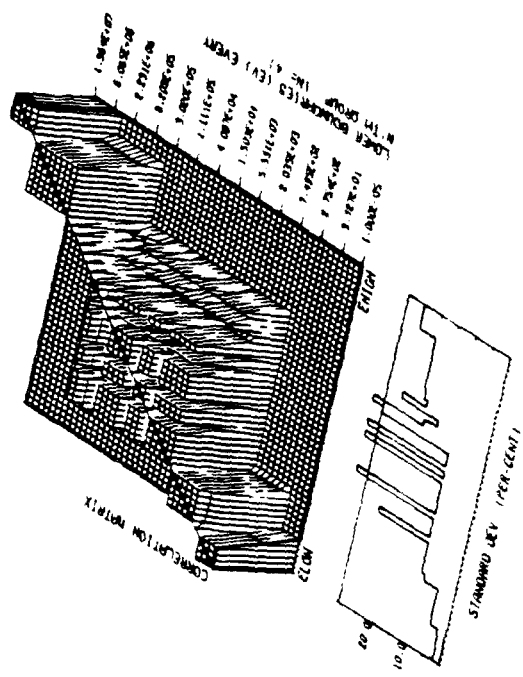


Fig. 44. Standard Deviation and Correlation Matrix for $Na(n,\gamma)$ Cross Sections.

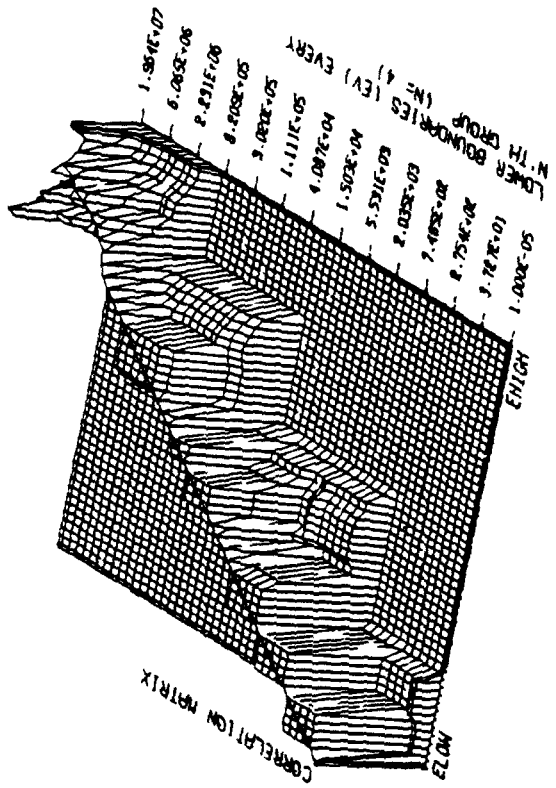


Fig. 47. Cross Correlation Matrix for Na elastic to Na Total Cross Sections.

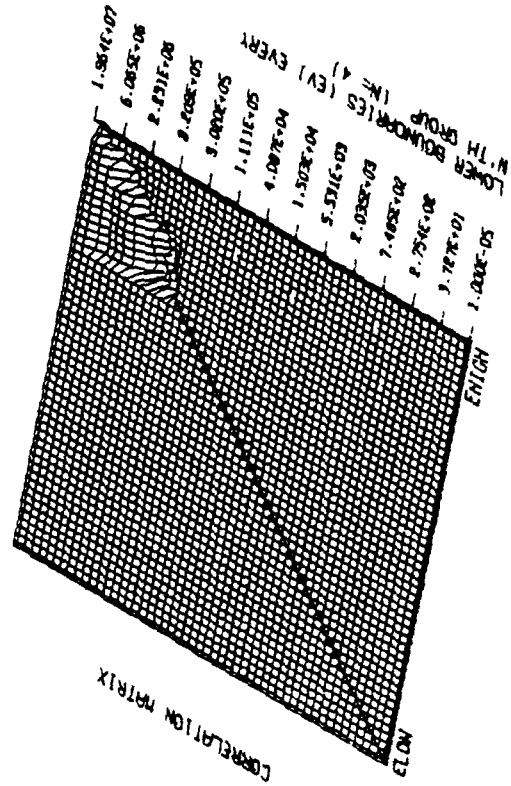


Fig. 49. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 1 Cross Sections.

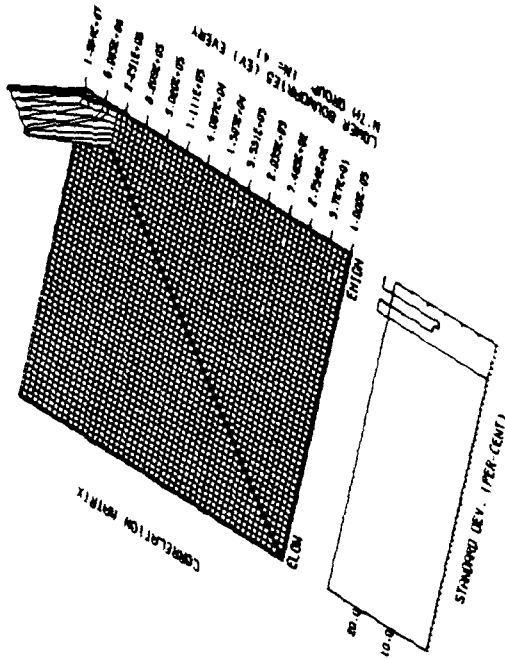


Fig. 46. Standard Deviation and Correlation Matrix for Na(n,a) Cross Sections.

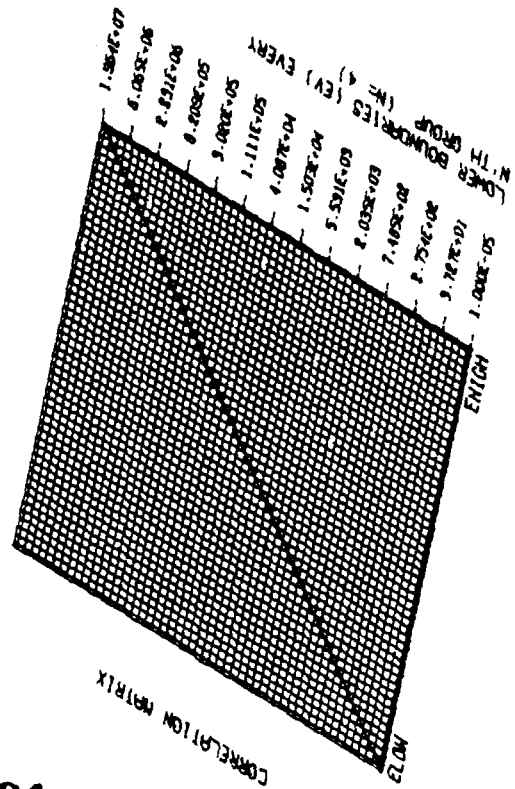


Fig. 48. Cross Correlation Matrix for Na Elastic to Na(n,2n) Cross Sections.

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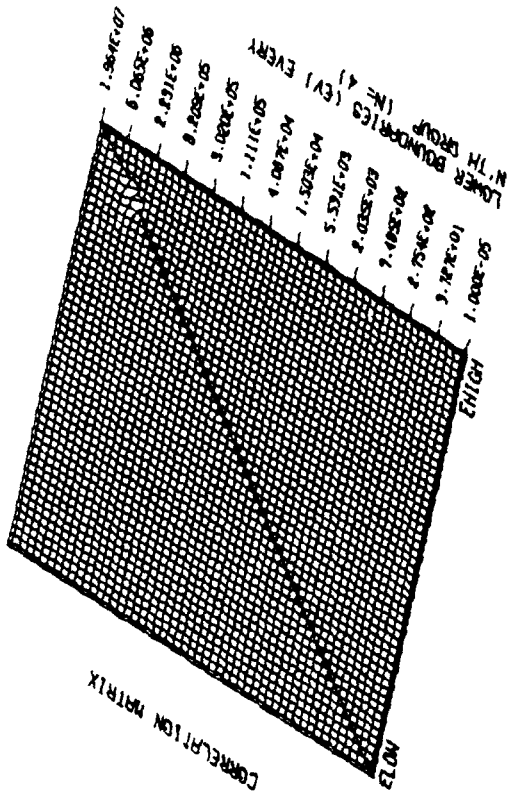


Fig. 51. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 3 Cross Sections.

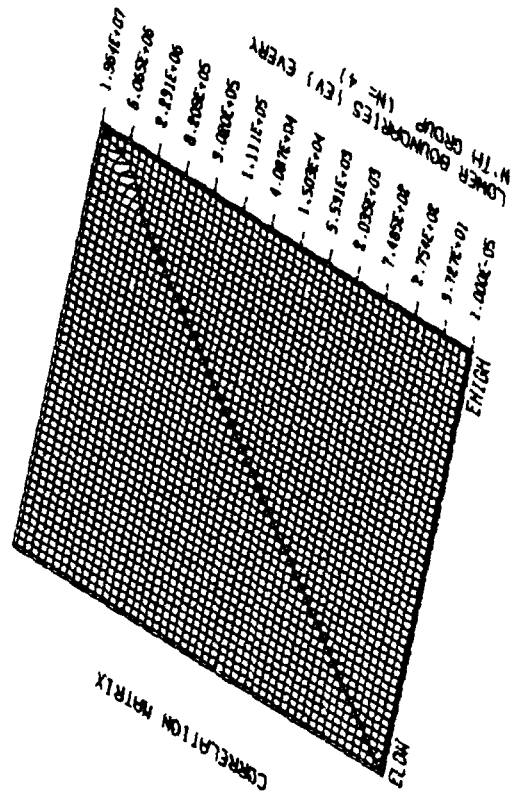


Fig. 53. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 5 Cross Sections.

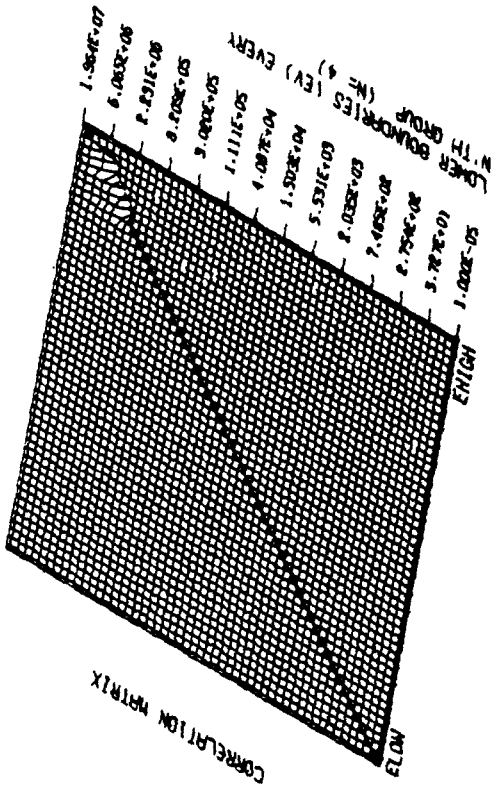


Fig. 50. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 2 Cross Sections.

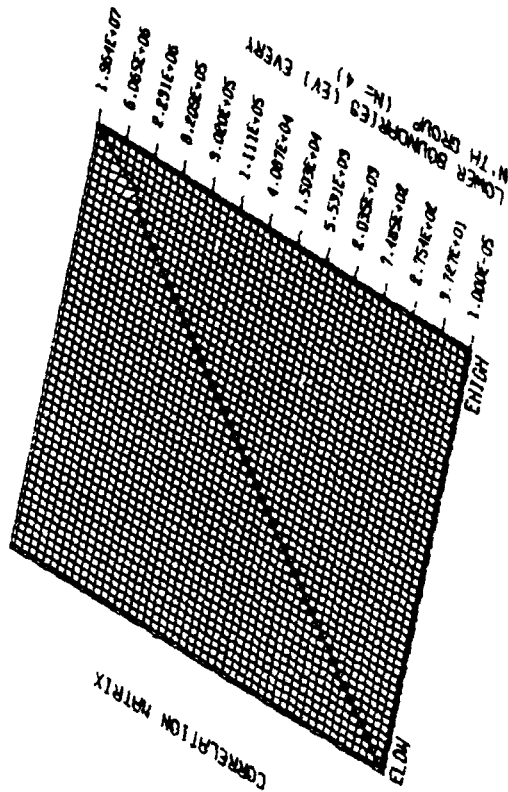


Fig. 52. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 4 Cross Sections.

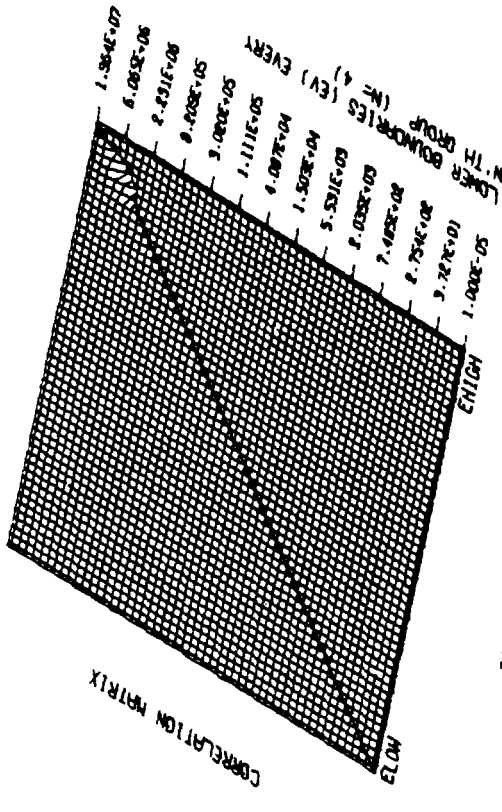


Fig. 54. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 6 Cross Sections.

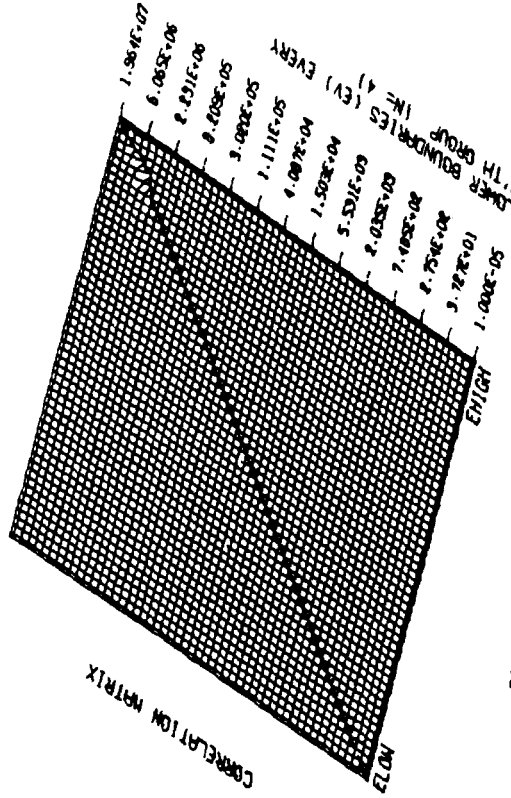


Fig. 55. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 7 Cross Sections.

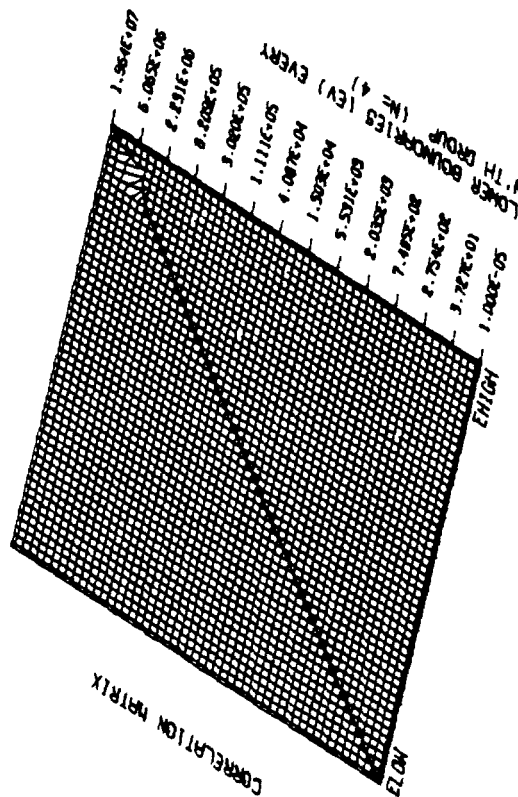


Fig. 56. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 8 Cross Sections.

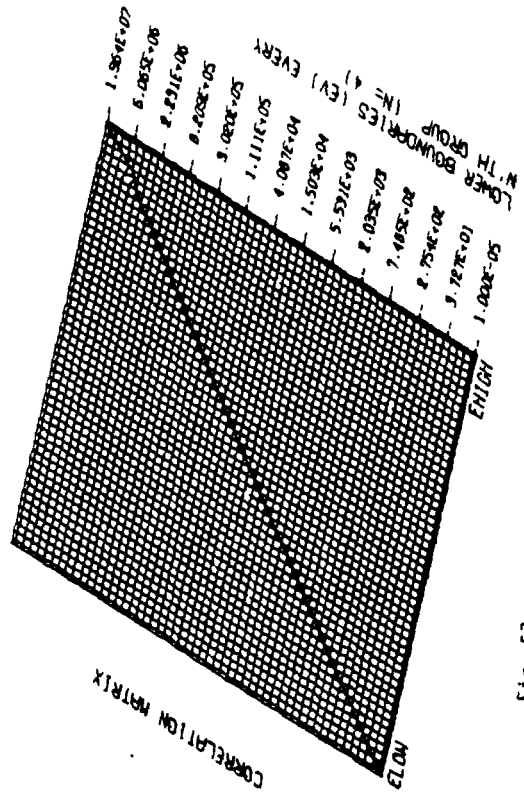


Fig. 57. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 9 Cross Sections.

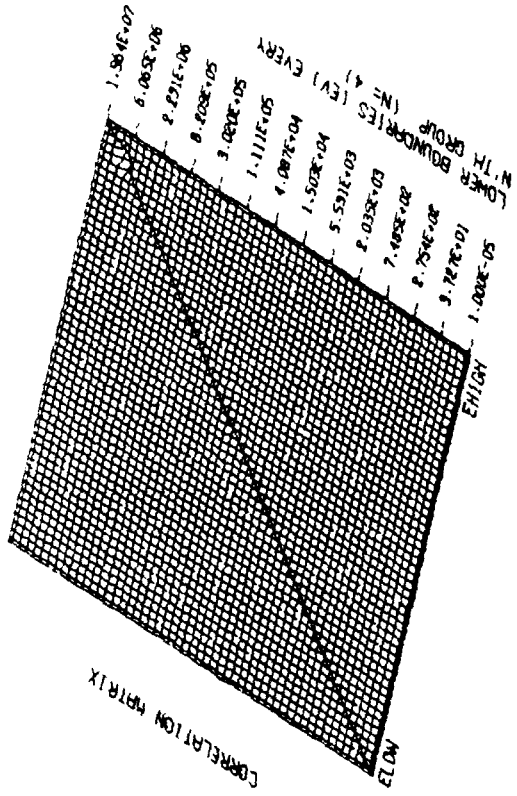


Fig. 59. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 11 Cross Sections.

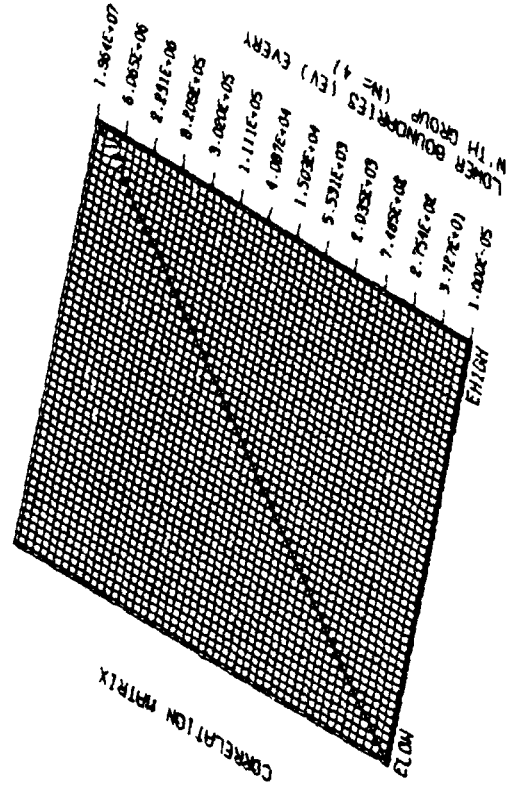


Fig. 61. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 13 Cross Sections.

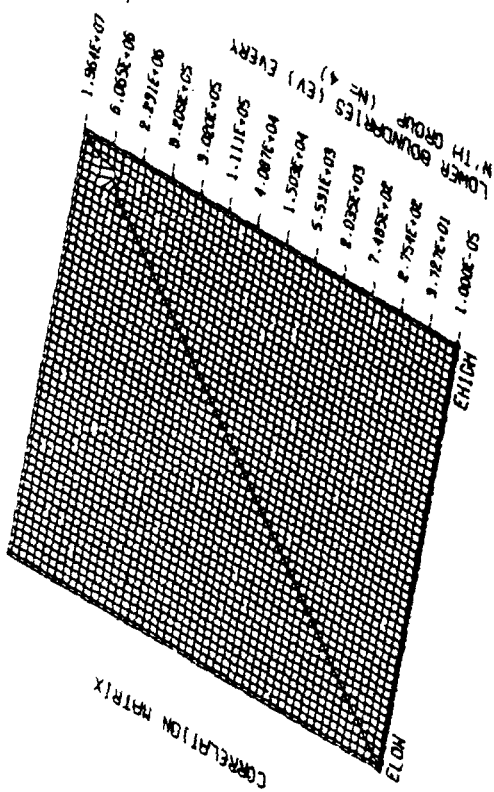


Fig. 58. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 10 Cross Sections.

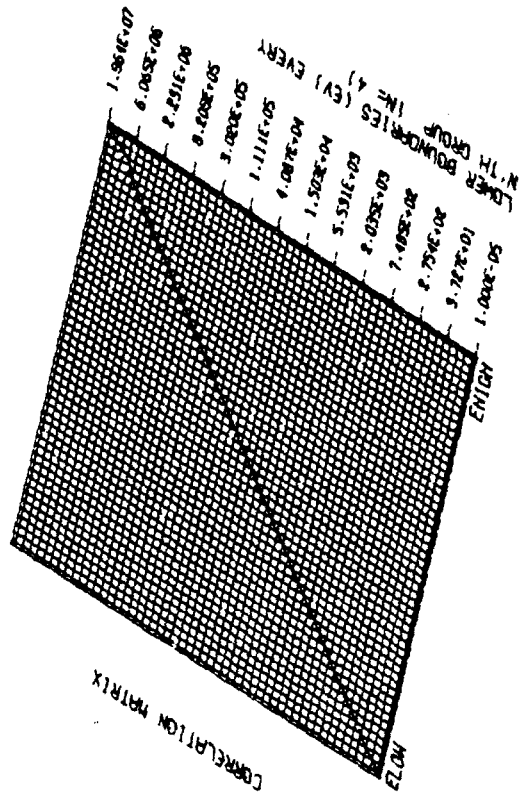


Fig. 60. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 12 Cross Sections.

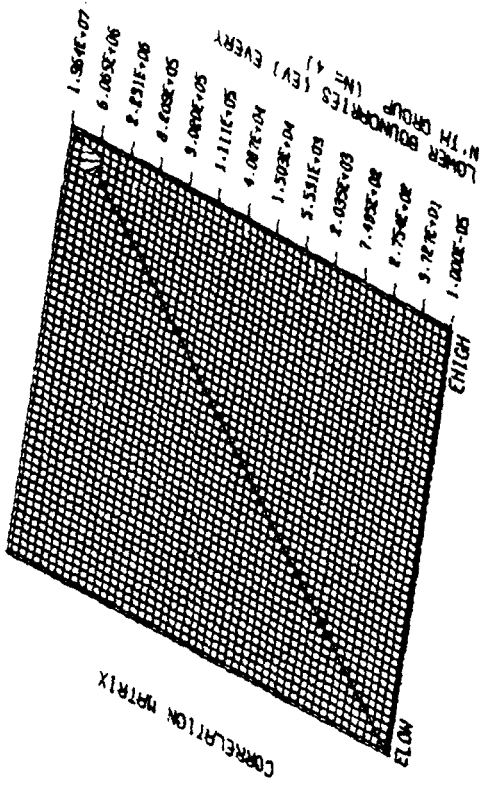


Fig. 63. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 15 Cross Sections.

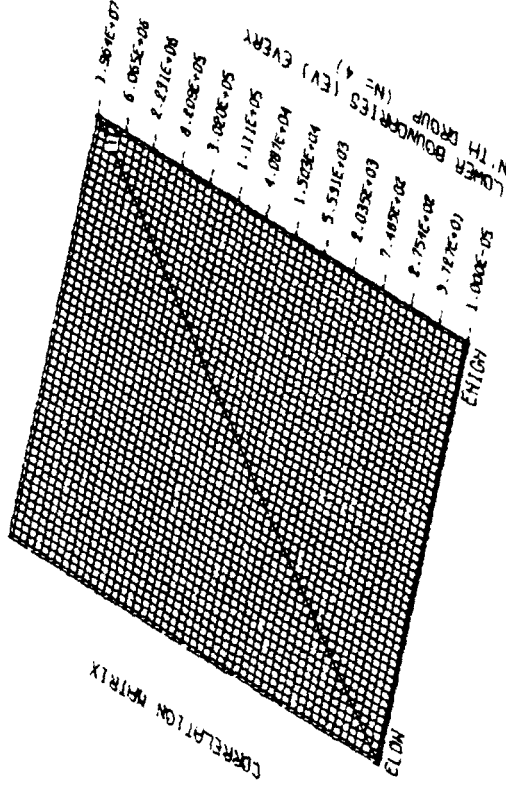


Fig. 65. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 17 Cross Sections.

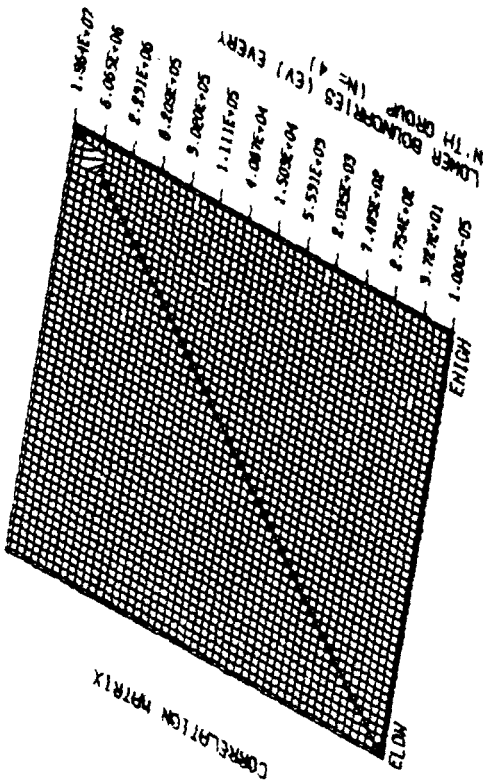


Fig. 62. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 14 Cross Sections.

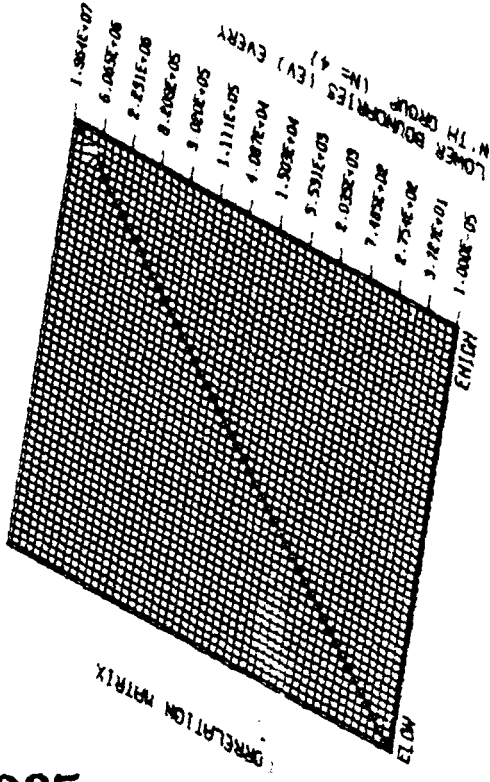


Fig. 64. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 16 Cross Sections.

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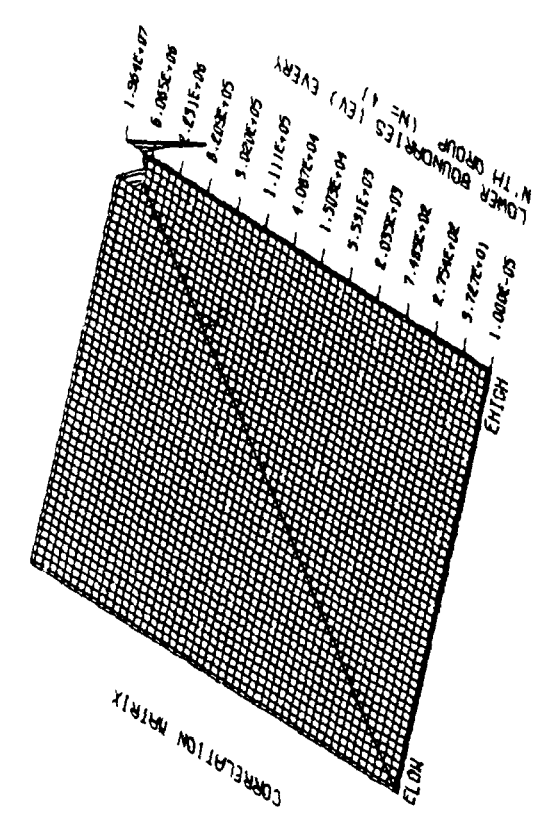


Fig. 66. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 18 Cross Sections.

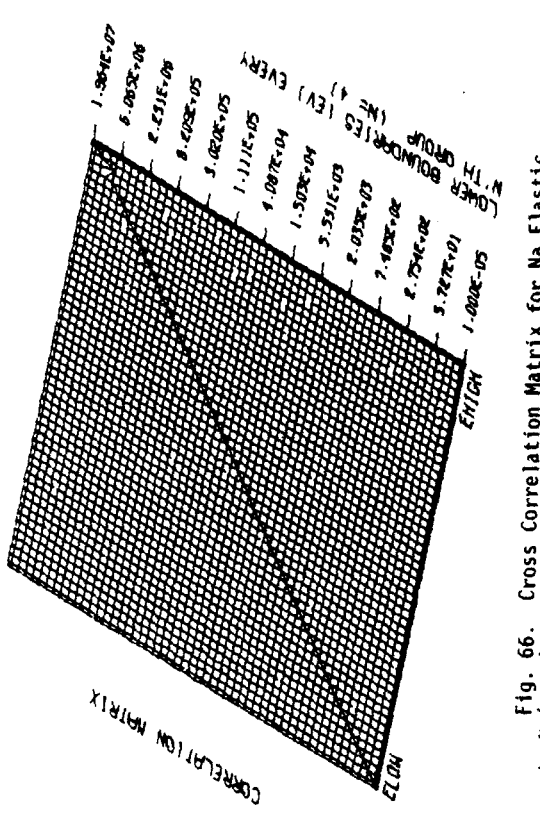


Fig. 67. Cross Correlation Matrix for Na Elastic to Na(n,n') Continuum Cross Sections.

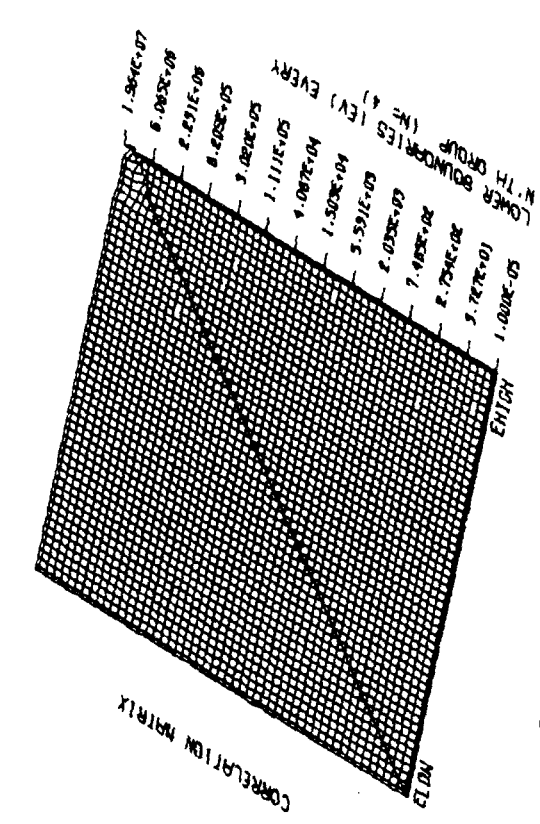


Fig. 68. Cross Correlation Matrix for Na Elastic to Na(n,y) Cross Sections.

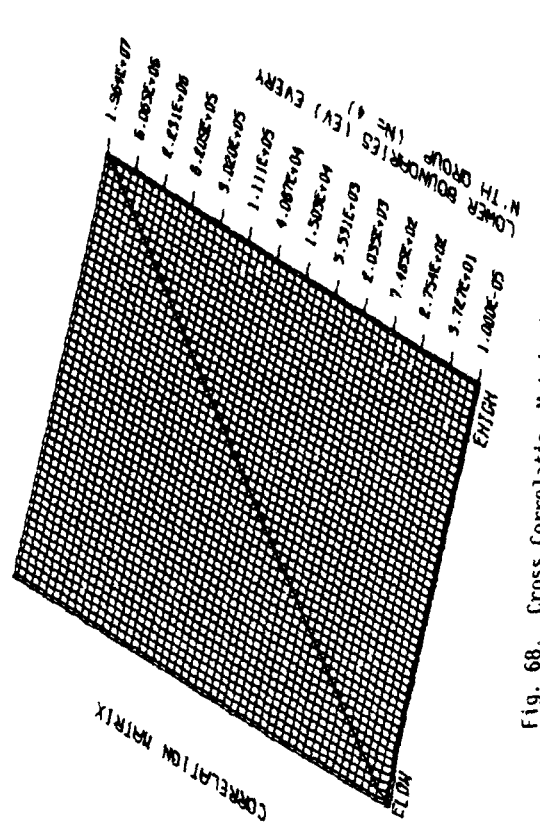


Fig. 69. Cross Correlation Matrix for Na Elastic to Na(n,p) Cross Sections.

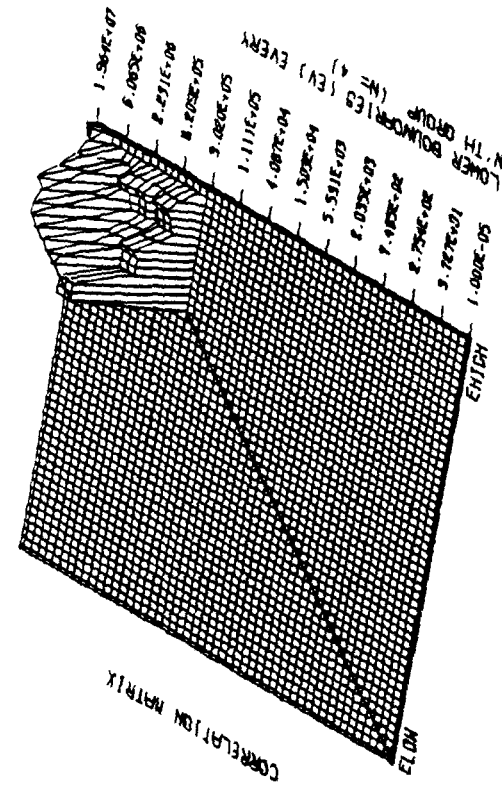


Fig. 70. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 0 Cross Sections.

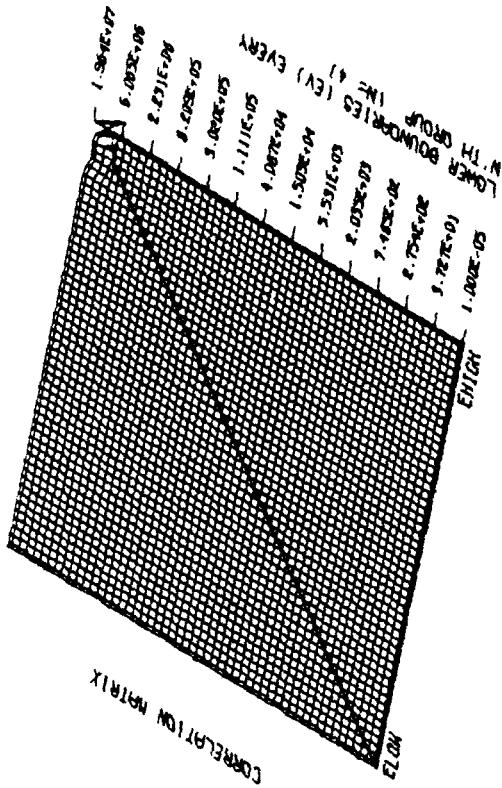


Fig. 71. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 1 Cross Sections.

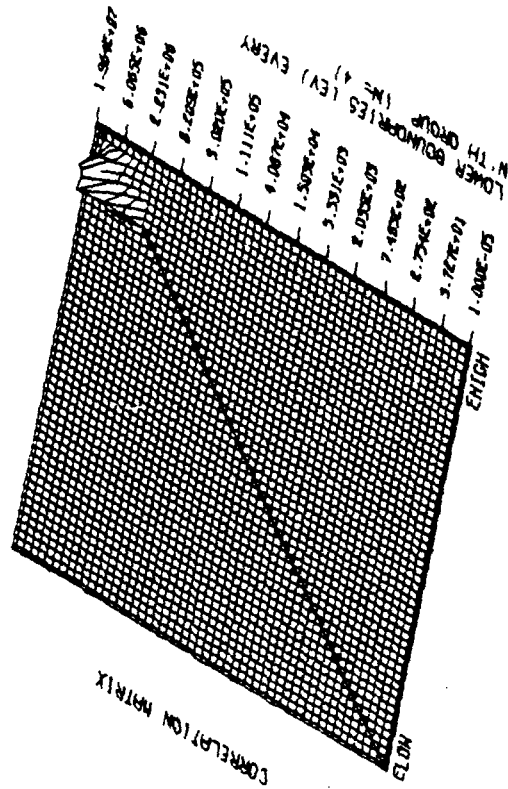


Fig. 72. Cross Correlation Matrix for Na Elastic to Na(n,n') Level 2 Cross Sections.

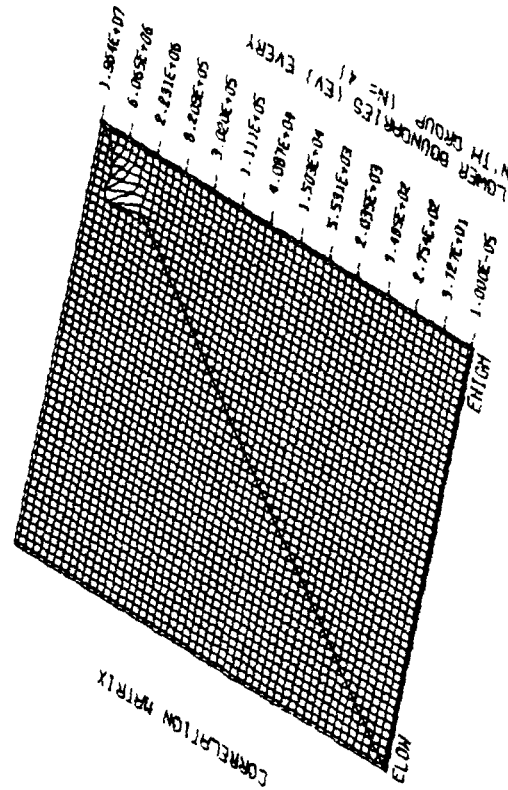


Fig. 73. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 3 Cross Sections.

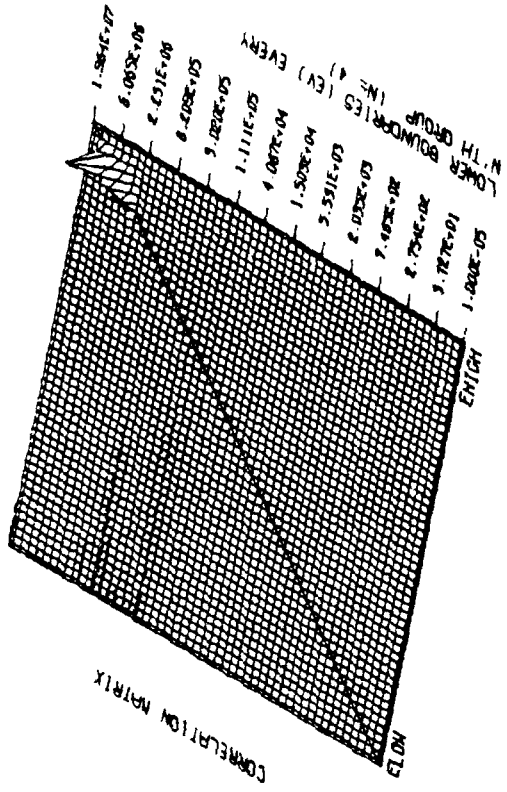


Fig. 75. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 5 Cross Sections.

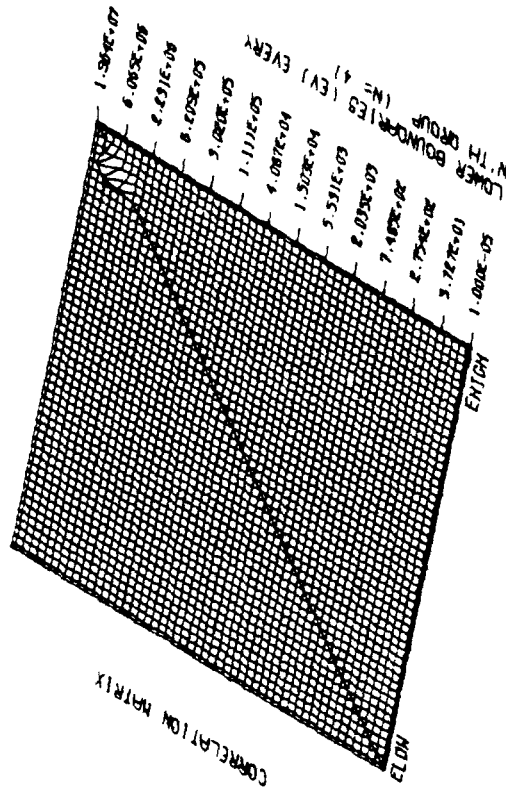


Fig. 77. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 7 Cross Sections.

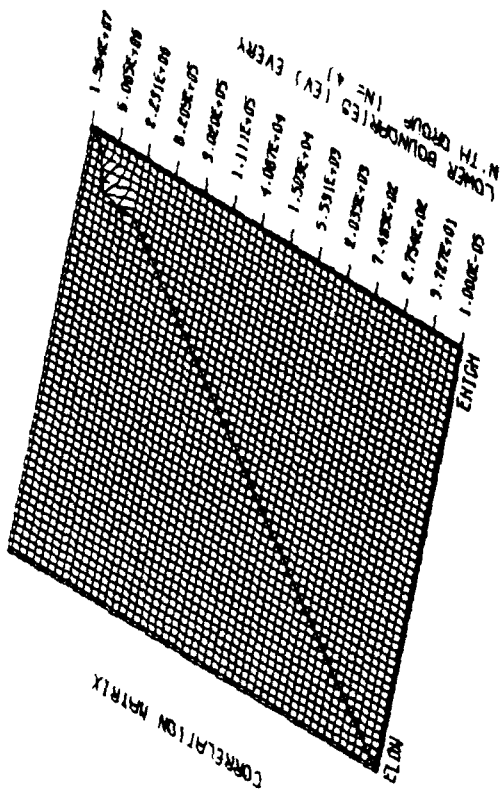


Fig. 74. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 4 Cross Sections.

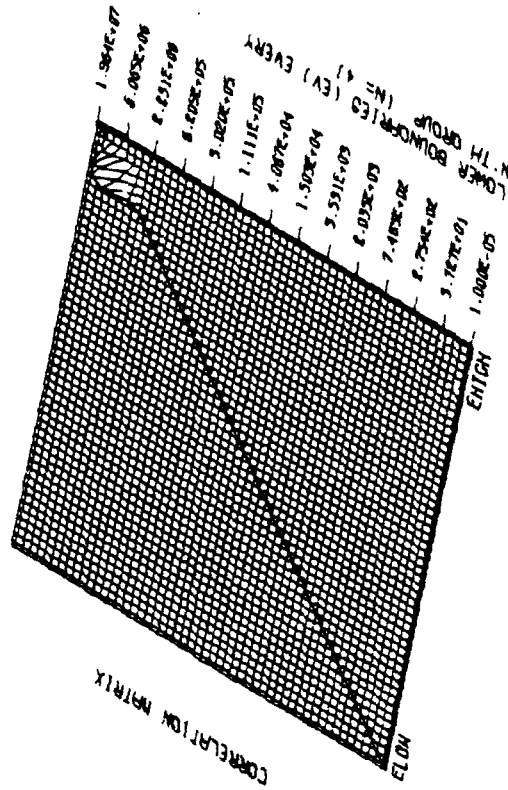


Fig. 76. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 6 Cross Sections.

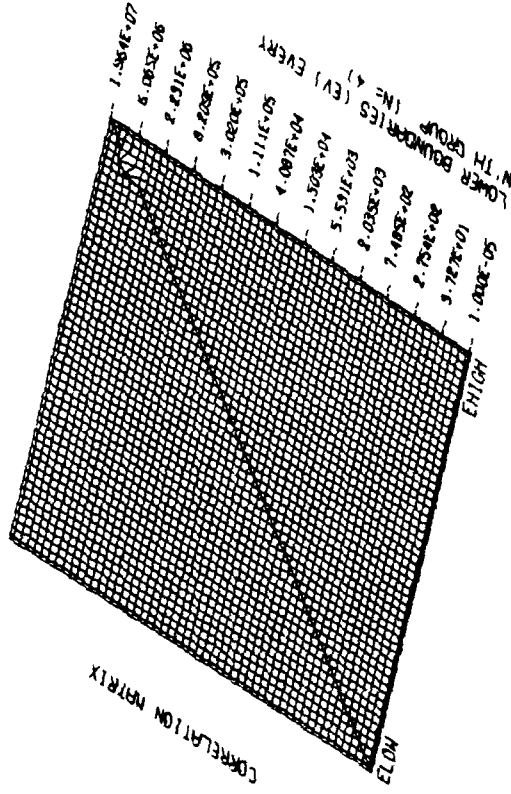


Fig. 79. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 9 Cross Sections.

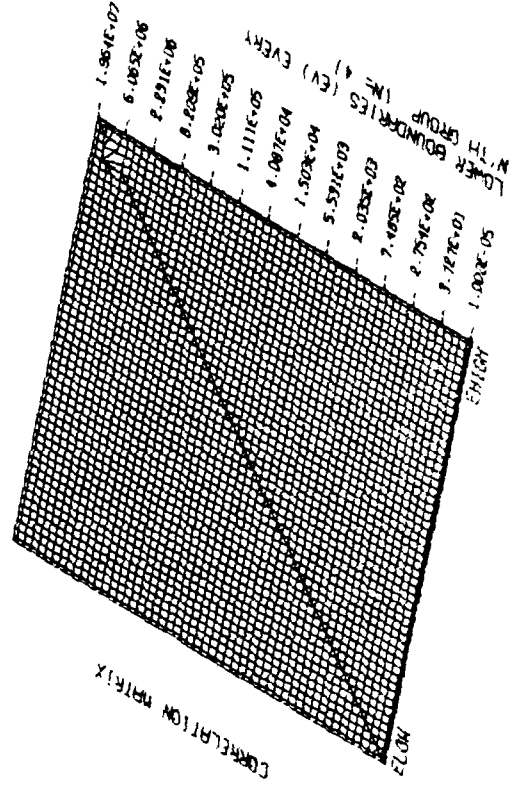


Fig. 81. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 11 Cross Sections.

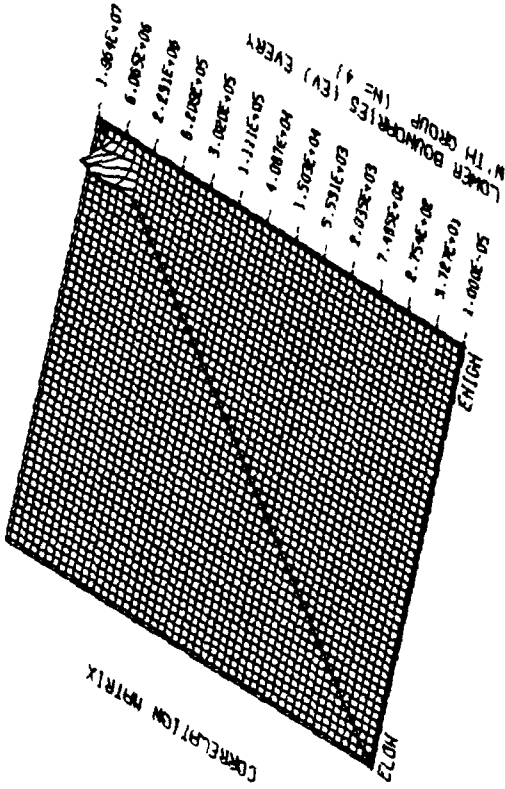


Fig. 78. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 8 Cross Sections.

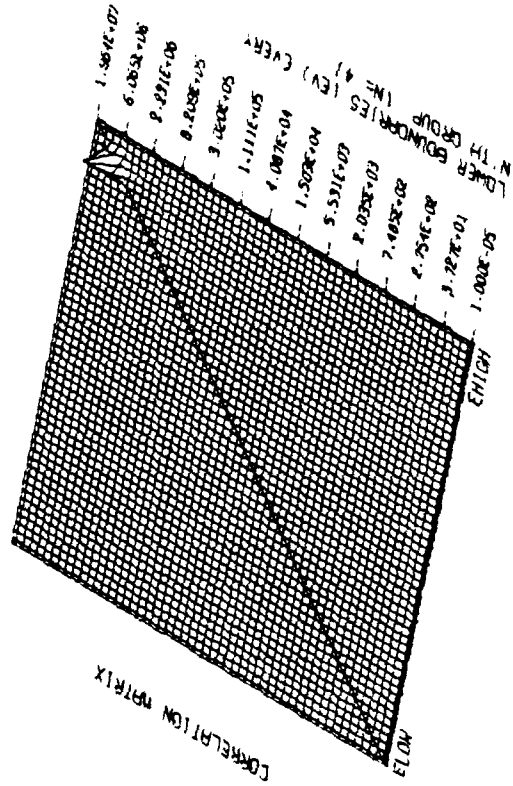


Fig. 80. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 10 Cross Sections.

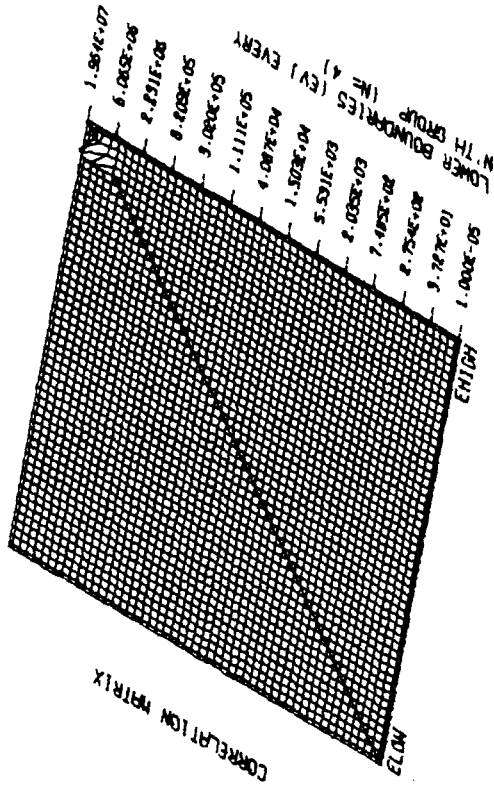


Fig. 83. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 13 Cross Sections.

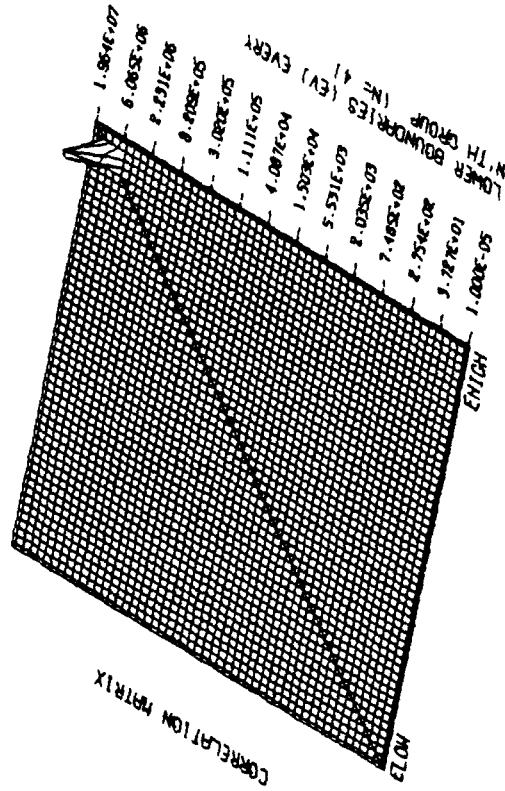


Fig. 85. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 15 Cross Sections.

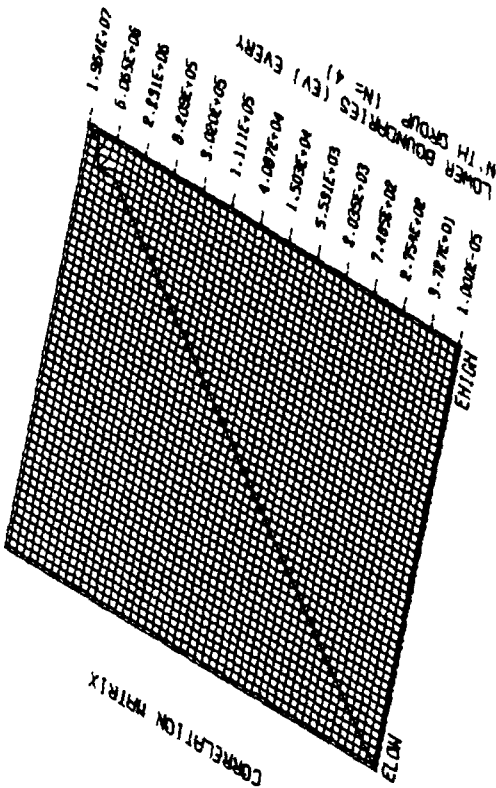


Fig. 82. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 12 Cross Sections.

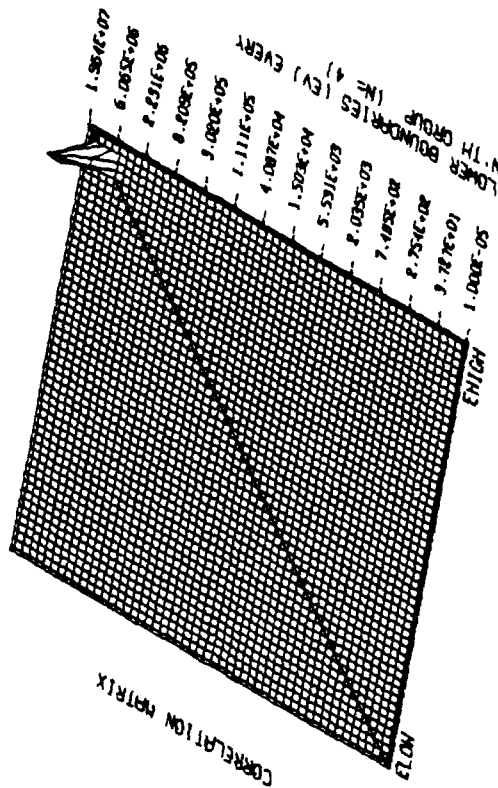


Fig. 84. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 14 Cross Sections.

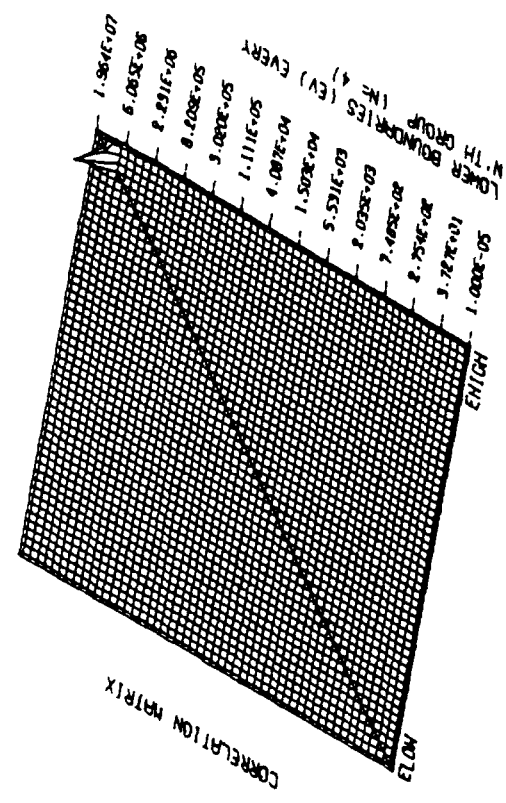


Fig. 87. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 17 Cross Sections.

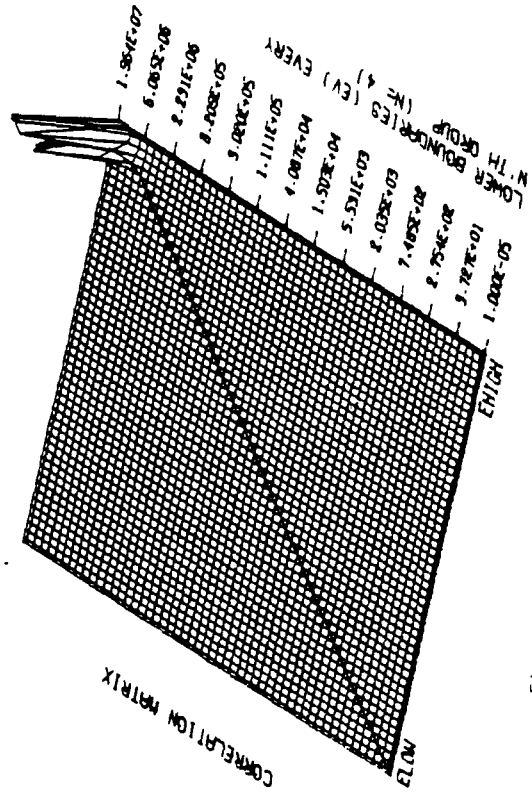


Fig. 89. Cross Correlation Matrix for Na Inelastic to Na(n,n') Continuum Cross Sections.

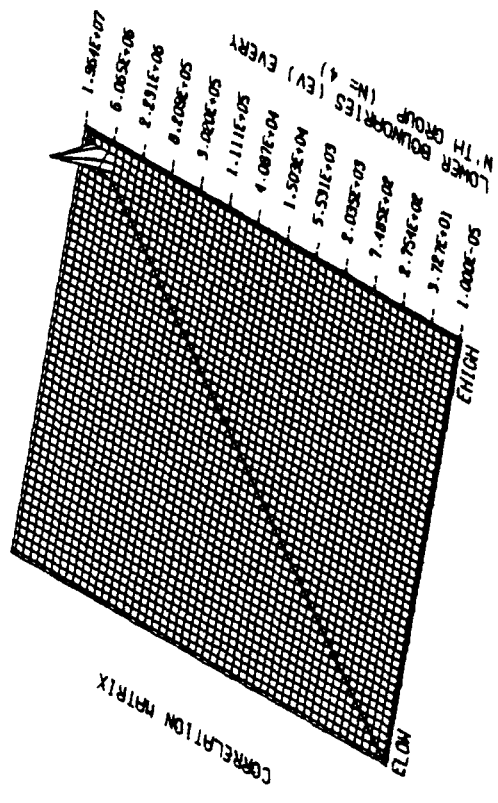


Fig. 86. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 16 Cross Sections.

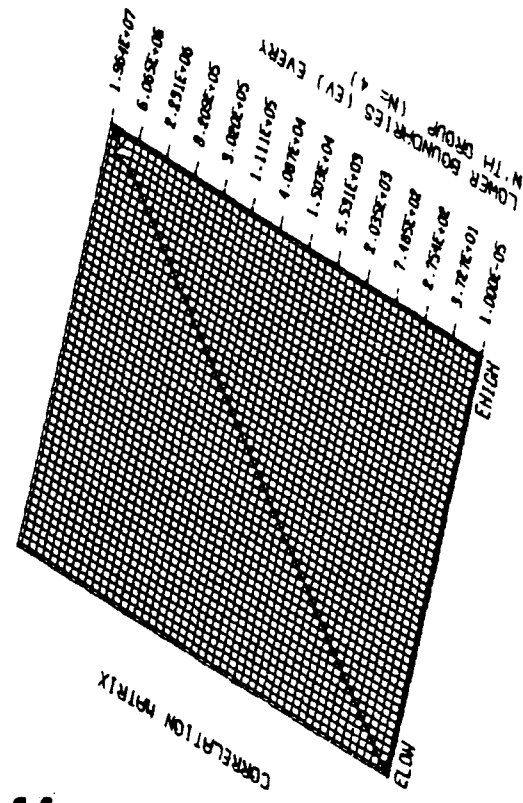


Fig. 88. Cross Correlation Matrix for Na Inelastic to Na(n,n') Level 18 Cross Sections.

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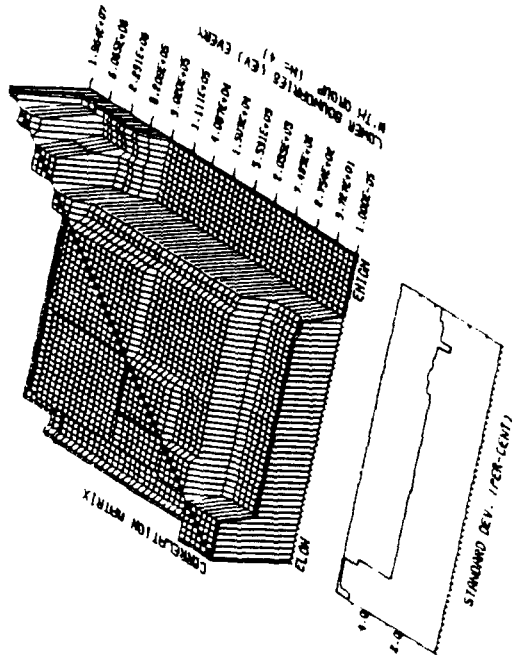


Fig. 91. Standard Deviation and Correlation Matrix for Fe Total Cross Sections.

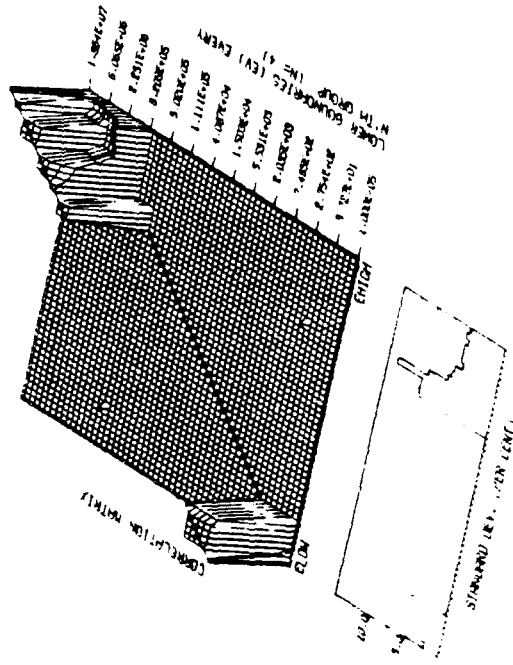


Fig. 93. Standard Deviation and Correlation Matrix for Fe Non-Elastic Cross Sections.

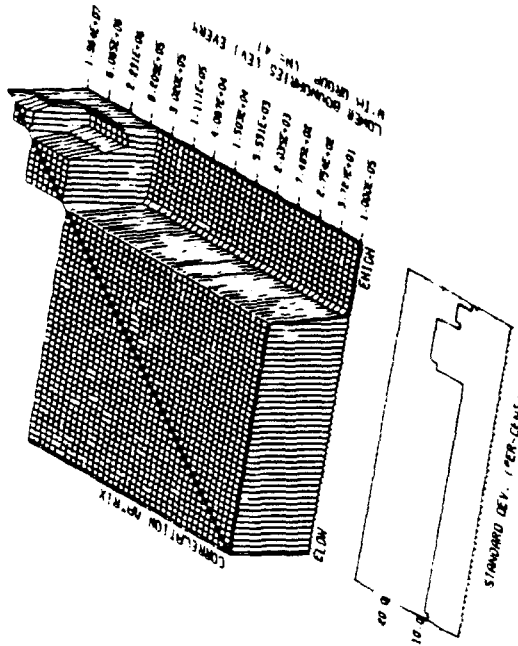


Fig. 90. Standard Deviation and Correlation Matrix for Cr(n,γ) Cross Sections.

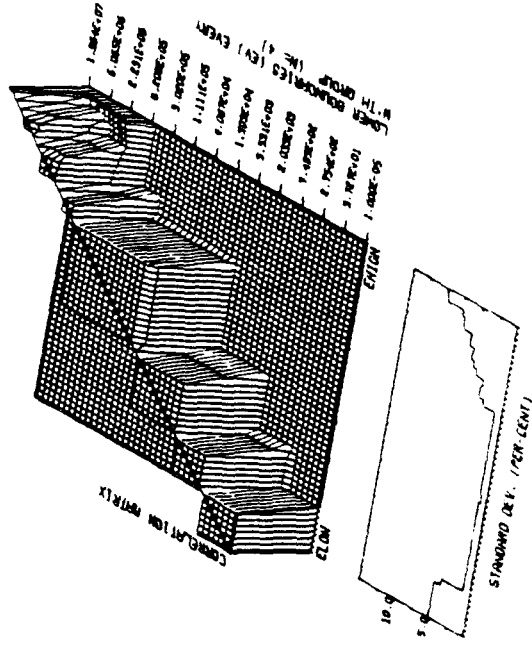


Fig. 92. Standard Deviation and Correlation Matrix for Fe Elastic Cross Sections.

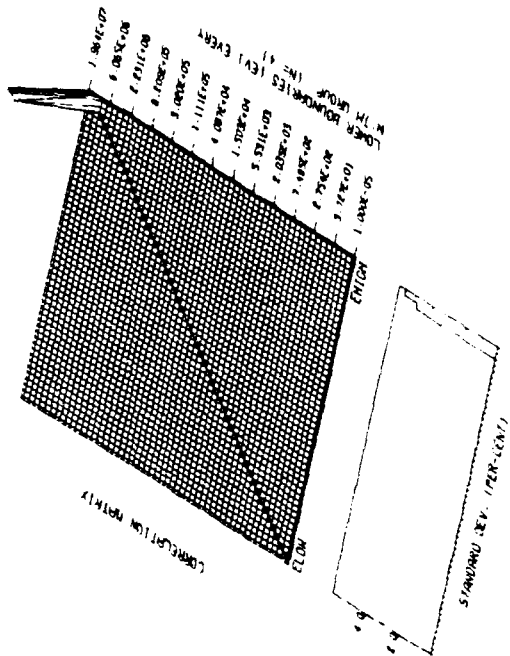


Fig. 95. Standard Deviation and Correlation Matrix for Fe(n,2n) Cross Sections.

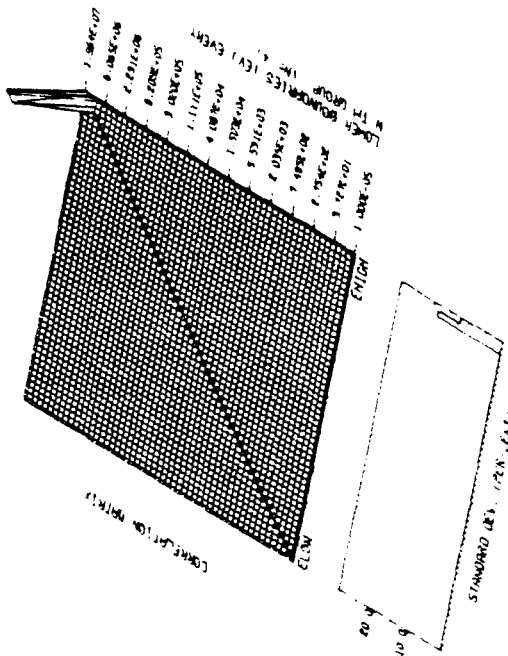


Fig. 97. Standard Deviation and Correlation Matrix for Fe(n,n'p) Cross Sections.

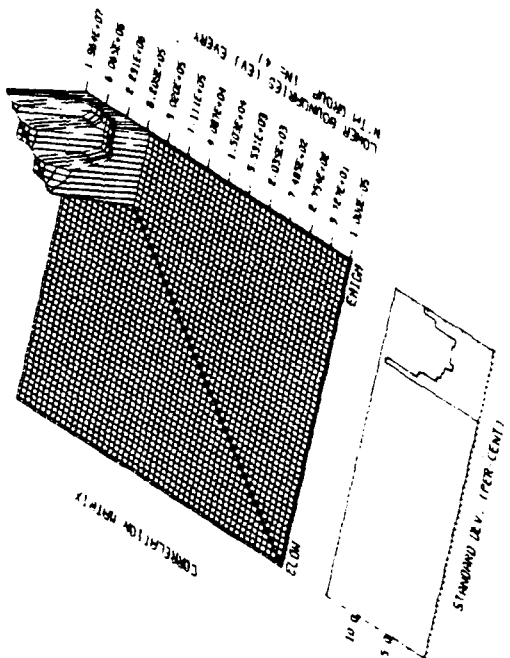


Fig. 94. Standard Deviation and Correlation Matrix for Fe Inelastic Cross Sections.

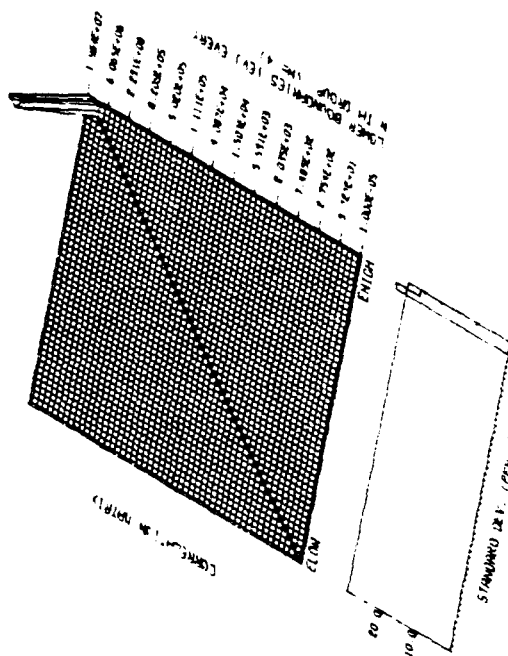


Fig. 96. Standard Deviation and Correlation Matrix for Fe(n,n'a) Cross Sections.

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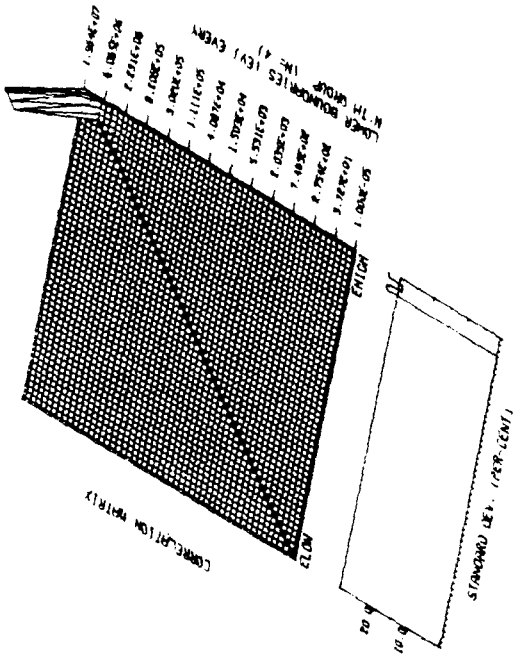


Fig. 99. Standard Deviation and Correlation Matrix for Fe(n,d) Cross Sections.

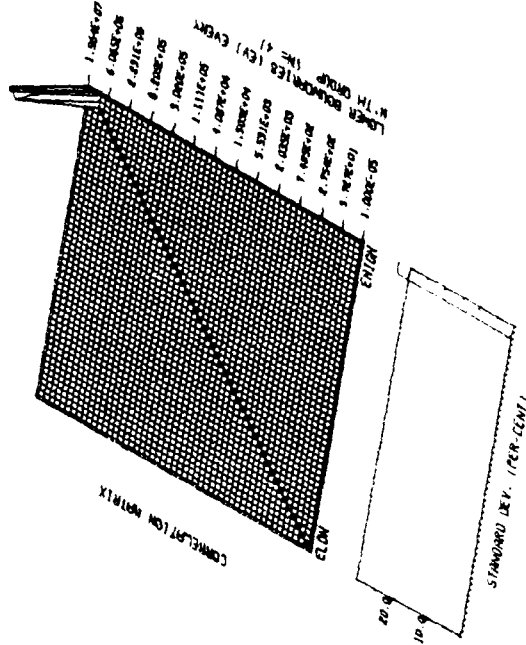


Fig. 101. Standard Deviation and Correlation Matrix for Fe(n,He) cross Sections.

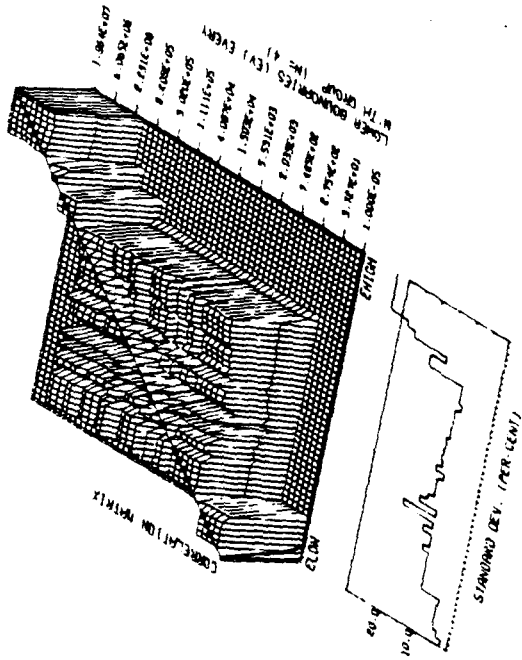


Fig. 98. Standard Deviation and Correlation Matrix for Fe(n,y) Cross Sections.

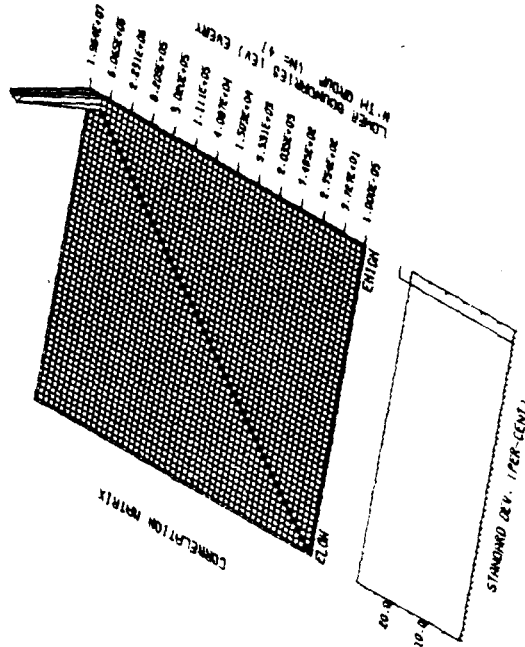


Fig. 100. Standard Deviation and Correlation Matrix for Fe(n,t) Cross Sections.

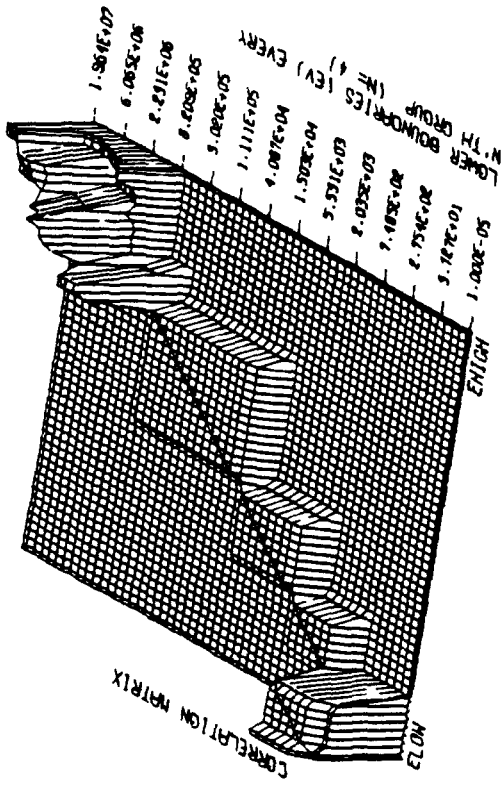


Fig. 103. Cross Correlation Matrix for Fe Total to Fe Elastic Cross Sections.

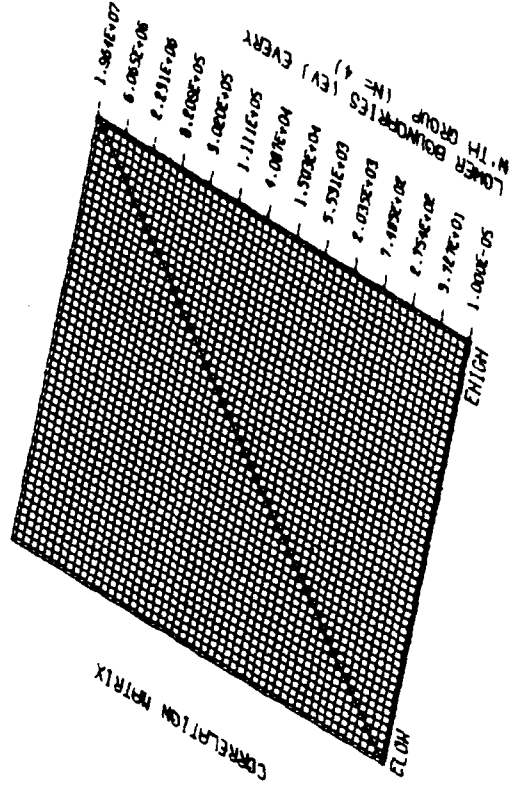


Fig. 105. Cross Correlation Matrix for Fe Elastic to Fe(n,y) Cross Sections.

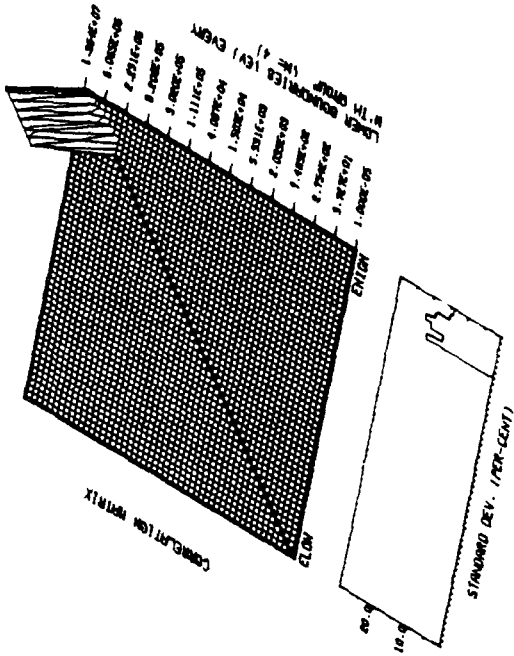


Fig. 102. Standard Deviation and Correlation Matrix for Fe(n,a) Cross Sections.

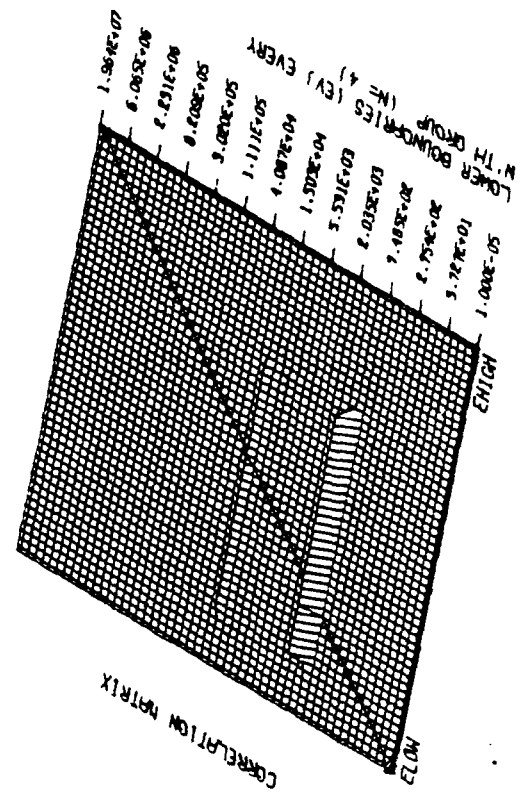


Fig. 104. Cross Correlation Matrix for Fe Total to Fe(n,gamma) Cross Sections.

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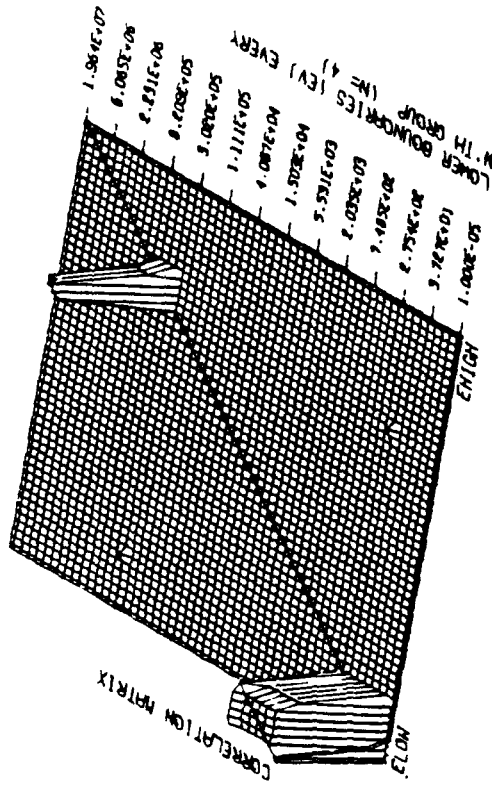


Fig. 107. Cross Correlation Matrix for Fe Non-Elastic to Fe(n,γ) Cross Sections.

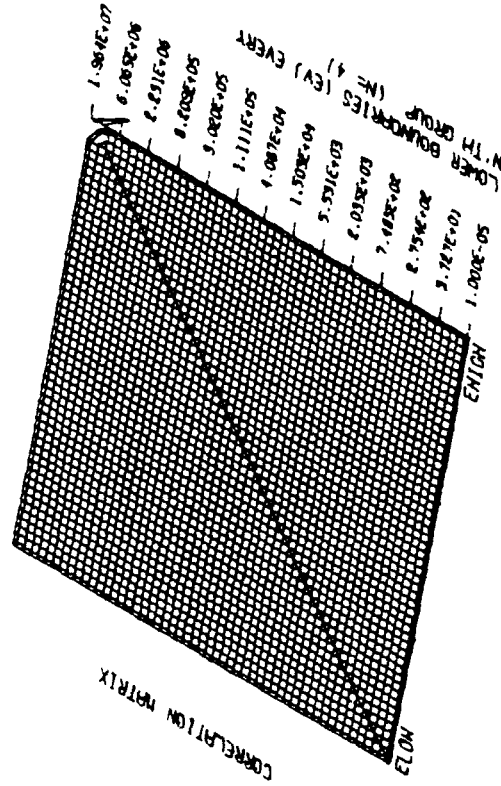


Fig. 109. Cross Correlation Matrix for Fe Inelastic to Fe(n,2n) Cross Sections.

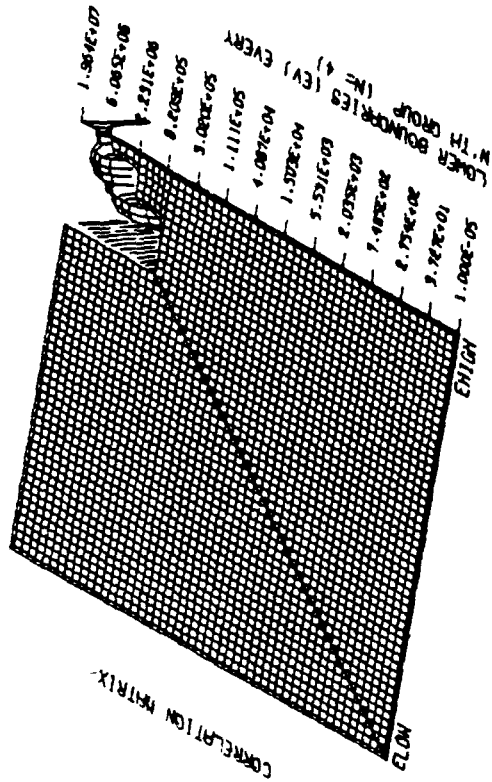


Fig. 106. Cross Correlation Matrix for Fe Elastic to Fe Non-Elastic Cross Sections.

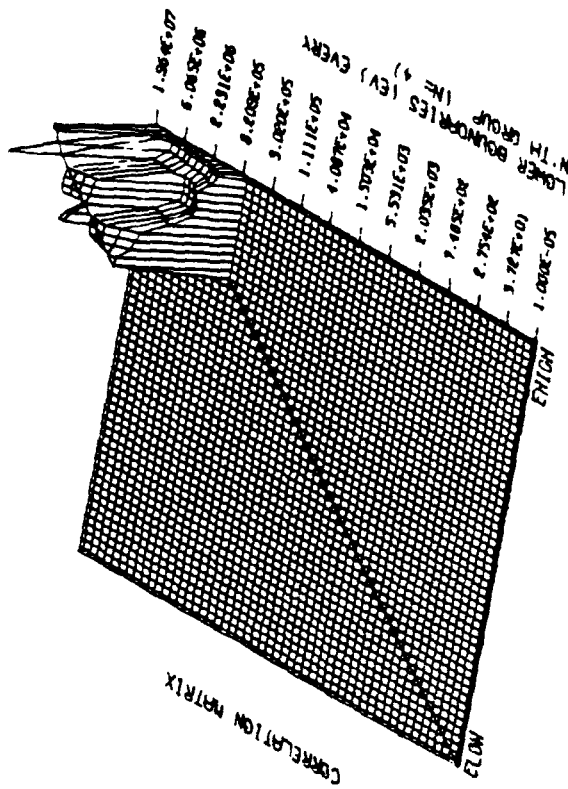


Fig. 108. Cross Correlation Matrix for Fe Inelastic to Fe Non-Elastic Cross Sections.

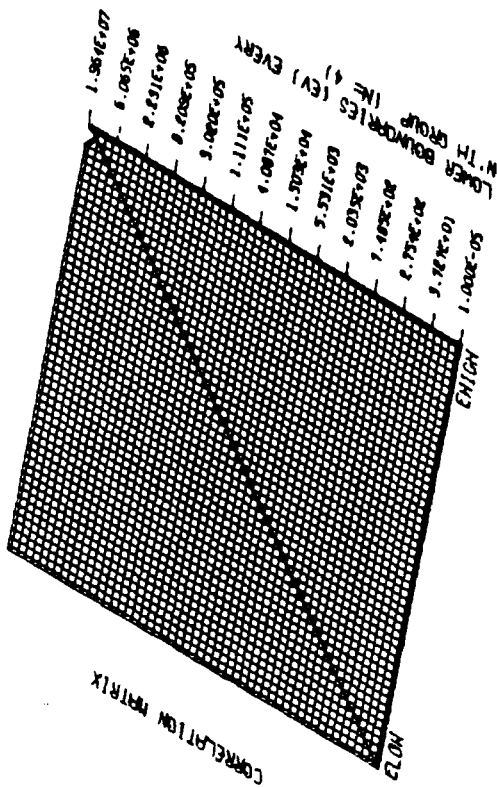


Fig. 110. Cross Correlation Matrix for Fe Inelastic to Fe(n,n'α) Cross Sections.

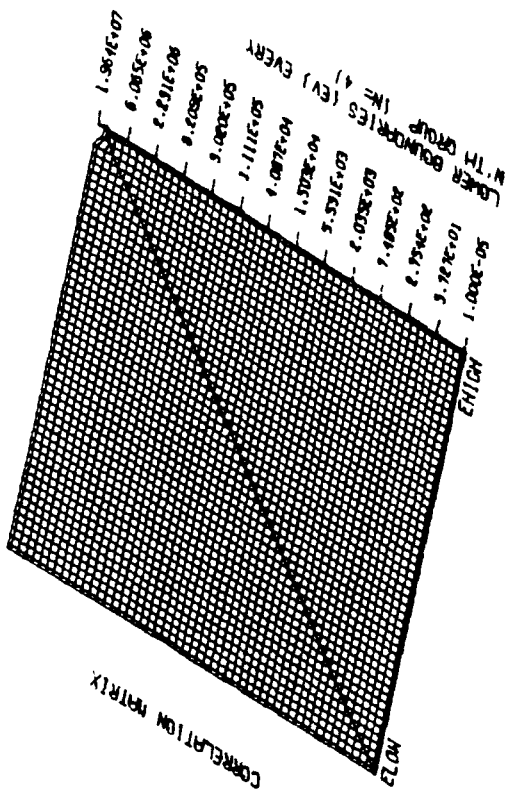


Fig. 111. Cross Correlation Matrix for Fe Inelastic to Fe(n,n'p) Cross Sections.

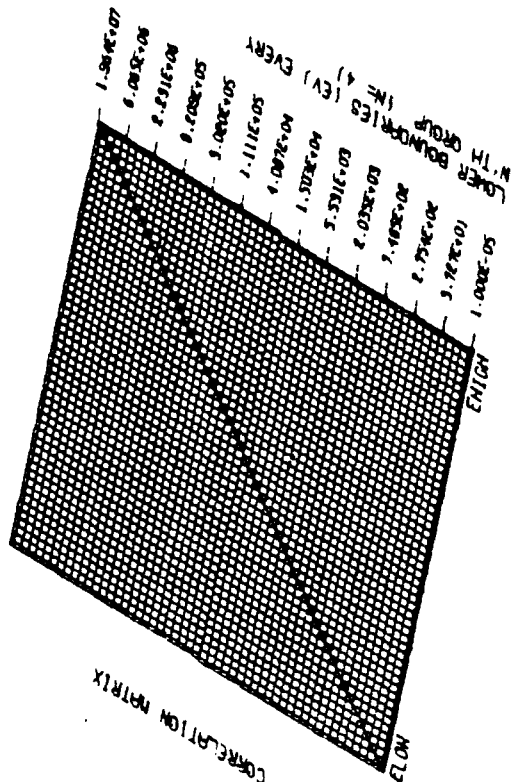


Fig. 112. Cross Correlation Matrix for Fe Inelastic to Fe(n,n'γ) Cross Sections.

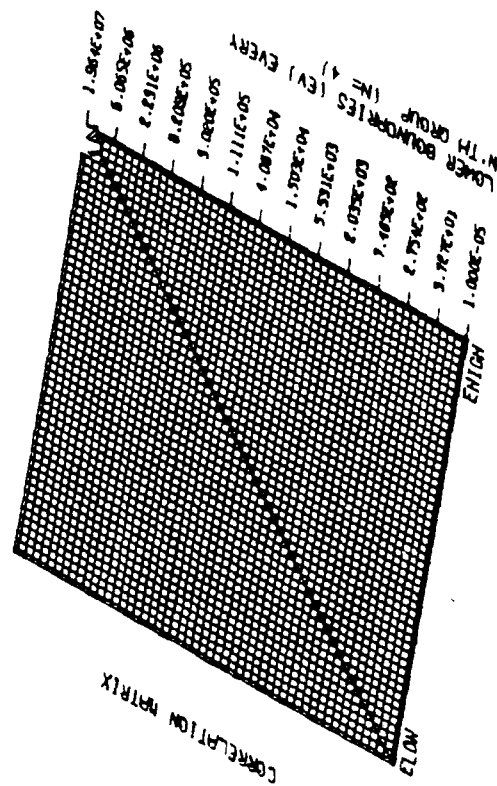


Fig. 113. Cross Correlation Matrix for Fe Inelastic to Fe(n,d) Cross Sections.

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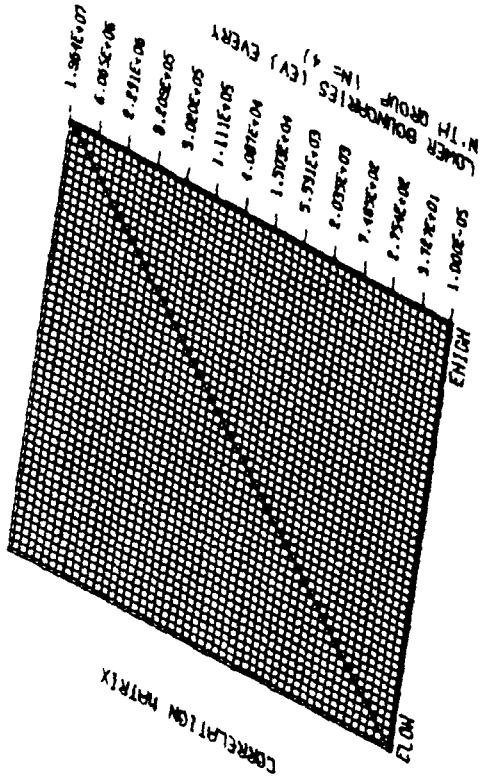


Fig. 115. Cross Correlation Matrix for Fe Inelastic to Fe(n,He) Cross Sections.

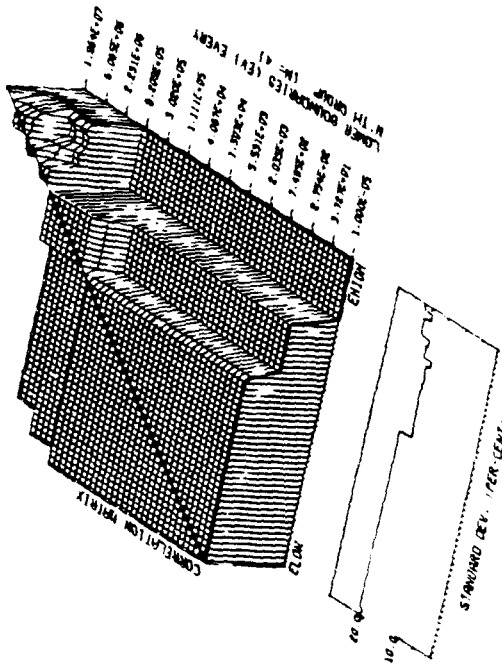


Fig. 117. Standard Deviation and Correlation Matrix for Ni(n, γ) Cross Sections.

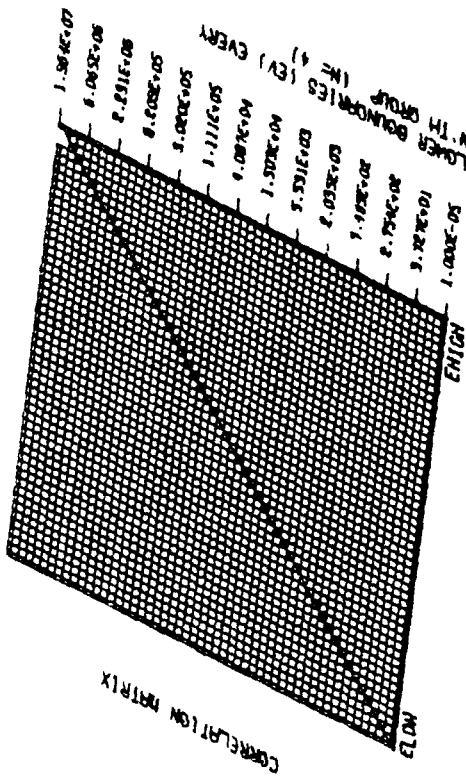


Fig. 114. Cross Correlation Matrix for Fe Inelastic to Fe(n,t) Cross Sections.

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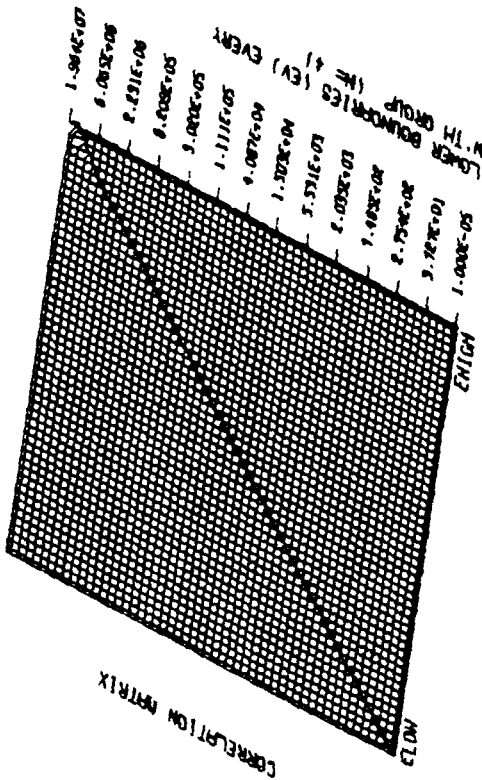


Fig. 116. Cross Correlation Matrix for Fe Inelastic to Fe(n, α) Cross Sections.

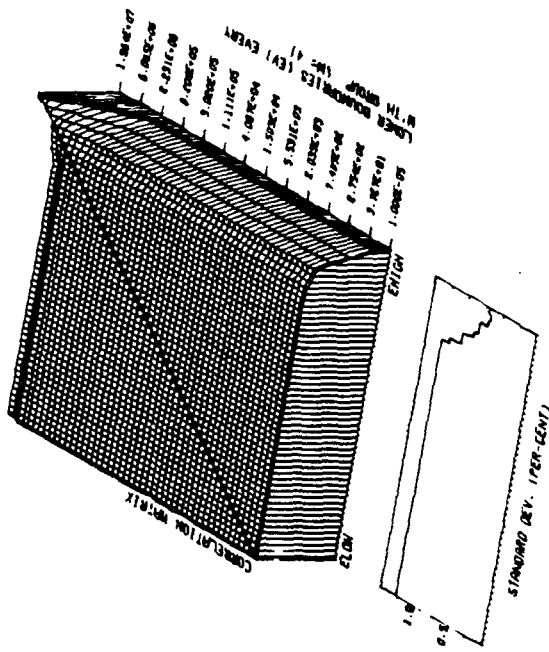


Fig. 119. Standard Deviation and Correlation Matrix for $^{240}\text{Pu}(\bar{\nu})$ Cross Section.

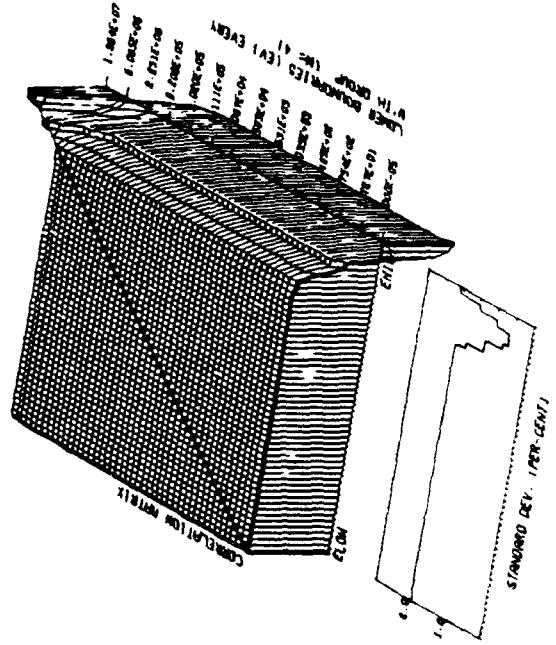


Fig. 121. Standard Deviation and Correlation Matrix for $^{241}\text{Pu}(\nu)$ Cross Section.

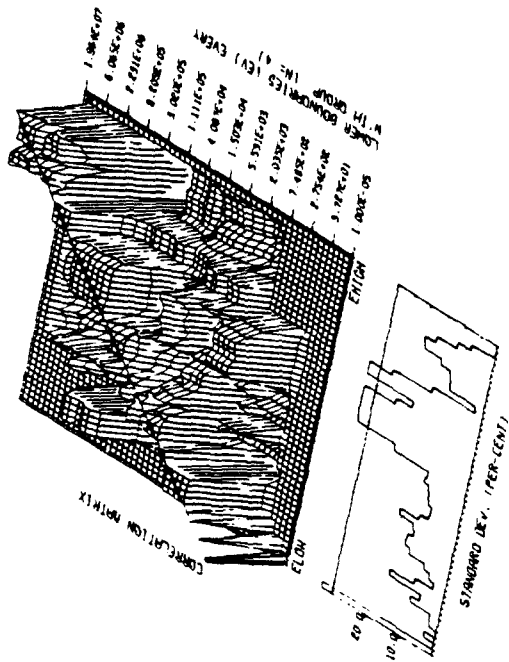


Fig. 118. Standard Deviation and Correlation Matrix for $^{240}\text{Pu}(n,\gamma)$ Cross Sections.

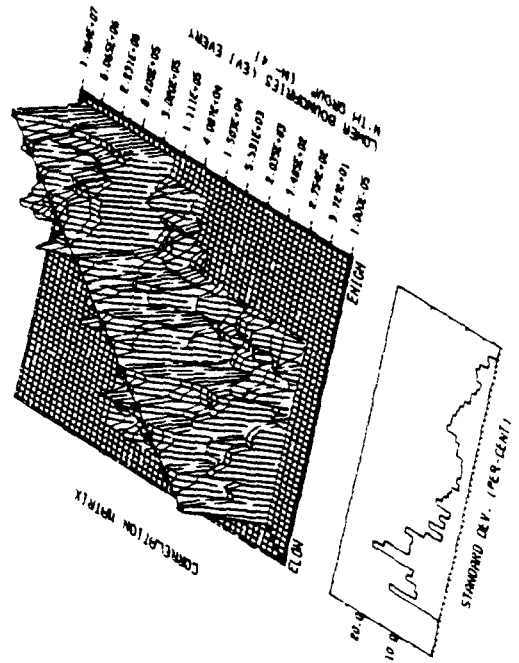


Fig. 120. Standard Deviation and Correlation Matrix for $^{241}\text{Pu}(n,f)$ Cross Sections.

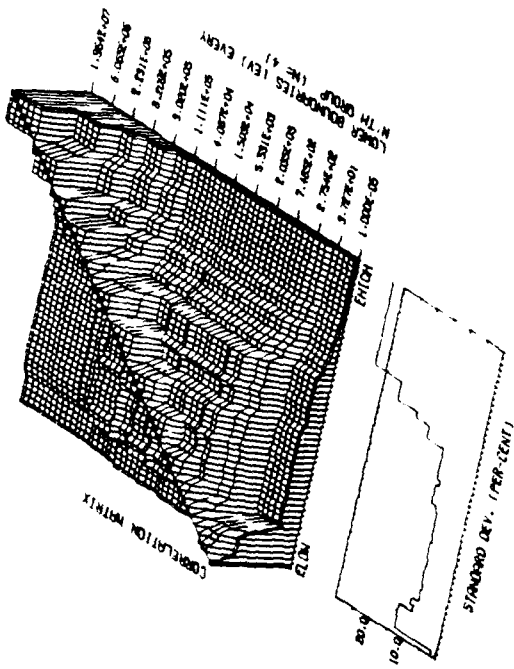


Fig. 123. Standard Deviation and Correlation Matrix for 235U(n,γ) Cross Sections.

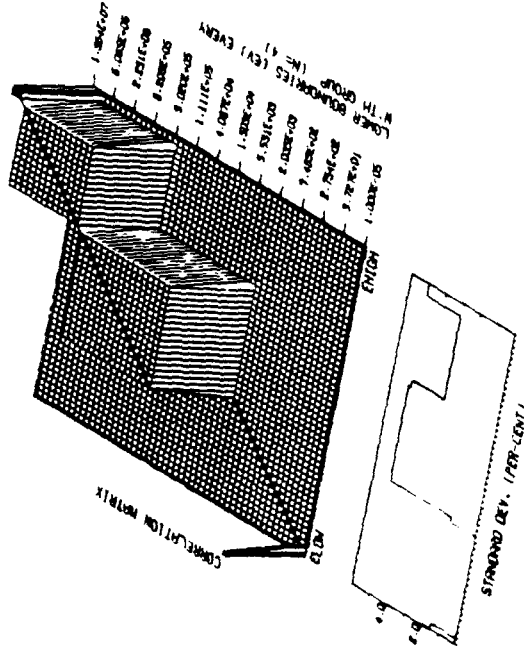


Fig. 125. Standard Deviation and Correlation Matrix for 238U Total Cross Sections.

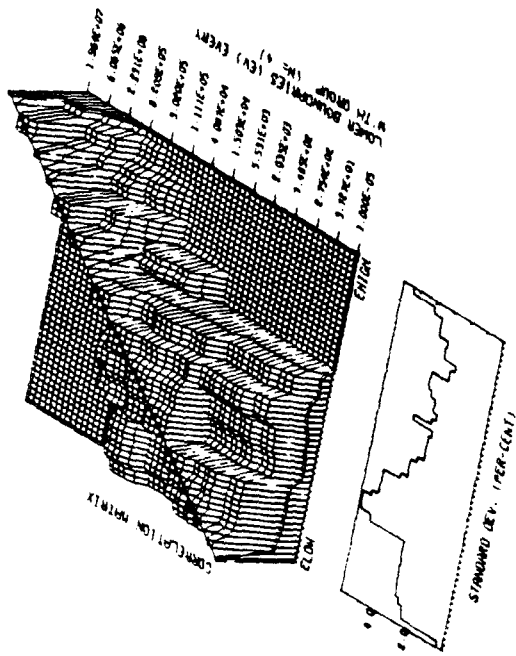


Fig. 122. Standard Deviation and Correlation Matrix for 235U(n,f) Cross Sections.

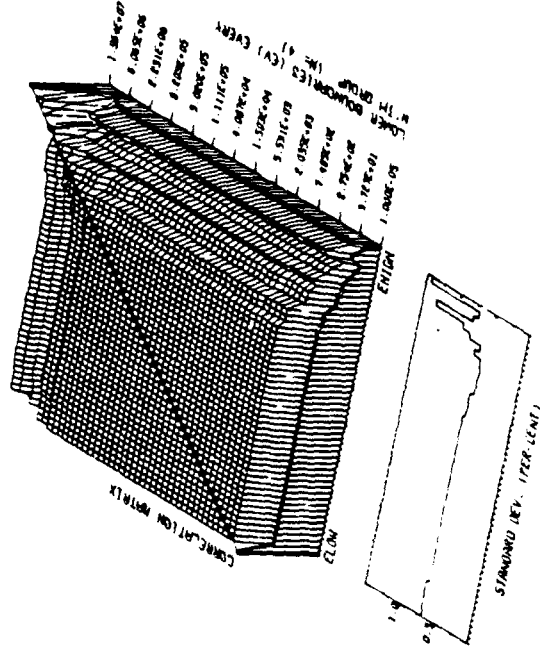


Fig. 124. Standard Deviation and Correlation Matrix for 235U(v) Cross Section.

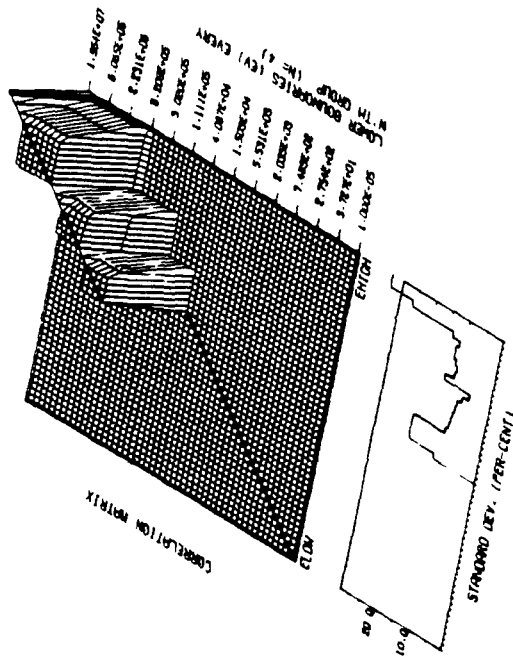


Fig. 127. Standard Deviation and Correlation Matrix for ^{238}U Inelastic Cross Sections.

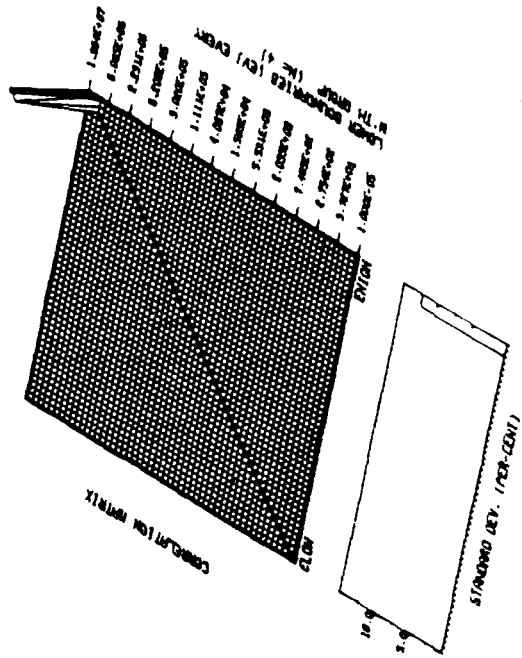


Fig. 129. Standard Deviation and Correlation Matrix for $^{238}\text{U}(n,3n)$ Cross Sections.

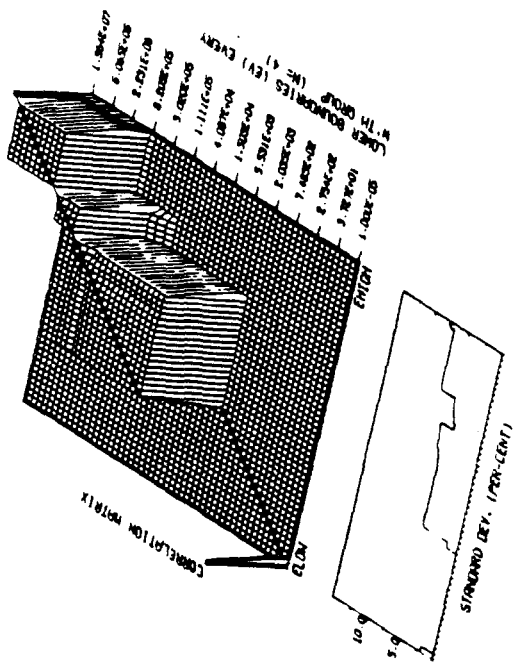


Fig. 126. Standard Deviation and Correlation Matrix for ^{238}U Elastic Cross Sections.

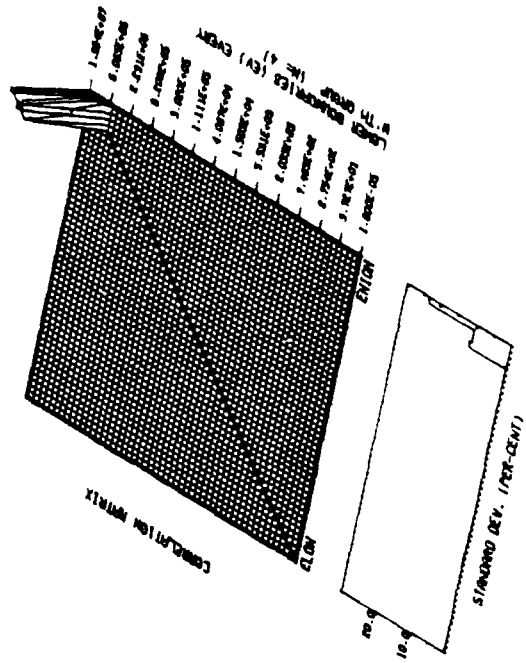


Fig. 128. Standard Deviation and Correlation Matrix for $^{238}\text{U}(n,2n)$ Cross Sections.

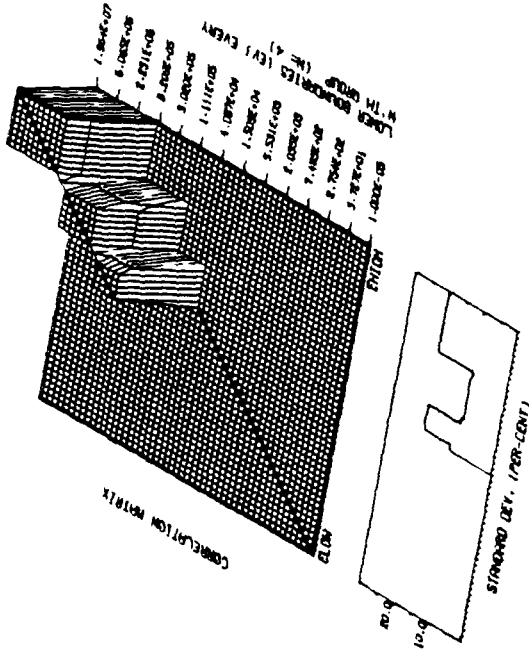


Fig. 131. Standard Deviation and Correlation Matrix for $^{238}\text{U}(n,n')$ Level 1 Cross Sections.

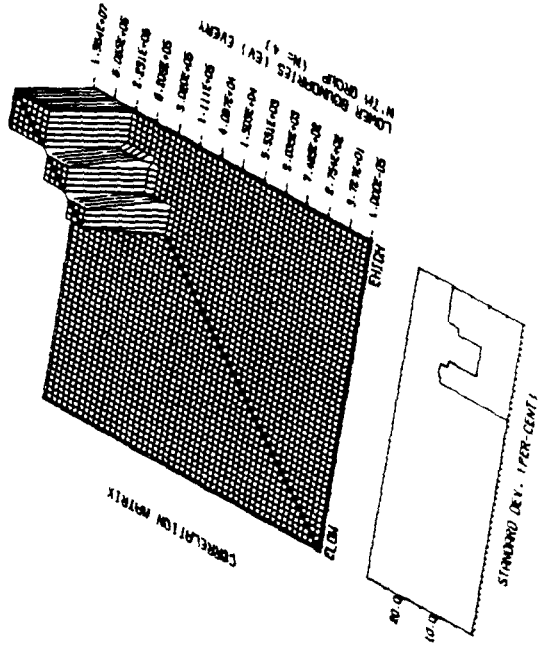


Fig. 133. Standard Deviation and Correlation Matrix for $^{238}\text{U}(n,n')$ Level 3 Cross Sections.

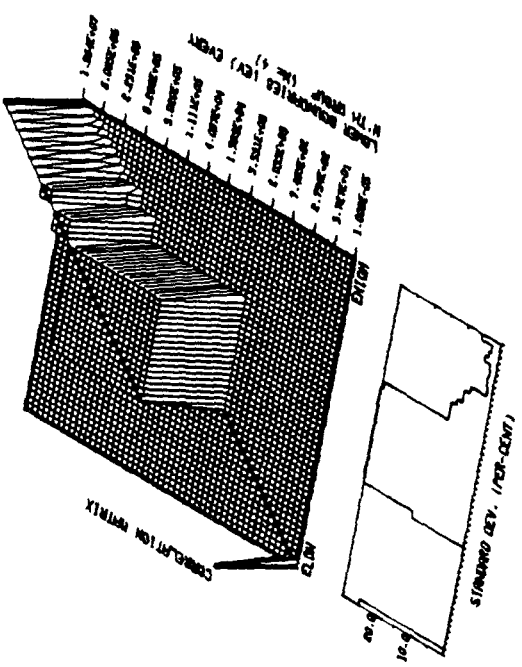


Fig. 130. Standard Deviation and Correlation Matrix for $^{238}\text{U}(n,f)$ Cross Sections.

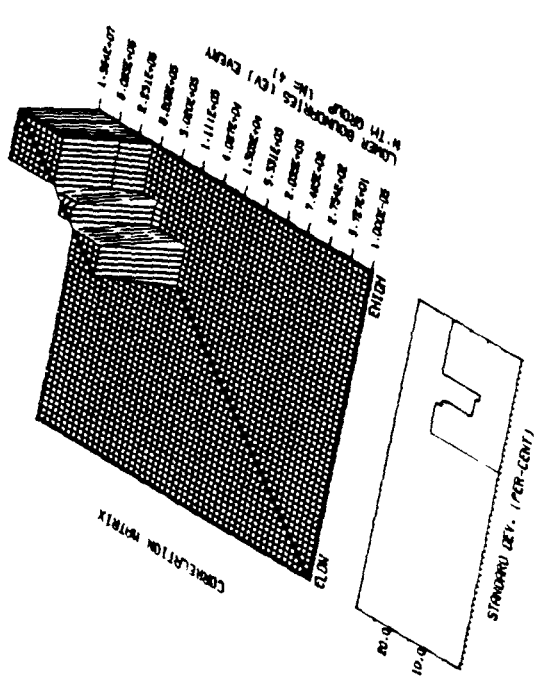


Fig. 132. Standard Deviation and Correlation Matrix for $^{238}\text{U}(n,n')$ Level 2 Cross Sections.

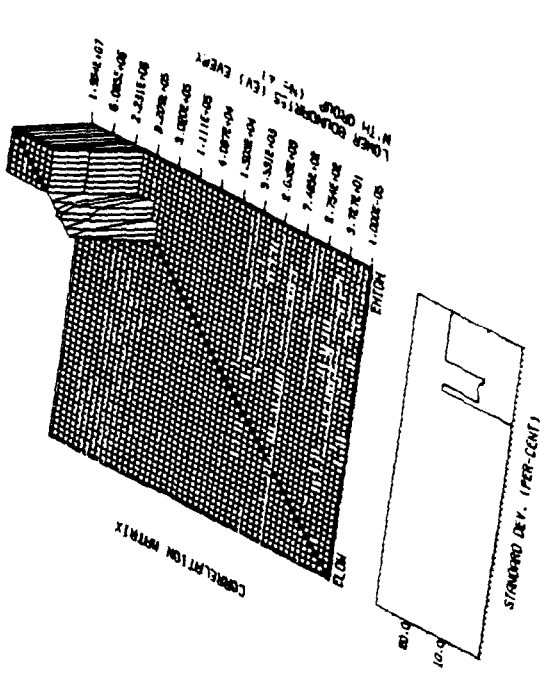


Fig. 135. Standard Deviation and Correlation Matrix for $^{238}\text{U}(n,n')$ Level 5 Cross Sections.

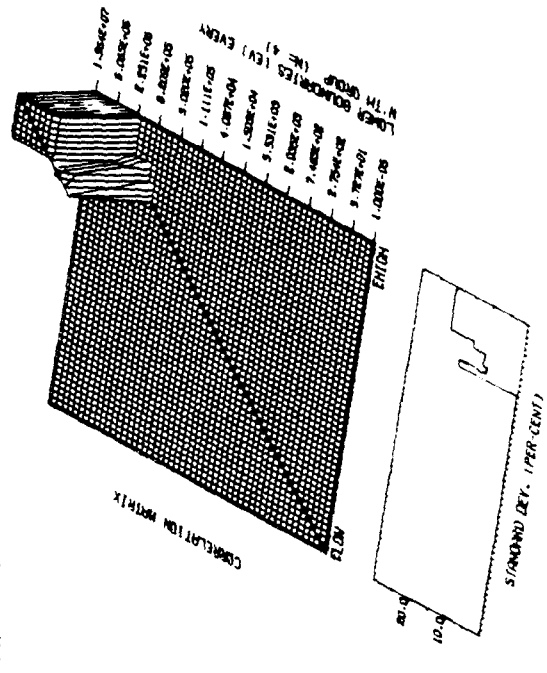


Fig. 137. Standard Deviation and Correlation Matrix for $^{238}\text{U}(n,n')$ Level 7 Cross Sections.

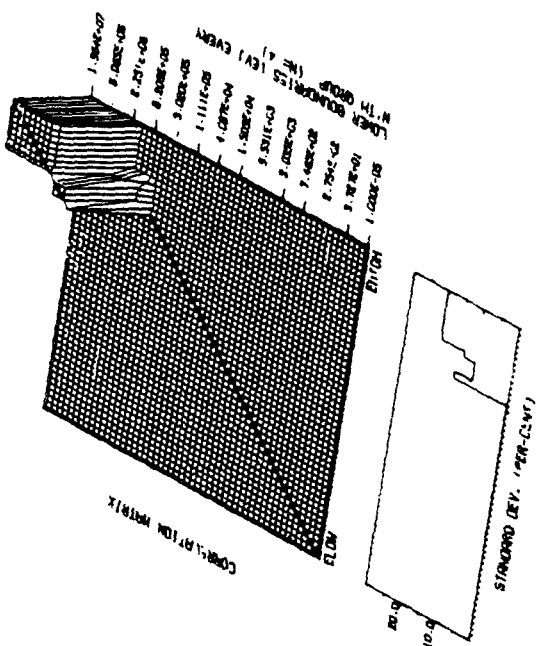


Fig. 134. Standard Deviation and Correlation Matrix for $^{238}\text{U}(n,n')$ Level 4 Cross Sections.

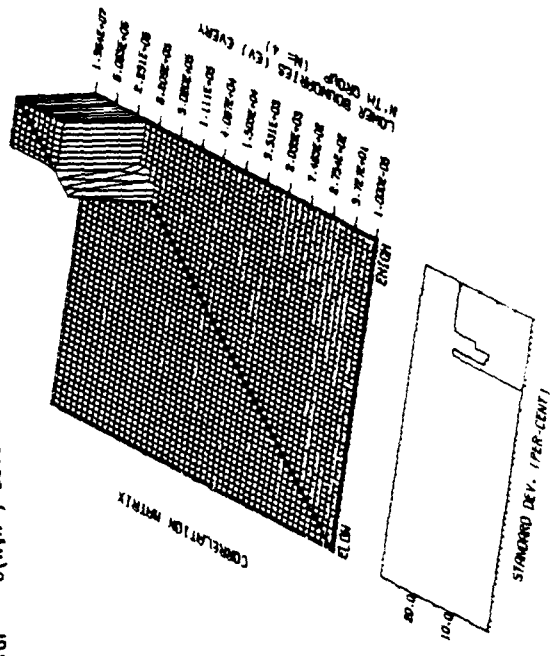


Fig. 136. Standard Deviation and Correlation Matrix for $^{238}\text{U}(n,n')$ Level 6 Cross Sections.

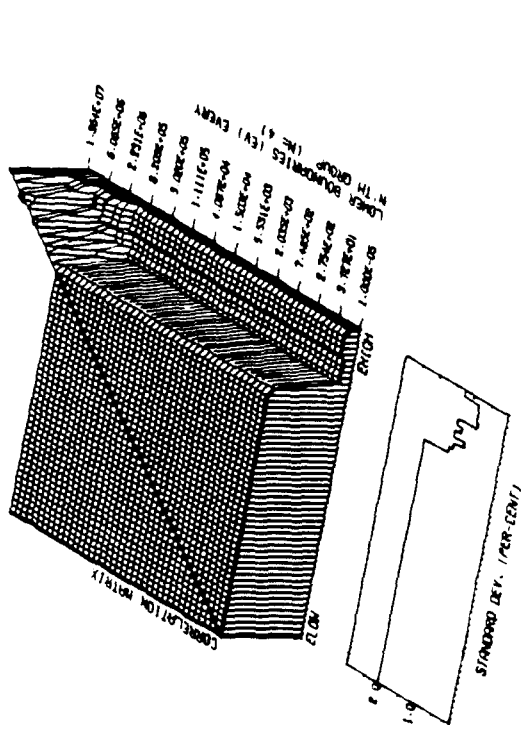


Fig. 139. Standard Deviation and Correlation Matrix for $^{238}\text{U}(v)$ Cross Sections.

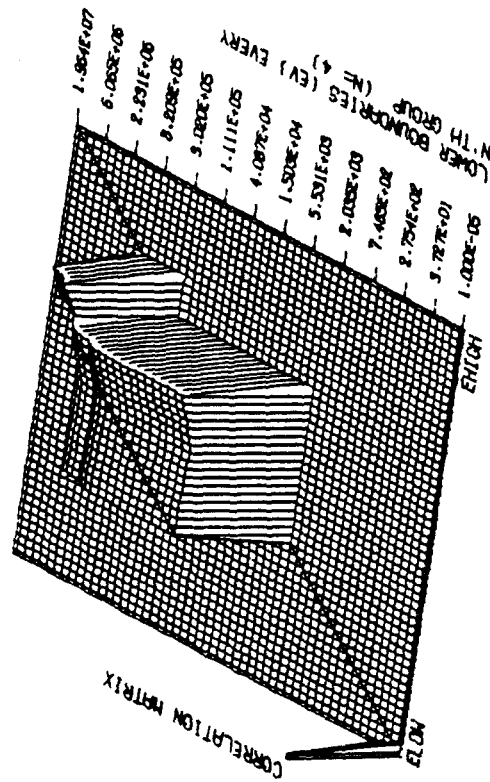


Fig. 141. Cross Correlation Matrix for ^{238}U Total to ^{238}U Elastic Cross Sections.

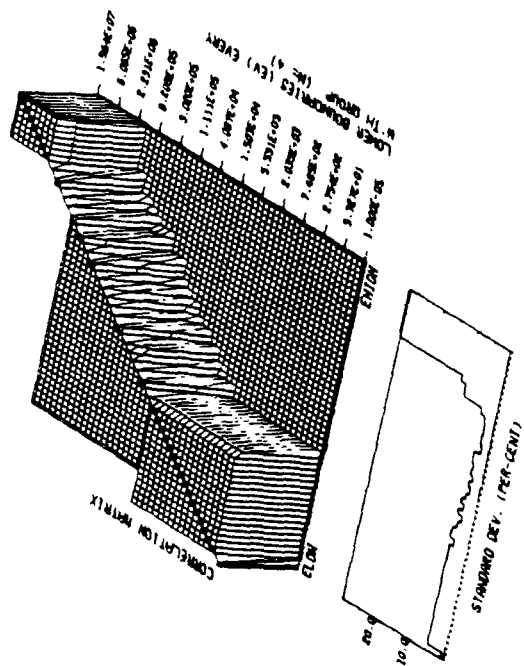


Fig. 138. Standard Deviation and Correlation Matrix for $^{238}\text{U}(n, \gamma)$ Cross Sections.

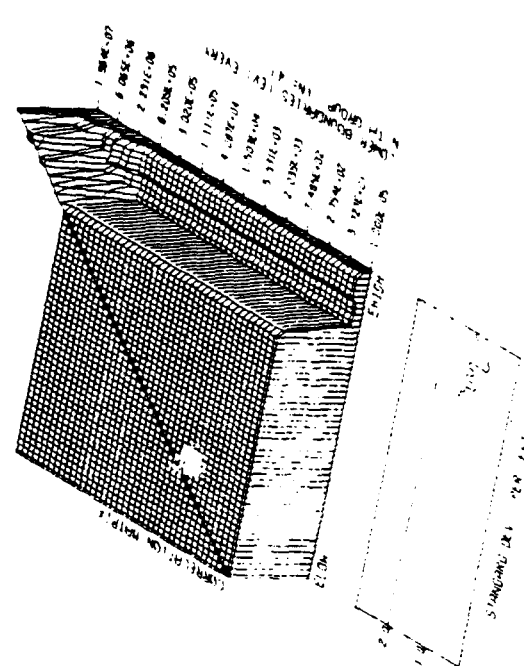


Fig. 140. Standard Deviation and Correlation Matrix for $^{238}\text{U}(v_p)$ Cross Sections.

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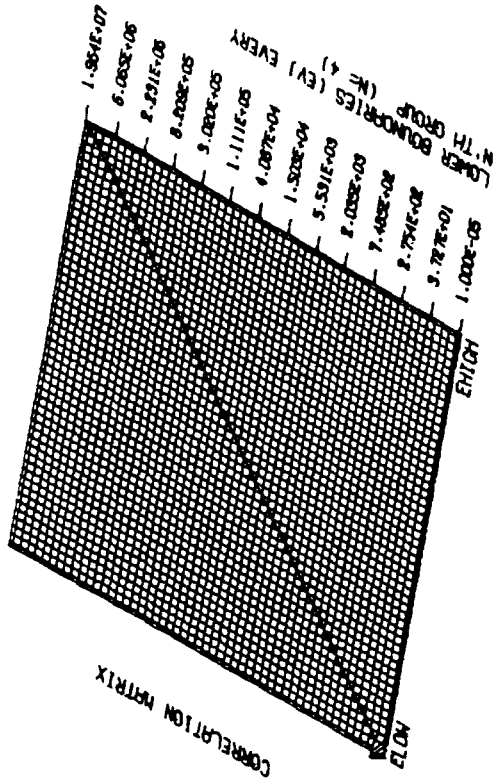


Fig. 143. Cross Correlation Matrix for 238U Total to 238U(n,y) Cross Sections.

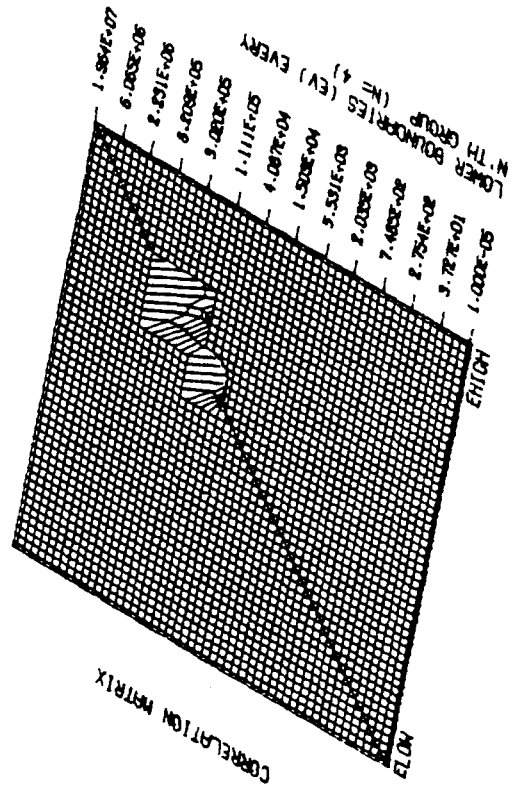


Fig. 145. Cross Correlation Matrix for 238U Elastic to 238U(n,n') Level 1 Cross Sections.

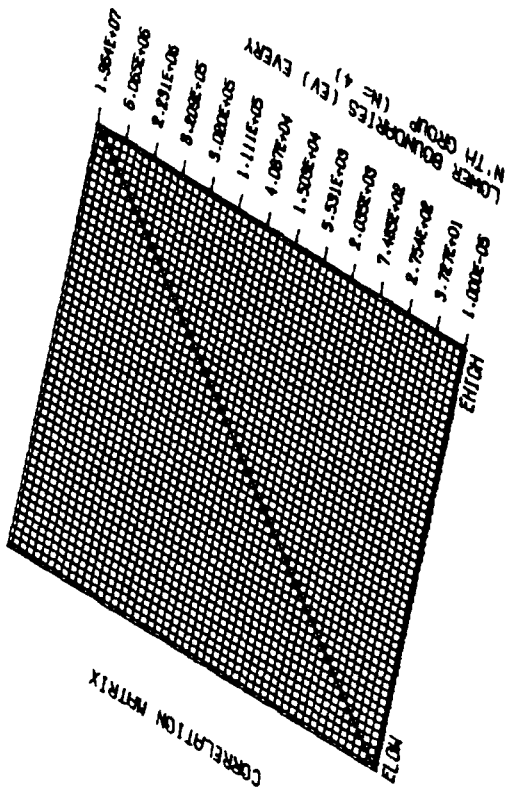


Fig. 142. Cross Correlation Matrix for 238U Total to 238U(n,f) Cross Sections.

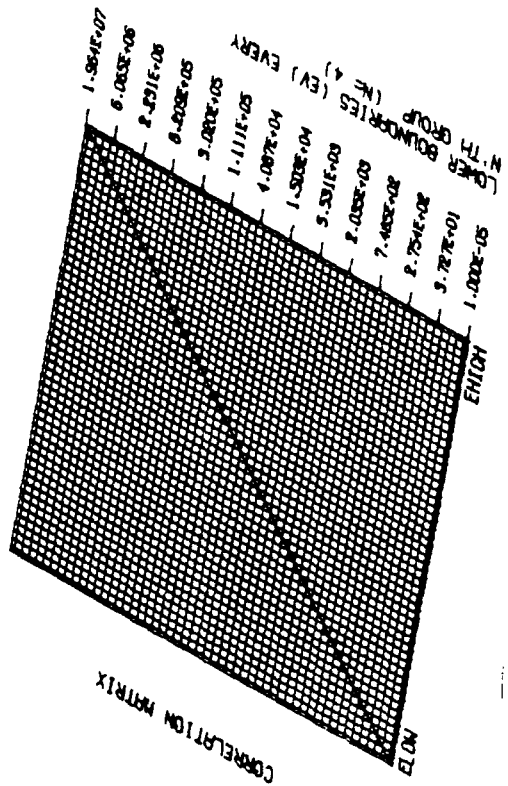


Fig. 144. Cross Correlation Matrix for 238U Elastic to 238U(n,f) Cross Sections.

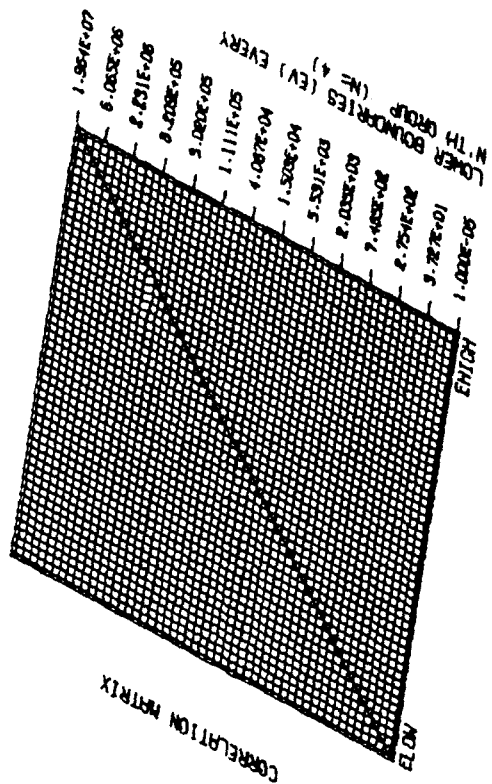


Fig. 147. Cross Correlation Matrix for ²³⁸U Elastic to ²³⁸U(n,n') Level 3 Cross Sections.

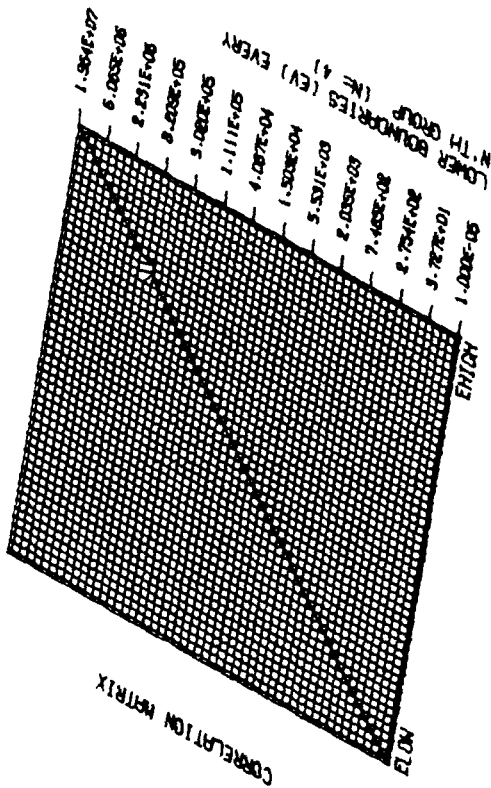


Fig. 149. Cross Correlation Matrix for ²³⁸U Elastic to ²³⁸U(n,n') Level 5 Cross Sections.

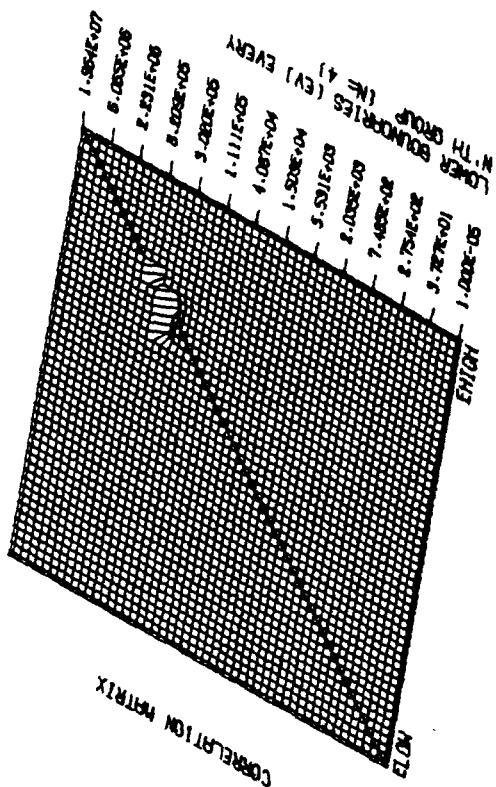


Fig. 146. Cross Correlation Matrix for ²³⁸U Elastic to ²³⁸U(n,n') Level 2 Cross Sections.

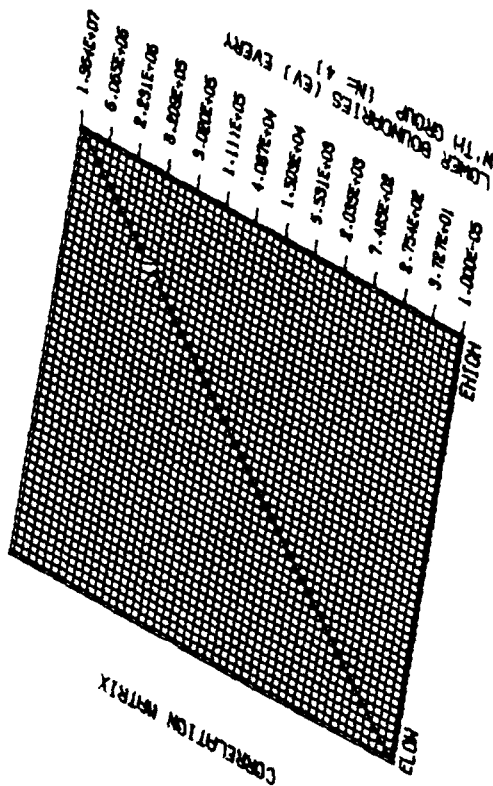


Fig. 148. Cross Correlation Matrix for ²³⁸U Elastic to ²³⁸U(n,n') Level 4 Cross Sections.

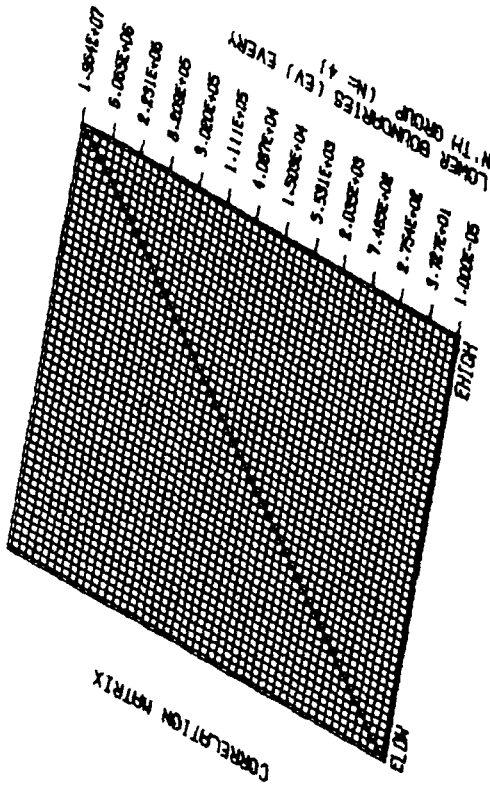


Fig. 151. Cross Correlation Matrix for 238U Elastic to 238U(n,n') Level 7 Cross Sections.

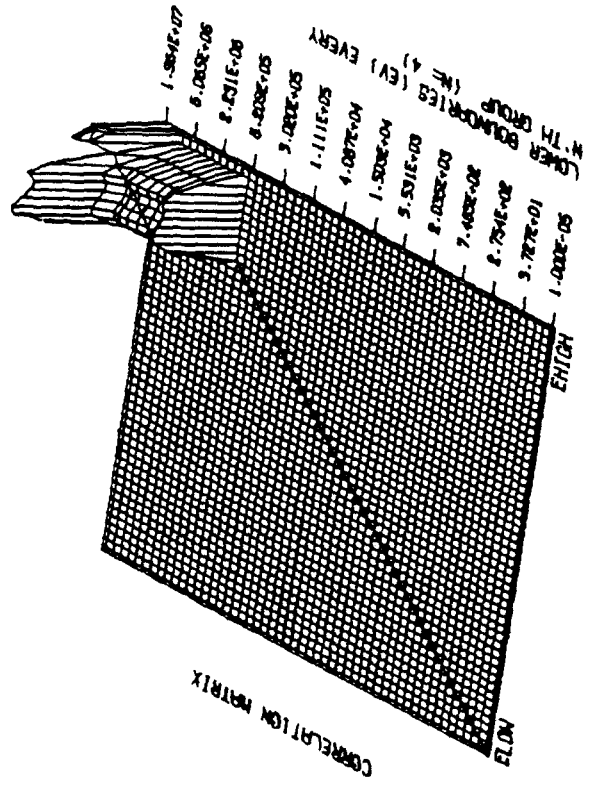


Fig. 153. Cross Correlation Matrix for 238U Inelastic to 238U Total Cross Sections.

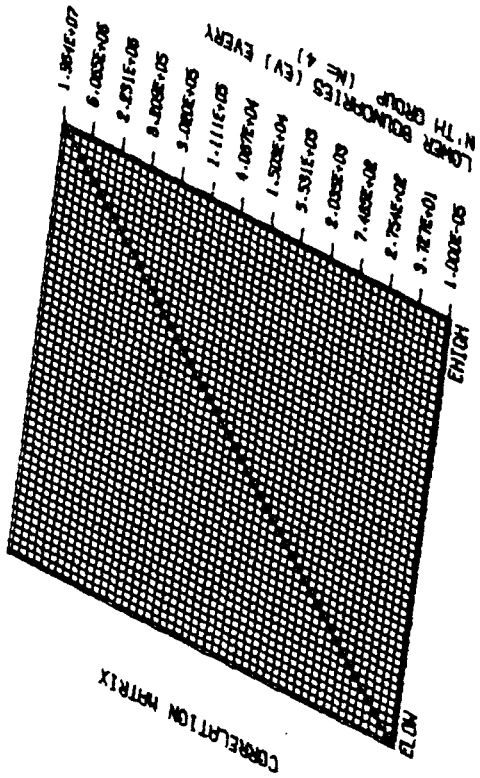


Fig. 150. Cross Correlation Matrix for 238U Elastic to 238U(n,n') Level 6 Cross Sections.

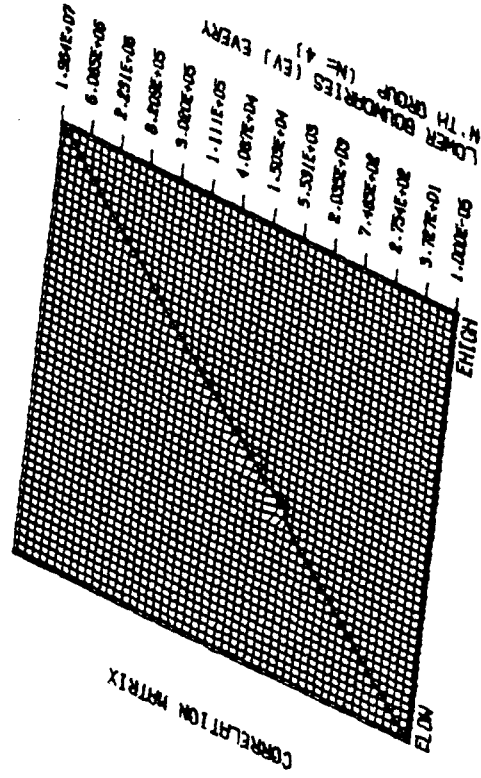


Fig. 152. Cross Correlation Matrix for 238U Elastic to 238U(n,gamma) Cross Sections.

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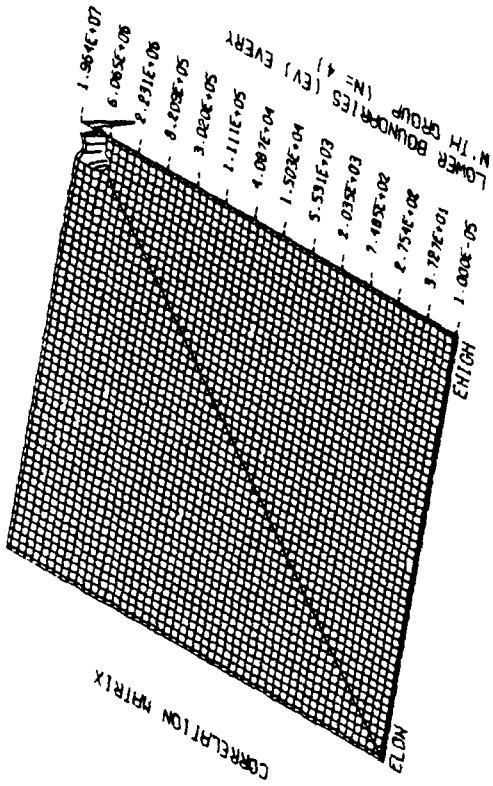


Fig. 155. Cross Correlation Matrix for 238U Inelastic to 238U(n,2n) Cross Sections.

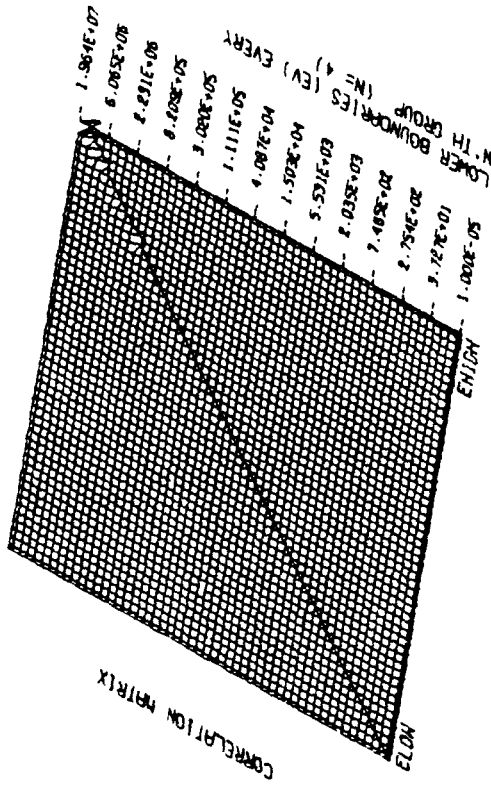


Fig. 157. Cross Correlation Matrix for 238U Inelastic to 238U(n,f) Cross Sections.

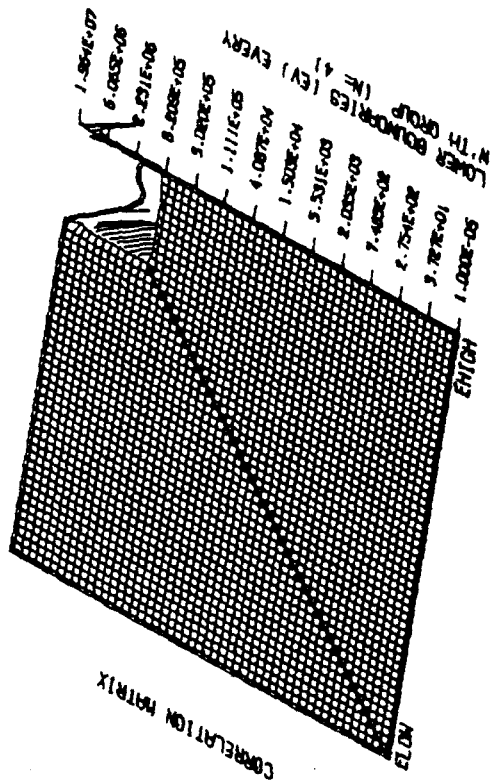


Fig. 154. Cross Correlation Matrix for 238U Inelastic to 238U Elastic Cross Sections.

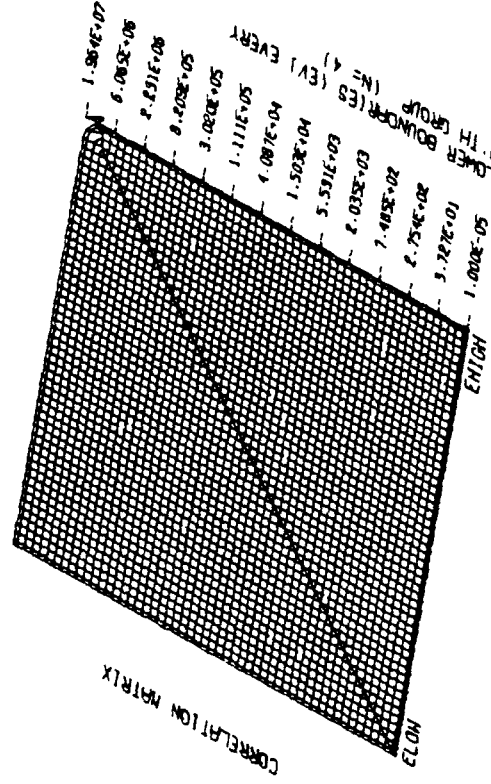


Fig. 156. Cross Correlation Matrix for 238U Inelastic to 238U(n,3n) Cross Sections.

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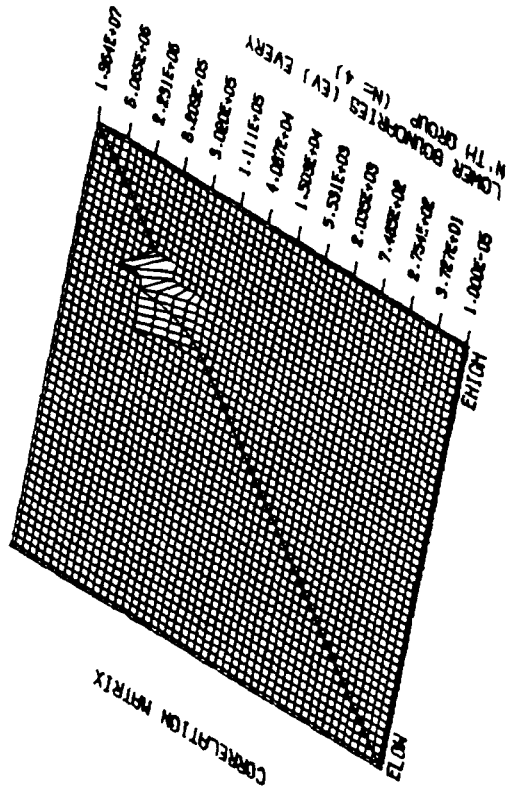


Fig. 159. Cross Correlation Matrix for ^{238}U Inelastic to $^{238}\text{U}(n,n')$ Level 2 Cross Sections.

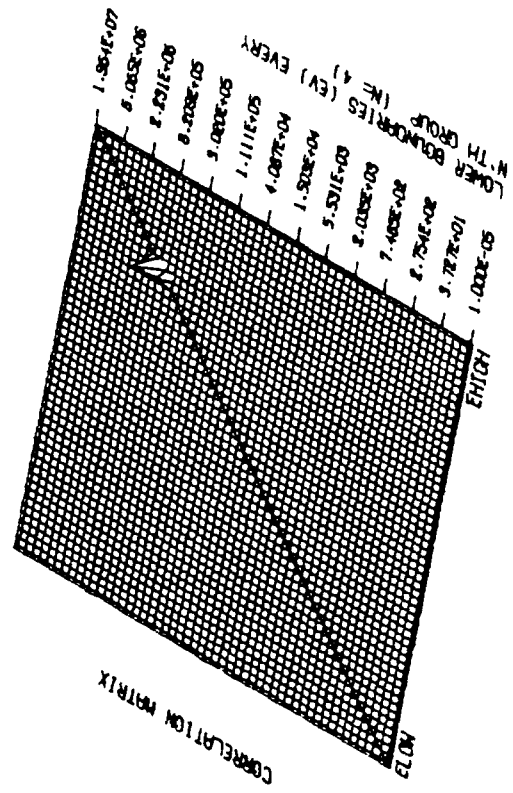


Fig. 161. Cross Correlation Matrix for ^{238}U Inelastic to $^{238}\text{U}(n,n')$ Level 4 Cross Sections.

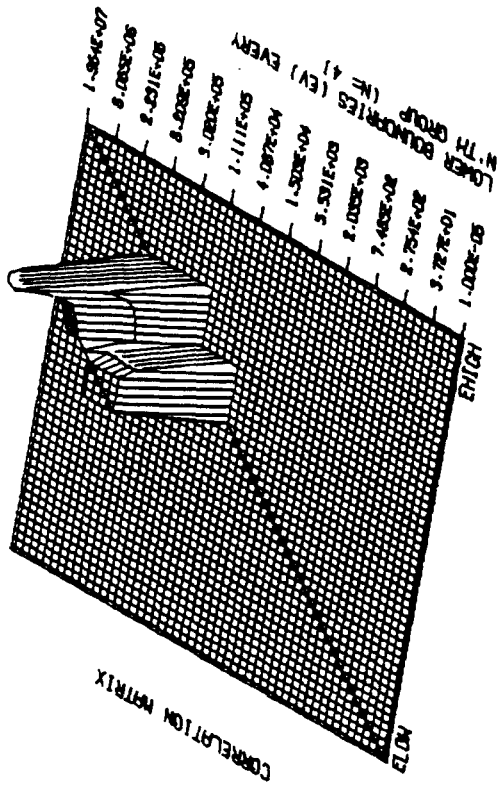


Fig. 158. Cross Correlation Matrix for ^{238}U Inelastic to $^{238}\text{U}(n,n')$ Level 1 Cross Sections.

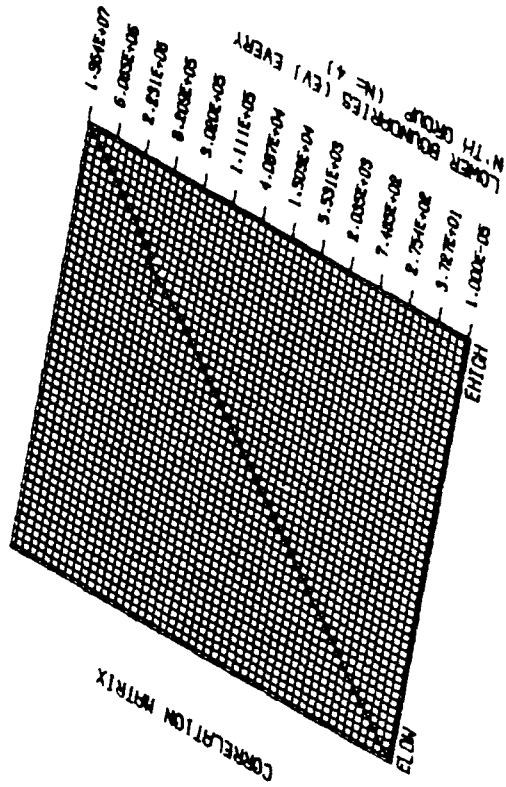


Fig. 160. Cross Correlation Matrix for ^{238}U Inelastic to $^{238}\text{U}(n,n')$ Level 3 Cross Sections.

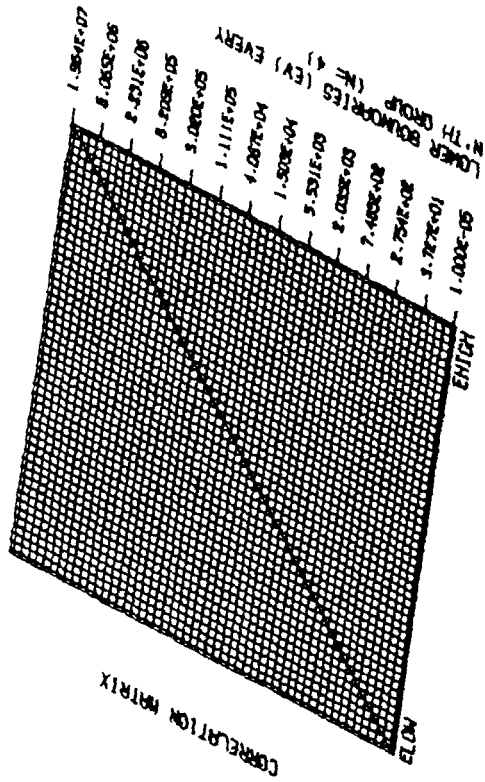


Fig. 163. Cross Correlation Matrix for ^{238}U Inelastic to $^{238}\text{U}(n,n')$ Level 6 Cross Sections.

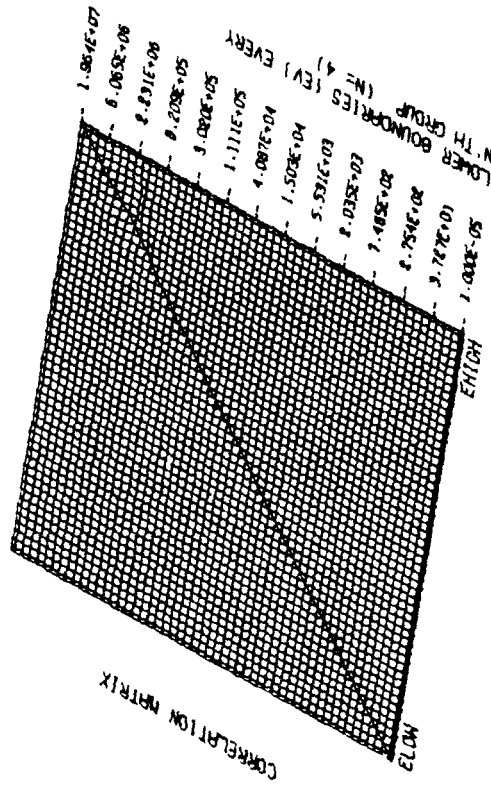


Fig. 165. Cross Correlation Matrix for ^{238}U Inelastic to $^{238}\text{U}(n,n')$ Cross Sections.

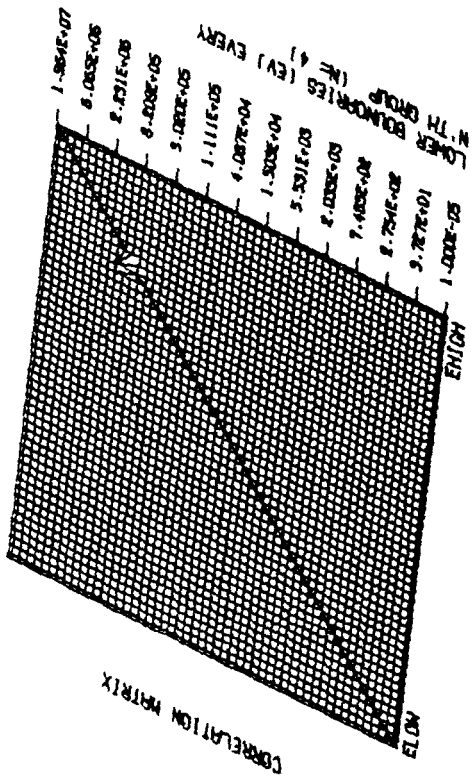


Fig. 162. Cross Correlation Matrix for ^{238}U Inelastic to $^{238}\text{U}(n,n')$ Level 5 Cross Sections.

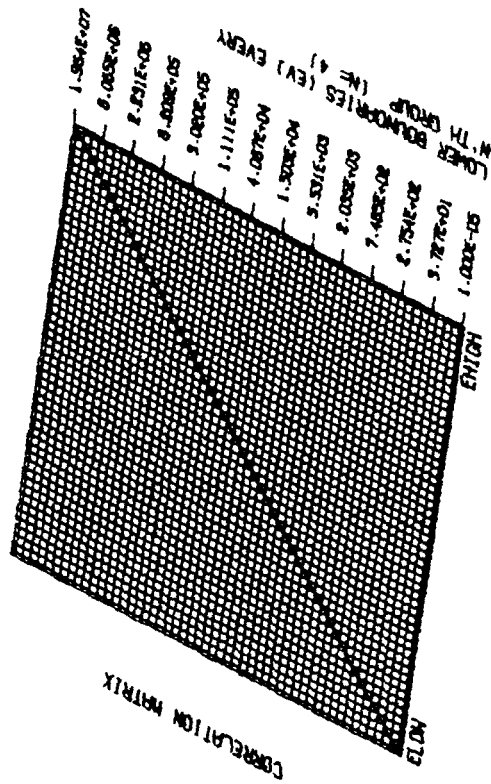


Fig. 164. Cross Correlation Matrix for ^{238}U Inelastic to $^{238}\text{U}(n,n')$ Level 7 Cross Sections.

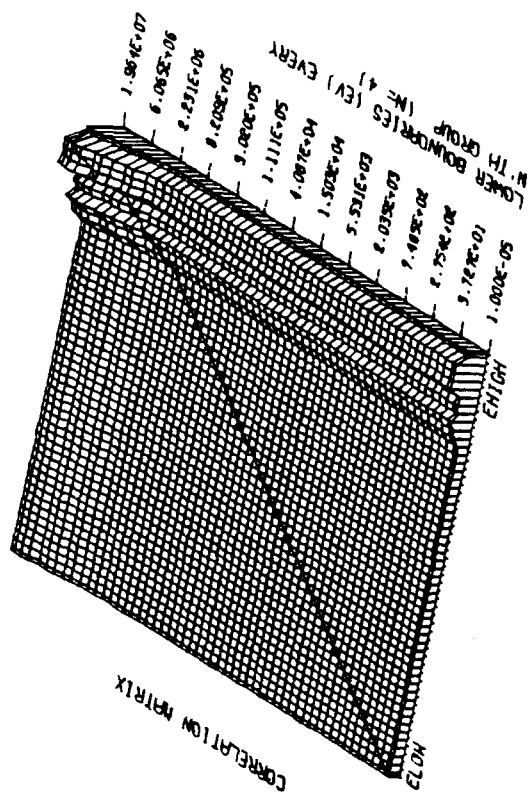


Fig. 167. Cross Correlation Matrix for $^{238}\text{U}(v_p)$ to $^{240}\text{Pu}(v)$ Cross Sections.

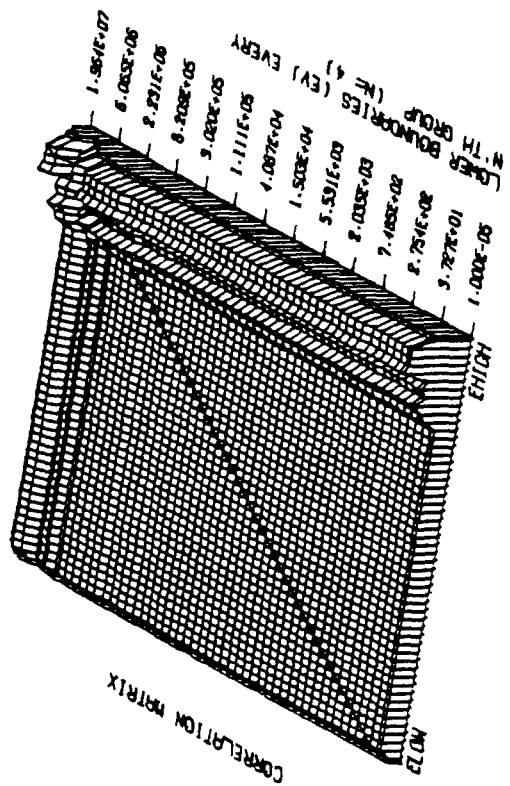


Fig. 169. Cross Correlation Matrix for $^{238}\text{U}(v_p)$ to $^{235}\text{U}(v)$ Cross Sections.

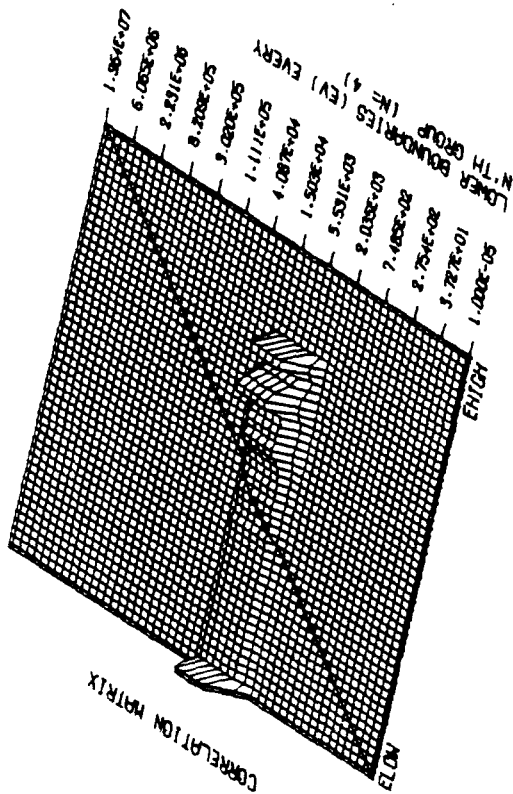


Fig. 166. Cross Correlation Matrix for $^{238}\text{U}(N,y)$ to $^{108}\text{n}(u)$ Cross Sections.

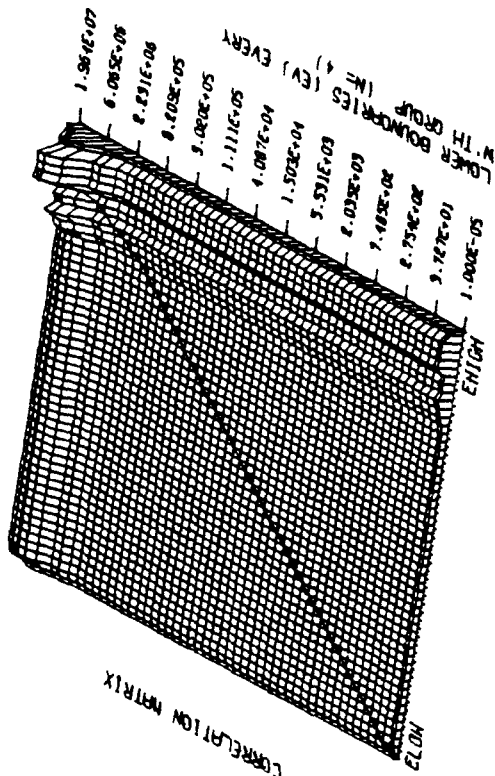


Fig. 168. Cross Correlation Matrix for $^{238}\text{U}(v_p)$ to $^{241}\text{Pu}(v)$ Cross Sections.

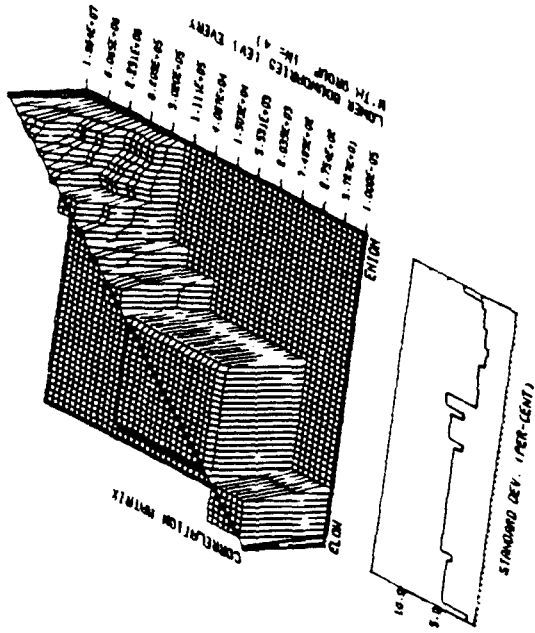


Fig. 171. Standard Deviation and Correlation Matrix for $^{239}\text{Pu}(n,f)$ Cross Sections.

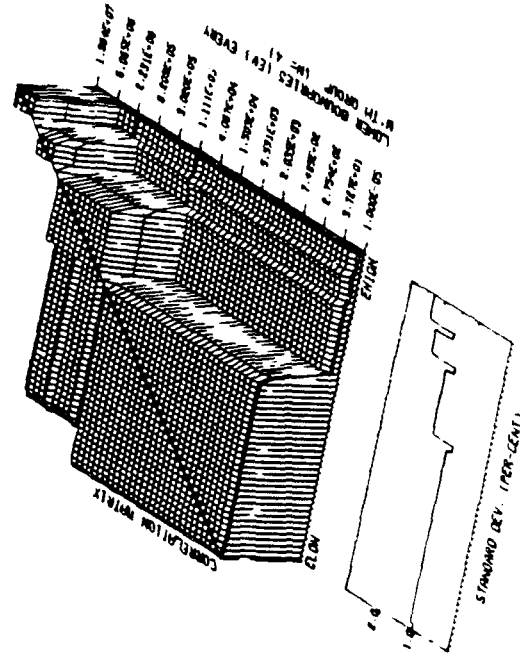


Fig. 173. Standard Deviation and Correlation Matrix for $^{239}\text{Pu}(v)$ Cross Sections.

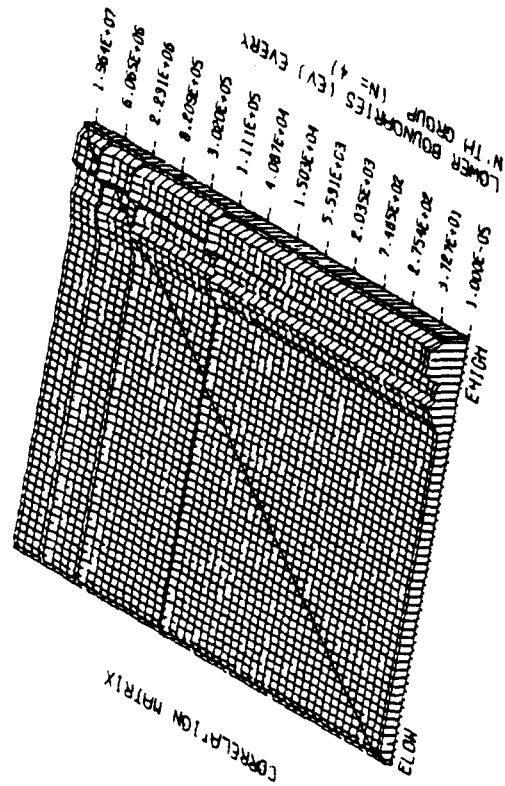


Fig. 170. Cross Correlation Matrix for $^{238}\text{U}(v_p)$ to $^{239}\text{Pu}(v)$ Cross Sections.

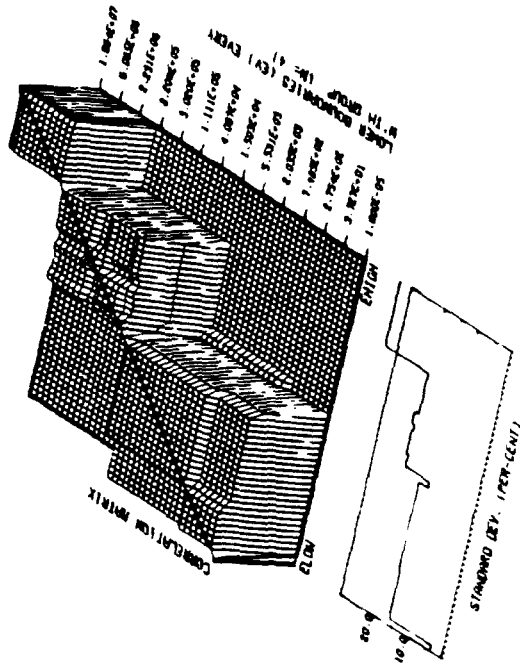


Fig. 172. Standard Deviation and Correlation Matrix for $^{239}\text{Pu}(n,\gamma)$ Cross Sections.

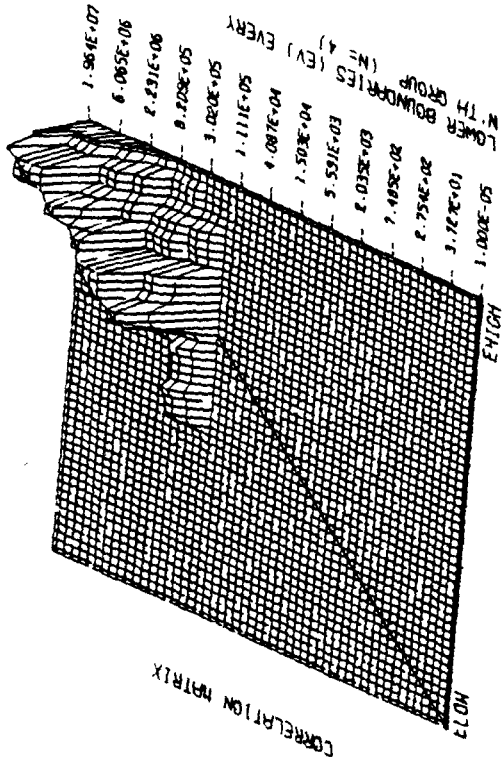


Fig. 175. Cross Correlation Matrix for $^{239}\text{Pu}(N,f)$ to $^{235}\text{U}(n,f)$ Cross Sections.

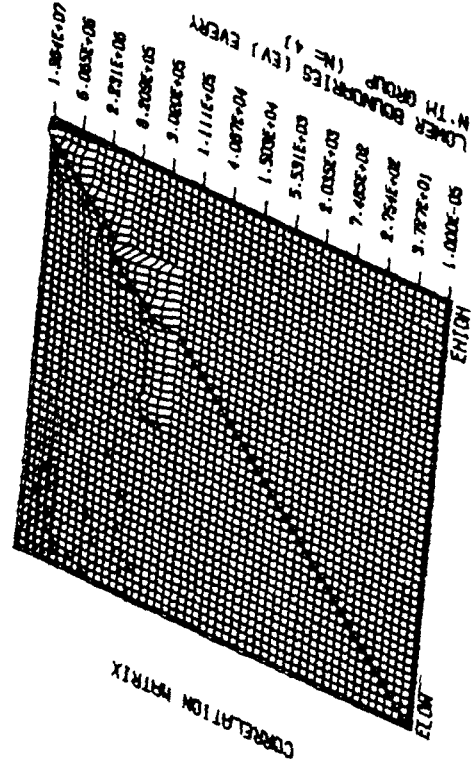


Fig. 176. Cross Correlation Matrix for $^{239}\text{Pu}(N,\gamma)$ to $^{235}\text{U}(n,f)$ Cross Sections.

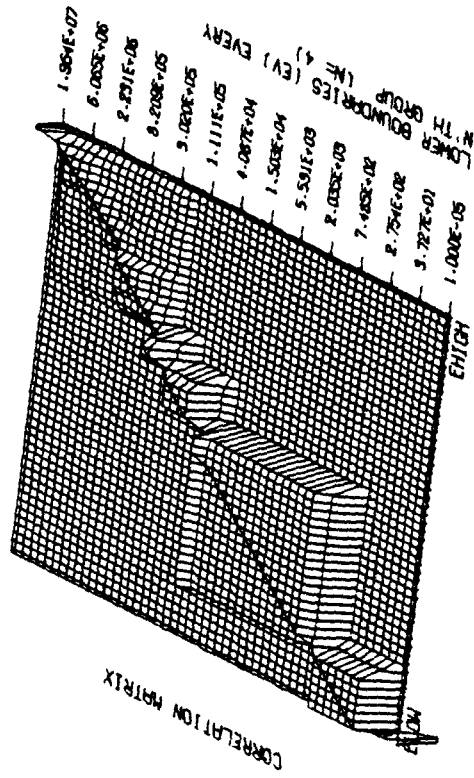


Fig. 174. Cross Correlation Matrix for $^{239}\text{Pu}(N,f)$ to $^{239}\text{Pu}(n,\gamma)$ Cross Sections.

VIII. 13-GROUP CORRELATION MATRIX TABULATIONS

The following tabulations have been collapsed from the 52-group covariance matrix library by the COVERX servic module¹⁰ using the collapsed 100-group weighting function to 13 groups. Correlation matrix elements have been multiplied by 1000 for ease in reading. Only the lower half of symmetric matrices is given. For convenience the diagonal elements of the correlation matrices are given as zero when the corresponding standard deviations are zero. The row and column materials are reversed with respect to the conventiona used in the plots. Here, the 'for' material corresponds to the column and the 'to' material to the row.

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ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1276 REACTION 2

Table with columns: ENERGY RANGE (EV), REL GROUP, STD-DEV, and 13 numbered columns representing material groups. Data includes energy ranges from 1.964E to 4.540E and correlation values.

ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1276 REACTION 4

Table with columns: ENERGY RANGE (EV), REL GROUP, STD-DEV, and 13 numbered columns representing material groups. Data includes energy ranges from 1.964E to 4.540E and correlation values.

ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1276 REACTION 4

Table with columns: ENERGY RANGE (EV), GROUP, and 13 numbered columns representing material groups. Data includes energy ranges from 1.964E to 4.540E and correlation values.

ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1305 REACTION 107

Table with columns: ENERGY RANGE (EV), REL GROUP, STD-DEV, and 13 numbered columns representing material groups. Data includes energy ranges from 1.964E to 4.540E and correlation values.

ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1306 REACTION 1

Table with columns: ENERGY RANGE (EV), REL GROUP, STD-DEV, and 13 numbered columns representing material groups. Data includes energy ranges from 1.964E to 4.540E and correlation values.

ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1306 REACTION 2

Table with columns: ENERGY RANGE (EV), GROUP, and 13 numbered columns representing material groups. Data includes energy ranges from 1.964E to 4.540E and correlation values.

ELEMENTS OF THE CORRELATION MATRIX (10000) FOR MATERIAL 1306 REACTION 102 WITH RESPECT TO MATERIAL 1306 REACTION 102

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns for correlation values. Rows list energy ranges from 1.964E 07 to 4.540E 02.

ELEMENTS OF THE CORRELATION MATRIX (10000) FOR MATERIAL 1306 REACTION 103 WITH RESPECT TO MATERIAL 1306 REACTION 103

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns for correlation values. Rows list energy ranges from 1.964E 07 to 4.540E 02.

ELEMENTS OF THE CORRELATION MATRIX (10000) FOR MATERIAL 1306 REACTION 104 WITH RESPECT TO MATERIAL 1306 REACTION 104

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns for correlation values. Rows list energy ranges from 1.964E 07 to 4.540E 02.

ELEMENTS OF THE CORRELATION MATRIX (10000) FOR MATERIAL 1306 REACTION 107 WITH RESPECT TO MATERIAL 1306 REACTION 107

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns for correlation values. Rows list energy ranges from 1.964E 07 to 4.540E 02.

ELEMENTS OF THE CORRELATION MATRIX (10000) FOR MATERIAL 1311 REACTION 1 WITH RESPECT TO MATERIAL 1311 REACTION 1

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns for correlation values. Rows list energy ranges from 1.964E 07 to 4.540E 02.

ELEMENTS OF THE CORRELATION MATRIX (10000) FOR MATERIAL 1311 REACTION 2 WITH RESPECT TO MATERIAL 1311 REACTION 2

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns for correlation values. Rows list energy ranges from 1.964E 07 to 4.540E 02.

ELEMENTS OF THE CORRELATION MATRIX (10883) FOR MATERIAL 1311 REACTION 4 WITH RESPECT TO MATERIAL 1311 REACTION 4

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns of correlation coefficients. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (10883) FOR MATERIAL 1311 REACTION 16 WITH RESPECT TO MATERIAL 1311 REACTION 16

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns of correlation coefficients. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (10883) FOR MATERIAL 1311 REACTION 51 WITH RESPECT TO MATERIAL 1311 REACTION 51

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns of correlation coefficients. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (10883) FOR MATERIAL 1311 REACTION 52 WITH RESPECT TO MATERIAL 1311 REACTION 52

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns of correlation coefficients. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (10883) FOR MATERIAL 1311 REACTION 53 WITH RESPECT TO MATERIAL 1311 REACTION 53

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns of correlation coefficients. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (10883) FOR MATERIAL 1311 REACTION 54 WITH RESPECT TO MATERIAL 1311 REACTION 54

Table with columns: ENERGY RANGE (EV), REL GROUP, and 13 columns of correlation coefficients. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 61 WITH RESPECT TO MATERIAL 1311 REACTION 61

Table with 15 columns: ENERGY RANGE (EV), 1 REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Data rows include energy ranges from 1.000E 07 to 4.840E 02.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 62 WITH RESPECT TO MATERIAL 1311 REACTION 62

Table with 15 columns: ENERGY RANGE (EV), 1 REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Data rows include energy ranges from 1.000E 07 to 4.840E 02.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 63 WITH RESPECT TO MATERIAL 1311 REACTION 63

Table with 15 columns: ENERGY RANGE (EV), 1 REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Data rows include energy ranges from 1.000E 07 to 4.840E 02.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 64 WITH RESPECT TO MATERIAL 1311 REACTION 64

Table with 15 columns: ENERGY RANGE (EV), 1 REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Data rows include energy ranges from 1.000E 07 to 4.840E 02.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 65 WITH RESPECT TO MATERIAL 1311 REACTION 65

Table with 15 columns: ENERGY RANGE (EV), 1 REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Data rows include energy ranges from 1.000E 07 to 4.840E 02.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 66 WITH RESPECT TO MATERIAL 1311 REACTION 66

Table with 15 columns: ENERGY RANGE (EV), 1 REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Data rows include energy ranges from 1.000E 07 to 4.840E 02.

ELEMENTS OF THE CORRELATION MATRIX (1983) FOR MATERIAL 1311 REACTION 67 WITH RESPECT TO MATERIAL 1311 REACTION 67

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (1983) FOR MATERIAL 1311 REACTION 68 WITH RESPECT TO MATERIAL 1311 REACTION 68

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (1983) FOR MATERIAL 1311 REACTION 91 WITH RESPECT TO MATERIAL 1311 REACTION 91

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (1983) FOR MATERIAL 1311 REACTION 102 WITH RESPECT TO MATERIAL 1311 REACTION 102

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (1983) FOR MATERIAL 1311 REACTION 103 WITH RESPECT TO MATERIAL 1311 REACTION 103

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (1983) FOR MATERIAL 1311 REACTION 107 WITH RESPECT TO MATERIAL 1311 REACTION 107

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07 and 1.000E 07.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 2 WITH RESPECT TO MATERIAL 1311 REACTION 55

Table with 13 columns (GROUP 1-13) and 13 rows (ENERGY RANGE 1.964E to 4.840E). Values are mostly 0, with some non-zero values in the first few columns.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 2 WITH RESPECT TO MATERIAL 1311 REACTION 56

Table with 13 columns (GROUP 1-13) and 13 rows (ENERGY RANGE 1.964E to 4.840E). Values are mostly 0, with some non-zero values in the first few columns.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 2 WITH RESPECT TO MATERIAL 1311 REACTION 57

Table with 13 columns (GROUP 1-13) and 13 rows (ENERGY RANGE 1.964E to 4.840E). Values are mostly 0, with some non-zero values in the first few columns.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 2 WITH RESPECT TO MATERIAL 1311 REACTION 58

Table with 13 columns (GROUP 1-13) and 13 rows (ENERGY RANGE 1.964E to 4.840E). Values are mostly 0, with some non-zero values in the first few columns.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 2 WITH RESPECT TO MATERIAL 1311 REACTION 59

Table with 13 columns (GROUP 1-13) and 13 rows (ENERGY RANGE 1.964E to 4.840E). Values are mostly 0, with some non-zero values in the first few columns.

ELEMENTS OF THE CORRELATION MATRIX (10003) FOR MATERIAL 1311 REACTION 2 WITH RESPECT TO MATERIAL 1311 REACTION 60

Table with 13 columns (GROUP 1-13) and 13 rows (ENERGY RANGE 1.964E to 4.840E). Values are mostly 0, with some non-zero values in the first few columns.

ELEMENTS OF THE CORRELATION MATRIX (L0893) FOR MATERIAL 1311 REACTION 91

ENERGY RANGE (EV)		GROUP	1	2	3	4	5	6	7	8	9	10	11	12	13
1.964E	07-	1.000E	07	1	997	7	0	0	0	0	0	0	0	0	0
1.000E	07-	3.679E	06	2	319	22	0	0	0	0	0	0	0	0	0
3.679E	06-	1.353E	05	3	0	0	0	0	0	0	0	0	0	0	0
1.353E	05-	4.979E	05	4	0	0	0	0	0	0	0	0	0	0	0
4.979E	05-	1.832E	05	5	0	0	0	0	0	0	0	0	0	0	0
1.832E	05-	1.111E	05	6	0	0	0	0	0	0	0	0	0	0	0
1.111E	05-	6.738E	04	7	0	0	0	0	0	0	0	0	0	0	0
6.738E	04-	2.479E	04	8	0	0	0	0	0	0	0	0	0	0	0
2.479E	04-	9.119E	03	9	0	0	0	0	0	0	0	0	0	0	0
9.119E	03-	3.355E	03	10	0	0	0	0	0	0	0	0	0	0	0
3.355E	03-	1.234E	03	11	0	0	0	0	0	0	0	0	0	0	0
1.234E	03-	4.540E	02	12	0	0	0	0	0	0	0	0	0	0	0
4.540E	02-	1.000E-05	05	13	0	0	0	0	0	0	0	0	0	0	0

ELEMENTS OF THE CORRELATION MATRIX (L0893) FOR MATERIAL 1324 REACTION 102

ENERGY RANGE (EV)		REL GROUP	STD-DEV	1	2	3	4	5	6	7	8	9	10	11	12	13
1.964E	07-	1.000E	07	1	1000											
1.000E	07-	2.479E	06	2	335	1000										
3.679E	06-	1.353E	05	3	404	972	1000									
1.353E	05-	4.979E	05	4	405	971	999	1000								
4.979E	05-	1.832E	05	5	0	0	0	46	1000							
1.832E	05-	1.111E	05	10.0	0	0	0	46	1700	1000						
1.111E	05-	6.738E	04	10.0	7	0	0	45	1000	1000	1030					
6.738E	04-	2.479E	04	10.0	8	0	0	45	1300	1000	1000	1000				
2.479E	04-	9.119E	03	10.0	9	0	0	45	1000	1000	1300	1000	1000			
9.119E	03-	3.355E	03	10.0	10	0	0	45	1300	1300	1300	1000	1000	1000		
3.355E	03-	1.234E	03	10.0	11	0	0	45	1000	1000	1000	1000	1000	1000	1000	
1.234E	03-	4.540E	02	10.0	12	0	0	45	1000	1000	1000	1000	1000	1000	1030	1000
4.540E	02-	1.000E-05	05	2.9	13	0	0	45	997	997	997	997	997	997	997	1000

ELEMENTS OF THE CORRELATION MATRIX (L0893) FOR MATERIAL 1326 REACTION 1

ENERGY RANGE (EV)		REL GROUP	STD-DEV	1	2	3	4	5	6	7	8	9	10	11	12	13	
1.964E	07-	1.000E	07	1	1000												
1.000E	07-	3.679E	06	2	254	1030											
3.679E	06-	1.353E	05	3	251	555	1000										
1.353E	05-	4.979E	05	4	330	332	549	1000									
4.979E	05-	1.832E	05	5	50	44	4	765	1000								
1.832E	05-	1.111E	05	6	0	0	0	597	993	1033							
1.111E	05-	6.738E	04	7	0	0	0	647	993	1003	1000						
6.738E	04-	2.479E	04	8	0	0	0	697	993	1300	1030	1070					
2.479E	04-	9.119E	03	9	0	0	0	776	994	998	998	998	1000				
9.119E	03-	3.355E	03	10	0	0	0	697	916	900	900	900	978	1000			
3.355E	03-	1.234E	03	11	0	0	0	697	916	900	900	900	928	1000	1000		
1.234E	03-	4.540E	02	12	0	0	0	708	931	915	915	915	931	935	935	1000	
4.540E	02-	1.000E-05	05	15.0	13	0	0	428	562	552	552	552	560	552	552	561	1000

ELEMENTS OF THE CORRELATION MATRIX (L0893) FOR MATERIAL 1326 REACTION 2

ENERGY RANGE (EV)		GROUP	1	2	3	4	5	6	7	8	9	10	11	12	13	
1.964E	07-	1.000E	07	1	805	204	202	123	0	0	0	0	0	0	0	
1.000E	07-	3.679E	06	2	205	807	285	142	0	0	0	0	0	0	0	
3.679E	06-	1.353E	05	3	231	324	918	362	0	0	0	0	0	0	0	
1.353E	05-	4.979E	05	4	160	212	475	787	232	0	0	0	0	0	0	
4.979E	05-	1.832E	05	5	0	0	0	482	348	222	222	222	190	0	0	
1.832E	05-	1.111E	05	6	0	0	0	0	245	316	316	316	269	0	0	
1.111E	05-	6.738E	04	7	0	0	0	0	245	316	316	316	269	0	0	
6.738E	04-	2.479E	04	8	0	0	0	0	245	316	316	316	269	0	0	
2.479E	04-	9.119E	03	9	0	0	0	0	241	317	313	310	274	58	12	
9.119E	03-	3.355E	03	10	0	0	0	0	0	0	0	0	50	316	316	316
3.355E	03-	1.234E	03	11	0	0	0	0	0	0	0	0	50	316	316	316
1.234E	03-	4.540E	02	12	0	0	0	0	0	0	0	0	12	77	77	260
4.540E	02-	1.000E-05	05	13	0	0	0	0	0	0	0	0	0	0	0	810

ELEMENTS OF THE CORRELATION MATRIX (L0893) FOR MATERIAL 1326 REACTION 102

ENERGY RANGE (EV)		GROUP	1	2	3	4	5	6	7	8	9	10	11	12	13
1.964E	07-	1.000E	07	1	0	0	0	0	0	0	0	0	0	0	0
1.000E	07-	3.679E	06	2	0	0	0	0	0	0	0	0	0	0	0
3.679E	06-	1.353E	05	3	0	0	0	0	0	0	0	0	0	0	0
1.353E	05-	4.979E	05	4	0	0	0	0	0	0	0	0	0	0	0
4.979E	05-	1.832E	05	5	0	0	0	0	0	0	0	0	0	0	0
1.832E	05-	1.111E	05	6	0	0	0	0	0	0	0	0	0	0	0
1.111E	05-	6.738E	04	7	0	0	0	0	0	0	0	0	0	0	0
6.738E	04-	2.479E	04	8	0	0	0	0	0	0	0	0	0	0	0
2.479E	04-	9.119E	03	9	0	0	0	0	0	0	0	0	0	0	0
9.119E	03-	3.355E	03	10	0	0	0	0	0	0	0	0	0	0	0
3.355E	03-	1.234E	03	11	0	0	0	0	0	0	0	0	0	0	0
1.234E	03-	4.540E	02	12	0	0	0	0	0	0	0	0	0	0	0
4.540E	02-	1.000E-05	05	13	0	0	0	0	0	0	0	0	0	0	0

00079

ELEMENTS OF THE CORRELATION MATRIX (112233) FOR MATERIAL 1326 REACTION 4 WITH RESPECT TO MATERIAL 1326 REACTION 4

Table with columns: ENERGY RANGE (EV), GROUP, and columns 1-13. Values include 1.964C, 1.000C, 3.679E, etc.

ELEMENTS OF THE CORRELATION MATRIX (112233) FOR MATERIAL 1326 REACTION 16 WITH RESPECT TO MATERIAL 1326 REACTION 16

Table with columns: ENERGY RANGE (EV), GROUP, and columns 1-13. Values include 1.964E, 1.000E, 3.679E, etc.

ELEMENTS OF THE CORRELATION MATRIX (112233) FOR MATERIAL 1326 REACTION 22 WITH RESPECT TO MATERIAL 1326 REACTION 22

Table with columns: ENERGY RANGE (EV), GROUP, and columns 1-13. Values include 1.964E, 1.000E, 3.679E, etc.

ELEMENTS OF THE CORRELATION MATRIX (112233) FOR MATERIAL 1326 REACTION 28 WITH RESPECT TO MATERIAL 1326 REACTION 28

Table with columns: ENERGY RANGE (EV), GROUP, and columns 1-13. Values include 1.964E, 1.000E, 3.679E, etc.

ELEMENTS OF THE CORRELATION MATRIX (112233) FOR MATERIAL 1326 REACTION 102 WITH RESPECT TO MATERIAL 1326 REACTION 102

Table with columns: ENERGY RANGE (EV), GROUP, and columns 1-13. Values include 1.964E, 1.000E, 3.679E, etc.

ELEMENTS OF THE CORRELATION MATRIX (112233) FOR MATERIAL 1326 REACTION 104 WITH RESPECT TO MATERIAL 1326 REACTION 104

Table with columns: ENERGY RANGE (EV), GROUP, and columns 1-13. Values include 1.964E, 1.000E, 3.679E, etc.

ELEMENTS OF THE CORRELATION MATRIX (GROUP 1) FOR MATERIAL 1326 REACTION 105

Table with columns: ENERGY RANGE (EVI), GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E 07, 1.000E 07, 3.679E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (GROUP 4) FOR MATERIAL 1326 REACTION 106

Table with columns: ENERGY RANGE (EVI), GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E 07, 1.000E 07, 3.679E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (GROUP 5) FOR MATERIAL 1326 REACTION 107

Table with columns: ENERGY RANGE (EVI), GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E 07, 1.000E 07, 3.679E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (GROUP 1) FOR MATERIAL 1326 REACTION 16

Table with columns: ENERGY RANGE (EVI), REL, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E 07, 1.000E 07, 3.679E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (GROUP 1) FOR MATERIAL 1326 REACTION 22

Table with columns: ENERGY RANGE (EVI), REL, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E 07, 1.000E 07, 3.679E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (GROUP 1) FOR MATERIAL 1326 REACTION 28

Table with columns: ENERGY RANGE (EVI), REL, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E 07, 1.000E 07, 3.679E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (1000) FOR MATERIAL 1326 REACTION 102

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.500E J7 and 1.000E J7.

ELEMENTS OF THE CORRELATION MATRIX (1000) FOR MATERIAL 1326 REACTION 104

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.500E J7 and 1.000E J7.

ELEMENTS OF THE CORRELATION MATRIX (1000) FOR MATERIAL 1326 REACTION 105

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.500E J7 and 1.000E J7.

ELEMENTS OF THE CORRELATION MATRIX (1000) FOR MATERIAL 1326 REACTION 106

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.500E J7 and 1.000E J7.

ELEMENTS OF THE CORRELATION MATRIX (1000) FOR MATERIAL 1326 REACTION 107

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.500E J7 and 1.000E J7.

ELEMENTS OF THE CORRELATION MATRIX (1000) FOR MATERIAL 1326 REACTION 108

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.500E J7 and 1.000E J7.

ELEMENTS OF THE CORRELATION MATRIX (L2223) FOR MATERIAL 1395 REACTION 452

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Includes sub-header 'STD-DEV'.

ELEMENTS OF THE CORRELATION MATRIX (L2223) FOR MATERIAL 1395 REACTION 1

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Includes sub-header 'STD-DEV'.

ELEMENTS OF THE CORRELATION MATRIX (L2223) FOR MATERIAL 1398 REACTION 2

Table with columns: ENERGY RANGE (eV), GROUP, and 13 columns of correlation values.

ELEMENTS OF THE CORRELATION MATRIX (L2223) FOR MATERIAL 1398 REACTION 102

Table with columns: ENERGY RANGE (eV), GROUP, and 13 columns of correlation values.

ELEMENTS OF THE CORRELATION MATRIX (L2223) FOR MATERIAL 1398 REACTION 2

Table with columns: ENERGY RANGE (eV), REL GROUP, and 13 columns of correlation values. Includes sub-header 'STD-DEV'.

ELEMENTS OF THE CORRELATION MATRIX (L2223) FOR MATERIAL 1398 REACTION 51

Table with columns: ENERGY RANGE (eV), GROUP, and 13 columns of correlation values.

ELEMENTS OF THE CORRELATION MATRIX (12223) FOR MATERIAL 1398 REACTION 2

Table with columns: ENERGY RANGE (eV), GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E 07-- 1.000E 07, 1.000E 07-- 3.675E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (12223) FOR MATERIAL 1398 REACTION 4

Table with columns: ENERGY RANGE (eV), REL GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Includes sub-labels 'STD-DEV' and '1000'. Rows include energy ranges like 1.964E 07-- 1.000E 07, 1.000E 07-- 3.675E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (12223) FOR MATERIAL 1398 REACTION 16

Table with columns: ENERGY RANGE (eV), GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E 07-- 1.000E 07, 1.000E 07-- 3.675E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (12223) FOR MATERIAL 1398 REACTION 17

Table with columns: ENERGY RANGE (eV), GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E 07-- 1.000E 07, 1.000E 07-- 3.675E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (12223) FOR MATERIAL 1398 REACTION 15

Table with columns: ENERGY RANGE (eV), GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E 07-- 1.000E 07, 1.000E 07-- 3.675E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (12223) FOR MATERIAL 1398 REACTION 51

Table with columns: ENERGY RANGE (eV), GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E 07-- 1.000E 07, 1.000E 07-- 3.675E 06, etc.

ELEMENTS OF THE CORRELATION MATRIX (L1003) FOR MATERIAL 1398 REACTION 17 WITH RESPECT TO MATERIAL 1398 REACTION 17

Table with 13 columns: ENERGY RANGE (EV), X REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E J7- and 1.030E J7-.

ELEMENTS OF THE CORRELATION MATRIX (L1003) FOR MATERIAL 1398 REACTION 18 WITH RESPECT TO MATERIAL 1398 REACTION 18

Table with 13 columns: ENERGY RANGE (EV), X REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E J7- and 1.030E J7-.

ELEMENTS OF THE CORRELATION MATRIX (L1003) FOR MATERIAL 1398 REACTION 51 WITH RESPECT TO MATERIAL 1398 REACTION 51

Table with 13 columns: ENERGY RANGE (EV), X REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E J7- and 1.030E J7-.

ELEMENTS OF THE CORRELATION MATRIX (L1003) FOR MATERIAL 1398 REACTION 52 WITH RESPECT TO MATERIAL 1398 REACTION 52

Table with 13 columns: ENERGY RANGE (EV), X REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E J7- and 1.030E J7-.

ELEMENTS OF THE CORRELATION MATRIX (L1003) FOR MATERIAL 1398 REACTION 53 WITH RESPECT TO MATERIAL 1398 REACTION 53

Table with 13 columns: ENERGY RANGE (EV), X REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E J7- and 1.030E J7-.

ELEMENTS OF THE CORRELATION MATRIX (L1003) FOR MATERIAL 1398 REACTION 54 WITH RESPECT TO MATERIAL 1398 REACTION 54

Table with 13 columns: ENERGY RANGE (EV), X REL STD-DEV, GROUP, 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13. Rows include energy ranges like 1.964E J7- and 1.030E J7-.

ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1340 REACTION 452

Table with columns: ENERGY RANGE (EV), GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07-- 1.000E C7 and material groups like 1.000E 07-- 3.679E C6.

ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1381 REACTION 452

Table with columns: ENERGY RANGE (EV), GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07-- 1.000E C7 and material groups like 1.000E 07-- 3.679E C6.

ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1395 REACTION 452

Table with columns: ENERGY RANGE (EV), GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07-- 1.000E C7 and material groups like 1.000E 07-- 3.679E C6.

ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1348 REACTION 456

Table with columns: ENERGY RANGE (EV), GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07-- 1.000E C7 and material groups like 1.000E 07-- 3.679E C6.

ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1399 REACTION 452

Table with columns: ENERGY RANGE (EV), GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07-- 1.000E C7 and material groups like 1.000E 07-- 3.679E C6.

ELEMENTS OF THE CORRELATION MATRIX WITH RESPECT TO MATERIAL 1395 REACTION 18

Table with columns: ENERGY RANGE (EV), GROUP, and 13 columns of correlation values. Rows include energy ranges like 1.964E 07-- 1.000E C7 and material groups like 1.000E 07-- 3.679E C6.

ELEMENTS OF THE COOPERATION MATRIX (GROUPS) FOR MATERIAL 1399 REACTION 18

ENERGY RANGE (eV)		X REL	GROUP												
STG-DLV			1	2	3	4	5	6	7	8	9	10	11	12	13
1.964E	07--	1.000E	07	1	1000										
1.964E	07--	3.0675E	06	2	102	1000									
3.0675E	06--	1.0352E	06	3	70	671	1000								
1.0352E	06--	4.0575E	05	4	38	412	674	1000							
4.0575E	05--	1.0822E	05	5	44	519	491	110	1000						
1.0822E	05--	1.0111E	05	6	0	0	0	0	233	1000					
1.0111E	05--	6.0728E	04	7	0	0	0	0	63	111	1000				
6.0728E	04--	2.477E	04	8	0	0	0	0	0	0	431	1000			
2.477E	04--	5.0119E	03	9	0	0	0	0	0	0	0	198	1000		
5.0119E	03--	3.0355E	03	10	0	0	0	0	0	0	0	198	1000	1000	
3.0355E	03--	1.0224E	03	11	0	0	0	0	0	0	0	198	1000	1000	1000
1.0224E	03--	4.0540E	02	12	0	0	0	0	0	0	0	198	1000	1000	1000
4.0540E	02--	1.0000E	02	13	0	0	0	0	0	0	0	0	0	0	1000

ELEMENTS OF THE COOPERATION MATRIX (GROUPS) FOR MATERIAL 1399 REACTION 102

ENERGY RANGE (eV)		X REL	GROUP												
STG-DLV			1	2	3	4	5	6	7	8	9	10	11	12	13
1.964E	07--	1.000E	07	1	234	0	19	11	10	0	0	0	0	0	0
1.964E	07--	3.0675E	06	2	12	106	38	34	41	0	0	0	0	0	0
3.0675E	06--	1.0352E	06	3	7	73	79	73	51	0	0	0	0	0	0
1.0352E	06--	4.0575E	05	4	2	53	112	274	171	0	0	0	0	0	0
4.0575E	05--	1.0822E	05	5	3	49	78	176	163	41	13	0	0	0	0
1.0822E	05--	1.0111E	05	6	0	0	0	0	73	171	116	0	0	0	0
1.0111E	05--	6.0728E	04	7	0	0	0	0	15	74	281	266	0	0	0
6.0728E	04--	2.477E	04	8	0	0	0	0	0	244	209	65	65	65	65
2.477E	04--	5.0119E	03	9	0	0	0	0	0	0	83	421	421	421	421
5.0119E	03--	3.0355E	03	10	0	0	0	0	0	0	74	371	371	371	371
3.0355E	03--	1.0224E	03	11	0	0	0	0	0	0	74	371	371	371	371
1.0224E	03--	4.0540E	02	12	0	0	0	0	0	0	74	371	371	371	371
4.0540E	02--	1.0000E	02	13	0	0	0	0	0	0	0	0	0	0	-375

ELEMENTS OF THE COOPERATION MATRIX (GROUPS) FOR MATERIAL 1399 REACTION 18

ENERGY RANGE (eV)		X REL	GROUP												
STG-DLV			1	2	3	4	5	6	7	8	9	10	11	12	13
1.964E	07--	1.000E	07	1	32	44	10	1	0	0	0	0	0	0	0
1.964E	07--	3.0675E	06	2	17	102	30	17	4	0	0	0	0	0	0
3.0675E	06--	1.0352E	06	3	8	58	72	63	28	0	0	0	0	0	0
1.0352E	06--	4.0575E	05	4	1	13	41	170	88	0	0	0	0	0	0
4.0575E	05--	1.0822E	05	5	0	5	17	131	127	0	0	0	0	0	0
1.0822E	05--	1.0111E	05	6	0	0	7	75	56	0	0	0	0	0	0
1.0111E	05--	6.0728E	04	7	0	0	2	19	53	0	0	0	0	0	0
6.0728E	04--	2.477E	04	8	0	0	0	0	49	0	0	0	0	0	0
2.477E	04--	5.0119E	03	9	0	0	0	0	35	0	0	0	0	0	0
5.0119E	03--	3.0355E	03	10	0	0	0	0	0	0	0	0	0	0	0
3.0355E	03--	1.0224E	03	11	0	0	0	0	0	0	0	0	0	0	0
1.0224E	03--	4.0540E	02	12	0	0	0	0	0	0	0	0	0	0	0
4.0540E	02--	1.0000E	02	13	0	0	0	0	0	0	0	0	0	0	0

ELEMENTS OF THE COOPERATION MATRIX (GROUPS) FOR MATERIAL 1399 REACTION 102

ENERGY RANGE (eV)		X REL	GROUP												
STG-DLV			1	2	3	4	5	6	7	8	9	10	11	12	13
1.964E	07--	1.000E	07	30.9	1	1000									
1.964E	07--	3.0675E	06	30.2	2	107	1000								
3.0675E	06--	1.0352E	06	31.2	3	969	995	1000							
1.0352E	06--	4.0575E	05	16.3	4	102	207	211	1000						
4.0575E	05--	1.0822E	05	20.3	5	0	0	9	972	1000					
1.0822E	05--	1.0111E	05	21.0	6	0	0	0	840	931	1000				
1.0111E	05--	6.0728E	04	20.8	7	0	0	0	219	150	718	1000			
6.0728E	04--	2.477E	04	20.8	8	0	0	0	327	953	894	995	1000		
2.477E	04--	5.0119E	03	14.3	9	0	0	0	225	212	214	225	254	1000	
5.0119E	03--	3.0355E	03	14.3	10	0	0	0	0	0	0	24	570	1000	
3.0355E	03--	1.0224E	03	14.3	11	0	0	0	0	0	0	24	970	1000	1000
1.0224E	03--	4.0540E	02	14.3	12	0	0	0	0	0	0	24	970	1000	1000
4.0540E	02--	1.0000E	02	14.3	13	0	0	0	0	0	0	0	0	0	1000

ELEMENTS OF THE COOPERATION MATRIX (GROUPS) FOR MATERIAL 1399 REACTION 452

ENERGY RANGE (eV)		X REL	GROUP												
STG-DLV			1	2	3	4	5	6	7	8	9	10	11	12	13
1.964E	07--	1.000E	07	2.2	1	1000									
1.964E	07--	3.0675E	06	1.6	2	159	1000								
3.0675E	06--	1.0352E	06	1.5	3	65	100	1000							
1.0352E	06--	4.0575E	05	1.6	4	77	117	172	1000						
4.0575E	05--	1.0822E	05	1.6	5	77	110	172	1000						
1.0822E	05--	1.0111E	05	1.6	6	77	110	172	1000						
1.0111E	05--	6.0728E	04	1.2	7	104	153	197	945	945	1000				
6.0728E	04--	2.477E	04	1.1	8	130	153	156	156	156	1300				
2.477E	04--	5.0119E	03	1.1	9	130	153	156	156	156	156	1300			
5.0119E	03--	3.0355E	03	1.1	10	130	153	156	156	156	156	1300			
3.0355E	03--	1.0224E	03	1.1	11	130	153	156	156	156	156	1300			
1.0224E	03--	4.0540E	02	1.1	12	130	153	156	156	156	156	1300			
4.0540E	02--	1.0000E	02	1.0	13	65	77	94	94	94	428	970	970	970	970

1HC0021 STOP C

ACKNOWLEDGEMENTS

This report represents a two-fold effort. (1) It demonstrates the processing capabilities of the authors' PUFF-II code and (2) multi-group covariance matrices from ENDF/B-V evaluations are now available for use.

Much of the important feedback necessary for organizing this report and the data presented herein has come from J. H. Marable, R. W. Peele and J. J. Wagschal.

The authors would also like to thank J. D. Drischler for his special help in preparing this report and to Ann Houston for preparing this report in its final form.

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APPENDIX A
COVERX Format

```

C*****
C              REVISED 11/01/77
C
C  COVERX
C  THIS FILE CONTAINS CROSS SECTIONS,
C  STANDARD DEVIATIONS, AND
C  BY DESIGNATION EITHER COVARIANCE,
C  RELATIVE COVARIANCE,
C  OR CORRELATION MATRICES.
C
C  A FILE SUCH AS THIS IS NEEDED BY ORNL - PORSS
C
C              J. L. LUCIUS
C*****
  
```

```

C-----
CS          FILE STRUCTURE
CS
CS          RECORD TYPE                PRESENT IF
CS          =====
CS          FILE IDENTIFICATION        ALWAYS
CS          FILE CONTROL                ALWAYS
CS          FILE DESCRIPTION            NHOLL.GT.0
CS          NEUTRON GROUP BOUNDARIES   NNGRUP.GT.0
CS          GAMMA GROUP BOUNDARIES     NGGRUP.GT.0
CS          MAT - MT CONTROL            ALWAYS
CS          ***** (REPEAT FOR ALL MATERIAL-
CS          *          REACTION TYPE PAIRS)
CS          *          MAT-MT CROSS SECTION AND
CS          *          STANDARD DEVIATIONS
CS          *****
CS
CS          ***** (REPEAT FOR ALL MATRICES)
CS          *          MATRIX CONTROL    ALWAYS
CS          *          BLOCK CONTROL     ALWAYS
CS          *          ***** (REPEAT FOR ALL BLOCKS)
CS          *          *          MATRIX DATA    ALWAYS
CS          *****
C-----
  
```

```

-----
C
CR          FILE IDENTIFICATION
C
CL      HNAME, (HUSE(I), I=1,2), IVERS
CW      1+3*MULT
C
CB      FORMAT(11H 0V COVERX ,A6,1H*,2A6,1H*,I6)
CD      HNAME          HOLLERITH FILE NAME-COVERX   (A6)
CD      HUSE           HOLLERITH USER IDENTIFICATION (A6)
CD      IVERS          FILE VERSION NUMBER
CD      MULT           1 - A6 IS SINGLE PRECISION WORD
CD                        2 - A6 IS DOUBLE PRECISION WORD
C
-----

```

```

-----
C
CR          FILE CONTROL
C
CL      NGROUP, NNGRUP, NGGRUP, NTYPE, NMMP, NMTRIX, NHOLL
C
CW      7
C
CB      FORMAT(4H 1D ,7I6)
C
CD      NGROUP        NUMBER OF ENERGY GROUPS
CD      NNGRUP        NUMBER OF NEUTRON GROUPS
CD      NGGRUP        NUMBER OF GAMMA GROUPS
CD      NTYPE         TYPE OF DATA
CD                        1 - COVARIANCE MATRIX, STANDARD DEVIATION
CD                        2 - RELATIVE COVARIANCE MATRIX,
CD                          RELATIVE STANDARD DEVIATION
CD                        3 - CORRELATION MATRIX, STANDARD DEVIATION
CD      NMMP          NUMBER OF MAT - MT PAIRS
CD      NMTRIX        NUMBER OF MATRICES
CD      NHOLL         NUMBER OF HOLLERITH WORDS IN DESCRIPTION
C
-----

```

```

-----
C
CR          FILE DESCRIPTION
C
CL      (WORDS(J), J=1, NHOLL)
CW      MULT*NHOLL
C
CB      FORMAT(4H 2D ,1H*,11A6/(11A6))
C
CD      WORDS(J)      HOLLERITH DESCRIPTION OF FILE
C
-----

```

```

-----
C
CR          NEUTRON GROUP BOUNDARIES
C
CL          (GPBN(J) ,J=1,NNGRUP) ,ENMIN
C
CC          PRESENT IF NNGRUP.GT.0
CW          NNGRUP+1
C
CB          FORMAT(4H 3D ,5E12.4/(6E12.4))
CD          GPBN(J)      MAXIMUM ENERGY BOUND OF NEUTRON GROUP(J) (EV)
CD          ENMIN       MINIMUM ENERGY OF NEUTRON ENERGY RANGE
C
-----

```

```

-----
C
CR          MAT - NT CONTROL
C
CL          (MATID(I) ,NTID(I) ,MWGT(I) ,I=1,NMMP)
C
CW          3*NMMP
C
CB          FORMAT(4H 5D ,11I6/(12I6))
C
CD          MATID(I)     MATERIAL IDENTIFICATION NUMBER
CD          NTID(I)      REACTION TYPE IDENTIFICATION NUMBER
CD          MWGT(I)      CROSS SECTION WEIGHTING OPTION
CD                      1 - CONSTANT
CD                      2 - 1/E
CD                      3 - THERMAL + 1/E + FISSION
CD                      4 - ARBITRARY
CD                      5 - COMBINED CTP CORR
C
-----

```

```

-----
C
CR          MATERIAL - REACTION TYPE CROSS SECTIONS
CR          AND ERROR FILES
CL          (CRS(J) ,J=1,NGROUP) , (ERROR(J) ,J=1,NGROUP)
CW          2=NGROUP
C
CB          FORMAT(4H 6D ,5E12.4/(6E12.4))
C
CD          CRS          CROSS SECTION
CD          ERROR        STANDARD DEVIATION
C
-----

```

```

-----
C
CR          MATRIX CONTROL
CL  MAT1,MT1,MAT2,MT2,NBLOK
CW          5
C
CB  FORMAT(4H 7D ,5I6)
C
CD  MAT1          MATERIAL 1 IDENTIFICATION NUMBER
CD  MT1          REACTION TYPE 1 IDENTIFICATION NUMBER
CD  MAT2          MATERIAL 2 IDENTIFICATION NUMBER
CD  MT2          REACTION TYPE 2 IDENTIFICATION NUMBER
CD  NBLOK        NUMBER OF BLOCKS INTO WHICH MATRIX IS SUBDIVIDED
C-----

```

```

-----
C
CR          GAMMA GROUP BOUNDARIES
C
CL  (GPBG(J) ,J=1,NGGRP) ,EGMIN
C
CC          PRESENT IF NGGRP.GT.0
CW  NGGRP+1
C
CB  FORMAT(4H 4D ,5E12.4/(6E12.4))
CD  GPBG(-J)     MAXIMUM ENERGY BOUND OF GAMMA GROUP(J) (EV)
CD  EGMIN        MINIMUM ENERGY OF GAMMA ENERGY RANGE
C-----

```

```

-----
C
CR          BLOCK CONTROL
CL  (JBAND(J) ,IJJ(J) ,J=1,NGGRP) , (LGRP(N) ,N=1 ,NBLOK)
C
CW  2*NGGRP +NBLOK
C
CB  FORMAT(4H 9D ,11I6/(12I6))
C
CD  JBAND(J)     BANDWIDTH FOR GROUP J
CD  IJJ(J)       POSITION OF DIAGONAL ELEMENT FOR GROUP J
CD  LGRP(N)      NUMBER OF GROUPS IN BLOCK(N)
C-----

```

```

-----
C
CR          MATRIX DATA
CL  (COV(K) ,K=1,KMAX)
C
CC  KMAX=SUM OVER JBAND(J) FOR ALL J IN BLOCK N
CW  KMAX
C
CB  FORMAT(4H 9D ,5E12.4/(6E12.4))
C
CD  COV          NTYPE MATRIX DATA
C-----
COEP

```

APPENDIX B

Sample Data Set in COVERX Format

The following page tabulates a six-group COVERX file for ^{239}Pu (n,f), ^{239}Pu (n, α), and their correlation to each other and ^{235}U (n,f).

00099

UV COVERX COVERX ORNL - FASS • 1

1D	6	6	0	2	2	5	5				
2D	*PU-239 WITH CRSS MATERIAL *										
3D	0.2000E+08	0.3679E+07	0.1353E+07	0.4979E+06	0.1832E+06						
4D	0.0870E+04	1.0000E-05									
5D	1399	1e	4	1399	102	4					
6D	0.2527E+01	0.1905E+01	0.1700E+01	0.1542E+01	0.1577E+01						
7D	6.8943E+02	7.1807E-02	3.1328E-02	3.4220E-02	3.3301E-02	5.2803E-02					
8D	1.1159E-02										
9D	0.2409E-02	0.7369E-02	0.5042E-01	0.1661E+00	0.3110E+00						
10D	2.7055E+02	3.0844E-01	3.0156E-01	1.8340E-01	2.0272E-01	2.0735E-01					
11D	3.2777E-02										
12D	1399	18	1395	18	1						
13D	6	1	6	2	6	3	6	4	6	5	6
14D	6	6									
15D	0.5226E-03	0.5994E-04	0.5904E-05	0.3307E-06	0.3658E-07						
16D	0.0000E-01	2.2059E-04	5.6112E-04	3.1519E-04	1.5050E-04	2.6206E-05					
17D	0.0000E-01	1.5923E-05	3.1589E-04	7.4648E-04	5.4840E-04	1.3548E-04					
18D	0.0000E-01	2.7077E-07	1.4659E-04	5.2944E-04	7.2653E-04	3.1184E-04					
19D	5.0867E-11	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01					
20D	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01					
21D	0.0000E-01										
22D	1399	18	1399	18	1						
23D	6	1	6	2	6	3	6	4	6	5	6
24D	6	6									
25D	0.5156E-02	0.1779E-03	0.1240E-03	0.1084E-03	0.0000E+00						
26D	0.0000E-01	1.7792E-04	9.8144E-04	7.2275E-04	5.1274E-04	0.0000E-01					
27D	0.0000E-01	1.2402E-04	7.2275E-04	1.1710E-03	9.2279E-04	0.0000E-01					
28D	0.0000E-01	1.0839E-04	5.1274E-04	9.2279E-04	1.1090E-03	2.1610E-04					
29D	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	2.1610E-04	2.7881E-03				
30D	6.1044E-11	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	6.1044E-11				
31D	1.2452E-04										
32D	1399	102	1395	18	1						
33D	6	1	6	2	6	3	6	4	6	5	6
34D	6	6									
35D	0.5305E-03	0.6019E-04	0.5826E-05	0.3551E-06	0.4393E-07						
36D	0.0000E-01	1.5549E-04	5.1331E-04	3.3768E-04	1.4556E-04	2.6384E-05					
37D	0.0000E-01	6.4966E-06	2.8125E-04	8.5504E-04	6.6841E-04	1.6726E-04					
38D	0.0000E-01	2.3163E-07	1.3554E-04	4.9092E-04	7.1516E-04	3.1742E-04					
39D	5.4195E-11	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01					
40D	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01					
41D	0.0000E-01										
42D	1399	102	1399	102	1						
43D	6	1	6	2	6	3	6	4	6	5	6
44D	6	6									
45D	0.9513E-01	0.9016E-01	0.1108E-01	0.1068E-03	0.0000E+00						
46D	0.0000E-01	9.0162E-02	9.0936E-02	1.1649E-02	4.8904E-04	0.0000E-01					
47D	0.0000E-01	1.1077E-02	1.1649E-02	3.3637E-02	3.6122E-02	3.5131E-02					
48D	1.4304E-09	1.0677E-04	4.8904E-04	3.6122E-02	4.1097E-02	4.0196E-02					
49D	1.6267E-09	0.0000E-01	0.0000E-01	3.5131E-02	4.0196E-02	4.2993E-02					
50D	1.6808E-09	0.0000E-01	0.0000E-01	1.4304E-09	1.6267E-09	1.6808E-09					
51D	1.0743E-03										
52D	1399	18	1399	102	1						
53D	6	1	6	2	6	3	6	4	6	5	6
54D	6	6									
55D	0.5144E-02	0.1616E-03	0.1208E-03	0.1060E-03	0.0000E+00						
56D	0.0000E-01	1.7298E-04	9.3325E-04	6.8386E-04	4.9390E-04	0.0000E-01					
57D	0.0000E-01	1.2473E-04	7.4912E-04	1.2815E-03	8.7607E-04	0.0000E-01					
58D	0.0000E-01	1.9913E-04	5.0818E-04	1.0461E-03	1.1000E-03	1.5933E-04					
59D	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	2.6594E-04	2.8283E-03					
60D	4.4394E-11	0.0000E-01	0.0000E-01	0.0000E-01	0.0000E-01	7.1726E-11					
61D	1.3718E-04										

Comments Concerning the Multigroup Cross Section Library



NUCLEAR DIVISION

INTERNAL CORRESPONDENCE

July 6, 1979

C. R. Weisbin, 6025, 18W, (4-6186)

100 group fast reactor data testing library appropriate for analysis of the elastic removal treatment and the carbide benchmarks

Several attempts have been made to assemble a fast reactor data testing library. Each effort was met with some shortcoming that limited the usefulness of the data. I now believe that we have a cross section tape which is suitable for the analysis of the benchmarks of interest to you. The preparation of the subject AMPX master resulted in a considerable amount of post-processing (MINX) data adjustment and manipulation. The purpose of this memo is to release the 100 group AMPX master to the data testing team for a continuation of the analysis project.

The resulting 100 group AMPX master tape has undergone the following (these items also refer to both the 174 group VITAMIN-E and 100 group preliminary tapes):

- * the elastic removal cross section, which appears in the record preceding the f-factors and the 1-D array string, was redefined to correspond to a summation over outscatter groups for the elastic scattering matrix.
- * an error in the MINX AMPX interface option, which produced extra data for the 2-D matrices, was corrected. B-11, which was processed on 79.045, was not affected by this program bug. Also, this correction disallows normalization problems in the COMET module.
- * the elastic smooth group cross section was redefined to be a summation over all sink groups for a given source group.
- * the total cross section was redefined to be the sum of all partial reactions.

C. R. Weisbin
Page 2
July 6, 1979

* the discrete and continuum inelastic scattering matrices were normalized to the smooth averaged ENDF/B File 3 total inelastic cross section.

For the record, the input/output interface files and the various paths taken to produce the final master tape are provided in figures 1-4. These figures illustrate the 4-step approach used to correct, manipulate, collapse and normalize the AMPX interfaces produced by MINX-I.3(V).

The contents of the 100 group library containing 18 nuclides are given in Table 1. The following DD card is required to access the data on K-25 tape 022405:

```
//GO.FTMNFOO1 DD UNIT=TAPE16,DISP=(OLD,KEEP),LABEL=(1,SL),  
//VOL=SER=022405,DSN=X.JEWDE637.AMPX.LIB100.NUC18,  
//DCB=(RECFM=VBS,LRECL=X,BLKSIZE=6447,BUFL=8148)
```

John

J. E. White, 6025, 3M, (4-5277)

JEW/tj

cc: File-NoRC
R. W. Wright, 6025, 5M, (4-5279)
J. L. Lucius, 6025, 21E, (4-5270)
W. E. Ford, III, 6025, 17E, (4-5272)
J. Barhen, 6002-A, 18W, (4-5264)
J. H. Marable, 6025, 18W, (4-6189)
Jim Smith, 3010, C009, (4-5585)

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Table C-1. 100 Group Fast Reactor Data Testing Materials

<u>ENTRY</u>	<u>DESCRIPTION</u>	<u>IDENTIFIER</u>
1	Fe	1326
2	Pu-240	380
3	Pu-241	381
4	U-235	395
5	U-238	9398
6	Pu-239	399
7	B-11	1160
8	Al-27	1313
9	Cr	1324
10	Mn-55	1325
11	Na-23	1311
12	Ni	1328
13	O-16	1276
14	Si	1314
15	C-12	1306
16	U-234	1043
17	Pu-242	1161
18	Mo	1287

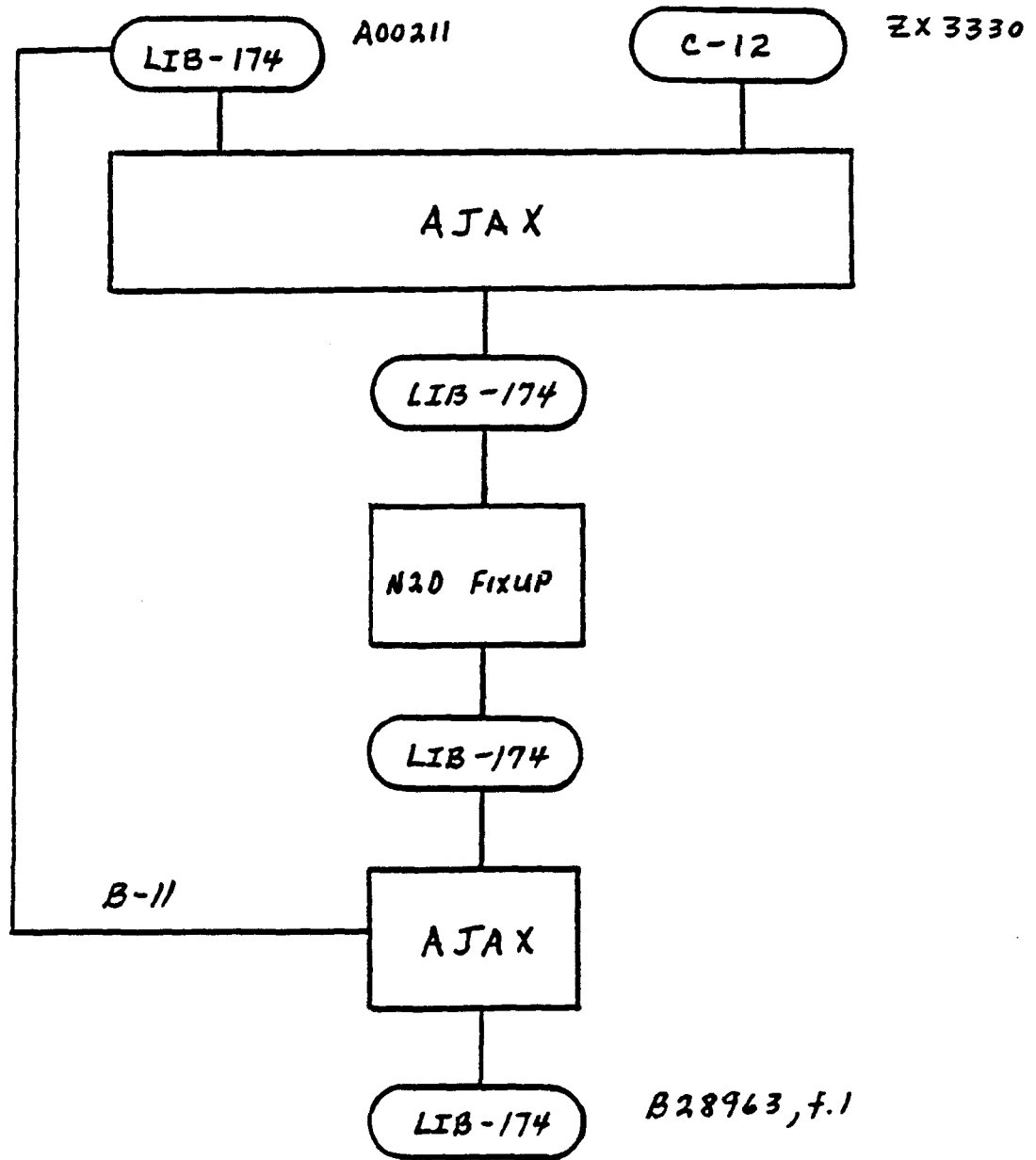


Fig. C-1. CORRECT N2D PROBLEM FOR VITAMIN-E NUCLIDES

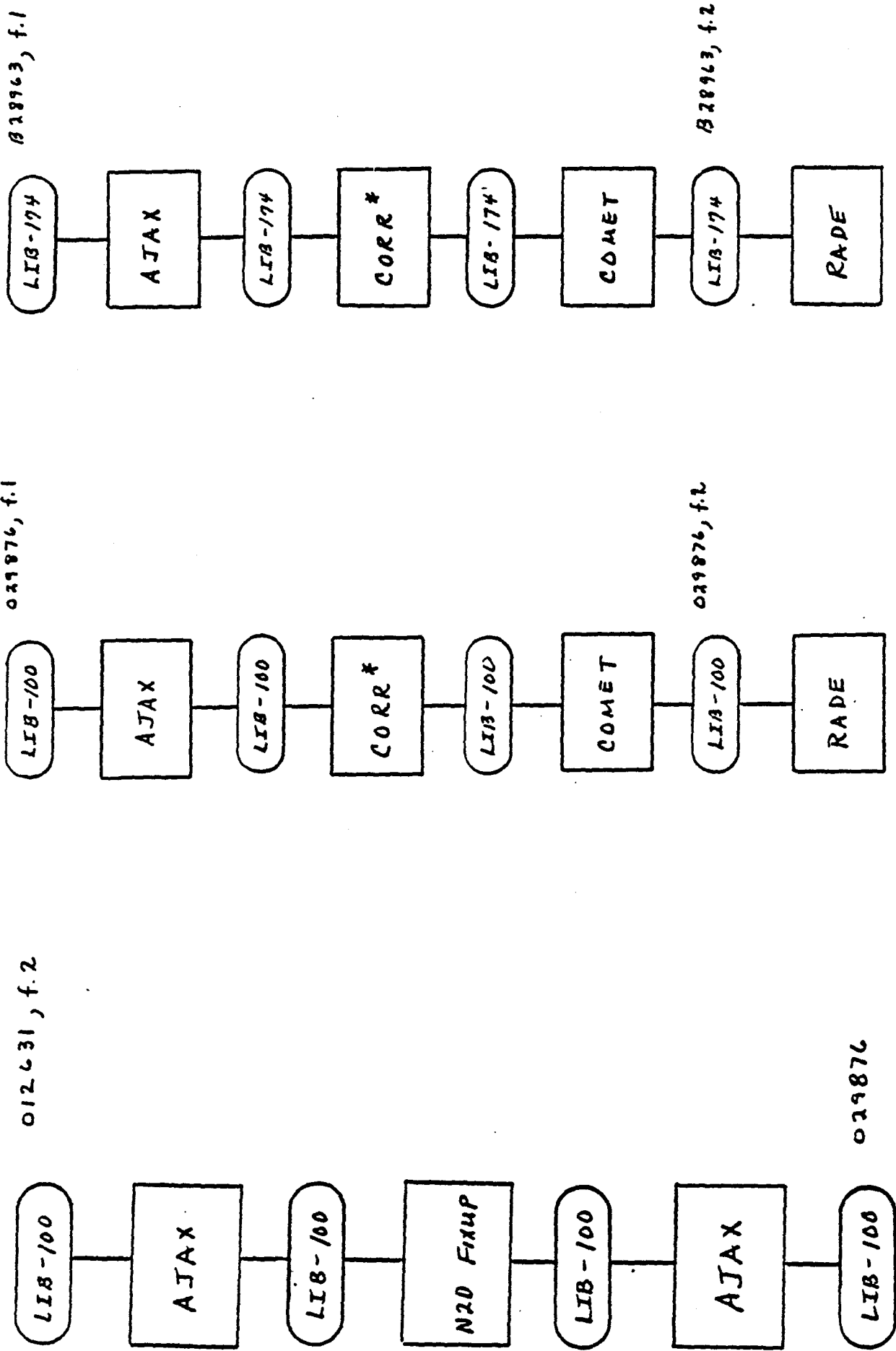


Fig. C-2.

CORRECT N2D PROBLEM FOR PRELIMINARY ENDF/B V NUCLIDES

Fig. C-3. REDEFINE THE ELASTIC REMOVAL CROSS SECTION AND NORMALIZE THE INELASTIC MATRICES

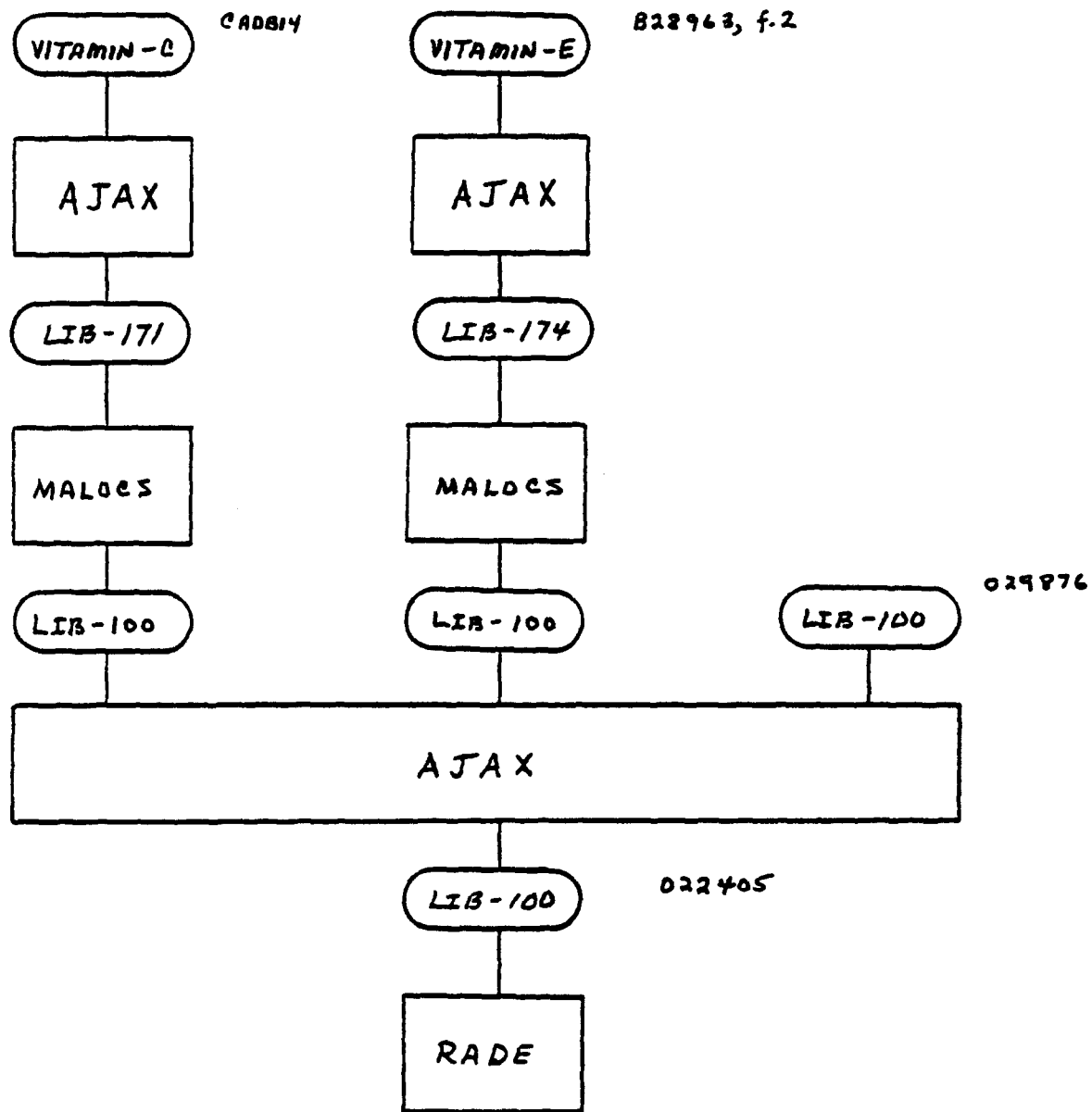


Fig. C-4. COLLAPSE VITAMIN-C AND VITAMIN-E FILES AND MERGE DATA



NUCLEAR DIVISION
INTERNAL CORRESPONDENCE

August 2, 1979

Y. Yeivin

100-Group AMPX Master Library for Fast-Reactor Data Testing--Mod. No. 1

John White's 100-group AMPX master library for fast-reactor data testing¹⁻⁴ has been modified by the addition of ¹⁰B data. The ¹⁰B master data set was obtained by using the weighting function described in Table 3 of Ref. 3 to collapse data set 1273 from the VITAMIN-C library^{5,6} into the 100-group structure. The materials in "Mod 1 to the 100-group master library" are listed in Table 1. The library is on CTC tape 4577 and can be read with the following DD card:

```
//GØ.FT--FOO1 DD UNIT=TAPE16,LABEL=(1,SL),VØL=SER=004577,
DISP=(ØLD,KEEP),DSN=X.JEWDE637.AMPX.LIB100.NUC19,
DCB=(RECFM=VBS,LRECL=X,BLKSIZE=6447,BUFL=8148)
```

Enclosed is the printout from the AJAX-MALOCS-AJAX case required to prepare the library. Tape 4577 has been assigned to J. L. Lucius.

This work was charged to 18075.

Eddy Ford

W. E. Ford, III, 6025, 17E, (4-5272)

Betsy Diggs

B. R. Diggs, 6025, 9M, (4-5281)

WEF/BRD/tj

cc: J. Barhen, 6002A, A3, (4-5264)
J. L. Lucius, 6025, 21E, (4-5270)
J. H. Marable, 6025, K5, (4-6189)
J. D. Smith, 6010
J. E. White, 6025

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TABLE -1. 100-GROUP AMPX MASTER LIBRARY FOR FAST-REACTOR DATA TESTING -- MOD. NO. 1

ENTRY	IDENTIFIER	ENDF/B	V	FE	PRE-FINAL	RELEASE	MAT	Y L E	(PRI	COMM)	SDU
1	1326	ENDF/B	V	PU-240	PRE-FINAL	RELEASE	MAT 1326		(PRI	COMM)	
2	380	ENDF/B	V	PU-241	PRE-FINAL	RELEASE	MAT 380		(PRI	COMM)	
3	381	ENDF/B	V	U-235	PRE-FINAL	RELEASE	MAT 381		(PRI	COMM)	
4	395	ENDF/B	V	U-238	PRE-FINAL	RELEASE	MAT 395		(PRI	COMM)	
5	9398	ENDF/B	V	PU-239	PRE-FINAL	RELEASE	MAT 9398		(PRI	COMM)	
6	399	ENDF/B	V	U-239	PRE-FINAL	RELEASE	MAT 399		(PRI	COMM)	
7	1160	U11		MINX CASE	(174 GRPS)	FOR VITAMIN E					
8	1313	AL27		MINX CASE	(174 GRPS)	FOR VITAMIN E					
9	1324	CR		MINX CASE	(174 GRPS)	FOR VITAMIN E					
10	1325	MN55		MINX CASE	(174 GRPS)	FOR VITAMIN E					
11	1311	NA-23		MINX CASE	(174 GRPS)	FOR VITAMIN E					
12	1328	N1		MINX CASE	(174 GRPS)	FOR VITAMIN E					
13	1276	D16		MINX CASE	(174 GRPS)	FOR VITAMIN E					
14	1314	S1		MINX CASE	(174 GRPS)	FOR VITAMIN E					
15	1306	ENDF/B	V	C-12	PRE-FINAL	RELEASE	MAT 1306		(PRI	COMM)	
16	1043	U234		CASE FOR	COMBINED	CTR &	CRUR	PROCESSING	DEC	.77	
17	1161	PU242		CASE FOR	COMBINED	CTR &	CRUR	PROCESSING	DEC	.77	
18	1287	NO		CASE FOR	COMBINED	CTR &	CRUR	PROCESSING	DEC	.77	
19	1273	B-10		CASE FOR	COMBINED	CTR &	CRUR	PROCESSING	DEC	.77	

REFERENCES

1. J. L. Lucius, J. E. White, and R. Q. Wright, "Fast Reactor Data Testing of ENDF/B-V - Status Report No. 1," UCC-ND IC (February 8, 1979).
2. J. L. Lucius, J. E. White, and R. Q. Wright, "Fast-Reactor Data Testing of ENDF/B-V - Status Report No. 2," UCC-ND IC (February 22, 1979).
3. R. Q. Wright, J. E. White, J. L. Lucius, W. E. Ford, III, "Fast-Reactor Data Testing of ENDF/B-V - Status Report No. 3," UCC-ND (May 11, 1979).
4. J. E. White to C. R. Weisbin, "100-Group Fast Reactor Data Testing Library Appropriate for Analysis of the Elastic Removal Treatment and the Carbide Benchmarks," UCC-ND (July 6, 1979).
5. R. W. Roussin, C. R. Weisbin, J. E. White, R. Q. Wright, N. M. Greene, W. E. Ford, III, J. B. Wright, and B. R. Diggs, "Experience in Developing and Using the VITAMIN-C 171- Neutron, 36-Gamma-Ray Group Cross-Section Library," A Review of Multigroup Nuclear Cross-Section Processing, Proceedings of a Seminar-Workshop, ORNL/RSIC-41, page 107 (October 1978).
6. C. R. Weisbin, R. W. Roussin, J. E. White, and R. Q. Wright, "Specification for Pseudo-Composition-Independent Fine-Group and Composition Dependent Fine- and Broad-Group LMFBR Neutron-Gamma Libraries at ORNL," ORNL/TM-5142 (ENDF-224) (December 1975).

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APPENDIX D

Comments Concerning Uncertainty File Information

INTRA-LABORATORY CORRESPONDENCE

OAK RIDGE NATIONAL LABORATORY

October 26, 1979

TO: J. J. Wagschal

FROM: J. D. Smith

SUBJECT: Documentation of Formation of B-10 (n, α) Uncertainty File

In ENDF/B-V, the U-238 capture covariance has been expressed as having been evaluated via a ratio measurement to B-10 (n, α). In order for PUFF-II to operate, the uncertainties of the standard or reference material from which another material is evaluated, must be given explicitly in its respective uncertainty file. This is not the case for B-10 (n, α). Instead, B-10 (n, α) uncertainty has been expressed as a "derived redundant cross section" uncertainty in which, from the energy range of 1.0×10^{-5} eV to 2.0×10^7 eV, B-10 (n, α) is derived from the uncertainties in (n, α_0), (n, α_1) and (n, α_0) to (n, α_1). This may be expressed as

$$\langle 107 \cdot 107 \rangle = \langle 780 \cdot 780 \rangle + \langle 781 \cdot 781 \rangle + 2\langle 780 \cdot 781 \rangle, \quad (1)$$

where I am now using the respective MT numbers for the reactions and the diamond brackets indicate covariances.

What has been given to me in the uncertainty files is the relative covariance matrices (in a LB=5 format) for each of the covariances on the righthand side of Eq. (1). A relative covariance matrix for (n, α) in a LB = 5 format is the desired result. Thus to form this matrix one must first convert each of the given relative covariances to absolute, sum each of these covariances as given in Eq. (1), and then divide by the (n, α) cross section to put the (n, α) covariance in relative form.

By appropriate input into the PUFF-II code, the relative covariance matrix for (n, α) has been formed. Also, a small code named FORM, FOR, which performs essentially the same operations as those needed in PUFF-II, was written to check the results. A hand check of the results was also performed.

One-hundred group cross sections from John White's GE library were used to form the matrices. The results have been recorded in a LB = 5 formatted uncertainty file for the single (n, α) reaction. This uncertainty file is on cards and may be obtained from either Bryan Broadhead or me.

00110

October 26, 1979

As a side note, the B-10 (n, α) uncertainty file is in error in ENDF/B-V since, according to the data formats (F. G. Perey, "The Data Covariance Files for ENDF/B-V"), the standard or reference material uncertainties are to be expressed explicitly over the energy range from which other materials are derived.

sah

cc: B. L. Broadhead
H. L. Dodds
J. H. Marable
F. G. Perey
C. R. Weisbin
Y. Yeivin

00111

INTRA-LABORATORY CORRESPONDENCE

OAK RIDGE NATIONAL LABORATORY

November 20, 1979

TO: J. D. Smith

FROM: G. de Saussure

SUBJECT: Your request for a provisional covariance file for ^{238}U ,
ENDF/B-V, in the resolved resonance region (1 eV to 4 keV).

The proper covariance file is that of the errors in the resonance parameters as given in Tables 22, 23, and 24 of Nuclear Energy, Vol. 3.87 (1979), and as confirmed in the memo of F. G. Perey to C. R. Weisbin dated May 24, 1979.

However, since that file cannot be processed properly at the present time, I have estimated roughly covariances for infinitely dilute cross sections as:

$$\left[\frac{\delta\sigma}{\sigma}\right]_{n,f} = 20\% \quad \left[\frac{\delta\sigma}{\sigma}\right]_{n,\gamma} = 5\% \quad \text{and} \quad \left[\frac{\delta\sigma}{\sigma}\right]_{n,n} = 4\%$$

These errors must be interpreted as fully correlated over the range 1 eV to 4 keV and uncorrelated with each other and with other cross sections. These estimates are very rough and should be used only until the proper file is processed, for infinitely dilute cross sections and for assemblies with zero sensitivity below 4 keV! I hope this information will be helpful.

GdS/ep

cc: J. H. Marable

00112

OAK RIDGE NATIONAL LABORATORY

OPERATED BY
UNION CARBIDE CORPORATION
NUCLEAR DIVISION



POST OFFICE BOX X
OAK RIDGE, TENNESSEE 37830

September 11, 1979

Dr. Robert R. Kinsey
Building 197
National Nuclear Data Center
Brookhaven National Laboratory
Upton, New York 11973

Dear Bob:

There is an error in the iron (MAT=1326) covariance file (MF=33) of ENDF/B-V. As Brian Broadhead has pointed out, the second energy point in the second NI sub-subsection of MT=1 needs to be $4.0E+5$ instead of $4.0E-5$. Also, for completeness, the NI sub-subsection of MT=2 should be extended to cover the full energy range. I have shown this to Peter Fu and he agrees. If there are any problems, let me know.

Sincerely,

A handwritten signature in black ink, appearing to read "J. D. Smith", with a large, stylized flourish extending to the left.

J. D. Smith

sah

cc: H: L. Dodds
P. Fu
F. G. Perey
R. W. Roussin
C. R. Weisbin
B. L. Broadhead

00113

APPENDIX E

Comments from file 1 of ENDF/B-V concerning the uncertainty information in file 31 through 33.

E-2

FILE 1 INFORMATION FOR ENDF/B-V OXYGEN	77	0	0	0
MF=33				1276 1451
MT=1, 2, 4, 103, AND 107 SMOOTH X/S COVARIANCES				1276 1451
COVARIANCES ARE BASED UPON ESTIMATES OF THE UNCERTAINTY IN				1276 1451
THE EXPERIMENTAL MEASUREMENTS AND THEORETICAL CALCULATIONS				1276 1451
USED IN THE EVALUATION. FORMAT UPDATED FOR VERSION V.				1276 1451
				1276 1451
FILE 1 INFORMATION FOR ENDF/B-V PU-239	77	0	0	0
MF=33				1399 1451
COVARIANCE FILE				1399 1451
- FISSION DATA FROM 200 KEV TO 20 MEV (MT=18).				1399 1451
CORRELATED TO FISSION CROSS SECTION OF U-235. NORMALIZATION				1399 1451
AND STATISTICAL ERRORS ARE INCLUDED.				1399 1451
- CAPTURE DATA (MT = 102) CORRELATED WITH PU-239 FISSION DATA				1399 1451
UNCERTAINTIES IN ALPHA ARE GIVEN.				1399 1451
- TOTAL NU-BAR (MT = 452) SIMPLIFIED REPRESENTATION OF LEAST				1399 1451
SQUARE FIT.				1399 1451
				1399 1451
FILE 1 INFORMATION FOR ENDF/B-V B-10	77	0	0	0
CHANGES FROM VERSION IV				1305 1451
				1305 1451
2. COVARIANCE FILE (33) ADDED FOR CROSS SECTIONS BELOW 1 MEV.				1305 1451
				1305 1451
MF=33 ----- CROSS-SECTION COVARIANCES -----				1305 1451
				1305 1451
THE RELATIVE COVARIANCES FOR THE MOST IMPORTANT REACTIONS OPEN				1305 1451
BELOW 1 MEV ARE GIVEN IN FILE 33. THESE ARE CALCULATED DIRECTLY				1305 1451
FROM THE COVARIANCES OF THE S-MATRIX PARAMETERS, USING FIRST-				1305 1451
ORDER ERROR PROPAGATION.				1305 1451
				1305 1451
MT=2, 780, 781 (N,N), (N,ALPHA), AND (N,ALPHA1) COVARIANCES				1305 1451
0 TO 1 MEV. RELATIVE COVARIANCES AMONG THESE THREE				1305 1451
REACTIONS ARE ENTERED EXPLICITLY USING NI-TYPE SUB-				1305 1451
SUBSECTIONS IN THE LINES (DIRECT) REPRESENTATION.				1305 1451
1 TO 20 MEV, ALL COVARIANCES SET EQUAL TO ZERO, NOT				1305 1451
INTENDED FOR USE IN THIS ENERGY RANGE.				1305 1451
				1305 1451
MT=1, 107 (TOTAL) AND (N,ALPHA) COVARIANCES				1305 1451
0 TO 1 MEV, FOR COMPACTNESS, THESE COVARIANCES ARE CON-				1305 1451
STRUCTED FROM THOSE DESCRIBED ABOVE, USING NC-TYPE SUB-				1305 1451
SUBSECTIONS. THE CONSTRUCTED COVARIANCES FOR THE TOTAL				1305 1451
CROSS SECTION THEREFORE REFLECT CONTRIBUTIONS FROM THE				1305 1451
(N,GAMMA), (N,P), (N,T), AND (N,N1) REACTIONS WHICH ARE				1305 1451
ALL PRESUMED TO BE SMALL IN MAGNITUDE BELOW 1 MEV.				1305 1451
NOTE THAT ALTHOUGH THE TOTAL-CROSS-SECTION COVARIANCES				1305 1451
ARE ENTERED IN THE NC-TYPE (DERIVED) FORMAT, TOTAL-				1305 1451
CROSS-SECTION DATA WERE INCLUDED IN THE FIT, AND THEY				1305 1451
INFLUENCED ALL THE CALCULATED COVARIANCES.				1305 1451
1 TO 20 MEV, SET EQUAL TO ZERO, NOT INTENDED FOR USE IN				1305 1451
THIS ENERGY RANGE.				1305 1451
				1305 1451

FILE 1 INFORMATION FOR ENDF/B-V U-235	77 0 0
*** COVARIANCE FILES ***	1324 1451
THE REPRESENTATION OF DEPENDENT DATA (E.G. MT=4) REFLECTS THE	1324 1451
MANNER IN WHICH REACTIVELY REACTS THE. IN THE CASE OF SOME	1324 1451
CODES SUCH AS WJY, THIS REPRESENTATION TENDS TO INCREASE	1324 1451
PROBABILITY VALUES, PARTICULARLY WITH REGARD TO MT=4 AND MT=51-91.	1324 1451
AN ALTERNATIVE REPRESENTATION WHICH REDUCES PROCESSING TIME IS	1324 1451
MT=3 (POSITIVE) AND MT=16, 17, 22, 23, 02, 07 (NEGATIVE) AND THE	1324 1451
ELIMINATION OF MT=51-91 IN THE COVARIANCE FILES.	1324 1451
HOWEVER, THE RESULTANT FILE WILL NO LONGER REPRESENT THE AUTHORS	1324 1451
BEST ESTIMATE OF THE UNCERTAINTIES.	1324 1451
***	1324 1451
FILE 1 INFORMATION FOR ENDF/B-V U-235	77 0 0
MF = 33	1395 1451
COVARIANCE FILE BY R.W. PELLE FROM REF 18	1395 1451
PRINCIPAL REFERENCES	1395 1451
18. R.W. PELLE (APP. 2 OF EPRI PROJ 512 REPORT) BY E.T. TOMLINSON ET AL	1395 1451
FILE 1 INFORMATION FOR ENDF/B-V PU-240	77 0 0
MF=32, MT=191 RES. PARAM. ERROR FILE FROM 0.5 TO 105 EV.,	1380 1451
ERRORS BASED ON DIFFERENCE IN MEASUREMENTS BECAUSE	1380 1451
QUOTED ERRORS NOT CONSISTENT IN REF 4, 5, 6.	1380 1451
MF=33, MT=102 BROAD GROUP ERROR FILE, SUBJECTIVE BECAUSE OF	1380 1451
INSUFFICIENT DATA FOR STATISTICAL ANALYSIS.	1380 1451
REFERENCES	1380 1451
4. H. ABIGANING, R. HERR, AND F. POERTMANS, PROC. CONF. RESONANCE PARAM. OF	1380 1451
FERTILE NUCLEI AND 239-Pu, SACLAY, 219, NEANDC(E) 1630 (1974).	1380 1451
5. M. HODDGE, SEE REF 4.	1380 1451
6. R. W. HOCKENBURY, W. R. MYER, AND R. C. BLACK, NUCL. SCI. ENG. 49,	1380 1451
193 (1972).	1380 1451
FILE 1 INFORMATION FOR ENDF/B-V C-12	77 0 0
33-1 TO 33-107 UNCERTAINTY FILES FOR FILE 3 DATA,	1306 1451
	1306 1451
FILE 1 INFORMATION FOR ENDF/B-V PU-241	77 0 0
MF=33 MT=10 BROAD GROUP ERROR FILE, SUBJECTIVE BECAUSE OF	1381 1451
INSUFFICIENT DATA FOR STATISTICAL ANALYSIS.	1381 1451
MF=33 MT=102 SAME AS ABOVE.	1381 1451
FILE 1 INFORMATION FOR ENDF/B-V FE	77 0 0
FILE 32 COVARIANCES FOR RESONANCE PARAMETERS PE77	1326 1451
FILE 33 COVARIANCES FOR FILE-3 DATA	1326 1451
REFERENCES	1326 1451
PE77 0.1 REPEY, PRIVATE COMMUNICATION, 1977 (TO BE PUBLISHED)	1326 1451

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FILE 1 INFORMATION FOR EUDF/B-V 0-23 ₀	77 0 0
MF = 31	1398 1451
MF = 465 BASED ON ERROR ESTIMATES IN REF. 1 AND 2.	1398 1451
MF = 426 BASED ON DATA OBTAINED FROM FITTING EXPT. NO. BAR PROMPT	1398 1451
MF = 33	1398 1451
POINTS 4 KEY THE ENRIANCES IN PTS = 2, 18, AND 102 HAVE BEEN	1398 1451
SET TO ZERO. THE UNCERTAINTY INFORMATION SHOULD BE TAKEN FROM	1398 1451
TAKEN FROM TABLES 22, 23, AND 24 OF REF. 7. AT HIGHER ENERGIES	1398 1451
INST MF FILE 33 WAS BASED ON DATA FROM ANL/NCH-32.	1398 1451
REFERENCES	1398 1451
1. G.E. KAISER AND S.G. CARPENTER (ANL-WEST) PRIV. COMM. (MAR. 78)	1398 1451
••DATA INSERTED INTO FILE AT 5% BY R. KINSEY 4/18/78••	1398 1451
2. S.A. GEA AND COLLEES (1974)	1398 1451

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Engineering Physics Division

PROCESSING ENDF/B-V UNCERTAINTY DATA INTO
MULTIGROUP COVARIANCE MATRICES *

J. D. Smith III *

Date Published: June 1980

* Submitted in partial fulfillment of the requirements for a Master of Science Degree in the Department of Nuclear Engineering, University of Tennessee

OAK RIDGE NATIONAL LABORATORY
Oak Ridge, Tennessee 37830
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UNION CARBIDE CORPORATION
for the
DEPARTMENT OF ENERGY

00117

PROCESSING ENDF/B-V UNCERTAINTY DATA INTO
MULTIGROUP COVARIANCE MATRICES

J. D. Smith III

ABSTRACT

The purpose of this work is to develop and demonstrate the capability of processing Evaluated Nuclear Data File, system B, version five (ENDF/B-V) uncertainty data into multigroup covariance matrices. These covariances may then be folded with sensitivity coefficients to obtain uncertainties in selected integral parameters such as K-effective and breeding ratio.

The project consisted of separating the previous uncertainty processor (PUFF) from the basic nuclear data cross section processor (MINX), updating the uncertainty processor to the ENDF/B-V format, programming the processor for new uncertainty data, and demonstrating the processor capabilities by producing a multigroup covariance library. These capabilities were verified in various ways including hand calculations and comparisons with other known results.

A computer code named PUFF-II was written to perform the task described above. The code is capable of processing all uncertainty data currently entered in ENDF/B-V. The only limitation of the code is the treatment of uncertainties in resonance data.

CHAPTER I

INTRODUCTION

The basic nuclear data in the Evaluated Nuclear Data Files System B (ENDF/B) has been broadened and improved upon for many years, by new discoveries, better understanding, and improved technical capabilities. However, improvements in ENDF/B data are still needed.¹ Specifically, it is now evident that some means must be developed to indicate just how good the basic nuclear data are. This measure of the goodness of data has been to include estimated uncertainties in the evaluated microscopic data in ENDF/B files in a standard manner. These uncertainty files, after processing, may be used in conjunction with sensitivity analysis to allow for propagation of uncertainties in basic nuclear data (i.e., ENDF/B) to uncertainties in reactor performance parameters such as K-effective and breeding ratio, thus allowing for systematic adjustment processes. This uncertainty analysis will also allow for valuable feedback to the nuclear data community as to which measurements and/or evaluations most need further refinement.

The objective of this thesis project is to develop the capability of processing uncertainty data in ENDF/B version 5 (ENDF/B-V). Just as the microscopic nuclear data of ENDF/B is processed according to specified algorithms into multigroup form, so is the uncertainty data processed by specific algorithms into multigroup covariance matrices. A covariance shall be defined statistically as the expected value of the product of the deviations of two random variables (may be the same random variable) from their respective means. Each variable is allowed to have its own energy intervals which forms the two dimensions of a covariance matrix.

Previous work in this field consisted of processing limited ENDF/B-IV data (ENDF/B-IV contained uncertainties for nitrogen, oxygen, and carbon only) using an uncertainty processor, PUFF², developed by extending the MINX³ cross section processor. Many additional unofficial cross section uncertainty evaluations were prepared at ORNL in an ENDF/B-IV format.⁴ From this data and the PUFF code, three multigroup covariance libraries were produced, which are available through the Radiation Shielding Information Center (RSIC) at ORNL. These three libraries are the fission spectrum covariance matrix library (with GODIVA^{5,6} weighting), the LMFBR core physics covariance matrix library (with ZPR-6/7⁷ weighting), and the LMFBR shielding covariance library (with 1/E weighting). These libraries are in a standard format, COVERX,⁸ for use in the FORSS⁹ system. The FORSS system is a collection of codes used in sensitivity and uncertainty analysis.

In the present work, the capability of processing newly formatted ENDF/B-V data has been developed. Specifically, processing capabilities have been added for new uncertainty relationships, explicit cross reaction and cross material relationships (cross is used to indicate that the two random variables are not the same), and derived uncertainties. Derived is used here in the context that a reaction type (and therefore its uncertainties) may be determined by summing other reaction types (e.g., the total cross section is the sum of its partial cross sections). Derived is also used in the context that some reaction types are determined by ratio measurements to a reference reaction type (e.g., ²³⁹Pu fission cross section is measured as a ratio to the ²³⁵U fission cross section). Capabilities have also been added to produce the off-diagonal submatrices resulting from derived (in the context of summing) uncertainties. Processing uncertainties in the average number of neutrons per fission ($\bar{\nu}$) and in the

resolved resonance parameters (for infinitely dilute systems only) have also been included. Finally, an important accomplishment of this work has been to separate the uncertainty processing from the cross section processing, originally suggested by Las Alamos Scientific Laboratory (LASL), to provide not only for a modular code system, but to reduce computing costs.

This new processing capability has been implemented in a new version of the PUFF code named PUFF-II and requires that the user supply only the multigroup cross sections (e.g., VITAMIN-C or -E libraries^{10,11}) with corresponding flux spectrum and, of course, the uncertainty file data of ENDF/B-V.

The text of this thesis is organized into six chapters. Chapter II includes definitions for some of the terminology used in the remainder of this thesis. Chapter III explains the basic formats for the uncertainty data expressed in ENDF/B-V. Chapter IV explains the specific processing techniques that are used to produce multigroup covariance matrices. Verification of PUFF-II is described in Chapter V. Chapter VI shows some typical results produced by PUFF-II. The conclusions of this work and recommendations for future work are given in the final chapter.

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CHAPTER II

DEFINITIONS

Because ENDF/B is, in effect, breaking new ground in the computation and recording of uncertainty data, several new terms will appear which need to be clearly defined.

Given two variables, X_i and Y_j , which, for this case, represent the multigroup cross section of reaction type X , energy group i , and reaction type Y , energy group j , the covariance matrix (or absolute covariance matrix), COV of such may be described as

$$\text{Cov}(X_i, Y_j) \equiv \langle (X_i - \hat{X}_i) (Y_j - \hat{Y}_j) \rangle, \quad (1)$$

where the diamond shaped bracket and the tilde indicate the expectation (mean) value. From this, several other qualities may be defined, namely the relative covariance matrix, Rel.Cov,

$$\text{Rel. Cov}(X_i, Y_j) = \frac{\text{COV}(X_i, Y_j)}{X_i Y_j}, \quad (2)$$

the standard deviation, Std.Dev,

$$\text{Std.Dev.}(X_i) = \sqrt{\text{Cov}(X_i, X_i)}, \quad (3)$$

and the relative standard deviation, Rel.Std.Dev.,

$$\text{Rel.Std.Dev}(X_i) = \frac{\text{Std.Dev}(X_i)}{X_i}. \quad (4)$$

Also, a correlation matrix, Corr, may be defined as:

$$\text{Corr}(X_i, Y_j) = \frac{\text{Cov}(X_i, Y_j)}{(\text{Std.Dev}(X_i))(\text{Std.Dev}(Y_j))}, \quad (5.1)$$

or

$$\text{Corr}(X_i, Y_j) = \frac{\text{Rel.Cov}(X_i, Y_j)}{(\text{Rel.Std.Dev.}(X_i))(\text{Rel.Std.Dev.}(Y_j))}. \quad (5.2)$$

The correlation matrix shows quantitatively the degree of correlation between X_i and Y_j . The correlation matrix is bounded by unity, i.e.,

$$| \text{Corr}(X_i, Y_j) | \leq 1. \quad (6)$$

When $\text{Corr}(X_i, Y_j) = 0$, the variables X_i and Y_j are said to be totally uncorrelated. When $\text{Corr}(X_i, Y_j) = +1$ or -1 , the variables are said to be fully correlated or fully anti-correlated, respectively.

It should also be noted that the term covariance and uncertainty are used interchangeably.

CHAPTER III

ENDF/B-V UNCERTAINTY DATA FORMATS

In the ENDF/B system the microscopic data are grouped into files according to the type of data. For example, file 1 contains the microscopic data for \bar{v} , file 2 contains the resolved resonance parameters, and file 3 is for the "smooth" microscopic cross sections. The uncertainty file number is determined by adding 30 to the respective microscopic data file number. Thus, file 31 contains uncertainty data for \bar{v} , file 32 contains uncertainties in the resolved resonance parameters, and file 33 contains uncertainties for the smooth microscopic cross sections. As a side note, these three uncertainty files are the current extent of the uncertainty data in ENDF/B-V, although future plans are to include uncertainties in the fission spectrum χ , and in secondary energy and angular distributions.

Files 31 and 33 have identical formats in the ENDF/B-V system and may thus be described together.

Files 31 and 33 are broken down into sections, subsections and sub-subsections. A section completely describes a specific reaction type which is classified by an MT number (e.g., MT=1 is the total cross section, MT=2 is the elastic scattering cross section, etc.). Thus, for example, a section related to the total cross section, MT=1, completely describes the uncertainty related to MT=1.

A subsection completely describes a single covariance matrix. A sub-subsection describes the various components of the covariance matrix and are independent of each other.

Two different types of sub-subsections are used in ENDF/B-V and are

referred to as "NI-type" and "NC-type" sub-subsections. The "NI-type" is used to explicitly describe the various components of the covariance matrix of the subsection. The "NC-type" is used to indicate that some or all of the contributing components to the covariance matrix, described in the subsection, are to be found in a different subsection already in the ENDF/B-V data. The idea behind this is, of course, to eliminate the large portion of the uncertainty data that would otherwise have to be repeated as "NI-type" sub-subsections. In each "NI-type" sub-subsection there is a flag which indicates the type of correlations as a function of energy described in the sub-subsection. The flag is called a LB number of which six are permitted in ENDF/B-V:¹²

LB=0 Absolute components only correlated within each E_k interval

$$\text{Cov}(X_i, Y_j) = \sum_k P_{j;k}^{i;k} F_{xy,k} \quad , \quad (7)$$

LB=1 Relative components only correlated within each E_k interval

$$\text{Cov}(X_i, Y_j) = \sum_k P_{j;k}^{i;k} F_{xy,k} X_i Y_j \quad , \quad (8)$$

LB=2 Relative components correlated over all E_k intervals

$$\text{Cov}(X_i, Y_j) = \sum_{k,k'} P_{j;k'}^{i;k} F_{xy,k} F_{xy,k'} X_i Y_j \quad , \quad (9)$$

LB=3 Relative components correlated over E_k and E_l intervals

$$\text{Cov}(X_i, Y_j) = \sum_{k,l} P_{j;l}^{i;k} F_{x,k} F_{y,l} X_i Y_j \quad , \quad (10)$$

LB=4 Relative components correlated over all E_l intervals within each E_k interval

$$\text{Cov}(X_i, Y_j) = \sum_{k,l,l'} P_{j;l'}^{i;k,l} F_k F_{xy,l} F_{xy,l'} X_i Y_j \quad , \quad (11)$$

and

LB=5 Relative covariance matrix components

$$\text{Cov}(X_i, Y_j) = \sum_{k,k'} P_{j;k}^{i;k'} F_{xy;k,k'} X_i Y_j. \quad (12)$$

Here the X_i and Y_j are as previously defined, the F's are the uncertainty components which come directly from the uncertainty file data, and the dimensionless operator P is defined in terms of the operator S as

$$P_{j;m,n,\dots}^{i;k,\ell,\dots} \equiv S_i^k S_i^\ell \dots S_j^m S_j^n \dots, \quad (13)$$

where,

$S_i^k = 1$ when the energy E_i is in the interval E_k to E_{k+1} of an E_k energy "table."

or

$S_i^k = 0$ when the energy E_i is outside the range of E_k to E_{k+1} of an E_k energy "table."

Again, the "NC-type" sub-section is used to describe the covariance matrices in the energy ranges where the reaction type desired may be derived in terms of other evaluated reaction types in the same energy ranges. The evaluated cross section referred to here is one in which the covariance matrix is given explicitly ("NI-type") over the energy range of interest.

The "NC-type" sub-subsections are further broken down into two categories, as alluded to earlier. The first is the "derived redundant reaction types", indicated in ENDF/B-V by the flag LTY=0. Here the reaction type, MT, of a certain material, MAT (materials are designated by MAT numbers in ENDF/B), is obtained as a linear combination of other evaluated reaction types having the same MAT number but different MT values in the energy ranges given by E1 and E2 in the uncertainty file. That is

$$X_{MT}^{MAT}(E) = \sum_{i=1}^{NCI} C_i X_{MTi}^{MAT}(E), \quad (14)$$

where the C_i 's are constant over the whole energy range of E1 to E2, and NCI designates the number of "NC-type" sub-subsections of interest.

The second type of "NC-type" sub-subsection is referred to as "covariances of cross sections derived via ratio measurements", flagged in ENDF/B-V as either LTY=1,2, or 3. Cross section evaluation by means of ratio measurements is a standard method in ENDF/B and one of the main sources of cross material correlations. This relationship can be shown for the cross section X_{MT}^{MAT} derived, in the energy range E1 to E2, through the evaluation of ratio measurements of the "standard" cross section X_{MTR}^{MATR} as

$$X_{MT}^{MAT}(E) = R(E) X_{MTR}^{MATR}(E) \quad (15)$$

where $R(E)$ is the measured ratio at energy E. LTY=1 is then used in one subsection of X_{MT}^{MAT} to indicate a ratio measurement to X_{MTR}^{MATR} . LTY=2 is used to indicate a correlation between X_{MT}^{MAT} and X_{MTR}^{MATR} . LTY=3 is used in the reference materials subsection to indicate a correlation between X_{MTR}^{MATR} and X_{MT}^{MAT} .

The final type of uncertainty file to be described is file 32, the uncertainties in the resolved resonance parameters. In file 32, the data necessary for both multi- and single-level Breit-Wigner representations and the correlated uncertainties in these data are given. Covariances are given for the resonance energy, E_r , the total angular momentum of the resonance, J , the neutron width, Γ_n , the radiation width, Γ_γ , and the fission width, Γ_f . This data is then propagated through to an uncertainty in a resonance cross section. These uncertainties are then added to the uncertainties formulated from file 33, the smooth cross section covariances, to form a complete covariance matrix.

CHAPTER IV

PROCESSING ENDF/B-V UNCERTAINTY DATA
INTO MULTIGROUP FORMALISM

Processing ENDF/B-V uncertainty data is a straightforward but strict operation. The matrix operations necessary must follow certain mathematical relationships or errors are prone to occur. With this in mind, and before describing the computational procedures, a brief explanation of the various energy grids used is necessary.

The first energy grid is the cross section energy grid. This grid is, of course, associated with the energy structure on which the multigroup cross sections have been processed. The multigroup cross sections may be in any group structure desired and are not necessarily dependent upon any other grid to be described.

The second energy grid is the user energy grid. This is the energy structure on which the code user wants to have the final multigroup covariances.

A third energy structure is associated with the various energy levels on which the evaluator has expressed the uncertainties. This energy structure will be referred to as the uncertainty file energy structure or grid.

A fourth energy structure, necessary for a unified energy grid on which the cross sections (and flux) are expressed, is called the "supergrid." This grid is the union of the user grid and the uncertainty file energy grid. The supergrid is also necessary, as will be explained later, to process covariances due to ratio measurements.

The fifth and final energy grid is named the super-user grid. This grid is the union of the user energy grid and the energy boundaries of the "derived redundant reaction type" covariances; the E1's and E2's. The super-user grid is necessary, as will be explained later, to process covariances which are linear summing operations.

Another area that should be discussed before describing the covariance computational procedures is that of interpolation of the multigroup cross sections and corresponding flux. In order to use the multigroup processing algorithms, the multigroup cross sections and flux must be expressed on the supergrid. One of the most convenient methods of interpolating the multigroup cross sections on to the supergrid, and the method chosen in PUFF-II, is to energy weight the cross section and collapse (or expand) as described below

$$\bar{\sigma}_{sb} = \frac{\sum_i \sigma_{Mi} \phi_{Mi} \left(\frac{E_{sb} - E_{M,i}}{E_{M,i+1} - E_{M,i}} \right)}{\sum_i \phi_{Mi} \left(\frac{E_{sb} - E_{M,i}}{E_{M,i+1} - E_{M,i}} \right)} \quad i = 1, 2, \dots, \text{Multi} \quad (16)$$

where $\bar{\sigma}_{sb}$ is the supergrid cross section for energy group b, $\sigma_{M,i}$ is the multigroup cross section for energy group i and ϕ_{Mi} is the corresponding flux, E_{sb} is a lower energy boundary for the supergrid, $E_{M,i}$ is the energy boundaries for the ith energy group in the multigroup cross section energy grid, and Multi is the number of groups in the multigroup energy grid.

The computation of multigroup covariances from files 31 and 33 using

covariances from the "NI-type" sub-subsections is performed according to the different LB flags and are given in multigroup formalism as shown below

$$\text{LB} = 0 \quad \text{Cov}(X_i, Y_j) = \frac{\sum_{k \in i, j} F_{xy, k} \phi_{i, k} \phi_{j, k}}{\phi_i \phi_j} \quad (17)$$

$$\text{LB} = 1 \quad \text{Cov}(X_i, Y_j) = \frac{\sum_{k \in i, j} F_{xy, k} \phi_{i, k} X_{i, k} \phi_{j, k} Y_{j, k}}{\phi_i \phi_j} \quad (18)$$

$$\text{LB} = 2 \quad \text{Cov}(X_i, Y_j) = \frac{\left(\sum_{k \in i} F_{xy, k} \phi_{i, k} X_{i, k} \right) \left(\sum_{k' \in j} F_{xy, k'} \phi_{j, k'} Y_{j, k'} \right)}{\phi_i \phi_j} \quad (19)$$

$$\text{LB} = 3 \quad \text{Cov}(X_i, Y_j) = \frac{\left(\sum_{k \in i} F_{x, k} \phi_{i, k} X_{i, k} \right) \left(\sum_{l \in j} F_{y, l} \phi_{j, l} Y_{j, l} \right)}{\phi_i \phi_j} \quad (20)$$

$$\text{LB} = 4 \quad \text{Cov}(X_i, Y_j) = \frac{\sum_{k \in i, j} F_k \left(\sum_{l \in i} F_{xy, l} \phi_{i, l} X_{i, l} \right) \left(\sum_{l' \in j} F_{xy, l'} \phi_{j, l'} Y_{j, l'} \right)}{\phi_i \phi_j} \quad (21)$$

and

$$\text{LB} = 5 \quad \text{Cov}(X_i, Y_j) = \frac{\sum_{k \in i} \sum_{k' \in j} F_{xy; k, k'} \phi_{i, k} X_{i, k} \phi_{j, k'} Y_{j, k'}}{\phi_i \phi_j} \quad (22)$$

The derivation of Eqs. (17-21) is fully described in Ref. 13. Equation (22) is obvious from the definition of covariance given earlier and from equation (12). The notation used here is:

$\text{Cov}(X_j, Y_j)$ = multigroup covariance between reaction X group i and reaction Y, group j.

ϕ_i = multigroup flux per super-user group (or supergrid) i.

$X_{i,k}$ = multigroup cross section for reaction X for a super-grid (i,k) constructed from the union of energy boundaries of the uncertainty file and those from the the user grid. $\phi_{i,k}$ is the flux for this group.

F's = components of covariance taken directly from the uncertainty file.

The "NI-type" sub-subsections are the basis for construction of the "NC-type" sub-subsections and are therefore by necessity processed first. The use of the "NI-type" sub-subsections for the production of the "NC-type" derived redundant cross section covariances is demonstrated as follows: let X be the cross section of interest expressed as a linear combination of n evaluated cross sections, Y, in the energy range from E1 to E2

$$X_i = \sum_{M=1}^n Y_{M,i} K_M \quad (23)$$

where i is the energy group index and K_M 's are constant values, usually +1 or -1. Then, to express the uncertainty in X we have

$$dX_i = \sum_{M=1}^n dY_{M,i} K_M, \quad (24)$$

where dX_i represents $(X_i - \hat{X}_i)$, the uncertainty in X_i ; similarly for $Y_{M,i}$. To find the covariance of X_i , Eq. (24) is squared, changing the second index of i to j (where i and j represent the same group structure) and then expectation values are taken

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$$\langle dX_i, dX_j \rangle = \sum_{M=1}^n \sum_{M'=1}^n K_M K_{M'} \langle dY_{M,i}, dY_{M',j} \rangle . \quad (25)$$

The diamond bracketed items in Eq. (25) are the covariances and may be more conveniently expressed as

$$\text{Cov}(X_i, X_j) = \sum_{M=1}^n \sum_{M'=1}^n K_M K_{M'} \text{Cov}(Y_{M,i}, Y_{M',j}) . \quad (26)$$

Similarly, taking the expected value of the product of X_i and the $Y_{M,i}$'s gives

$$\langle dX_i, dY_{M,j} \rangle = \sum_{M'=1}^n K_{M'} \langle dY_{M',i}, dY_{M,j} \rangle \quad M = 1, 2, \dots, n \quad (27)$$

or

$$\text{Cov}(X_i, Y_{M,j}) = \sum_{M'=1}^n K_{M'} \text{Cov}(Y_{M',i}, Y_{M,j}) \quad M = 1, 2, \dots, n . \quad (28)$$

Equation (26) is the mathematical expression of the processing procedure to produce the multigroup covariances for the derived redundant cross section covariances. Equation (28) is the mathematical expression of the process to produce the multigroup covariances between the reaction of interest, X_i , and each of the reaction types, $Y_{M,i}$'s, from which X_i is evaluated.

Each of the derived redundant cross section covariances are derived for an explicit energy range, E1 to E2. Outside of this energy range the derived covariance matrix is zero. In effect, this requires that the multigroup covariances be produced on an energy grid that not only contains the desired energy boundaries of the user, but must also contain the E1's and E2's. This grid was defined as the super-user grid.

If the derived energy range points are not present numerical errors occur. This may best be explained pictorially as is shown in this partial covariance matrix

			Eu_{j+1}	
0		0	ϕ_z	
- - -	- - -	- - -	$E2$	ϕ_j
0		A	ϕ_y	
			Eu_j	
ϕ_w	$E1$	ϕ_x		
Eu_i	ϕ_i	Eu_{i+1}		

where Eu represents the user-energy boundaries for group i and j , $E1$ and $E2$ are as explained before, ϕ_w is the super-user grid flux, ϕ_i is the sum of ϕ_w and ϕ_x , likewise for ϕ_j , and A is the covariance element produced from Eq. (26) or (28) (all other elements are zero). If the derived redundant cross section energy boundaries were not present (in the energy grid scheme), the covariance element for user covariance group i,j would simply be A , which is incorrect. The correct covariance value for user group i,j is given in general as

$$\text{Cov}(X_i, Y_j) = \frac{\phi_x A \phi_y}{(\phi_w + \phi_x)(\phi_y + \phi_z)}, \quad (29)$$

where the covariance element A is flux weighted and collapsed to the user covariance group i,j .

In the second type of "NC-type" sub-subsection, covariances may be wholly or partially derived from measurements made on the relationship one cross section of a certain material has to a reference cross section of another material. This is known as a ratio measurement. To illustrate

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this, let X_i be the cross section of interest and Z_i be the cross section from which X_i is evaluated, and then

$$X_i = R_i Z_i, \quad (30)$$

where R_i is the measured ratio of X_i to Z_i at energy group i . Then the uncertainty in X_i may be determined with use of the chain rule as

$$dX_i = dR_i Z_i + R_i dZ_i \quad (31)$$

With this, the covariance of X may be determined as

$$\begin{aligned} \langle dX_i dX_j \rangle &= \langle dR_i dR_j \rangle Z_i Z_j + 2R_i Z_j \langle dR_i dZ_j \rangle \\ &\quad + \langle dZ_i dZ_j \rangle R_i R_j \end{aligned} \quad (32)$$

Rearrangement of Eq. (32) gives

$$\begin{aligned} \frac{\langle dX_i dX_j \rangle}{R_i R_j Z_i Z_j} &= \frac{\langle dR_i dR_j \rangle}{R_i R_j} + \frac{2\langle dR_i dZ_j \rangle}{R_j Z_i} \\ &\quad + \frac{\langle dZ_i dZ_j \rangle}{Z_i Z_j} \end{aligned} \quad (33)$$

R and Z (or R and any other cross section) are assumed to be uncorrelated (i.e., $\langle dR_i dZ_j \rangle = 0$) and the three remaining terms follow from the definition of a relative covariance matrix; thus

$$\text{Rel. Cov}(X_i, X_j) = \text{Rel. Cov}(R_i, R_j) + \text{Rel. Cov}(Z_i, Z_j) \quad (34)$$

Also, from Eq. (31) a covariance may be derived between X and Z , namely,

$$\text{Rel. Cov}(X_i, Z_j) = \text{Rel. Cov}(Z_i, Z_j) \quad (35)$$

Other relationships¹² exist due to ratio measurements, but Eqs. (34) and (35) represent the basic mathematical expressions for processing covariances due to ratio measurements. Equation (34) states that the relative covariance of X is determined by adding the relative covariance of the ratio, R, to the relative covariance of the reference cross section, Z. The uncertainties in R are given in "NI-type" sub-subsections in the subsection given for X. The uncertainties for the reference cross section are in the "NI-type" sub-subsections of Z.

Normal processing procedures of summing two collapsed multigroup covariance matrices cannot be followed in processing ratio measurements. This is because forming a collapsed multigroup covariance for the ratio, R, requires having the covariance matrix for X, which is the desired result. Instead, the covariance matrices of R and Z must be summed while in the supergrid structure. The covariance matrix of X is then collapsed to the user group structure.

This concludes a description of the processing procedures necessary to form multigroup covariances from files 31 or 33. The multigroup covariances due to the uncertainties in the resolved resonance parameters, file 32, must now be formed and added to the smooth cross section covariances of file 33.

The processing of the resolved resonance parameter uncertainties requires an uncertainty analysis approach. The basic equation is the single-level Breit-Wigner formula given as

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$$\sigma_i = \frac{\pi}{k^2} g \frac{\Gamma_n \Gamma_i}{(E-E_r)^2 + (1/4)\Gamma_T^2}, \quad (36)$$

where Γ_n is the neutron width, Γ_i is the radiation or fission width (i.e., $i = \gamma$ or f), E_r is the resonance energy, and Γ_T is the resonance total width given by

$$\Gamma_T = \Gamma_n + \Gamma_f + \Gamma_\gamma. \quad (37)$$

σ_i is the capture or fission cross section, g is the statistical spin factor given as

$$g = \frac{2J+1}{2(2I+1)}, \quad (38)$$

where J is the spin of compound nucleus, or the total angular momentum and I is the spin of the target nucleus. K is given in ENDF/B as

$$K = (2.196771 \times 10^{-3}) \left(\frac{AWRI}{AWRI+1.0} \right) \sqrt{E_r} \quad (39)$$

where $AWRI$ is the ratio of the mass of a particular isotope to that of a neutron. Only the single-level Breit-Wigner formulae is used because no data have been cast in multi-level form to date.

Equation (36) is then integrated from $-\infty$ to $+\infty$ to obtain a representation for the resonance area given as

$$A_i = \frac{2\pi^2}{K^2} g \frac{\Gamma_n \Gamma_i}{\Gamma_T} \quad (40)$$

where A_i is the resonance area in barns-eV for capture or fission reactions (i.e., $i = \gamma$ or f). Sensitivities are then taken with respect to each parameter for which uncertainties are expressed (see Chapter III).

For example, the sensitivity of A_i to Γ_n may be shown as

$$\frac{\partial A_i}{\partial \Gamma_n} = \frac{2\pi^2}{k^2} g \frac{\Gamma_i}{\Gamma_T} (1 - \Gamma_n/\Gamma_T) . \quad (41)$$

Similar expressions are derived for each of the other parameters which have uncertainties in file 32 and a matrix is formed which looks like

$$H \equiv \begin{bmatrix} \frac{\partial A_Y}{\partial \Gamma_Y} & \frac{\partial A_Y}{\partial \Gamma_n} & \frac{\partial A_Y}{\partial \Gamma_f} & \frac{\partial A_Y}{\partial J} & \frac{\partial A_Y}{\partial E_r} \\ \frac{\partial A_f}{\partial \Gamma_Y} & \frac{\partial A_f}{\partial \Gamma_n} & \frac{\partial A_f}{\partial \Gamma_f} & \frac{\partial A_f}{\partial J} & \frac{\partial A_f}{\partial E_r} \end{bmatrix} . \quad (42)$$

The covariance matrix of the resolved resonance parameters is defined as

$$D = \begin{bmatrix} DG^2 & & & & \\ DNDG & DN^2 & & & \\ DGDF & DNDF & DF^2 & & \\ DJDG & DJDN & DJDF & DJ^2 & \\ 0 & 0 & 0 & 0 & DE^2 \end{bmatrix} , \quad (43)$$

where

DG^2 is the variance of Γ_Y , [ev^2],

DN^2 is the variance of Γ_n , [ev^2],

DF^2 is the variance of Γ_f , [ev^2],

DJ^2 is the variance of J ,

DE^2 is the variance of E_r [ev^2],

$DNDG$ is the covariance of Γ_n and Γ_Y [ev^2],

$DGDF$ is the covariance of Γ_Y and Γ_f [ev^2],

$DNDF$ is the covariance of Γ_n and Γ_f [ev^2],

$DJDG$ is the covariance of J and Γ_Y [ev],

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DJDN is the covariance of J and Γ_n [ev],
and DJDF is the covariance of J and Γ_f [ev] .

The covariance of E_r and the other parameters is very small, in practice, and therefore set to zero.¹² Also, the D matrix is symmetric (i.e., DNDG = DGDN, etc.).

A covariance matrix for the resonance area is produced by folding the sensitivity matrix, H, with the covariance matrix, D, and is given as

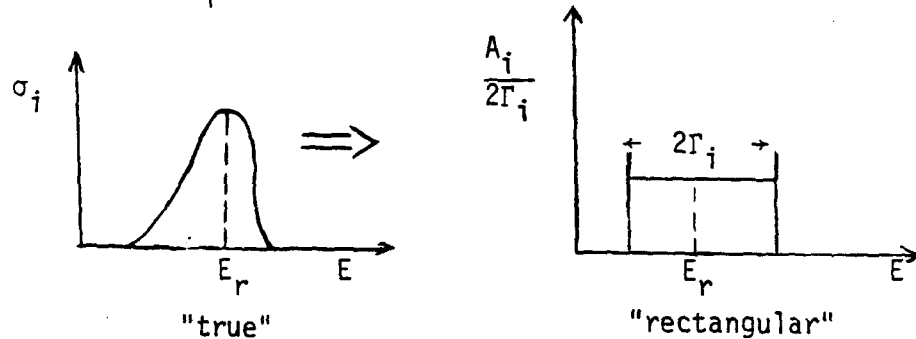
$$\langle dAdA^T \rangle = \begin{bmatrix} \langle dA_Y dA_Y \rangle & \langle dA_Y dA_f \rangle \\ \langle dA_f dA_Y \rangle & \langle dA_f dA_f \rangle \end{bmatrix}. \quad (44)$$

As shown in Eq. (44), not only is a covariance matrix formed for the capture and fission area, but a cross reaction covariance is given between capture and fission. The matrix shown in equation (44) is also symmetric (i.e., $\langle dA_f dA_Y \rangle = \langle dA_Y dA_f \rangle$).

The matrix described in Eq. (44) is summed for each resonance, ℓ -state (neutron angular momentum quantum number), and isotope within each super-user grid (or supergrid) K (if more than one isotope exists, the abundance is used to weight the contribution). This expression is then divided by the square of the width of energy group K (i.e., $(E_{k+1} - E_k)^2$) to form the cross section covariances due to the resolved resonance parameters. These covariances are then summed to the proper absolute covariances of the smooth cross sections formed from file 33.

The approach described above assumes a constant or flat weighting for each resonance within energy group k. A second approach, suggested by Y. Yeivin and J. J. Wagschal¹⁴ is to give each resonance an 1/E weighting. In this approach, the model for averaging a resonance cross

section, σ_i , consists of replacing the "true" cross section by a "rectangular" one of width $2\Gamma_i$, where $i = \gamma$ or f .



Letting E_{k+1} and E_k be the upper and lower k th group boundaries, the average cross section would be given by

$$\bar{\sigma}_i = \frac{\int_{E_k}^{E_{k+1}} \sigma_i(E) \frac{dE}{E}}{\int_{E_k}^{E_{k+1}} \frac{dE}{E}} \quad (45)$$

$$\approx \frac{A_i}{2\Gamma_i} \ln \left(\frac{E_r + \Gamma_i}{E_r - \Gamma_i} \right) / \ln \left(\frac{E_{k+1}}{E_k} \right) \quad i = \gamma \text{ or } f. \quad (46)$$

Sensitivities are formed from Eq. (46) in the same fashion as described in the first approach and folded with the covariance matrix, D , Eq. (43). This time the covariance matrix of the resonance cross section is formed directly. The rest of the processing is the same as for the constant weighting approach. Both processing modes are allowed in PUFF-II.

Several assumptions have been made in processing the resolved resonance data. One of the more important assumptions is that no uncertainties are due to self-shielding. Normally, self-shielding is accounted for by Bonderinko f -factors¹⁵, which are functions that relate cross section behavior to temperature and material compositions. Inclusion for these f -factors would require not only some very complicated

analysis scheme, but would force the covariance calculations to become problem-dependent, which is not the intent for the processor.

Other assumptions are (1) only Breit-Weigner resonance representation (and of course the assumptions of a Breit-Weigner representation such as widely spaced resonances) are applicable, and (2) the resonance area is assumed to lie fully within the energy group k .

Using the procedures described above, the ENDF/B-V uncertainty data may be processed into multigroup covariances. However, due to situations which arise in the "NC-type" sub-subsections, the covariances are produced on an energy grid associated with either the super-user grid or super-grid. The matrices must then be collapsed to the user grid as described by Eq. (29). Finally, the collapsed matrices are prepared for output which usually consists of a COVERX file and correlation matrices.

CHAPTER V

VERIFICATION OF THE PUFF-II CODE

The objective in developing the PUFF-II code -- namely, to process ENDF/B-V uncertainty data into multigroup covariance matrices -- precludes "easy" evaluation and verification of the code because of the following two reasons. First, standard computational benchmark problems with known solutions, which could be solved by PUFF-II to check if the code is working properly, simply do not exist. Secondly, other codes which perform the same tasks as PUFF-II and, therefore, could be used to produce results for comparison with PUFF-II results, simply do not exist. In other words, standard techniques for verification of a newly developed code are not possible in this work.

However, it is possible to compare some PUFF-II results with results of hand calculations. This was done for the covariance of the Aluminum total elastic scattering cross section to the total inelastic scattering cross section. The hand calculated result and the PUFF-II result were identical.

It is also possible to evaluate LB=3 and LB=5 processing from the standpoint of internal consistency. Specifically, uncertainty files in LB=3 format, where E_k and E_l energy intervals (see Chapter III, Eq. 10) are the same, were converted to LB=5 and then processed using PUFF-II. The results from both formats were compared and shown to be identical.

Finally ENDF/B-V results obtained with PUFF-II were compared with ENDF/B-IV results obtained with the old PUFF code. Differences between the two results should, of course, exist because the basic input data is different for the two cases. However, the two results should be at least

similar in appearance. This similarity is demonstrated in Figs. 1 and 2 which show a six group representation of the correlation matrix for the ^{239}Pu fission cross section based on ENDF/B-V and ENDF/B-IV, respectively. Note that the version V result is less correlated in the low energy range than the version IV result. In particular, version V exhibits little or no off-diagonal correlation in the low energy range while version IV's off-diagonal low energy correlation ranges from 27% to 50%. Also, the standard deviation of the version V ^{239}Pu fission cross section is $\sim 4\%$ higher in energy group 1 while it is $\sim 2\%$ lower in energy group 6 than the version IV results. The differences in the intermediate energy ranges are less significant than those of the extremes.

Some of the discrepancy in the standard deviations presented in Fig. 1 and 2 is due to the use of different weighting spectrums. Also, the discrepancy in the degree of correlation in the low energy range is due to the fact that the version IV result assumed a long range correlation (i.e., a correlation over a large energy range) at low energy whereas in the ENDF/B-V ^{239}Pu (n,f) uncertainty file, no such assumption was made.

In summary, the verification checks described in this chapter and the results presented in the next chapter, which appear quite reasonable from a physical point of view, lead us to conclude that the new code, PUFF-II, works properly.

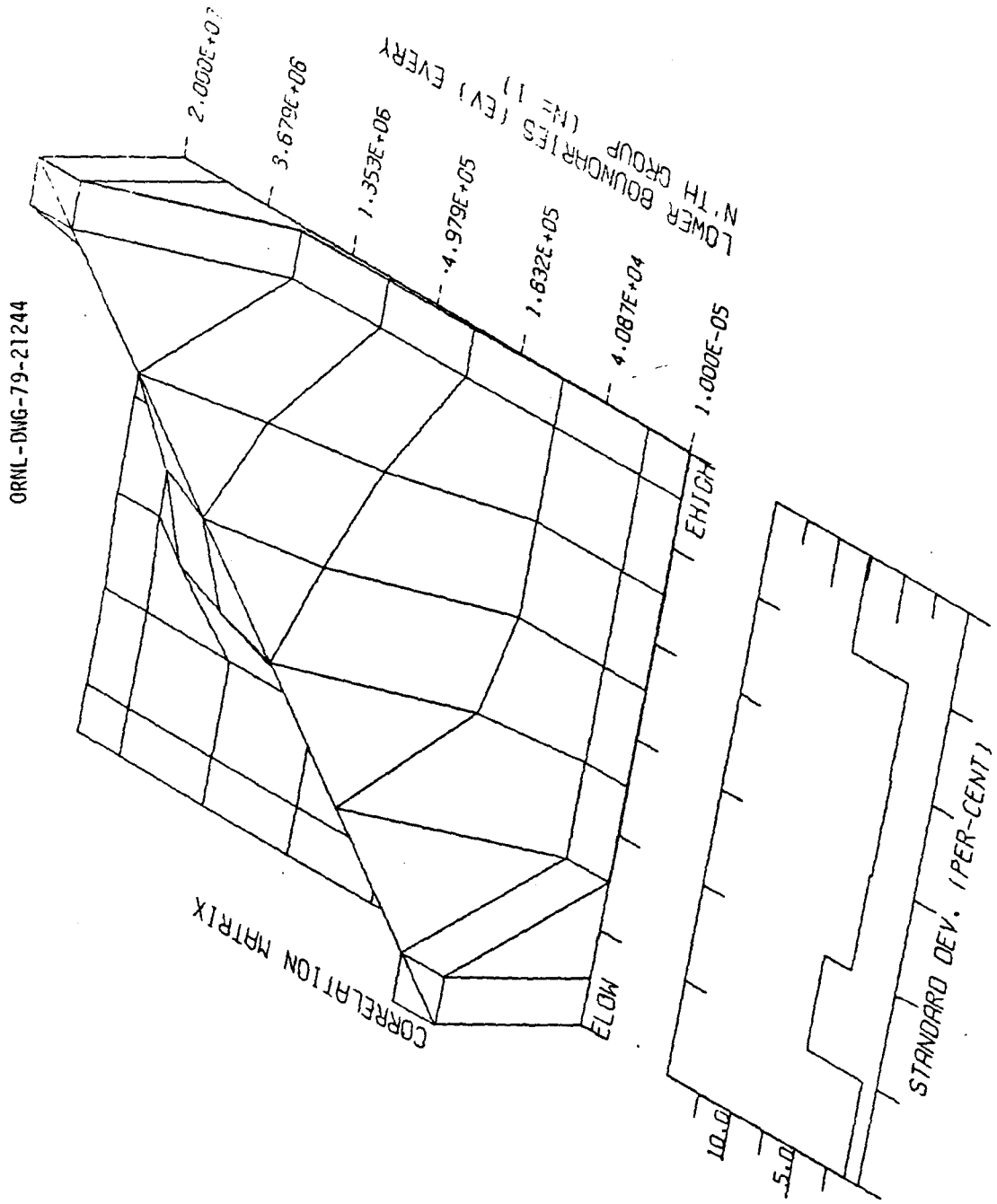


Fig. 1. Standard Deviation and Correlation Matrix of the ²³⁹Pu(n,f) Cross Sections -- ENDF/B-V

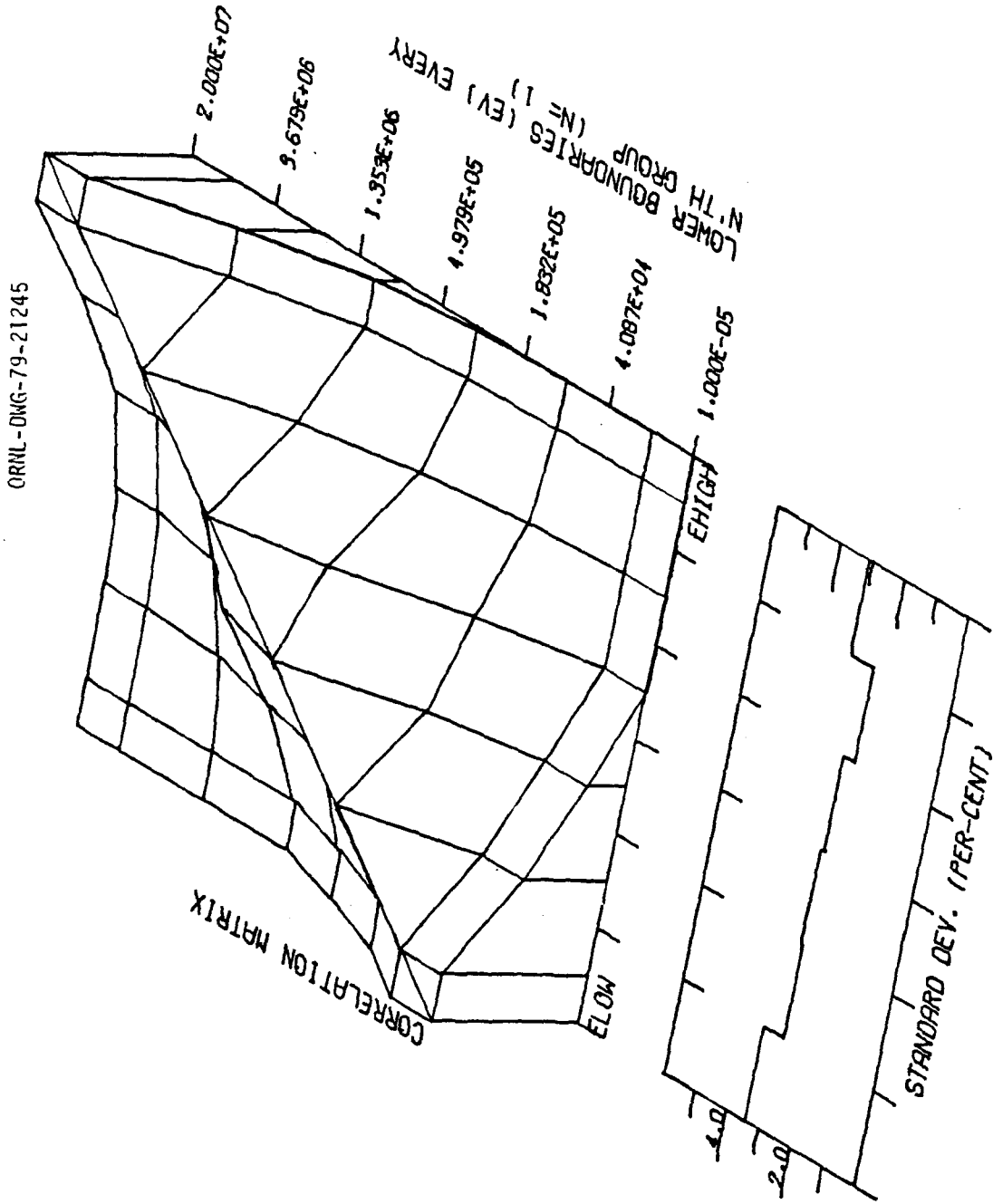


Fig. 2. Standard Deviation and Correlation Matrix of the ²³⁹Pu(n,f) Cross Sections -- ENDF/B-IV

CHAPTER VI

RESULTS

One of the most illustrative ways of demonstrating the results of PUFF-II is by plotting the correlation matrices. These plots are produced by inputting the COVERX file into a program called PLTCOR, which was developed by Francis Perey and Jim Drischler. In these plots, the energy boundaries of the reaction (or reactions) of interest form the "X and Y" dimensions and the correlation coefficients are plotted in the "Z" direction. Also produced on the plots are the relative standard deviations for a correlation matrix of a specific material and reaction relative to itself (i.e., not for a cross material or cross reaction).

An illustration of this plotting and of the 52 group covariance matrix library¹⁶ produced by PUFF-II is shown in Fig. 3. Fig. 3 is a correlation matrix plot for B-10 (MAT number 1305) (n, α) reaction (MT number 107). Note that it is fully correlated from 1.000×10^{-5} ev to about 6.738×10^4 ev. From 6.738×10^4 to about 1.353×10^6 ev the off-diagonal elements are between 0 and 1. From $\sim 1.353 \times 10^6$ ev to higher energies, the uncertainty in the B-10 (n, α) reaction is zero in ENDF/B-V uncertainty file 33. Since, in ENDF/B-V, the B-10 (n, α) cross section is given over the full energy range (1.0×10^{-5} ev to 2.0×10^7 ev) and is non-zero,¹⁸ it is highly unlikely that there is no uncertainty in the cross section above 1.353×10^6 ev. In other words, the covariance of B-10 (n, α) is incomplete, either because the uncertainty in this high ev region is difficult to determine or the evaluator was unsure of how to express the uncertainty.

Also note that the relative standard deviation indicates that the

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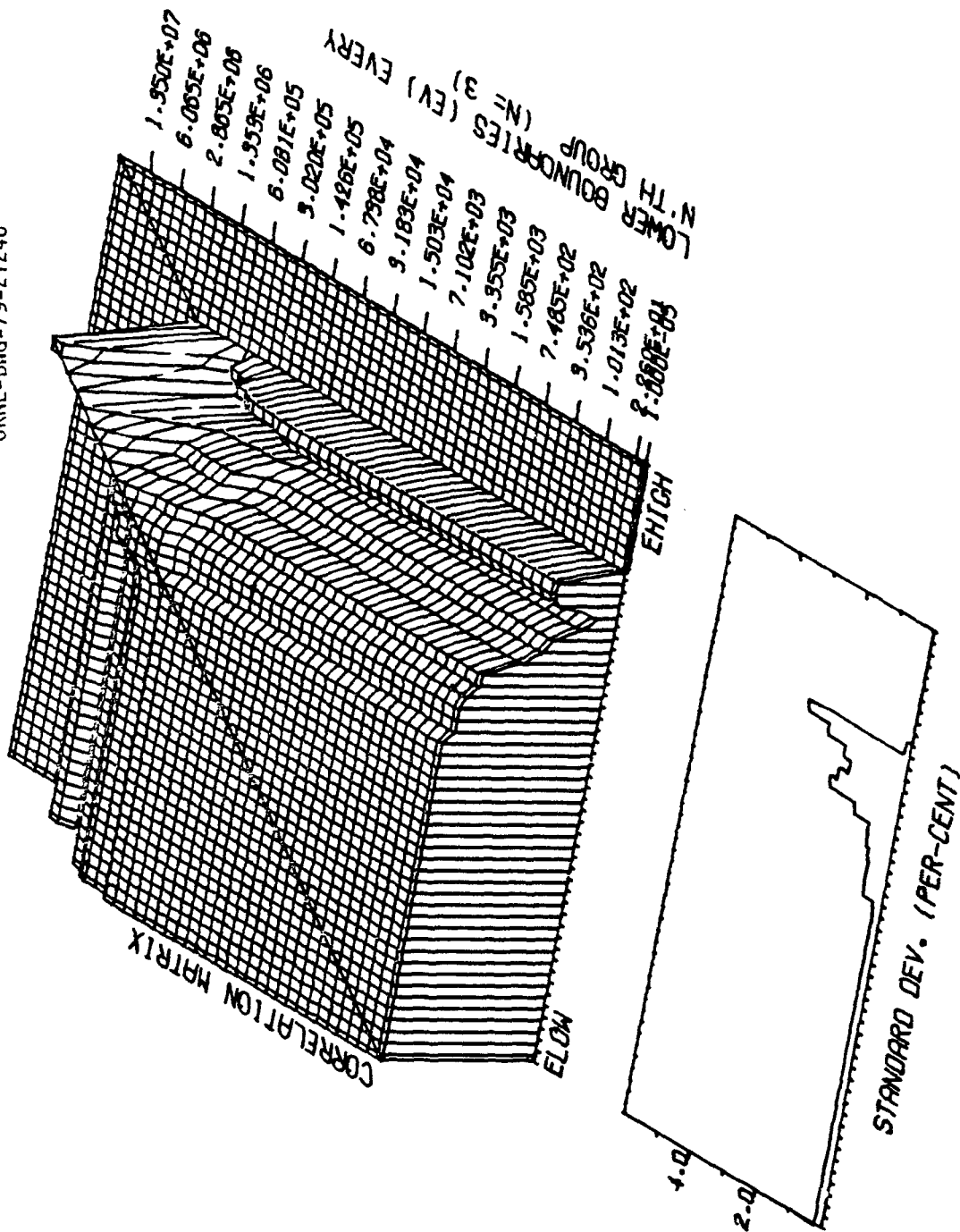


Fig. 3. Standard Deviation and Correlation Matrix of the $^{10}B(n,\alpha)$ Cross Section

cross section is fairly well known (less than 1% uncertainty) from 1.0×10^{-5} ev to about 6.738×10^4 ev and is known to within 4% (relative standard deviation) for energies greater than 6.738×10^4 ev but less than 1.353×10^6 ev.

Figs. 4 and 5 represent the correlation matrix for Fe-56 (MAT number 1326) capture cross section (MT number 102) with and without the resolved resonance uncertainty data, respectively. As can be seen, the addition of the resolved resonance uncertainty increases the relative standard deviation in the resolved resonance region. This also causes the off-diagonal elements not to be fully correlated (see equation 5.2). Also note that the relative standard deviation is off the chart in the Mev region. This merely indicates a relative standard deviation greater than 30%.

Fig. 6 is an illustration of a reaction which has been partially derived from ratio measurements; in particular, the capture covariance of U-238 (MAT number 1398). The U-238 capture cross section is derived via ratio measurements from B-10 (n, α) in the energy range of 4.0×10^3 ev to 2.0×10^4 ev. Also note the blank area of the U-238 capture covariance. In this case the uncertainty has been set to zero in the ENDF/B-V uncertainty file and referenced as to where this missing data may be found.¹⁹

Fig. 7 illustrates the correlation between U-238 capture (rows) and B-10 (n, α) (columns). Note here that while the U-238 capture uncertainty is for a fixed energy interval (4.0×10^3 ev to 2.0×10^4 ev), the uncertainty in B-10 (n, α) is for the entire energy range (1.0×10^{-5} ev to 1.964×10^7 ev).

Figs. 8 and 9 illustrate two $\bar{\nu}$ relationships. Fig. 8 is the correlation matrix for U-238 prompt $\bar{\nu}$ (MT number 456). Fig. 9 is the correlation matrix between U-238 prompt $\bar{\nu}$ and Pu-240 (MAT number 1380) $\bar{\nu}$ (MT number 452). This is an explicit cross material relationship given in ENDF/B-V.

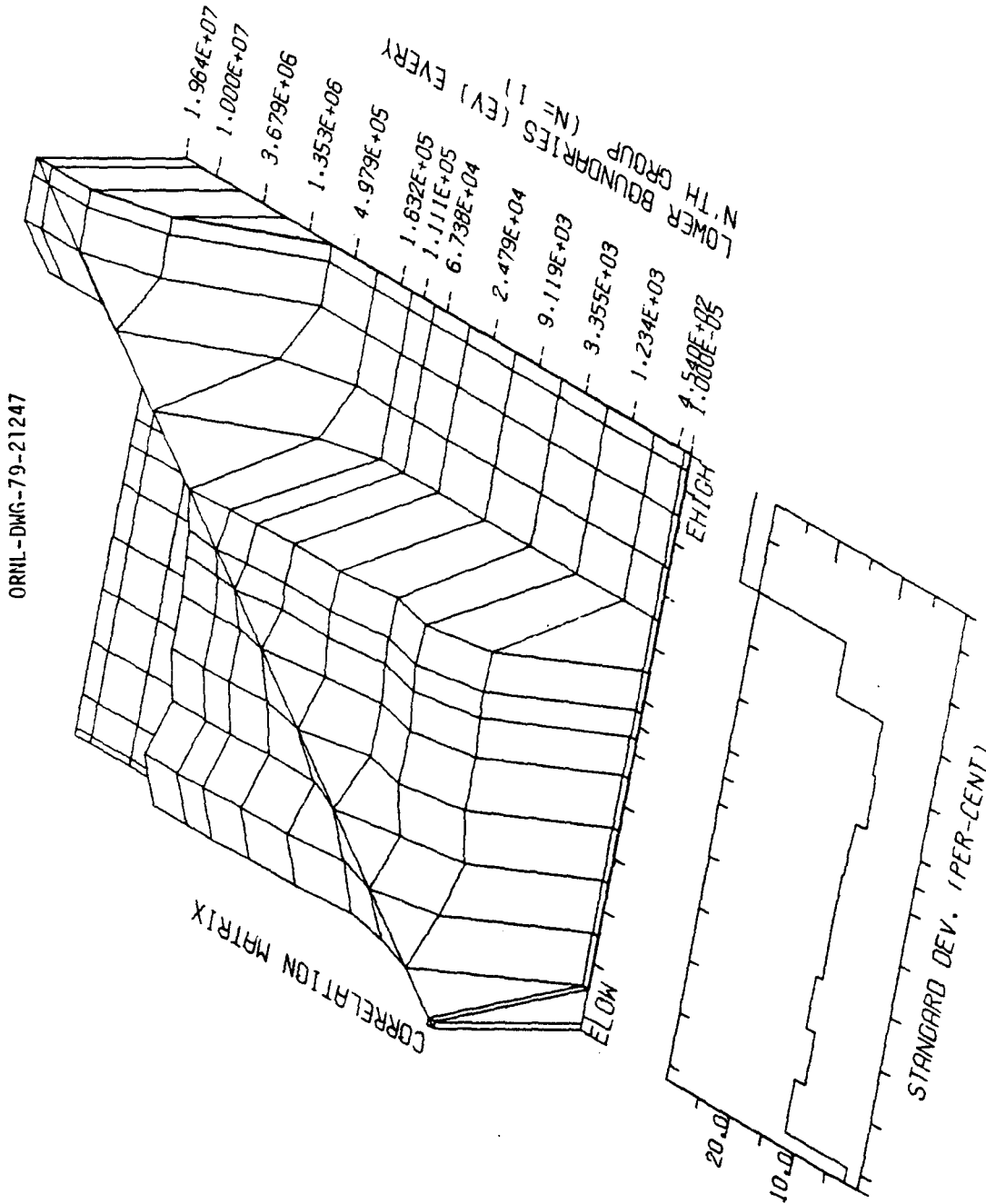


Fig. 4. Standard Deviation and Correlation Matrix of the $^{56}\text{Fe}(n,\gamma)$ Cross Section with Resonance Data

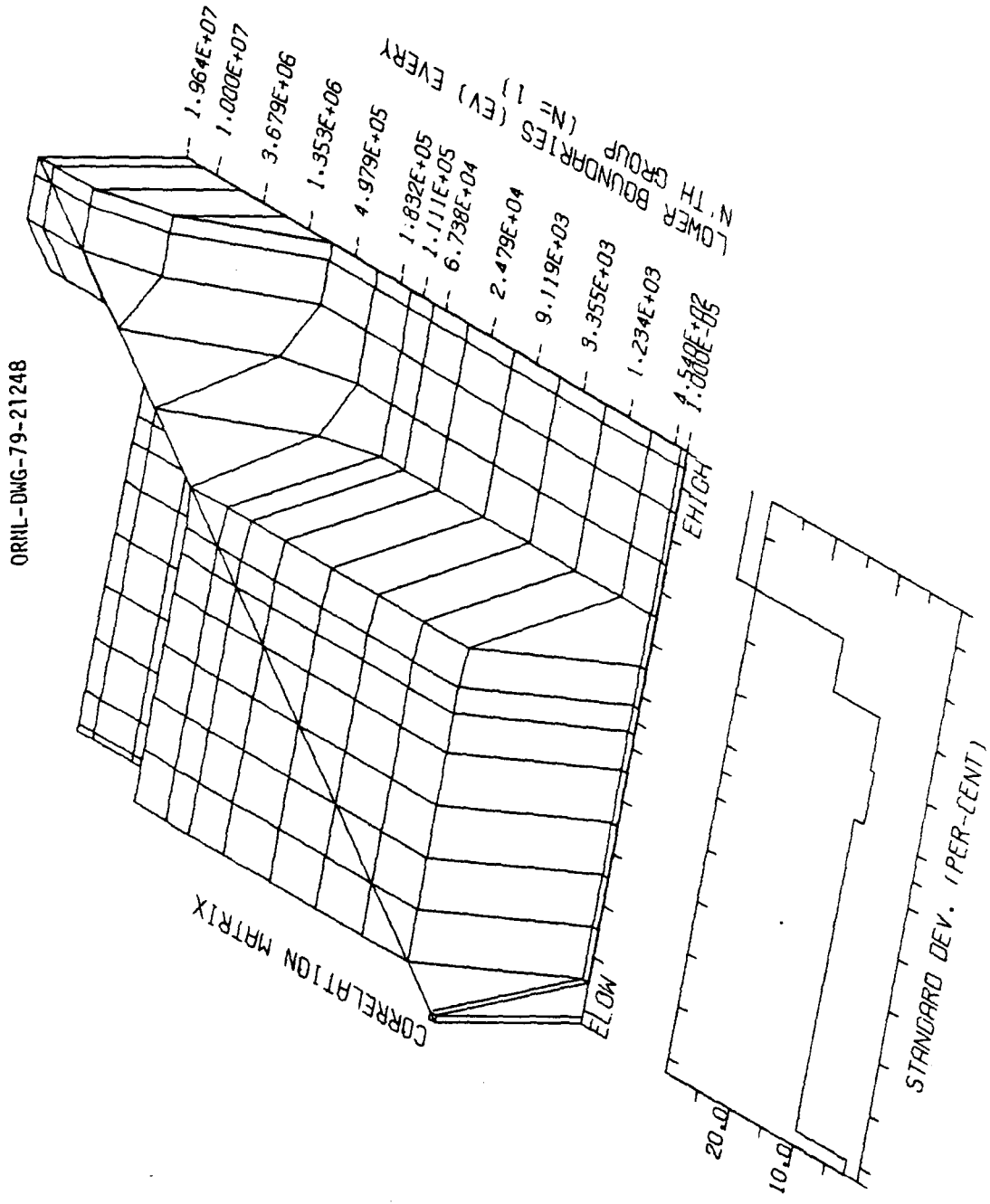


Fig. 5. Standard Deviation and Correlation Matrix of the ⁵⁶Fe(n,γ) Cross Section without Resonance Data

ORNL-DWG-79-21249

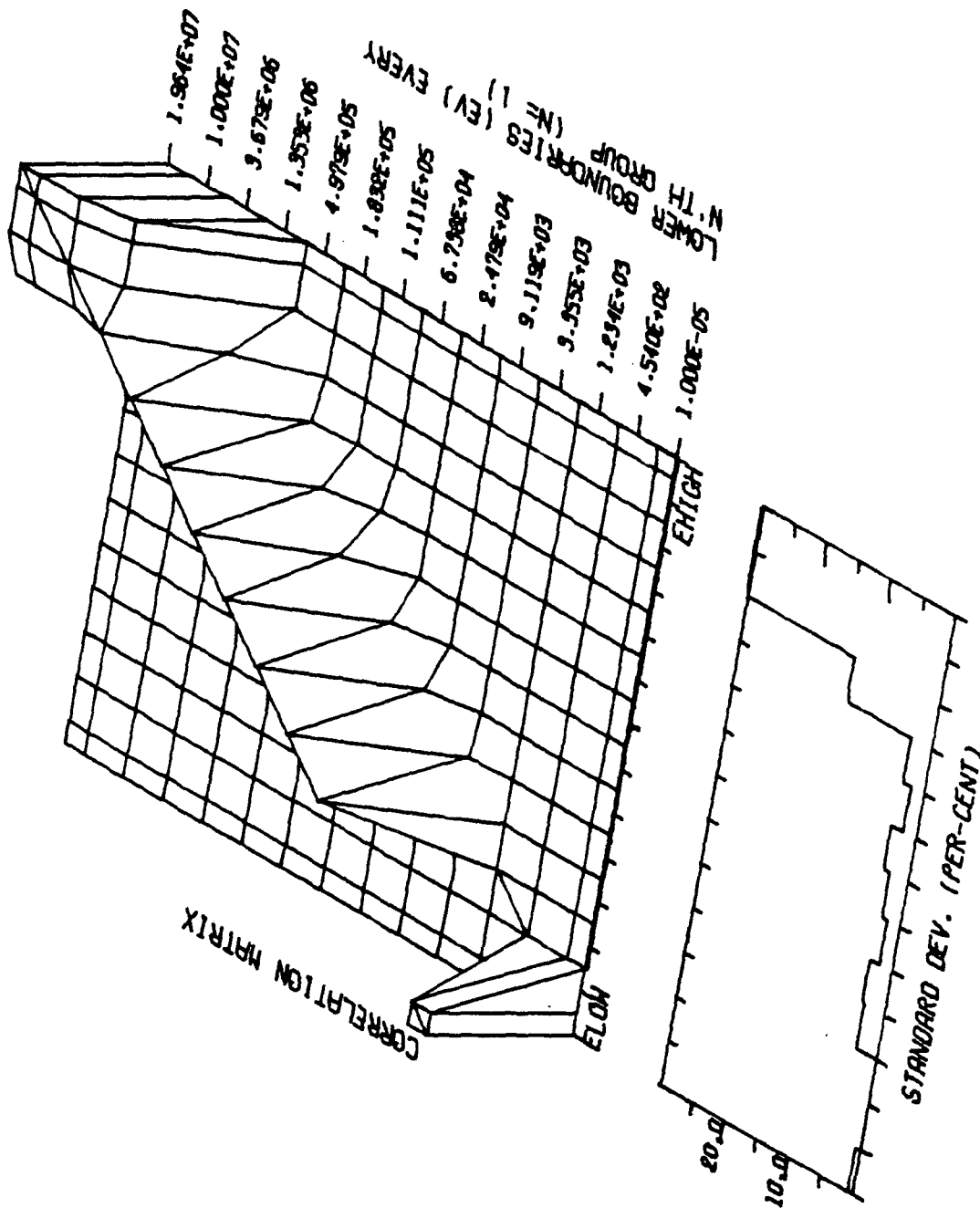


Fig. 6. Standard Deviation and Correlation Matrix of the $^{238}\text{U}(n,\gamma)$ Cross Section

ORNL-DWG-79-21250

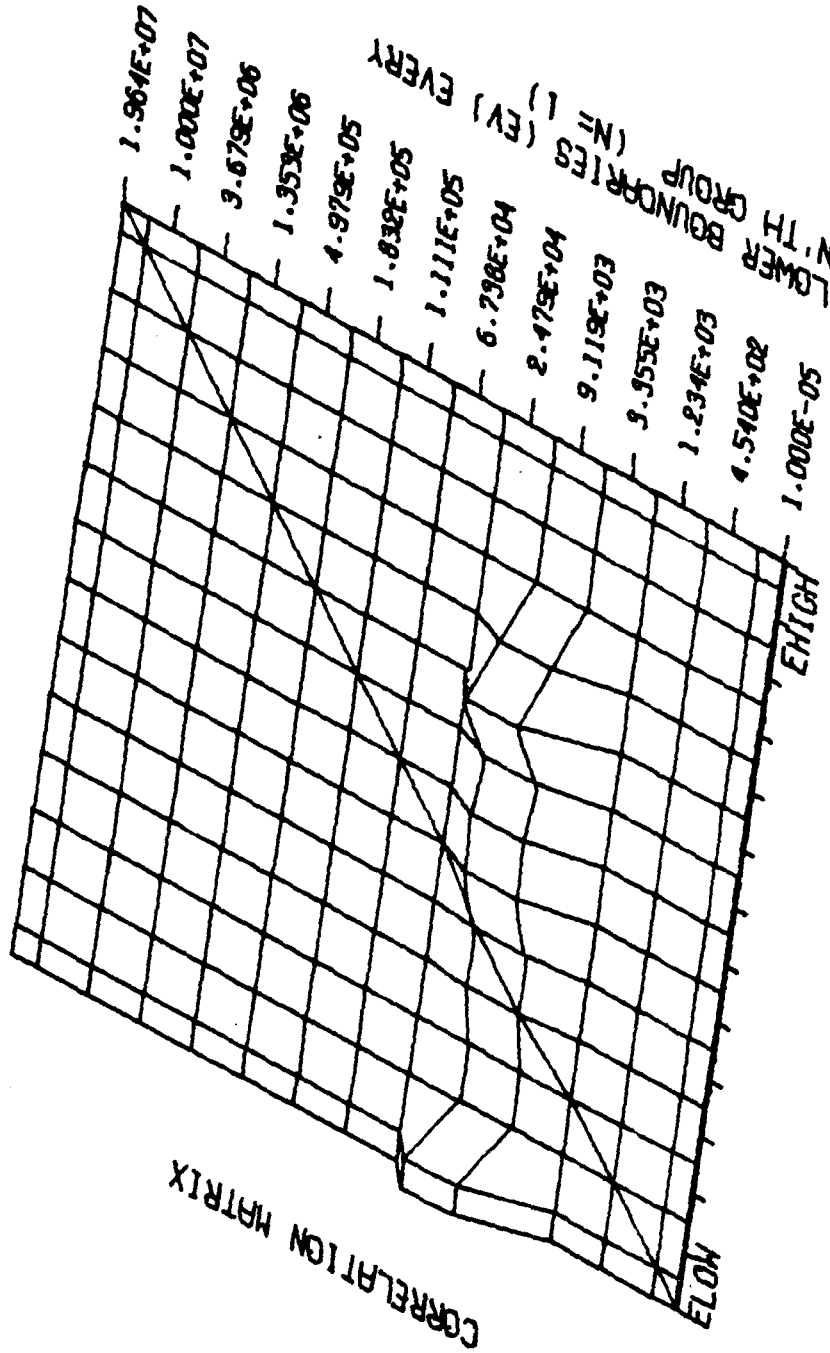


Fig. 7. Correlation Matrix Between $^{238}\text{U}(n,\gamma)$ and $^{10}\text{B}(n,\alpha)$ Cross Sections
(row = $^{238}\text{U}(n,\gamma)$)

ORNL-DWG-79-21251

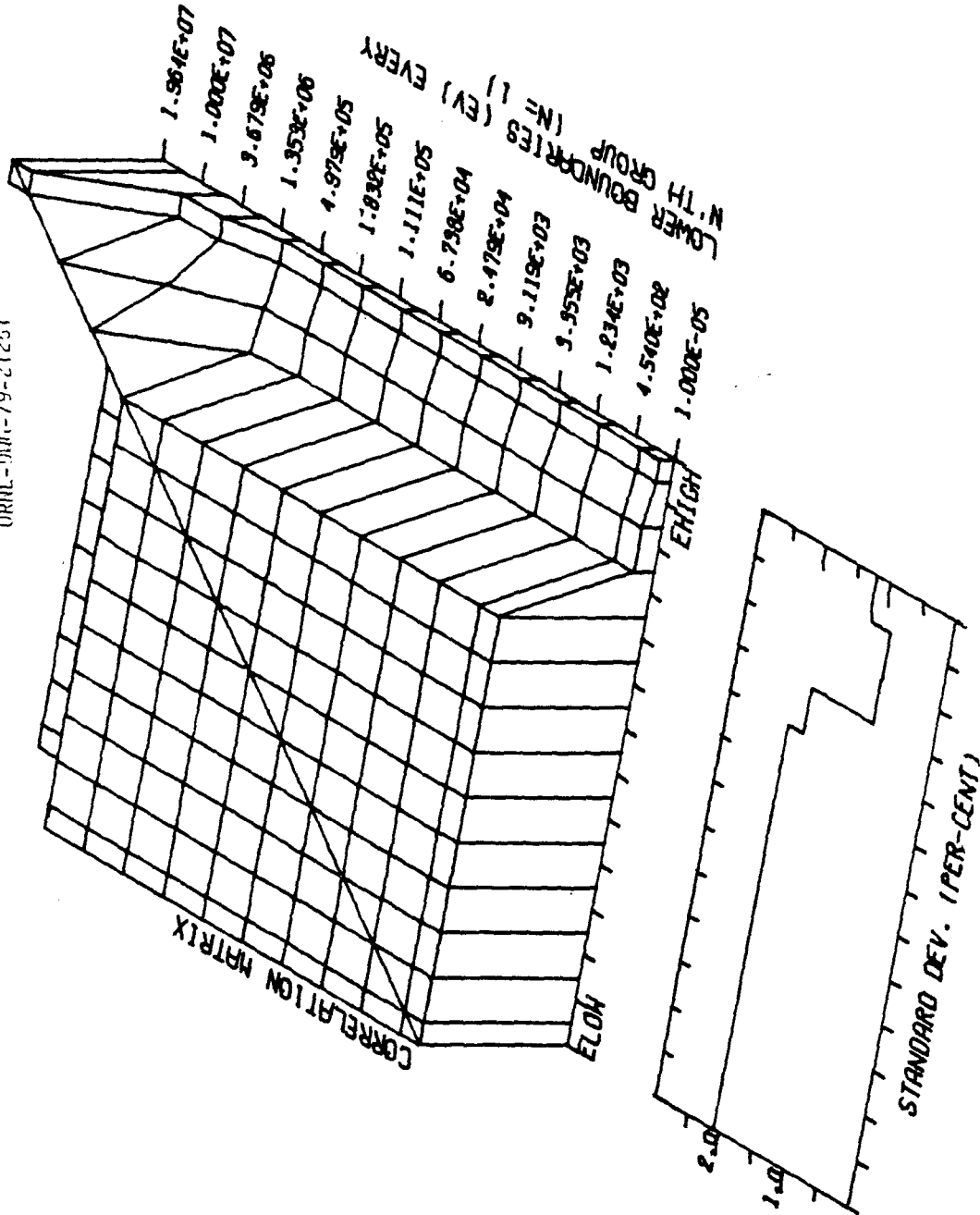


Fig. 8. Standard Deviation and Correlation Matrix of the ²³⁸U prompt ν

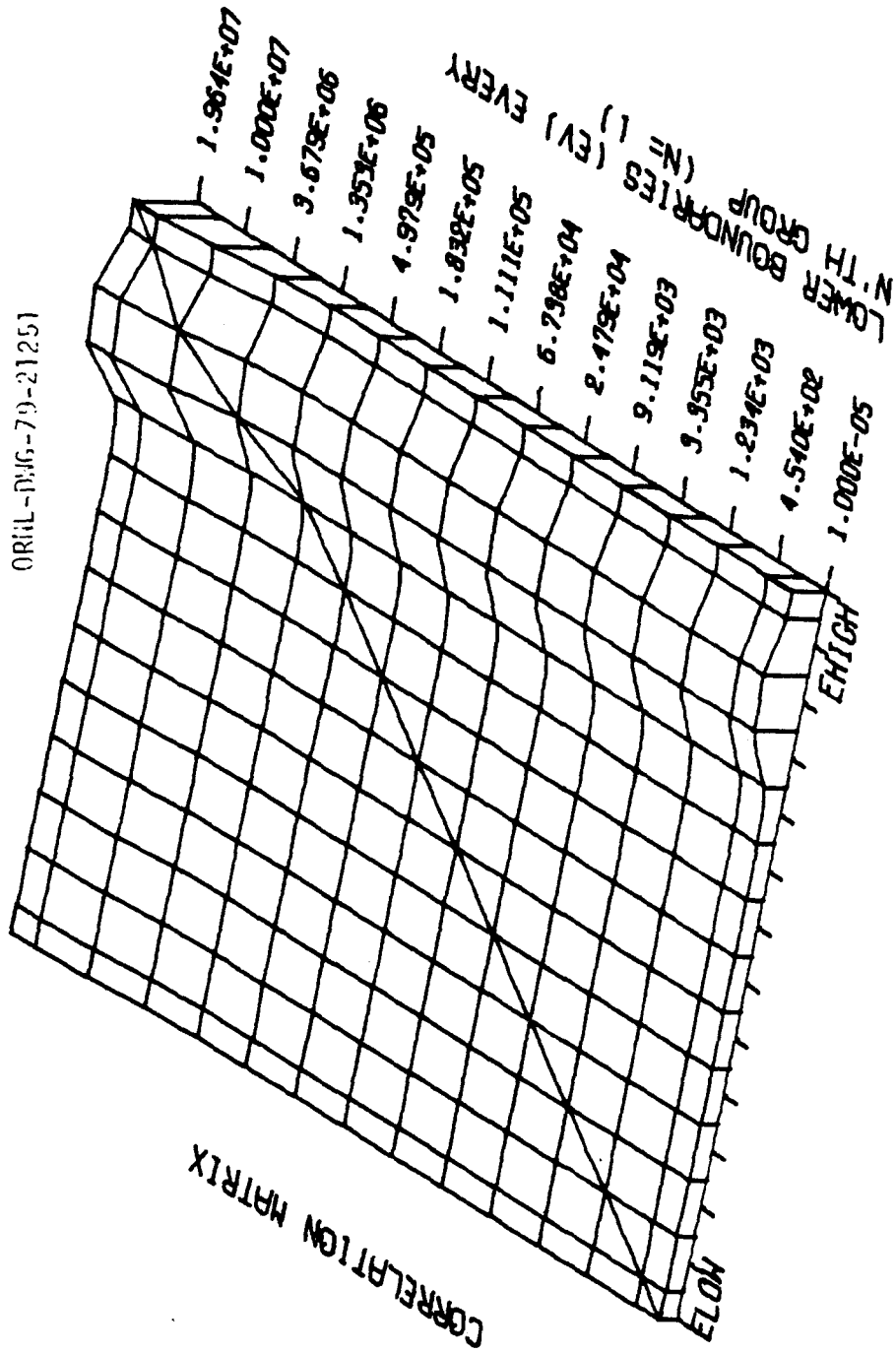


Fig. 9. Correlation Matrix Between ^{238}U prompt \bar{v} and ^{240}Pu \bar{v}
(row = $^{238}\text{U}(\bar{v})$)

As a demonstration of the use of these covariance matrices, the 52 group covariance library was collapsed to 26 groups^{16,20} and folded with sensitivity data⁹ produced from ENDF/B-V cross sections to produce an uncertainty in K_{eff} for an experimental reactor (ZPR 6/7)⁷. The calculated K_{eff} is .985 with a standard deviation of 1.574%. The experimental value for K_{eff} is 1.0 with a standard deviation of .1%. Thus it is seen that the standard deviation of the calculated value due to uncertainties in cross sections can account for the entire discrepancy between the calculated and experimental value.

The results presented above from the PUFF-II code were obtained on a PDP-10 timesharing system requiring approximately 50K of core. Typical time requirements in cpu ranged from ~1 minute for a single 52 group covariance matrix to ~3 hours for a multiple 52 group covariance matrices. The coding language is FORTRAN IV.

CHAPTER VII

CONCLUSIONS AND RECOMMENDATIONS

PUFF-II is a stand alone module capable of processing all types of uncertainty data currently present in ENDF/B-V (i.e., files 31 through 33). Specifically, processing capabilities have been added for new uncertainty relationships, explicit cross reaction and cross material relationships, and derived uncertainties. Capabilities for processing uncertainties in $\bar{\nu}$ and in the resolved resonance parameters (for infinitely dilute system only) have also been included. A final important accomplishment of this work has been to separate the uncertainty processing from the cross section processing to provide for a modular code system and reduce computing costs. The actual processing time and core requirement has been kept to a minimum by minimizing the size of the energy grid on which the covariance matrices must first be processed.

The only current limitation of the code involves the treatment of uncertainties in resolved resonance data. Specifically, the code will process only infinitely dilute resonance data.

The code has been evaluated by hand calculations and by comparison to ENDF/B-IV results for reasonableness. Results of the evaluation indicate that the code works correctly.

It should be pointed out that a problem may result from the use of the multigroup covariance matrices produced by PUFF-II. In particular, a cross section may be present for each of the user energy groups while the standard deviation determined from the uncertainty data may be zero. This problem occurs in one of three instances: 1.) The uncertainty data is incomplete;

2.) The multigroup cross section is produced in an energy structure in which one group includes the threshold energy boundary of the reaction and a user group is specified such that its upper boundary is smaller than the threshold energy and is contained within the boundaries of the larger group; or 3.) There is not a resonance energy present for one or more of the user energy groups and no uncertainty is given for the smooth cross sections in file 33 for this energy range or ranges.

Thus, the following recommendations are made regarding future work:

1.) A more detailed analysis should be given to the resolved resonance data uncertainties; specifically, a multi-level Breit-Wigner formalism should be programmed assuming future data uses this form and a treatment should be given for the uncertainties in the Bordorenko f-factors in conjunction with the resonance cross section; and 2.) The problem described above regarding the use of the multigroup covariances should be solved by writing a subroutine in the COVERX service module²¹ to eliminate discrepancies between cross sections and uncertainties.

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APPENDIX A

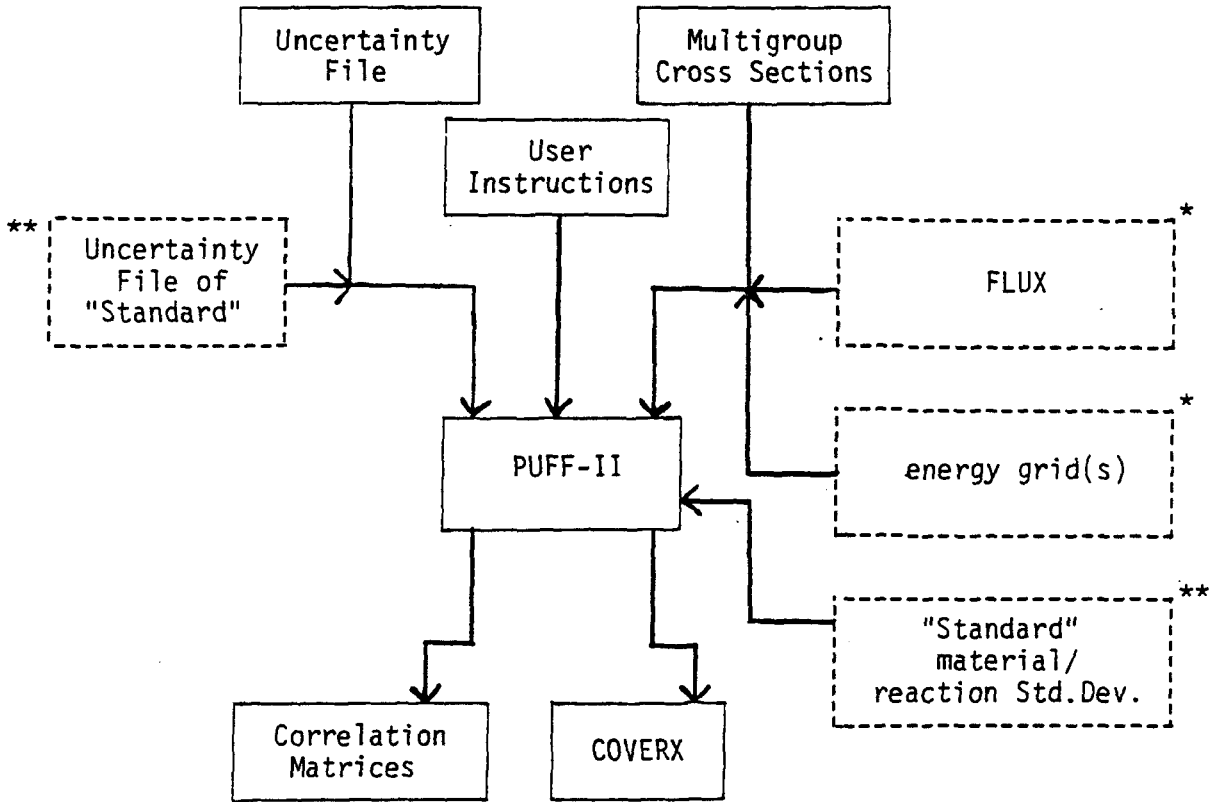
USER'S MANUAL FOR PUFF-II ON THE PDP-10

PUFF-II was written to process ENDF/B-V uncertainty files into multigroup covariance matrices. The multigroup covariance matrices are formed according to the procedures outlined in the body of this report.

Three basic types of input are required by PUFF-II; the ENDF/B-V uncertainty data, the multigroup cross sections, and the user instructions. The ENDF/B-V data may be obtained from the Radiation Shielding Information Center (RSIC) at ORNL and from many other locations. This data may be reduced to just the desired input results by RIGEL.²² Multigroup cross sections are read in from a file containing cross sections punched by PAL²² with the fixed format option. An option allowing for the reading of cross sections libraries in AMPX²² master interface formats is also incorporated into PUFF-II; however, this is not considered practical while on the PDP-10 and will not be described. The user input instructions, as described below, are dependent upon the material to be processed.

Two basic types of output are also supplied by PUFF-II. The first, which may be used to check the results is a printout consisting of the user group structure, cross sections, standard deviations, and correlation matrices for each reaction(s) for which cross sections and uncertainties have been supplied. The second type of output is the COVERX formatted files. This data contains relative covariance matrices and is useful for sensitivity investigations in the FORSS system. The basic inputs and outputs are illustrated in Fig. A-1.

This description of how to use PUFF-II will be based on a batch



*Dashed lines indicate that the input is optional

**This input is needed only for cross material processing

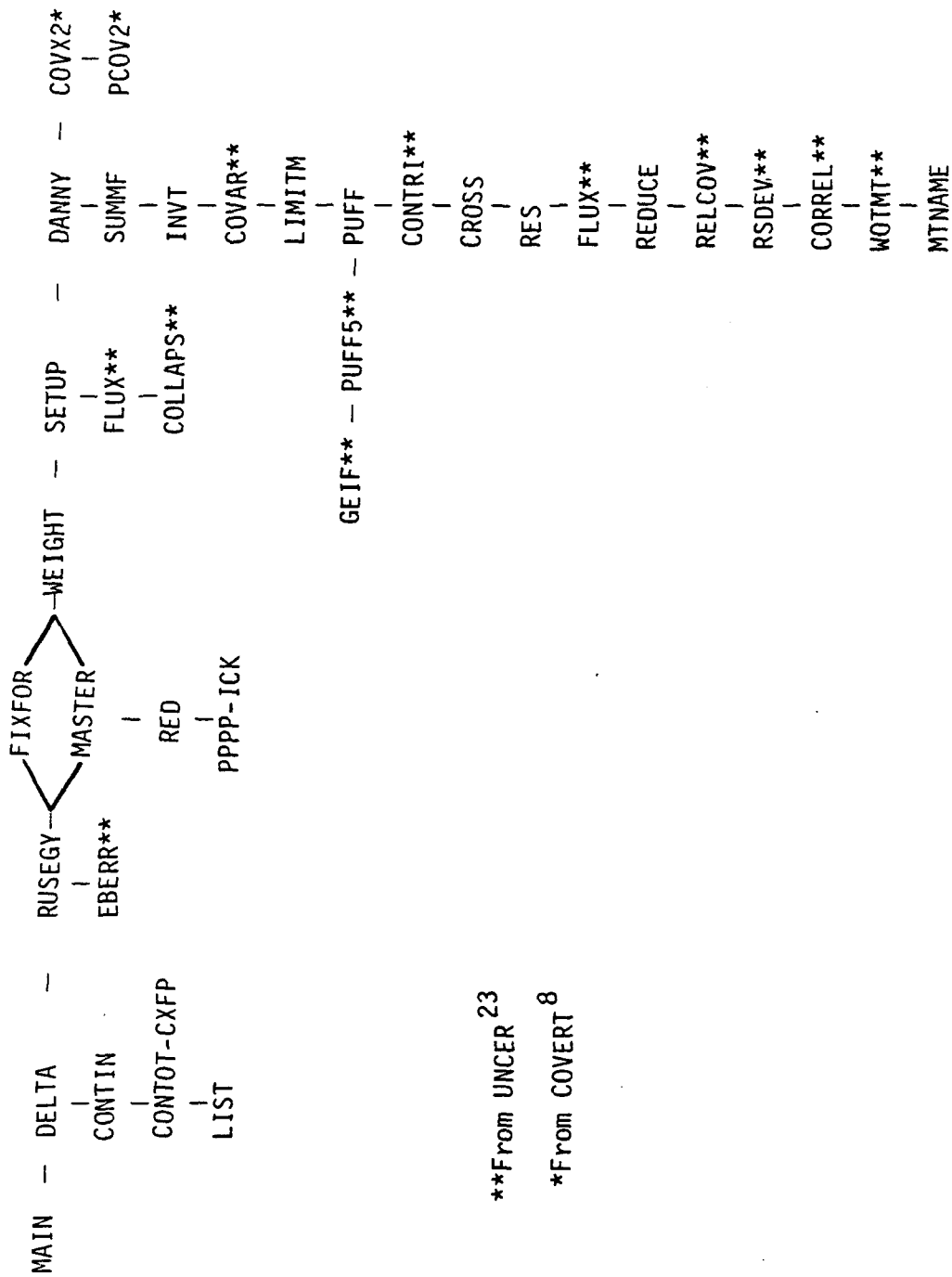
Fig. A-1. Input and Output of PUFF-II

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processing mode for the PDP-10. Batch processing is performed by creating a file consisting of the responses one would normally type in directly and then submitting this file to the queue. Also, for this time-sharing system certain liberties have been taken which are not currently possible on a non-interacting system.

The ENDF/B-V uncertainty file data is read in subroutine DELTA (see Fig. A-2) and is converted to binary with appropriate flags for subsequent processing. The input file is defined explicitly by an open statement in DELTA for unit I032 (I032=60). If the material to be processed has a reaction which is derived via ratio measurements to a referenced material's reaction, the reference material's reaction must be in a separate file in the user's area. This file is also defined explicitly by an open statement in DELTA for unit 19.

The energy grids are handled by subroutine RUSEGY. RUSEGY first forms the user grid. The user grid is formed in one of two ways. The user grid may be selected as one of nine grids stored in RUSEGY or may be read in from a separate file. If read in, the file is explicitly defined by an open statement in RUSEGY for unit 20. The energy grid may be either low to high or high to low energy in a 6E12.5 format. RUSEGY then continues to form the super-user grid and/or supergrid as flagged by the binary uncertainty file. Next, the cross section grid is formed. The cross section grid may again be chosen as one of nine optional grids or may be read in from a separate file as described above. If both the user grid and cross section grid are to be read in, then the user grid should be "stacked" on top of the cross section grid.



**From UNCR²³

*From COVERT⁸

Fig. A-2. Flow Chart for PUFF-II

The multigroup cross sections are read in by subroutine FIXFOR. Here again the cross section file is defined explicitly by an open statement in FIXFOR for unit 10.

The flux may be read in and/or produced in subroutine WEIGHT. If read in, the file is defined explicitly by an open statement in WEIGHT for unit 50 and is given in a 6E12.5 format. Other options are explained below.

Two other input files may be required. The first is involved with cross material processing. If correlations exist between reactions of different materials, then the standard or reference material must be processed first and its standard deviation saved on unit 16. This file is then defined explicitly in subroutine DANNY by an open statement for unit 17. Note that the user grid must be the same for both the reference material processing and the material desired.

The second file is associated with resonance data uncertainty processing. If resonance data uncertainty processing is to take place, the file containing the data must be defined explicitly in subroutine RES for unit I032. Note that this is the same unit and usually the same file as that which was defined explicitly in subroutine DELTA.

The first of the output units containing the correlation matrices is unit I06 (I06=6). This unit is the line printer unit and creates a file named Q??.LPT for each run, where ? represents a letter or interger variable.

The second type of output is for the COVERX file. Both a card image and a binary file are created in COVERX format on units 26 and 27 respectively.

The user instructions depend upon the desired results and the type material to be processed. The first response is to give the number of

groups in the user group structure and the weighting option desired where the numerical response and the options are shown below as

- 1 : $1/E$,
 - 2 : $1/(E \sigma_T)$,
 - 3 : input weighting/ E ,
- or
- 4 : input weighting,

where E is the energy points associated with the cross sections and σ_T is the total cross section. The second response is the option to read an AMPX master library or not where 0=No and 1=Yes. The third response is to give the number of energy groups associated with the cross sections. The fourth response is the option to read either file 31 or 33, where 0=file 33 and 1=file 31. The fifth response is the option to process file 32, where 0=No and 1=Yes. The sixth response is to give the MAT number of the material to be processed. The seventh response is to give the optional user energy grid desired where the numerical response and the associated energy grid is given as

- 1 : input grid,
 - 2 : 240 group structure,
 - 3 : GAM2 (99 groups),
 - 4 : SAND2 (620 groups),
 - 5 : LASL (30 groups),
 - 6 : GAM1 (68 groups),
 - 7 : Vitamin-C (171 groups),
 - 8 : 26 groups (ORNL-TM 5517),
 - 9 : 100 groups (GE Library),
- and
- 10 : 6 groups (ENDF/B-IV cross section covariances)

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where the actual group structures may be found in subroutine RUSEGY. The eighth response is to give the cross section energy grid where the options are the same as described above for the user grid. The ninth response is to tell the number of reactions to be read in from the cross section file. The tenth response is to give a title to the COVERX file (limited to 72 characters) and the final response is to give the weighting option used so that, when the COVERX file is formed, there is some reference to the weighting used in its production.

As an illustration of the user instructions and of a sample problem the following batch file is shown:

```

EX PUFF2.FOR
*6 4
*0
*100
*0
*0
*1399
*10
*9
*3
*PU-239 WITH CROSS MATERIAL
*4

```

where it is seen that a six group user structure is desired using 100 group cross sections and a flux which is read in and that the material to be processed is Pu-239 (MAT#1399). Pu-239 is known from the uncertainty file to have a cross material relationship to U-235 so a set up run for U-235 was produced first.

For each run executed in the batch system a log is kept of the transactions between the batch file and the computer system. This log is created under the same file name as the batch file with an extension of .LOG. The log file for this sample problem is shown on the following page.

TY BATCH.LOG

```

13:39:48 BAJOB  BATCHON VERSION 13(1071)-2 RUNNING BATCH SEQUENCE 3585 IN
STREAM 2
13:39:48 BAFIL  INPUT FROM OREL0: BATCH.(104,1134)
13:39:48 BAFIL  OUTPUT TO OREL0: BATCH.LOG(104,1134)
13:39:48 BASUM  JOB PARAMETERS
TIME: 01:00:00  UNIQUE: YES  RESTART: NO

13:39:48 MONTR
13:39:48 MONTR  .LOGIN 104,1134 /CHARGE:18075 /SPOOL:ALL/TIME:3600/NAME:
"JDS 6010"
13:39:49 USER  JOB 16 ORELA/602.3 TTY63
13:39:49 USER  [LGNJSP OTHER JOBS SAME PPN:13]
13:39:49 USER  CHARGE = 18075
13:39:49 USER  1339 30-OCT-79 TUE
13:39:51 MONTR
13:39:51 MONTR  .EX PUFF2.FOR
13:39:53 USER  LINK: LOADING
13:40:24 USER  [LNKXCT PUFF2 EXECUTION]
13:40:24 USER  GIVE # OF GROUPS IN USER GROUP STRUCTURE AND AND TYPE O
F WEIGHTING SPECTRUM DESIRED, WHERE 1=1/E, 2=1/(F*SIGMA TOTAL), 3=1/E*IN
PUT, AND 4=INPUT.>*6 4
13:40:26 USER  SPECIFY OPTION TO READ MASTER LIBRARY (0=NO,1= YES).>*0
13:40:27 USER  GIVE # OF X-SEC GROUPS>*100
13:40:27 USER  READ FILE 31(NUBAR) OR FILE 33?(0=33;1=31)>*0
13:40:28 USER  PROCESS FILE 32 ?(0=NO;1=YES)>*0
13:40:28 USER  MAT # OF MATERIAL PROCESSING>*1399
13:40:46 USER  SPECIFY TYPE OF USER GRID STRUCTURE(I FORMAT), 1-ARBITRA
RY,2-240 GROUP,3-GAM2(99 GRPS),4-SAND2(620 GRPS), 5-LASL(30 GRPS),6-GAM1
(6P GRPS),7-171 GROUPS,8-26 GROUPS, 9-100 GROUPS,10- 6 GROUPS.>*10
13:40:53 USER  SPECIFY THE TYPE GROUP STRUCTURE THE CROSS SECTIONS ARE
ON( SAME OPTIONS AS FOR USER GRID).>*9
13:40:55 USER  GIVE # OF MT >*3
13:43:59 USER  TYPE IN FILE DESCRIPTION, 1 CARD FORMAT(12A6)
13:43:59 USER  >*PU-239 WITH CROSS MATERIAL
13:44:00 USER  TYPE IN NUMBER CORRESPONDING TO WEIGHTING FUNCTION (15)
>*4
13:44:04 USER  STOP
13:44:05 USER
13:44:05 USER  END OF EXECUTION
13:44:05 USER  CPU TIME: 2:4.58 ELAPSED TIME: 3:40.33
13:44:06 MONTR  EXIT
13:44:06 MONTR
13:44:06 MONTR  .KJOB OREL0: BATCH.LOG=/W/B/Z:4/VR:10/VS:3585/VL:200/VP:1
0/VD: D
13:44:07 KJOB  OTHER JOBS SAME PPN
13:44:07 LGOUT JOB 16, USER (104,1134) LOGGED OFF TTY63 1344 30-OC
T-79
13:44:07 LGOUT ANOTHER JOB STILL LOGGED IN UNDER (104,1134)
13:44:07 LGOUT CPU TIME = 2.22 MINUTES
13:44:07 LGOUT CON TIME = 0.07 HOURS
13:44:07 LGOUT KILO CORE = 2.12 HOURS
13:44:07 LGOUT JOB COST = 5.30 DOLLARS
13:44:07 LGOUT PRIME RATES

```

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Tables A-1 through A-5 illustrates the output from PUFF-II which contains the standard deviations and correlation matrices. Table A-6 illustrates the COVERX formatted output file from PUFF-II.

The computer code PUFF-II has been checked by hand calculations and by comparison of results to previous ENDF/B-IV results for reasonableness. Running time varies and is dependent upon the order of the matrices and on the amount of correlations between reactions. For the sample problem which has been used for illustration thus far, a cpu time of two minutes and four seconds was recorded on the PDP-10. The coding language is Fortran IV. The only limitation of PUFF-II, at the present, is the limited treatment given to the resonance data uncertainty.

Table A-1. Correlation Matrix and Standard Deviations for ²³⁹Pu(n,f) to ²³⁵U(n,f)

MATERIAL 1= 1399, REACTION 1= 10 , MATERIAL 2= 1395, REACTION 2= 18

GROUP	E HIGH	E LOW	X-IGN(1)	X-IGN(2)	REL.S.D.(1)	REL.S.D.(2)
1	2.0000E+07	3.6790E+06	2.5270E+00	2.0500E+00	7.1807E-02	5.2079E-02
2	3.6790E+06	1.3530E+06	1.9055E+00	1.2550E+00	3.1328E-02	2.3702E-02
3	1.3530E+06	4.9790E+05	1.6996E+00	1.1749E+00	3.4220E-02	2.7380E-02
4	4.9790E+05	1.8320E+05	1.5423E+00	1.2700E+00	3.3301E-02	2.7812E-02
5	1.8320E+05	4.0870E+04	1.5770E+00	1.6328E+00	5.2803E-02	2.6331E-02
6	4.0870E+04	1.0000E+05	6.8942E+02	4.9976E+02	1.1159E-02	3.3689E-03

*** CORRELATION MATRIX ***

	COLUMN MATERIAL 1						ROW MATERIAL 2					
	1	2	3	4	5	6	1	2	3	4	5	6
1	141	135	9	0	0	0						
2	35	756	389	186	0	0						
3	3	367	797	581	0	0						
4	0	173	576	784	0	0						
5	0	32	150	356	0	0						
6	0	0	0	0	0	0						

Table A-2. Correlation Matrix and Standard Deviation for ²³⁹Pu(n,f)

MATERIAL 1= 1399, REACTION 1= 18 , MATERIAL 2= 1399, REACTION 2= 18

GROUP	E HIGH	E LOW	X-I0N(1)	X-I0N(2)	REL.S.D.(1)	REL.S.D.(2)
1	2.0000E+07	3.6790E+06	2.5270E+00	2.5270E+00	7.1807E-02	7.1807E-02
2	3.6790E+06	1.3530E+06	1.9055E+00	1.9055E+00	3.1328E-02	3.1328E-02
3	1.3530E+06	4.9790E+05	1.6996E+00	1.6996E+00	3.4220E-02	3.4220E-02
4	4.9790E+05	1.8320E+05	1.5423E+00	1.5423E+00	3.3301E-02	3.3301E-02
5	1.8320E+05	4.0870E+04	1.5770E+00	1.5770E+00	5.2803E-02	5.2803E-02
6	4.0870E+04	1.0000E-05	6.8942E+02	6.8942E+02	1.1159E-02	1.1159E-02

*** CORRELATION MATRIX ***

COLUMN=MATERIAL 1 ROW=MATERIAL 2

ROW	COLUMN					
	1	2	3	4	5	6
1	1000	79	50	45	0	0
2	79	1000	674	491	0	0
3	50	674	1000	810	0	0
4	45	491	810	1000	123	0
5	0	0	0	123	1000	0
6	0	0	0	0	0	1000

Table A-3. Correlation Matrix and Standard Deviations for ²³⁹Pu(n,γ) to ²³⁵U(n,f)

MATERIAL 1 = 1399, REACTION 1 = 102 , MATERIAL 2 = 1395, REACTION 2 = 18

GROUP	E HIGH	E LOW	X-1MN(1)	X-1MN(2)	REL.S.D.(1)	REL.S.D.(2)
1	2.0000E+07	3.6790E+06	2.4085E-03	2.0500E+00	3.0843E-01	5.2079E-02
2	3.6790E+06	1.3530E+06	7.3689E-03	1.2550E+00	3.0156E-01	2.3702E-02
3	1.3530E+06	4.9790E+05	5.0417E-02	1.1749E+00	1.8340E-01	2.7380E-02
4	4.9790E+05	1.8320E+05	1.6607E-01	1.2700E+00	2.0272E-01	2.7812E-02
5	1.8320E+05	4.0870E+04	3.1099E-01	1.6328E+00	2.0735E-01	2.6331E-02
6	4.0870E+04	1.0000E-05	2.7055E+02	4.9976E+02	3.2777E-02	3.3689E-03

*** CORRELATION MATRIX ***

	COLUMN=MATERIAL 1						ROW=MATERIAL 2					
	COLUMN											
ROW	1	2	3	4	5	6	1	2	3	4	5	6
1	33	10	1	0	0	0						
2	8	72	65	28	0	0						
3	1	41	170	88	0	0						
4	0	17	131	127	0	0						
5	0	3	35	59	0	0						
6	0	0	0	0	0	0						

Table A-4. Correlation Matrix and Standard Deviation for ²³⁹Pu(n,γ)

MATERIAL 1= 1399, REACTION 1= 102 , MATERIAL 2= 1399, REACTION 2= 102

GROUP	E HIGH	E LOW	X-I0N(1)	X-I0N(2)	REL.S.D.(1)	REL.S.D.(2)
1	2.0000E+07	3.6790E+06	2.4085E-03	2.4085E-03	3.0843E-01	3.0843E-01
2	3.6790E+06	1.3530E+06	7.3689E-03	7.3689E-03	3.0126E-01	3.0156E-01
3	1.3530E+06	4.9790E+05	5.0417E-02	5.0417E-02	1.8340E-01	1.8340E-01
4	4.9790E+05	1.8320E+05	1.6607E-01	1.6607E-01	2.0272E-01	2.0272E-01
5	1.8320E+05	4.0870E+04	3.1099E-01	3.1099E-01	2.0735E-01	2.0735E-01
6	4.0870E+04	1.0000E-05	2.7055E+02	2.7055E+02	3.2777E-02	3.2777E-02

*** CORRELATION MATRIX ***

COLUMN=MATERIAL 1 ROW=MATERIAL 2

ROW	COLUMN					
	1	2	3	4	5	6
1	1000	969	196	2	0	0
2	969	1000	211	8	0	0
3	196	211	1000	972	924	0
4	2	8	972	1000	956	0
5	0	0	924	956	1000	0
6	0	0	0	0	0	1000

Table A-5. Correlation Matrix and Standard Deviations for ²³⁹Pu(n,f) to ²³⁹Pu(n,γ)

MATERIAL 1 = 1399, REACTION 1 = 18 , MATERIAL 2 = 1399, REACTION 2 = 102

GROUP	E HIGH	E LOW	X-I0N(1)	X-I0N(2)	REL.S.D.(1)	REL.S.D.(2)
1	2.000E+07	3.6790E+06	2.5270E+00	2.4085E-03	7.1807E-02	3.0843E-01
2	3.6790E+06	1.3530E+06	1.9055E+00	7.3689E-03	3.1328E-02	3.0156E-01
3	1.3530E+06	4.9790E+05	1.6996E+00	5.0417E-02	3.4220E-02	1.8340E-01
4	4.9790E+05	1.8320E+05	1.5423E+00	1.6607E-01	3.3301E-02	2.0272E-01
5	1.8320E+05	4.0870E+04	1.5770E+00	3.1099E-01	5.2803E-02	2.0735E-01
6	4.0870E+04	1.0000E-05	6.8942E+02	2.7055E+02	1.1159E-02	3.2777E-02

*** CORRELATION MATRIX ***
 COLUMN=MATERIAL 1 ROW=MATERIAL 2

	COLUMN					
	1	2	3	4	5	6
ROW	1	232	19	12	11	0
2	7	99	73	51	0	0
3	9	119	204	171	0	0
4	7	78	126	163	25	0
5	0	0	0	23	258	0
6	0	0	0	0	0	-375

 * PUFF PROCESSING COMPLETED *

Table A-6. Sample COVERX file

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OV COVERX COVERX*JRNL - FCRSS*      1
1D      6      6      0      2      2      5      5
2D *PU-239 WITH CROSS MATERIAL *
3D  0.2000E+08  0.3679E+07  0.1353E+07  0.4979E+06  0.1832E+06
4.0870E+04  1.0000E-05
5D  1399      18      4  1399      102      4
6D  0.2527E+01  0.1905E+01  0.1700E+01  0.1542E+01  0.1577E+01
6.8943E+02  7.1807E-02  3.1328E-02  3.4220E-02  3.3301E-02  5.2803E-02
1.1159E-02
6D  0.2409E-02  0.7369E-02  0.5042E-01  0.1661E+00  0.3110E+00
2.7055E+02  3.0844E-01  3.0156E-01  1.8340E-01  2.0272E-01  2.0735E-01
3.2777E-02
7D  1399      18  1395      18      1
8D      6      1      6      2      6      3      6      4      6      5      6
6      6
9D  0.5226E-03  0.5994E-04  0.5904E-05  0.3307E-06  0.3658E-07
0.0000E-01  2.2059E-04  5.6112E-04  3.1519E-04  1.5050E-04  2.6206E-05
0.0000E-01  1.5923E-05  3.1589E-04  7.4648E-04  5.4840E-04  1.3548E-04
0.0000E-01  2.7077E-07  1.4659E-04  5.2944E-04  7.2653E-04  3.1184E-04
5.0867E-11  0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01
0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01
0.0000E-01
7D  1399      18  1399      18      1
8D      6      1      6      2      6      3      6      4      6      5      6
6      6
9D  0.5156E-02  0.1779E-03  0.1240E-03  0.1084E-03  0.0000E+00
0.0000E-01  1.7792E-04  9.8144E-04  7.2275E-04  5.1274E-04  0.0000E-01
0.0000E-01  1.2402E-04  7.2275E-04  1.1710E-03  9.2279E-04  0.0000E-01
0.0000E-01  1.0839E-04  5.1274E-04  9.2279E-04  1.1090E-03  2.1610E-04
0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01  2.1610E-04  2.7881E-03
6.1044E-11  0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01  6.1044E-11
1.2452E-04
7D  1399      102  1395      18      1
8D      6      1      6      2      6      3      6      4      6      5      6
6      6
9D  0.5305E-03  0.6019E-04  0.5826E-05  0.3551E-06  0.4393E-07
0.0000E-01  1.5549E-04  5.1331E-04  3.3768E-04  1.4556E-04  2.6384E-05
0.0000E-01  6.4966E-06  2.8125E-04  8.5504E-04  6.6841E-04  1.6726E-04
0.0000E-01  2.3163E-07  1.3554E-04  4.9092E-04  7.1516E-04  3.1742E-04
5.4195E-11  0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01
0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01
0.0000E-01
7D  1399      102  1399      102      1
8D      6      1      6      2      6      3      6      4      6      5      6
6      6
9D  0.9513E-01  0.9016E-01  0.1108E-01  0.1068E-03  0.0000E+00
0.0000E-01  9.0162E-02  9.0936E-02  1.1649E-02  4.8904E-04  0.0000E-01
0.0000E-01  1.1077E-02  1.1649E-02  3.3637E-02  3.6122E-02  3.5131E-02
1.4304E-09  1.0677E-04  4.8904E-04  3.6122E-02  4.1097E-02  4.0196E-02
1.6287E-09  0.0000E-01  0.0000E-01  3.5131E-02  4.0196E-02  4.2993E-02
1.6808E-09  0.0000E-01  0.0000E-01  1.4304E-09  1.6287E-09  1.6808E-09
1.0743E-03
7D  1399      18  1399      102      1
8D      6      1      6      2      6      3      6      4      6      5      6
6      6
9D  0.5144E-02  0.1616E-03  0.1208E-03  0.1060E-03  0.0000E+00
0.0000E-01  1.7896E-04  9.3325E-04  6.8386E-04  4.9390E-04  0.0000E-01
0.0000E-01  1.2473E-04  7.4912E-04  1.2815E-03  6.7607E-04  0.0000E-01
0.0000E-01  1.0913E-04  5.0818E-04  1.0461E-03  1.1000E-03  1.5933E-04
0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01  2.6594E-04  2.8283E-03
4.4394E-11  0.0000E-01  0.0000E-01  0.0000E-01  0.0000E-01  7.1726E-11
-1.3718E-04
    
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