ORNL-5336 (ENDF-253)

# A Compendium of Energy-Dependent Sensitivity Profiles for the TRX-2 Thermal Lattice

E. T. Tomlinson J. L. Lucius J. D. Drischler

OAK RIDGE NATIONAL LABORATORY OPERATED BY UNION CARBIDE CORPORATION · FOR THE DEPARTMENT OF ENERGY

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- A Compendium of Energy-Dependent Sensitivity Profiles for the TRX-2 Thermal Lattice\*
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 $^{\star} {\rm The}$  organization of the graphs and data is given on page iv.

# ORGANIZATION OF GRAPHS AND DATA

					Page	e No.				
		k	2 8	βρ .	2	<sup>5</sup> δ	2	8 <sub>8</sub>	CR	
	Graph	SENPRO Data								
<sup>238</sup> U V	17	116	35	122	53	128	71	134	93	141
<sup>238</sup> U <sup>o</sup> f	18	116	36	122	54	128	72	134	99	141
<sup>238</sup> U <sup>o</sup> c	19	116	37	122	55	128	73	134	95	142
<sup>238</sup> U <sub>o</sub> s	20	117	38	123	56	129	74	135	96	142
<sup>238</sup> U σ <sub>s</sub> in(21s	t)						75	135		
<sup>238</sup> U σ <sub>s</sub> in(22n	nd)						76	135		
2 <sup>38</sup> U σ <sub>s</sub> in(con	nt.)						. 77	136		
<sup>238</sup> U σ <sub>s</sub> in(tot	al)						78	136		
<sup>235</sup> U <del>v</del>	21	117	39	123	57	129	79	136	97	142
235U of	22	117	40	123	58	129	80	137	98	143
<sup>235</sup> U σ <sub>c</sub>	23	118	41	124	59	130	81	137	99	143
<sup>235</sup> U σ <sub>s</sub>	24	118	42	124	60	130	82	137	100	143
Al o <sub>c</sub>	25	118	43	124	61	130	83	138	101	144
Al o <sub>s</sub>	26	119	44	125	62	131	84	138	102	144
Н σ <sub>с</sub>	27	119	45	125	63	131	85	138	103	144
Ησ <sub>s</sub>	28	119	46	125	64	131	86	139	104	145
0 σ <sub>c</sub>	29	120	47	126	65	132	87	139	105	145
0 σ <sub>s</sub>	30	120	48	126	66	132	88	139	106	145
DB² fuel	31	120	49	126	67	132	89	140	107	146
$\rm DB^2$ void	32	121	50	127	68	133	90	140	108	146
DB² clad	33	121	51	127	69	133	91	140	109	146
DB <sup>2</sup> moderator	34	121	52	127	70	133	92	141	110	147

### ABSTRACT

Energy-dependent sensitivity profiles for five responses calculated for the TRX-2 thermal lattice with the ORNL sensitivity code system FORSS are presented here both in graphical form and in SENPRO format. The responses are the multiplication factor,  $k_{eff}$ ; the ratio of epithermal-tothermal captures in <sup>238</sup>U, <sup>28</sup>p; the ratio of epithermal-to-thermal fissions in <sup>235</sup>U, <sup>25</sup> $\delta$ ; the ratio of fissions in <sup>238</sup>U to fissions in <sup>235</sup>U, <sup>28</sup> $\delta$ ; and the ratio of captures in <sup>238</sup>U to fissions in <sup>235</sup>U, CR. A summary table of the total sensitivities is also presented.

#### INTRODUCTION

The ORNL sensitivity code system FORSS,<sup>1,2</sup> a modular computer code system for studying relationships between nuclear cross sections, integral experiments, and calculated performance parameters for a given system, together with the associated uncertainties, has been applied to the CSEWG TRX-2 thermal lattice benchmark.<sup>3</sup> Of special interest are the sensitivity profiles, which show the sensitivity of the calculated responses to the various material cross sections as a function of neutron energy and to the resonance parameters. These profiles may be used in a myriad of ways; however, much insight can be gained merely through studying the profiles themselves. This report presents a set of typical sensitivity profiles for the selected system. In addition, for those interested in applying the sensitivity coefficients, the SENPRO format<sup>4</sup> for reporting sensitivity coefficients is presented in Appendix A, and the data are tabulated in Appendix B.

## THE SCOPE OF THE REPORT

The TRX-2 thermal lattice was selected for this study because it represents a well-documented and often-calculated thermal benchmark. It was a slightly enriched (1.3%) water-moderated assembly with uranium metal rods clad in aluminum. The rods were 121.92 cm in length and 0.983 cm in diameter in a hexagonal pitched array with a water-to-fuel ratio of 4.02. This resulted in a spectrum that was considerably softer than that of a typical pressurized water reactor. The calculations were done using a single assembly cell (i.e., a single fuel rod surrounded by water).

A total of five responses were calculated for the assembly:

- (1) the multiplication factor,  $k_{eff}$ ;
- (2) the ratio of epithermal-to-thermal captures in  $^{238}$ U,  $^{28}\rho$ ;
- (3) the ratio of epithermal-to-thermal fissions in  $^{235}U$ ,  $^{25}\delta$ ;
- (4) the ratio of  $^{238}$ U fissions to  $^{235}$ U fissions,  $^{28}\delta$ ;
- (5) the ratio of  $^{238}$ U captures to  $^{235}$ U fissions, CR.

All reaction rate ratios were averaged over the fuel pin. An upper energy bound of 0.625 eV was assumed for the thermal region. The nuclear data

included were fission yields and neutron interaction cross sections for fission, capture, total scattering, and total inelastic scattering, as well as scattering from each inelastic level and from the inelastic continuum. Inelastic scattering sensitivities were considered only for  $^{238}$ U and reported only if the magnitude of the sensitivity was greater than  $10^{-6}$ .

The sensitivities presented represent a portion of what is presently available at ORNL in the thermal reactor field and is in no sense complete. Preliminary sets of sensitivity profiles are available for a number of mixed oxide lattices.<sup>5</sup> It was felt, however, that these data are of sufficient interest to warrant presentation in this report. The sensitivities have been compiled in a computer-readable format and are available from the Radiation Shielding Information Center at Oak Ridge National Laboratory. This RSIC library, which also presently contains a number of fast reactor benchmark sensitivities,<sup>6</sup> continues to grow and will be documented at appropriate intervals in the sense of the "open code package."

#### THE METHOD

The method of calculating the sensitivity coefficients for TRX-2 has been extensively described elsewhere<sup>7</sup> and only a brief description will be presented here.

A 131 energy group cross-section library<sup>8</sup> was developed for use in this study. The energy boundaries for this library are presented in Table 1. The weight function used for the averaging process consisted of a Maxwellian at  $300^{\circ}$ K in the thermal range with an upper energy cutoff of 0.625 eV coupled to a 1/E spectrum joined to a fission spectrum at high energies. (The breakpoint was taken to be 67 keV and the temperature of the fission spectrum was taken to be 1.27 MeV, corresponding to the ENDF/B-IV value for the thermal fissions in <sup>235</sup>U.) The thermal cross sections generated during this process were not used because of the inability of the MINX code to perform upscatter corrections. The upscatter corrected and self-shielded thermal data, including bound atom effects, used in this

	<u> </u>				
Group	Upper Energy (eV)	Group	Upper Energy (eV)	Group	Upper Energy (eV)
1.	1 00000+7	45	6 61558+1	80	2 10000+1
2	6 06531+6	45	6 61/62+1	09	2.100001
2	2 67070+6	40	6 61266+1	90	2.090201
1	2 22120+6	47	6 61270+1	91	2.092321
5	1 25225+6	40		92	2.09102+1
5	0 2005015	49	0.00980+1	93	2.0905371
0 7	0.2000070	50		94	2.0090371
/	4.9/8/1+5	51	0.59900+1	. 95	2.08854+1
0	3.019/4+5	52	0.58/00+1	90	2.08/54+1
9	1.83150+5	53	6.55100+1	97	2.083/7+1
10	1.11090+5	54	6.52300+1	.98	2.08000+1
	6./3/95+4	55	6.50400+1	99	2.0/600+1
12	4.08677+4	56	6.46200+1	100	2.06000+1
13	2.47875+4	57	6.38000+1	101	2.04000+1
14	1.50344+4	58	6.32200+1	102	2.01500+1
15	9.11882+3	59	5.30000+1	103	2.00000+1
16	5.53084+3	60	3.97000+1	104	1.98000+1
17	3.35463+3	61	3.87600+1	105	1.92600+1
18	2.03468+3	62	3.81850+1	106	1.05000+1
19	1.23410+3	63	3.78100+1	107	9.93000+0
20	7.48518+2	64	3.75200+1	108	8.06000+0
21	4.53999+2	65	3.72100+1	109	7.51000+0
22	2.75364+2	66	3.69800+1	110	7,19000+0
23	1,67017+2	67	3,69146+1	111	7.01000+0
24	1.01310+2	68	3.68491+1	112	6.90000+0
25	9.36000+1	69	3 68300+1	113	6 78000+0
26	9.30000+1	70	3.68108+1	114	6 71000+0
27	9 12800+1	71	3 67917+1	115	6 69690+0
28	9 06250+1	72	3 67725+1	116	6 68387+0
29	8 97500+1	73	3 6753/1+1	117	6 67830+0
30	8 87500+1	73	3 66767+1	110	6 67280+0
31	8 39200+1	75	3 66000+1	110	6 66720+0
32	8 32000+1	76	3 65000+1	120	6 66170+0
32	8 18000+1	70	3 63800+1	120	6 65616+0
3/	8 00000+1	70	3 60055+1	121	6 6/210+0
25		70	2 57000±1	122	6 6200010
20	6 7000011	/ 9	3.57600+1	123	
30 27	0.79800+1	80	3.54900+1	124	6.50000+0
3/	0./5000+1	81	3.51200+1	125	6.40000+0
38	0.08/00+1	82	3.46000+1	120	6.25000+0
39	6.65900+1	83	2.30000+1	127	6.15000+0
40	6.63800+1	84	2.24500+1	128	5.95000+0
41	6.62200+1	85	2.19500+1	129	5.50000+0
42	6.61975+1	86	2.15800+1	130	1.00000+0
43	6.61750+1	87	2.13000+1	131	6.25000-1
44	6.61654+1	88	2.11000+1		1.00000-5

Table 1. 131 Group Energy Boundaries for the TRX-2 Sensitivity Study

study were supplied by EPRI.<sup>8</sup> These were obtained from a 30-group THERMOS<sup>9</sup> calculation.

The scattering cross section for all the energy groups above thermal were expanded through  $P_1$  except for hydrogen. The hydrogen scattering matrices were expanded through order 5. This was done to correctly account for the forward peaked angular distribution of neutrons scattering from hydrogen in the laboratory system, leading to an energy distribution appropriate for the fine energy mesh used in this study. Later results indicated that a  $P_3$  expansion would have been sufficient. The thermal cross section data consisted of a transport corrected  $P_0$  set. (In practice, this was run as  $P_5$ , with the higher moments set to zero.) This involved the assumption that all anisotropic scattering effects can be accounted for by use of the transport cross section instead of the total cross section.

The ANISN discrete ordinate transport code<sup>10</sup> (using an  $S_{16}P_5$  approximation) was applied to a one-dimensional model of a TRX-2 cell, described in Table 2, for the calculation of the forward and adjoint fluxes, as well as the multiplication eigenvalue. These in turn were used in the JULIET<sup>2</sup> module for calculating the values of the performance parameters and the corresponding sources for the generalized-adjoint transport equations. The generalized adjoint solutions of these generalized equations were provided by ANISN (modified to allow negative sources and fluxes) and then used in JULIET for the calculation of sensitivity coefficients. Further details concerning these codes and procedures can be found in Ref. 7.

### RESULTS

The results of this sensitivity study are presented here in the form of tables and graphs. The nominal values of the performance parameters calculated using ENDF/B-IV cross sections are in good agreement with previously reported values <sup>11</sup> and experimental values (see Table 3). <sup>12</sup> The calculated resonance parameter sensitivities for the first four s wave resonances in <sup>238</sup>U are also in good agreement with previously reported results. <sup>13</sup> The

<sup>&</sup>lt;sup>\*</sup>The tables are in Appendix B, page 115, and the graphs begin on page 17; see page iv for page numbers of specific data.

Region	Outer Radius (cm)	Isotope	Concentration atoms/barn-cm
Fuel	0.4915	235 <sub>U</sub> 238 <sub>U</sub>	0.0006253 0.047205
Void	0.5042	-	-
Clad	0.5753	<sup>23</sup> A1	0.06025
oderator	1.14109	1 <sub>H</sub>	0.06676
		16 <sub>0</sub>	0.03338

Table 2. The Cylindricized Calculation Model of the TRX-2 Hexagonal Lattice

Table 3. TRX-2 Performance Parameters Based Upon ENDF/B-IV

Parameter	Experiment <sup>a</sup>	ORNL Calculation	
k <sub>eff</sub>	1.0000	1.0012	
<sup>28</sup> ρ	0.837 <u>+</u> 0.016	0.867	
258	0.0614 <u>+</u> 0.0008	0.0602	
288	0.0693 <u>+</u> 0.0035	0.0698	
CR	0.647 <u>+</u> 0.006	0.645	

graphs, Figs. 1-94, present relative sensitivities per unit lethargy as a function of neutron energy. The profiles were plotted in this form because the relative sensitivity per unit lethargy is independent of group structure if the group structure is sufficiently fine. Thus these plots can be compared directly with similar plots which use a different group structure. Note that these are log-log plots in which a solid curve represents a negative quantity and a broken line (dashed) curve represents a positive quantity.

The total sensitivities for each response, nuclide, and reaction are presented in Tables 4-8. The total sensitivity is the sum over all energy groups of the sensitivities of the response with respect to the group reaction cross sections. Such a total sensitivity is actually a relative sensitivity with respect to a single group-independent scale factor  $\lambda$  which affects the associated cross section in the same proportion at all energies and small groups. Thus, if the scale factor  $\lambda$  increases by 10%, all the group cross sections for the associated reaction type increase by the same 10%. For convenience  $\lambda$  may be set to unity when the group cross sections have their nominal values  $\sigma_{\alpha}^{0}$ . Then the group cross sections are given by

$$\sigma_{g}^{\prime} = \lambda \sigma_{g}^{0}. \tag{1}$$

The energy dependent sensitivity profiles provide a quantitative assessment of the rate of change in a particular response, R, with respect to the rate of change in some multigroup constant. Of more immediate interest is the sensitivity with respect to a specific resonance parameter,  $\Gamma_{\rm y}$ . The latter can be obtained from

$$\frac{dR/R}{d\Gamma_{\chi}/\Gamma_{\chi}} = \sum_{g} \left( \frac{dR/R}{d\overline{\sigma}_{g}/\overline{\sigma}_{g}} \right) \frac{d\overline{\sigma}_{g}/\overline{\sigma}_{g}}{d\Gamma_{\chi}/\Gamma_{\chi}}$$
(2)

The first term in each element of the sum is the sensitivity profile  $(dR/R/d\overline{\sigma}_g/\overline{\sigma}_g)$ , whereas the second derivation  $(d\overline{\sigma}_g/\overline{\sigma}_g/d\Gamma/\Gamma)$  can be obtained numerically.

The numerical derivatives were obtained by direct recalculation of the group averaged cross section with a perturbed set of resonance parameters. The results of these calculations are given in Table 9 for the parameters

Nuclide	Item	<u>δR/R</u> δσ/σ
235U	v	0.925
2 3 5 U	σ <sub>£</sub>	0.430
238U	σ	-0.265
Н	σ <sub>ε</sub>	0.183
Н	σc	-0.160
Moderator	DB <sup>2</sup>	-0.105
235U	ď	-0.092
238U	- -	0.075
238U	σ <sub>f</sub>	0.048
Fuel	DB <sup>2</sup>	-0.027
Clad	DB <sup>2</sup>	-0.008
A1	σ	-0.007
238U	σs	-0.002
0	σ	-0.002
0	σ <b>ς</b>	0.002
Void	DB <sup>2</sup>	-0.002
A1	σ	-0.0001
<sup>235</sup> ປ	σs	-0.00002

Table 4. Total Sensitivities for k in the TRX-2 Thermal Lattice

Table 5	. Total	Sensitiv	ities	for	28 <sub>0</sub>
in	the TRX-2	2 Thermal	Latti	ce	

in the	1111-2	merman	Lattice
Nuclide		Item	<u>δR/R</u> δσ/σ
Н		σς	-1.035
235U		σ <sub>f</sub>	0.549
н		σ	0.182
<sup>235</sup> U		σc	0.096
Moderator		DB <sup>2</sup>	0.029
238U		σc	-0.024
0		σs	-0.011
Al		σc	0.008
<sup>238</sup> U		σs	0.004
Fuel		DB <sup>2</sup>	0.004
Clad		DB <sup>2</sup>	0.002
Void		$DB^2$	0.0005
Al		σς	-0.0005
2 3 5 U		$\overline{v}$	-0.0003*
238U		σ <sub>f</sub>	-0.0001
0		σc	0.00006
2 3 5U		σ	-0.00002
2.38U		_ <b>`</b>	-0,00002*

\*These sensitivities should sum to zero, but due to numerical precision a small residual remains.

Nuclide	Item	<u>δR/R</u> δσ/σ
Н	σ	-1.035
235U	с С <sub>Г</sub>	0.538
2 3 8 U	σ	0.201
Н	σ	0.181
235U	σ	0.092
Moderator	$DB^2$	0.029
2 3 8 U	σ	-0.013
0	σς	-0.013
Al	σc	0.008
Fuel	DB <sup>2</sup>	0.003
Clad	DB <sup>2</sup>	0.002
A1	σs	-0.0003
238U	σ <sub>f</sub>	-0.0008
Void	DB <sup>2</sup>	0.0005
2 3 5 J	σs	-0.0001
235U	$\overline{v}$	0.00004*
0	σc	-0.00003
2 3 8 U		-0.00001*

Table 6. Total Sensitivities for  $^{25}\delta$  in the TRX-2 Thermal Lattice

\*These sensitivities should sum to zero, but due to numerical precision a small residual remains.

----

Table 7. Total Sensitivities for  $^{28} \delta$ in the TRX-2 Thermal Lattice

Nuclide	Item	$\frac{\delta R/R}{\delta \sigma/\sigma}$
<sup>238</sup> U	σ <sub>f</sub>	0.975
н	σ	-0.749
235U	σ <sub>f</sub>	-0.467
238U	٥	0.284
238U	σs	-0.193
Н	σ	0.173
235U	σ	0.099
Moderator	DB <sup>2</sup>	0.069
0	σs	-0.043
Fuel	DB <sup>2</sup>	0.016
A1	σ <sub>s</sub>	-0.013
A1	σ	0.007
Clad	DB <sup>2</sup>	0.005
0	σc	-0.003
Void	DB <sup>2</sup>	0.002
<sup>235</sup> U	σ <sub>c</sub>	-0.001
238U	-3	-0.001*
2 3 5 J		-0.0002*

\* These sensitivities should sum to zero, but due to numerical precision a small residual remains.

Nuclide	Item	<u>δR/R</u> δσ/σ
2380	σ	0.978
235U	σ <sub>f</sub>	-0.776
Н	ر م	-0.422
Н	σc	0.074
235U	σc	0.039
Moderator	DB <sup>2</sup>	0.012
0	σ	-0.004
AT	σ	0.003
<sup>238</sup> U	σ	0.003
Fuel	DB <sup>2</sup>	0.002
Clad	DB <sup>2</sup>	0.001
235U	$\overline{v}$	-0.0003*
Void	DB <sup>2</sup>	0.0002
A1	٥	-0.0002
0	σc	0.00003
2 3 8 U	σ <sub>f</sub>	-0.00003
2381	<b>~</b> '	-0.00002*
235U	σ	-0.000004

# Table 8. Total Sensitivities for CR in the TRX-2 Thermal Lattice

These sensitivities should sum to zero, but due to numerical precision a small residual remains.

Table	9.	Performanc	e Parameter	Sensitivities	to
	2 3 8 U	Resolved	Resonance P	arameters	

E <sub>o</sub> Parameter	6.67 eV		20.9 eV		36.8 eV		66.15 eV	
	Гn	Гү	<sup>г</sup> n	Γγ	<sup>г</sup> n	Γ <sub>γ</sub>	<sup>г</sup> п	Г
k	-0.018	-0.018	-0.008	-0.008	-0.006	-0.006	-0.002	-0.002
28 <sub>p</sub>	0.149	0.147	0.068	0.066	0.055	0.055	0.020	0.020
25 <sub>8</sub>	0.004	0.004	-0.0007	-0.0007	-0.002	-0.002	0.0004	0.0004 <sup>a</sup>
288	0.013	0.019	0.009	0.009	0.007	0.007	0.003	0.003
CR	0.069	0.068	0.031	0.031	0.026	0.026	0.009	0.009

<sup>a</sup>This value borders on the limit of computational precision.

of interest with respect to the capture and scattering widths of the first four resolved resonances.

The sensitivities given in Appendix B using the SENPRO format are not per unit lethargy but are simply relative sensitivities to the group cross sections. These relative sensitivities are the quantities currently used in numerical computations.

#### DISCUSSION

A study of the energy-dependent profiles can provide valuable insight into the interrelations between the various nuclides in the assembly. Large quantities of structure are readily observable in their profiles. This structure can often be traced back to resonances, thresholds, etc. in the cross sections. However, a more detailed examination of these effects is beyond the scope of this report.

The remainder of this discussion is concerned with a few items which are useful in interpreting the profiles presented here. The total sensitivity is a useful figure-of-merit indicating what reactions are likely to be important for a given response. However, since the total sensitivity is often composed of large positive and negative contributions (particularly for epithermal-to-thermal reaction rate ratios), one must be careful not to be misled by relatively small values of the total sensitivity such as that for the sensitivity of  $28_{\rho}$  to 238U capture. The graphical displays of the sensitivity profiles illustrate the detailed energy dependence.

The shape of the sensitivity profile of k and  ${}^{28}\rho$  to  ${}^{238}U(n,\gamma)$  show the effects of resonance self-shielding. The major portion of the captures (71%) in each resonance occur in the wings where the sensitivity is the highest. The self-shielded resonance peak, where the flux is depressed, has a low sensitivity. Similar behavior can be seen in other profiles.

The reaction rate ratios, in particular the epithermal-to-thermal ratios, have sensitivities to the hydrogen scattering cross section that are near unity, which is much higher than the sensitivities to most of the other nuclides and reaction types. The dominance of the hydrogen scattering sensitivity is due to the importance of hydrogen in the neutron thermalization process.

This study revealed that the total sensitivities are dominated by the contributions made in the thermal energy region. The lack of a fine energy mesh below 0.625 eV was a definite disadvantage during this study and it is highly recommended that future studies of thermal lattices use a fine energy mesh to perform detailed studies in this energy range.

The sensitivity of the performance parameters to the  $^{238}$ U resonance data is dominated by the resolved resonance parameter of the 6.67 eV resonance. This is as expected since approximately 70% of the captures in  $^{238}$ U occur below 100 eV and the majority of these are in the 6.67 eV resonance. It is also interesting to note that the sensitivity to the neutron width  $\Gamma_n$  is almost identical to the sensitivity to the capture width  $\Gamma_{\sim}$ .

The sensitivities quoted as sensitivity to neutron scattering refer to the total scattering cross section (i.e., the sum of elastic, inelastic, etc.). The DB<sup>2</sup> sensitivity components refer to the pseudo-absorption term which was added to the total cross section to account for leakage from the lattice. The only performance parameters that have a relatively high sensitivity to leakage are  $k_{eff}$  and  $2^{28}\delta$ . This is as expected since these are the only two parameters that are affected directly by fission in  $2^{38}$ U. A detailed discussion of this leakage treatment can be found in Ref. 7.

For interpreting the summary tables, it is useful to first calculate the direct effect contribution to the total relative sensitivity. This contribution is that which arises from the explicit dependence of the performance parameter on the nuclear data parameter of interest, which, as discussed in the previous section for a total relative sensitivity, is a scale factor. In calculating the direct effect contribution, the shape of the forward flux (as well as that of the adjoint flux) is assumed to remain unchanged.

The following theorem is especially applicable to the calculation of direct effects to total sensitivities of reaction rate ratios: If the mathematical expression for a response is explicitly homogeneous of degree n in a nuclear data parameter, then the direct effect contribution to the relative sensitivity of that response with respect to the nuclear data

parameter is n. Reaction rate ratios are typically homogeneous of degree +1, -1, or 0 in the scale factors (not the group cross sections). Accordingly, the direct effect contribution to the total sensitivity of a reaction rate ratio is typically +1, -1, or 0.

For example, the ratio of  $^{238}$ U capture to  $^{235}$ U fission is homogeneous of degree 1 in the  $^{238}$ U-capture scale factor, of degree -1 in the  $^{235}$ U-fission scale factor, and of degree 0 in the  $^{235}$ U-capture scale factor. The corresponding direct effect contributions to the total relative sensitivities are 1, -1, and 0, respectively.

The direct effect gives the contributions to the sensitivity coefficients ignoring explicit variations in the forward (and adjoint) flux. Frequently, however, it is just those effects due to flux modifications, the indirect effects, which are most interesting. These indirect effects arise largely through the shielding of one reaction by another (or itself) and include self shielding as well as the shadowing of one resonance by another. There are also resulting modifications to the leakage and to the slowing down.

For those total relative sensitivities of reaction rate ratios with a direct effect contribution of unit magnitude, the indirect effect contribution is frequently of opposite sign to the direct effect contribution, resulting in total relative sensitivities with magnitudes less than unity. These illustrate that a reaction cross section commonly shields itself more than it shields another reaction cross section.

On the other hand, there are several examples for which the magnitude of the total relative sensitivity is greater than the unit contribution given by the direct effect. This illustrates shielding (or another cross section) which is a greater effect than the self shielding. Thus, the relative sensitivity of  $^{28}\rho$  to the scattering cross section of hydrogen is -1.035, which is greater in magnitude than the direct effect (0.0). This shows that an increase in the hydrogen scale factor results in a flux spectrum modification (due to changes in the rate of neutron thermalization) which greatly decreases the epithermal captures relative to the thermal captures. That is, it increases the resonance escape probability.

The above discussion and results apply to sensitivity coefficients for reaction rate ratios, which are generally homogeneous in the nuclear data

scale factors. Generally, they do not apply to sensitivity coefficients for the multiplication factor k because the mathematical expression for k is generally not homogeneous in any scale parameter.

For this and other reasons, it is not convenient to divide ksensitivities into the direct-effect and the indirect-effect contributions. The sensitivity coefficient for k with respect to nuclear data parameter a naturally breaks up into two terms - one from the source and the other from the losses. The expressions for these are given by

$$\frac{a}{k}\frac{dk}{da} = f_a - k \alpha_a , \qquad (3)$$

where  $f_a$  is the fraction of adjoint-weighted fission sources which are of degree 1 in the parameter a and  $\alpha_a$  is the ratio of loss terms of degree 1 in the parameter a to the total adjoint-weighted fission source. The mathematical expressions for these are

$$f_{a} \equiv \frac{(\phi^{*}, B_{a}\phi)}{(\phi^{*}, B\phi)}, \qquad (4)$$

$$^{\alpha}a \equiv \frac{(\phi^{*}, A_{a}\phi)}{(\phi^{*}, B\phi)}, \qquad (5)$$

where  $B_a$  is the part of the fission source proportional to parameter a,  $A_a$  is the loss operator (everything but fission) proportional to parameter a, and  $\phi$  and  $\phi^*$  are the forward and adjoint fluxes, respectively.

Equation (2) immediately shows that the sum of all the sensitivity coefficients with respect to the neutron fission yields is unity. Another relation which is obvious from Eq. (2) is that the capture sensitivities are simply given by -k times the adjoint-weighted nuclide capture to total fission ratio. Only slightly less obvious is that the difference between the yield sensitivity and the corresponding fission reaction sensitivity is simply k times the nuclide capture sensitivity divided by the nuclide capture-to-fission ratio (adjoint weighted). The unity sum rule given above for sensitivity coefficients of k with respect to neutron yield  $\overline{v}$  should be compared with the zero sum rule for sensitivity coefficients of other performance parameters which do not depend explicitly on the multiplication factor or a neutron yield. Such sensitivity coefficients add algebraically to zero when summed over all neutron yields because the resulting change in k (assuming k is not reset) exactly compensates for the changes in the neutron yields.

#### CONCLUSIONS

The sensitivity coefficients are an important tool for the calculation of many quantities of interest in reactor design. A comprehensive set of sensitivity profiles has been determined for integral performance parameters measured in TRX-2. These sensitivities are being used by the Cross Section Evaluation Working Group in providing additional guidance for future evaluations. These sensitivity profiles and summary tables are contained in this report; the data files in SENPRO format are in Appendix B.

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Fig. 1. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to  $^{238}\mbox{U}$   $\overline{\nu}.$ 



Fig. 2. The Energy-Dependent Sensitivity Profile of  $k_{eff}$  in TRX-2 to  $^{238}\text{U}~\sigma$  (n,f).



Fig. 3. The Energy-Dependent Sensitivity Profile of  $k_{eff}$  in TRX-2 to  $^{238}\text{U}$  (n,\_).



Fig. 4. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to  $^{238}\mbox{U}$  (n,n).



Fig. 5. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to  $^{235}\mbox{U}$   $\overline{\nu}_{\bullet}$ 



Fig. 6. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to  $^{235}\mbox{U}$  (n,f).



Fig. 7. The Energy-Dependent Sensitivity Profile of  $k_{eff}$  in TRX-2 to  $^{235}\text{U}$  (n, $_{\gamma}).$ 



Fig. 8. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to  $^{235}\mbox{U}$  (n,n).



Fig. 9. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to Al  $(n,\gamma).$ 



Fig. 10. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to Al (n,n).


Fig. 11. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to H  $(n,_{\gamma}).$ 



Fig. 12. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to H (n,n).



Fig. 13. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to 0  $(n,\gamma).$ 



Fig. 14. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to O (n,n).



Fig. 15. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to  $DB^2$  in the fuel.



Fig. 16. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to  $DB^2$  in the void.



Fig. 17. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to  $DB^2$  in the clad.



Fig. 18. The Energy-Dependent Sensitivity Profile of  $k_{\mbox{eff}}$  in TRX-2 to  $DB^2$  in the moderator.



Fig. 19. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $^{238}U~\overline{\nu}_{\bullet}$ 



Fig. 20. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $^{238}\text{U}$  (n,f).



Fig. 21. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $^{238}U$  (n, $_{\gamma}).$ 



Fig. 22. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $^{238}\text{U}$  (n,n).



Fig. 23. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $^{235}U~\overline{\nu}.$ 

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Fig. 24. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $^{235}U$  (n,f).



Fig. 25. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $^{235}U$  (n, $_{\gamma}).$ 



Fig. 26. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $^{23}5U$  (n,n).



Fig. 27. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to Al (n, $\gamma).$ 



08-17-77EPRI SENS. OF 238U CRPTURE EPI/THR TO AL SCATTERING A= -5.2187E-04

Fig. 28. to Al (n,n). The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2



Fig. 29. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to H (n, $\gamma).$ 



Fig. 30. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to H (n,n).



Fig. 31. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to 0 (n, $_{\gamma}).$ 



Fig. 32. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to 0 (n,n).



Fig. 33. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $DB^2$  in the fuel.



Fig. 34. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $DB^2$  in the void.



Fig. 35. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $DB^2$  in the clad.



Fig. 36. The Energy-Dependent Sensitivity Profile of  $^{28}\rho$  in TRX-2 to  $DB^2$  in the moderator.



Fig. 37. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $^{238}U\ \overline{\nu}.$ 



Fig. 38. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $^{238}\text{U}$  (n,f).



Fig. 39. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $^{238}U$  (n,\_).

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Fig. 40. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $^{238}U$  (n,n).



Fig. 41. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $^{235}\text{U}~\overline{\nu}.$ 



Fig. 42. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $^{235}U$  (n,f).



Fig. 43. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $^{235}U$  (n,\_).



Fig. 44. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $^{235}U$  (n,n).



Fig. 45. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to Al  $(n,\gamma).$ 



Fig. 46. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to Al (n,n).


Fig. 47. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to H (n,\_{\gamma}).



Fig. 48. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to H (n,n).



Fig. 49. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to 0 (n, $_{\gamma}).$ 



Fig. 50. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to 9 (n,n).



Fig. 51. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $DB^2$  in the fuel.



Fig. 52. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $DB^2$  in the void.



Fig. 53. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $DB^2$  in the clad.

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Fig. 54. The Energy-Dependent Sensitivity Profile of  $^{25}\delta$  in TRX-2 to  $DB^2$  in the moderator.



Fig. 55. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $^{238}U~\overline{\nu}.$ 



Fig. 56. The Energy-Dependent Sensitivity Profile of  $^{28} {}_{\delta}$  in TRX-2 to  $^{238} U$  (n,f).



Fig. 57. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $^{238}U$  (n,\_).







Fig. 59. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $^{238}U$  (n,n) inelastic level 21.



Fig. 60. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $^{238}U$  (n,n) inelastic level 22.







Fig. 62. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $^{238}U$  (n,n) inelastic total.



Fig. 63. The Energy-Dependent Sensitivity Profile of  $^{28} \delta$  in TRX-2 to  $^{235} U \ \overline{\nu} \bullet$ 



Fig. 64. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $^{235}U$  (n,f).



Fig. 65. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $^{235}U$  (n, $_{\gamma}).$ 



Fig. 66. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $^{23}5U$  (n,n).



Fig. 67. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to Al (n, $_{\gamma}).$ 



Fig. 68. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to Al (n,n).



Fig. 69. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to H  $(n,_{\Upsilon}).$ 



Fig. 70. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to H (n,n).



Fig. 71. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to 0  $(n,\gamma).$ 



Fig. 72. The Energy-Dependent Sensitivity Profile of  $^{28} \delta$  in TRX-2 to 0 (n,n).



Fig. 73. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $DB^2$  in the fuel.



Fig. 74. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $DB^2$  in the void.



Fig. 75. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $DB^2$  in the clad.



Fig. 76. The Energy-Dependent Sensitivity Profile of  $^{28}\delta$  in TRX-2 to  $DB^2$  in the moderator.



Fig. 77. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $^{238}\text{U}~\overline{\nu}\text{.}$ 



Fig. 78. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $^{238}\text{U}$  (n,f).



Fig. 79. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $^{238}\text{U}$   $(n,\gamma).$ 



Fig. 80. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $^{2\,3\,8}\text{U}$  (n,n).



Fig. 81. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $^{235}\text{U}~\overline{\nu}.$ 



Fig. 82. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $^{2\,3\,5}\text{U}$  (n,f).


Fig. 83. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $^{2\,3\,5}U$   $(n,_{\gamma}).$ 



Fig. 84. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $^{2\,3\,5}\text{U}$  (n,n).



Fig. 85. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to Al  $(n,\gamma).$ 



Fig. 86. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to Al (n,n).



Fig. 87. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to H  $(n,\gamma).$ 



Fig. 88. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to H (n,n).



Fig. 89. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to 0  $(n,\gamma).$ 



Fig. 90. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to 0 (n,n).



Fig. 91. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $\mathsf{DB}^2$  in the fuel.



Fig. 92. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $\mathsf{DB}^2$  in the void.



Fig. 93. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $\mathsf{DB}^2$  in the clad.



Fig. 94. The Energy-Dependent Sensitivity Profile of CR in TRX-2 to  $\mathsf{DB}^2$  in the moderator.

## APPENDIX A

The Format for Standard Interface File SENPRO for Group-Dependent Sensitivity Coefficients

C\*\*\*\*\*\*\*\*\* с REVISED 05/12/76 С CF SENFRO CE THIS FILE CONTAINS SENSITIVITY \_ CE COEFFICIENTS BY GROUP AS A FUNCTION OF CE MATERIAL - REACTION TYPE, ASSEMBLY, AND RESPONSE С **EIVISION BY GROUP LETHARGY WIDTHS MAY BE** -CN NECESSARY FOR MIANINGPUL GRAPHIC DISPLAY. INCLUDEE ARE, TOTAL SENSITIVITY COEFFICIENTS BY GROUP SUMMED OVER EFFECT TYPES, ZONES, AND CN \_ CN CN CN SCATTEBING ORDERS. ON OPTION, PARTIAL \_ COEFFICIENTS MAY ALSO BE REPRESENTED AS VARIOUS -CN CN COMBINATIONS OF DIRECT AND INDIRECT EFFECT, -ZONE, AND SCATTERING ORDER CN -С A FILE SUCH AS THIS IS NEEDED BY CENL - FORSS CE -С J. L. LUCIUS С С с \*\*\*\*\*\*\*\* C\*\* C-----FILE STRUCTURE СS cs RECOFD TYPE PRESENT IF сs ---------------------сs ===== FILE IDENTIFICATION ALWAYS -СS FILE CONTROL ALWAYS сs NEUTECN GROUP BOUNDARIES NNGRUP\_GT\_0 сs GAMMA GROUP BOUNDARIES \*\*\*\*\*(REPEAT FOR ALL MATERIAL -FEACTION PAIRS, MAT - MT) MAT - MT CONTROL cs NGGRUP.GT.O CS CS ALWAYS CS RESPONSE DESCRIPTION сs \* NWRD\_GT\_0 NZDEN.GT.O cs ZONE DENSITIES сs \* HCLLEBITH DESCRIPTION OF TOTAL ALWAYS cs \* SENSITIVITY COEFFICIENTS сs \* TOTAL SENSIVITITY COFFFICIENTS ALWAYS BY GROUP SUMMED OVER, TYPE, ZONE, AND SCATTEFING ORDER сs cs PARTIAL CONTROL \*\*\*\*\* (REPEAT FOR ALL PARTIAL NPART. GT. 0 cs CS cs \* \* COEFFICIENT SETS) \* HOLLEBITH DESCRIPTION OF NPART.GT.O СS \* сs \* PARTIAL SET \* \_ CS PARTIAL COEFFICIENTS BY GROUP NPART. GT. 0 сs \*\*\*\*\* С C-C-CR FILE IDENTIFICATION C H NAME, (HUSE(I), I= 1, 2), IVERS 1+3\*MULT CL CW \_ С 

 FORMAT(11H OV SENPRC , A6, 1H\*, 2A6, 1H\*, 16)

 HNAME
 HCLLERITH FILE NAME-SENPRO- (A6)

 HUSE
 ECLLERITH USER IDENTIFICATION (A6)

 СВ СĽ CD FILE VERSION NUMBER \_ IVERS CE 1 - A6 IS SINGLE PRECISION WORD 2 - A6 IS DOUBLE PRECISION WORD \_ MULT CD CD C-C----CR FILE CONTROL -С NGBOUP, NNGBUP, NGGRUF, NMAT, MAXCRD, MZONE CL C CW 6 -C CE FORMAT(4H 1D ,616) -NUMBER OF ENERGY GROUPS NGROUF CD NUMBER OF NEUTRON GROUPS NNGFP CC СĽ NUMBER OF GAMMA GROUPS NGGFUP CD NMAT NUMBER OF MAT- MT PAIRS \_ MAXIMUM SCATTERING ORDER MAXOFE СD \_ CD MZONF MAXIMUM NUMBER CF ZONES c-\_\_\_\_

C-CR NEUTRON GROUP ECUNDARIES С CL (GPBN(J), J=1, NNGRP), ENMIN с сс PRESENT IF NNGFP.GT.O CR NNGRE+1 С FCRMAT(4H 2D5E12\_4/(6E12\_4))GFBN(J)MAXIMUM ENERGY ECUND OF NEUTRON GROUP(J) (EV)ENMINFINIMUM ENERGY OF NEUTRON ENEBGY RANGE СВ СĒ CD с C---CR GAMMA GECUP BCUNDARIES С (GPBG(J), J=1, NGGBP), EGMIN CL С PRESENT IF NGGRP.GT.0 сс CW NGGRP+1 ¢ CE FORMAT(4H 3D .5E12.4/(6E12.4)) GPEG (J) PAXIMUM ENERGY ECUND OF GAMMA GROUP(J) (EV) MINIMUM ENERGY OF GAMMA ENERGY RANGE CE CD EGMIN C-C---CR MAT - MT CONTROL С CL IASE, IRESP, MATID, MT, NZONE, ISTC, NPART, NWED, NZDEN, MATRIX, NTRN, NTRD C₩ 12 с FORMAT (4H 4D , 1116/16) CE с CD IASB ASSEMBLY IDENTIFICATION CD REFERENCE ENL 19302 (ENDF-202) F-1 CD IRESP FFSPONSE IDENTIFICATION 1 - K 2 - EREFDING RATIO CC CC 3 - WORTH CD 4 - REACTION RATE RATIO 5 - OTHER CD СĽ CD MATID MATERIAL IDENTIFICATION CE MT **BEACTION TYPE IDENTIFICATION** NZONE CD NUMBER OF ZONES SCATTERING ORDER FOR TOTAL COEFFICIENTS CD ISTC NPART NUMBER OF PARTIAL SETS NUMBER CF HOLLEFITH(A6) WORDS USED TO DESCRIBE CD CD NWRD CD THE RESPONSE CE NZDEN ZONE DENSITY OPTION 0 - ZONE DENSITIES ARE CMITTED 1 - ZONE DENSITIES ARE PRESENT CD CĒ \_ CD MATRIX FESERVED CD NTRN BESERVED -CD NTRD FESERVED C٠ с-CR RESPONSE DESCRIPTION С сL (PDES(I), I=1, NWRD) ¢ сс PRESENT IF NWRD.GT.O c CW NWRD\*MULT С FORMAT (4H 5D , 1H\*, 11A6/(11A6)) СE С сp ARRAY CONTAINING HOLLERITH DESCRIPTION OF RDES (I) CD RESPONSE C---C---CB ZONE DENSITIES С CL (2DEN (J) , J=1, NZONE) \_ С сc PRESENT IF NZDEN.EQ.1 С ĊW NZONE CĐ FORMAT(4H 6D ,5F12.4/(6E12.4)) с C D ZDEN ZONE DENSITIES C---

C---HOLLERITH DESCRIPTION OF TOTAL SENSITIVITY COEFFICIENTS CR С CL (HOL(I),I=1,11) Ċ₩ 11\*MULT c. FORMAT(4H 7D ,1H\*,11A6,1H\*) СВ c---C-----CR TOTAL SENSITIVITY COEFFICIENTS BY GROUP С (TOTS (J), J=1, NGROUP) CL C CW NGECUP \_ С CP FCRMAT(4H 8D ,5E12.4/(6E12.4)) С SENSITIVITY COFFFICIENTS CD TCTS C---C---PARTIAL CONTROL CE С (ITYPE(I), IZON1(I), IZCN2(I), ISCAT(I), I=1, NPAPT) CL С сс PRESENT IF NPARI.GI.O C C₩ 4\*NPART С FORMAT(4H 9D ,416/(416)) СP С \_ CĽ ITYPE(I) TYPE IDENTIFICATION 1 - H1 DIRICT EFFECT (H1DE) 2 - H2 DIRICT EFFECT (H2DE) CC СĽ 3 - FORWAFE FLUX PERTURBATION (FFP)
 4 - ADJOINT FLUX PERTURBATION (AFP) C٢ СĽ 5 - H1DE+H2CE+FFP СĈ 6 - HIDE+H2CE+FFP+AFP CĽ IZON1(I) LOWER DO LIMITEF FOR ZONE SUMMATION IZON2(T) UFPER CO LIMITEF FOR ZONE SUMMATION ISCAT(I) SCATTERING CRDEF SPECIFICATION CD \_ СĽ CE LF.ISTC - SCATTERING ORDER GT.ISTC - SUM OVEP ALL SCATTERING ORDERS ----СĽ CD C---\_\_\_\_ ----\_\_\_\_ ----C-----HOLLERITH DESCRIPTION OF PARTIAL SET CR С (HOLP(1), T=1, 11)CL PRESENT IF NPART.GT.O сс \_ C 11\*MULT ----C₩ -

C -----CR PARTIAL SENSITIVITY COFFFICIENTS BY GROUP -С CL (PARTS(J), J=1, NGROUE)с сс PRESENT IF NPARI.GI.O С ČW NGROUP C FORMAT(4H11D \_5E12.4/(6E12.4)) -CE С PARTS SENSITIVITY COEFFICIENTS C.D. \_ \_ \_ \_ \_ \_ \_ \_ \_ C--

C C E

C--

FOEMAT(4H10D ,1H\*,11A6,1H\*)

## APPENDIX B

The Sensitivity Coefficients for the Profiles of Figures 1-94 in SENPRO Format

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4C	107	1	1262	452	4	3	0	8	0	0	0
5 D J	0 *******	<b>TC M</b>		CITTON	RACTO	ROD	<b></b>				
70	FOFSS, EI	PRI,	SENS. O	F K TO	2380 1	UEAR	( K X - 2	-	λ= 7	. 4977 E-	-02*
6D	7.2882E-	0.3	1.6012E	-02 2.	7921E-	-02 2.	.2216E-	02 1.	4566E-	03	
6.	5324E-05	4-46	77E-06	1.4900	)E-C6	8.536	9E-07	5-8040	E-07	4.60961	E-07
7.	4333E-07	8.20	95E-07	6 2674	4E-C7	2.139	4E-08 8F-10	3.5830	2-13 P-11	3.8881	2-12 P-11
1.	8160E-11	1.09	1 EE-12	3-1299	9E-12	1.191	38-12	1.6241	e−12	1.7113	E-12
9_0	600 1E- 12	1.47	5 EE-12	2.924	2E-12	2.657	3E-12	2.6739	E-11	1.7260	E-12
1.	1211E-12	1.23	74E-12	3.3919	9E-13	7.980	0E-14	9.3244	E-15	7.11981	E-16
6.	7359E-16	2.81	25E-16	2.7880	)E-16	2.788	712-16	2.7995	E-16 E-12	2-83081	8-16 8-12
5.	69776-10 45386-13	1_08	278-12	2-063	78-12 78-12	1.572	38-14 18-12	3. 31041	E-13 R-11	5.86881	6-13 R-11
4.	5715E-12	2.60	19E-12	1.439	7E-12	8.484	3E-13	5.2602	E-13	1.0892	E-13
4_0	6786E-15	2.39	27E-15	5.496	3E-16	5.286	6E-16	5.1739	E-16	5.2814	E-16
5-	5243E-16	3.05	01E-15	7.031	3E-15	3.259	48-14	1.2499	E-13 E-11	7.6409	E-13
5-1	2898E-12	3.39	45E-12	1.7692	2E-12	5-039	2E-12 5E-13	3.7880	E-14	3.6733	E-12 E-15
2.	3840E-15	5.48	47E-16	5.288	5E-16	5.283	4E-16	5.2786	e-16	5.4558	E-16
2.	3723E-15	3.48	68E-15	6.8119	9E-15	2.054	4E-13	1.0748	E-12	2.0557	E-12
1.	4797E-12 7015E-11	2.10	85E-12	5 9595 6 4254	9E-12 SP-12	1.93/	2E-10	2.0557	E-11 E-12	7 35851	2-17 2-14
3.1	9094E-15	3.19	86E-15	1.248	2E-15	1.191	0E-15	1.1876	E-12 E-15	1.0551	2-15
1.	0873E-15	2.77	78E-15	3.336	9E-15	6.391	1E-14	1.8906	E-12	4.5954	8-12
4_	5408E-12	1.14	23E-11	3.269	1E-11	1.268	5E-09	3.9146	E-10	0.0	
	107		• 16 2	10	"	2	0	0	0	0	0
40	107	ł	1262	16	4	3	0	8	U	U	U
5 D	*RESPONSE	ISM	UITIPLI	CATION	FACTO	R FOR	TRX-2	*			
7 D	*POFSS, E	PRI,	SENS. O	FRTO	2380	FISSIO	N	<b>a</b> a a	A= 4	1.7880E	-02*
ED a	4.8482E	-03	1.0634E	-02 1	-7736E 28-07	-02 1 4 820	- 3/23E-	-02 8. 3.2474	9013E- 8-07	-04 2.5714	F-07
4.	1324E-07	4_54	73E-07	4.053	3E-07	1_181	7E-08	1.9745	E-13	2.1355	E-12
1.	7000E-10	5.90	74E-07	3.400	9E-06	6.856	1E-11	4.5128	E-11	3.8899	E-11
9_	7003E-12	5.79	7CE-13	1.645	4E-12	6.324	9E-13	8.5803	E-13	9_6844	E-13
4.	9619E-12	9.76	252-13	1.581	68-12 58-13	6 815	35-12	7 9400	E-11 8-15	9.9/90	E-13 F-16
5.	7026E-16	2.37	86E-16	2.356	1E-16	2.354	8E-16	2.3627	E-16	2.3872	E-16
7.	4939E-16	7.91	53E-16	3.134	4E-15	1.313	5E-14	4.7381	E-13	5.4450	E-13
3.	3764E-13	6.46	686E-13	1.149	5E-12	8.297	8E-13	1.6847	E-11	3.0080	E-11
2	5932E-12	1.70	182E-12 1458-15	1.089	5E-12	4 675	28-15	4. 7954	E-13 F-16	4.6514	E-13 E-16
4_	8562E-16	2 6	05E-15	6.097	2E-15	2.823	3E-14	1.0944	E-13	6.4294	E-13
9.	5742E-13	8.34	194E-13	9.129	7E-13	1.474	8E-12	4.9962	E-11	3.2693	E-12
3.	1412E-12	2.34	170E-12	1.478	6E-12	4.781	9E-13	3.6777	E-14	3.5410	E-15
2.	28328-15	3.20	1002-10 154F-15	6-425	1E-16	1.968	2E-10	9.3885	E-10 F-13	1_4692	E-12
9.	570 IE-13	1.3	310F-12	3.298	0E-12	9.726	6E-11	1.0523	E-11	3.8957	E-11
1.	5370E-11	9.4	169E-12	4.735	8E-12	2.245	3E-12	1.0287	E-12	7.3165	E-14
3.	8825E-15	3.1	738E-15	1.237	98-15	1.180	8E-15	1.1770	E→15	1.0450	E-15
3.	10628-10	7.0	2745-12	1.796	6E-11	6.137	3E-10	1.8267	E-10	0_0	
•••											
									_	_	_
4 D	107	1	1262	102	4	3	0	8	0	0	0
50	*RESPONSI	IS	NUITIPL		PACTO	R FOR	ŤRX-2	*			
7 D	*FOFSS, 1	PRI,	SENS.	OF K TO	2380	CAPTU	RE		A= -	2.65411	E-01*
80	-1.1266	3-05	-1.01921	E-04 -5	5.22C8E	-04 -	1.32828	-03 -2.	.1794E	-03	(P_^3
-2.	. 1218E-U3	-1.4	1858-03	-2,358	295-03 518-03	-1-20.	16E-03	-2.849	7E-03	-3_248	1E-03
- 3.	1464E-03	-3.7	766E-03	-3.769	90E-C3	- 3. 28	03E-03	-3.957	5E-03	-5. 191	5E-03
-9.	.4993E-04	-2.4	221E-05	-2.122	28E-05	-2.62	84E-05	-9.592	5E-06	-2.5350	0E-04
-4.	2461E-05	-3.3	232E-05	-2.61	97E-C5	-1.18	12E-03	-2.667	5E-04	-7.9429	9E-05
- 6.	- 77328-05	-7_6	4858-04	-7,69	39E-04	-7.74	85E-06	-7.798	0E-06	-7.838	6E-06
-2	4017E-C5	-2.3	60CE-05	-6-94	59E-05	-1.08	50E-04	-4.054	3E-04	-2.569	3E-04
- 1	.0549E-04	-1.3	125E-04	-1.31	53E-C4	-8.67	46E-05	-2.699	6E-04	-7.119	2E-04
- 3.	-407CE-04	-3.2	150E-04	-2-45	278-04	-1.78	112-04	-1-564	0 E-04	-1.359	3E-04
- 2	_3395E-05	-9-7	2901-05	-1_01	66E-04	-1-31	56E-04	- 1- 504	6E-04	-4_041	8E-04
-4	.5872E-04	-2.6	145E-04	-2.40	23E-04	- 3, 37	37E-04	-2.197	1E-03	-3.468	5E-04
-5	.3290E-04	-5.8	394E-04	-4.25	48E-04	-1.43	028-04	-5.222	5E-05	-2-450	0E-05
-2	.7989E-05	-7-9	759E-06	-8.10	88E-06	-8.37	62E-06	-8.467	2E-06	-8.710	9E-06
-3.	-4018E-05	-3.5	2201-05	-5.50	338-05 138-04	- 1.04	488-04 528-03	-5_411	0 E-04	-1.275	42-03
- 1	.3181E-03	-1-5	718E-03	-1.14	00E-03	-4,97	17E-04	-1.475	6E-04	-1.970	7E-05
-4	.3657E-06	-4.8	163E-06	-2.16	60E-Ç6	-2.19	04E-06	-2.324	3E-06	-2.193	7E-06
- 2	. 3523E-06	-5-9	598E-06	-6-49	15E-06	-2.74	83E-05	-1.947	58-04	-9.710	7E-04
-1	_ 898/E-04	- 1 - 4	0156-01	- Z_ 091	046-01	-8-45	∠ot-U1	- 1.024	35-03	-1. /20	1.0-0.1

4 D	107	1	1262	904	4	3	0	8	0	0	0
50 70 80	*RESPONSI *EPRI SEI 5.86491	E IS NS. 0 E-04	MUITIPLE F K TO -5.23361	CATION 2380 S 2404 -7	PACT CATTE 5241	DR FOR RING E-04 -9	TRX-2	* E-05 8.	A= - 2454	-1.8496 E-04	E-03*
3. 4. 4.	3836E-06 3994E-06 4317E-06	7.0 1.2 7.0 2.3	338E-05 365E-06 449E-06	2.906 3.816 7.807 -3.427	4E-C5 5E-06 5E-C6 5E-C6	2.066 5.082 4.261 -4.088	5E-05 3E-06 6E-06 6E-06	3.176 6.189 4.992 -2.138	0E-06 6E-06 2E-06 0E-05	2.183 8.857 1.591 3.595	0E-06 5E-06 7E-04 9E-05
-1. -1. 1. 2.	3967E-05 7648E-04 7725E-05 3866E-05	-1_2 -3_1 7_6 2_3	587E-05 085E-04 375E-06 375E-05	-1-581 -1-843 7-682 6-817	6E-C4 5E-C5 2E-06 4E-05	1.478 1.035 7.726	7E-04 5E-04 1E-06 0E-04	- 1. 299 1. 149 7. 769	2E-04 4E-04 4E-06	-1.389 1.745 7.803	6E-04 1E-05 4E-06
-1.	2040E-06 3716E-04 4302E-05	1.9 -3.2 7.1	577E-06 96EE-04 143E-05	7.044 -2.799 2.203	3E-06 2E-04 3E-05	1.272 -1.669 2.272	9E-05 4E-04 0E-05	-4.853 -3.712 2.296	6E-06 4E-05 7E-05	-4.865 -1.322 1.265 2.323	3E-06 4E-04 5E-04 0E-05
9. -1. 2.	3587E-06 7335E-04 9070E-05	9.5 -3.6 -2.6 8.1	083E-05 301E-06 345E-04 182E-06	9-438 -2-527 -1-879 8-176	2E-05 4E-C6 3E-C4 6E-06	1.123 2.161 -2.783 8.370	4E-04 3E-06 0E-05 7E-06	1.100 -4.888 4.449 8.384	1E-04 0E-05 3E-05 6E-06	1.069 -7.763 2.634 8.545	2E-04 5E-05 2E-05
	258 1E- 05 584 6E- 07 452 9E- 05 658 5E- 06	3.2 4.2 -1.1	331E-05 63CE-06 638E-04 834E-06	3.215 1.499 -7.412	5E-05 0E-05 6E-05	6.819 -9.136 -1.275	6E-05 1E-06 3E-05	-5.218 2.115 2.742	0E-05 2E-05 5E-05	-8.722 -7.057 1.408	2E-06 5E-05 7E-05
2.	1439E-06 1333E-05	5.1 3.4	802E-06 203E-05	5.293 4.841	6E-06 6E-06 6E-05	2.015 5.052	3E-05 2E-05	-4.561 1.234	2E-05 2E-04	2.060 2.126 -1.426	82-06 3E-05 8E-03
4C	107 0	1	1261	452	4	3	0	8	0	0	0
50 70 80	*RESPONSE *FORSS, E	IS PRI,	SENS. C	CATION F K TO	FACTO 2350	NUBAR	TRX-2	*	A=	9.25001	E-01*
7.	0269E-04	5.3	4.2167E 723E-04	4.375	.3905E 4E-C4	-04 9. 3.648	-1095E 4E-04	-04 8. 3.2575	.3198∄ }e−04	2.934	1E-04
7.	908 IE-04 69 15E-04	9.4	474E-04 78CE-04	3.372	9E-04 1E-C3	3.921 1.485	9E-04 4E-03	4.9770	)E-04	5.922	4E-04
5. 3.	0195E-04 1091E-04	3.2	176E-C5 422E-05	9.392	7E-05	3.634	0E-05 7E-05	5.0046	E-05	5.3470	6E-05
2.	2892E-06	4.7	216E-06	1.525	7E-06	1.522	0E-06	1.4489	E-07	3.515	1E-09
3.	4523E-C9	3.6	742E-09	1.635	7E-C8	2.201	6E-05	8.3429	E-09	2.7838	9E-09 BE-06
3.	6244E-06 4645E-04	4.5 5.2	198E-06 361E-05	4.624	7E-05 2E-05	4.658	1E-05 BE-06	1.6885	E-03	2.4890	)E-03
3.	7966E-08	2.0	376E-C8	4-839	2E-05	4.731	6E-09	4.7171	E-09	4.9115	5E-09
3.	3597E-05	6.79	905E-05	3.984	48-04	4.660	BE-04	1.5869	E-06	1.2096	5E-05 3E-04
1.	0251E-C5 0875E-08	4_30	781E-06 338E-08	1.120	58-05 38-(8	3.952	5E-05	9.4717	E-06	2.2436	5E-07
3_	5759E-CE	4.4(	042E-08	7.984	0E-08	5.387	1E-06	2.1209	E-05	2.6790	)E-09
4_	4824E-05	4.04	235E-05 182E-05	8.558	7E-04 7E-04	4.886	5E-03 9E-05	2.4976	E-04	4-2364	E-03
8. 2	1826E-09	6.80	27E-09	2.695	5E-C9	2.601	2E-09	2.6231	E-09	2_3577	E-09
9	7730E-05	1.39	974E-04	2.071	2E-04	7.829	9E-07 7E-03	3.7909	E-05	1.8904	E-04
4D	107 0	1	1261	18	4	3	0	8	0	0	0
50 70 -	*RESPONSE *FORSS, E	IS PRI,	SENS. O	CATION F K TO	FAC10 2350	R FOR T	rrx-2	*	<b>1</b> =	4. 29611	-01#
8D 4	1.1121E	-04	2_8048E	-04 5.	.34COE	-04 5.	6732E	-04 5.	1544E	-04	2-01+
1.	6684E-04	1.68	865E-04	1.928	4E+04	2.122	2E-04 1E-04	1.8803	E-04	1.6894	12-04 12-04
4.	3490E-04 7778E-04	5.36	511E-04	8.153	6E-04	8.278	2E-04	1.2157	E-03	1.1699	E-03
1.	6690E-04	2.69	963E-05	5.044	9E-05	4.2920	)E-05	5.5001	E-05 E-04	3.1222	2E-05 5E-06
2.	4666E-06 5753E-09	3.40	020E-06	1-248	78-06 38-10	1.3090	)E-06	1.2427	E-07	3-0032	2E-09
2-	9301E-09	3.11	18E-09	1.3818	80-3E	1_854	E-07	5.400/ 6.6625	£-10 E-06	9-4654 1-8642	E-10 E-06
2-0	0312E-06 0272E-04	2.77	156E-06	2.6612	28-05	2.6126	6E-05	8.9349	E-04	1.3257	E-03
3.4	44872-08	1.82	66E-08	4.313	5E-05	4.2069	9E-09	4.1853	E-09	4.3498	E-07
4.0	5308E-09 5270E-05	2.66	94E-C8	6.5792	2E-C8	3.2766	E-07	1.3976	E-06	1.0257	E-05
6.2	2594E-06	3.08	2 SE-06	9.4409	E-06	3.7589	E-05	9.2072	E-03 E-06	2.1661	E-05 E-07
7.7	1594E-08	1.32	38E-08	1.1507	E-C8	1.0457	E-08	9-5965	E-09	9-1490	E-09
1.7	7263E-05	2.02	99E-05	4.8939	E-04	2.5541	E-03	1.3289	E-05 E-04	1.9463	E-05
2.5	512E-05	2.57	52E-05	1.4732	E-04	2.3474	E-05	3-3948	E-06	1.6715	E-07
2.4	432E-09	6.40	53E-09	8.0208	E-09	1.9928	E-07	2.0005	E-09 E-05	2.3359	E-09 E-04
6.8	8130E-05	8.81	88E-05	1.1768	E-04	3,9553	E-03	2.4325	E-03	4.0075	E-01

4D	107	1	1261	102	4	3	0	8	0	0	0
5 D	0 *D2 500 855	2 7 5					<b>TPY-</b> 2	*			
70	*FOBSS, 1	EPRI,	SENS. (	OF K TO	2350	CAPTUR	E		A= •	-9.2418	E-02*
8D	-4.37721	2-07	-2.78448	3-06 -9	3.28841	8-06 -1	72221	8-05 -2.	8075	E-05	
-3.	6010E-05	-3-6	193E-05	-3_802	22E-05	-3.759	9E~05	-3.9125	E-05	-4-008	92-05
- 4.	2851R-04	-2.1	0778-04	-2-25	68-05	-2.875	25-03	-4.8155	E-03 ₽-04	-9.420	22-05
-1.	78998-04	-1.0	09CE-05	-2.85	54E-C5	-1.048	8E-05	-1.4141	E-05	-1.347	7E-04
-7.	8601E-05	-1_1	128E-05	-1.897	72B-05	-7.245	4E-06	- 1. 5688	E-04	-1.694	7E-06
-3.	13298-07	-8.5	878E-07	-2.214	19E-C7	-2.066	2E-07	-1.9738	E-08	-4.166	8E-10
- 3.	5198E-10	-1-3	787E-10	-1.320	01E-10	-1.296	2E-10	-1.2747	E-10	-1.272	9E-10
-2-	44258-07	-1.1	049F-06	-3.906	55E-C5	-3.031	0E-06	-3.1938	E-04	-5.813	4E-07 1E-04
-8.	4634E-05	-3.3	757E-06	-7.789	95E-07	-1.540	4E-07	-4-9380	E-08	-8.780	0E-09
-5.	1173E-10	-3-0	614E-10	-7.542	26E-11	-7.479	3E-11	-7.5330	E-11	-7.907	7E-11
-8-	4991E-11	-4-9	914E-10	-1.303	13E-09	-6-629	68-09	-2.6365	E-08	-2.670	8E-07
-3.	8741E+CE	-1.9	367E-06	-1-749	92E-06	-2-264	2E-06	-3-3415	E-04	-1-013	3E-05
-4.	4887E-09	-8.5	792E-10	-7.818	34E-10	-7.388	2E-10	-7.0078	E-10	-6.902	7E-10
-2-	7322E-09	-3-6	612E-09	-6.502	23E-09	-2.054	9E-07	-1.8623	E-06	-3.819	3E-06
-2-	9879E-06	-4.6	2281-06	-2.04	138-04	-2.098	0E-03	-4-7225	E-05	-7.202	0E-04
-8	2635E-11	-7_9	395E-11	-3_416	57E-11	-3.445	6E-11	-3.6983	E-11	-3.600	9E-11
-4.	0541E-11	-1.1	624E-10	-1.63	8E-10	-3.900	8E-09	-3.0273	E-06	-9.560	5E-05
- 1.	7822F-05	-1-8	929E-05	-2.14	78E-C5	-1.808	0E-03	-2:6882	E-04	-8.172	5E-02
						_					
4 D	107	1	1261	904	4	3	0	8	0	0	0
5 D	*RESPONSE	IS	MULTIPLI	CATION	FACTO	R FOR	r R X - 2	. *			
7 D	*EPRI SEN	IS. 0	FKTO	2350 5	CATTER	ING			A= -	2.21061	3-05*
60	3.18608	2-06	-4.0349E		1.7493E	-06 -3.	.9734E	-06 6.	57711	3-06	
з. Ц	21052-06	-1-2	409E-08	4.427	6E-08	6.036	UE-07	8.1314	E-08	1. 2260	)E-08
6	6141E-08	1.6	208E-07	1.645	6E-(7	6.772	7E-08	-2.4759	E-10	5.8476	5E-07
1.	3547E-07	7.1	553E-C8	-9_478	9E-08	-1.116	3E-C7	-5.2585	E-07	8.521	72-07
-2.	7824E-07	-2.3	814E-07	-2-806	7E-C6	2_488	3E-06	-1.2362	E-06	-1.1408	3E-06
1.	23688-09	5_2	673F-10	5.274	12E-00	5-327	5E-10	5.4085	E-00 E-10	5-5228	3E-10
1.	7712E-09	1.9	253E-09	8.080	9E-09	3.758	8E-08	1.1708	E-06	6.788	6E-07
З.	1614E-07	5.4	13CE-07	3,933	5E-07	4.660	2E-07	-8.2134	E-08	-1_2013	3E-06
~1.	1142E-06	-1.4	337E-06	-9_013	3E-07	-3-826	3E-07	-4.4464	E-08	4.752	1E-08
6.	5533E-10	3.8	1158-09	9,449	28-09	4.793	38-08	2-0268	E-10 E-07	1.1188	3E-10 3E-06
1.	1371E-06	1.6	124E-06	3.110	7E-06	4.871	1E-07	-5.3130	E-07	-7.1099	9E-07
-1.	4112E-06	-1.7	473E-06	-9-229	5E-07	-1-057	2E- C7	3.1075	E-08	1.896	3E-09
1.	26365-09	4.0	694E-10	4.118	2E-10	4.295	JE-10	4.4673	E-10 E-06	4.793	5E-10 NR-07
5.	1151E-07	8.8	375E-07	3.078	16E-06	-1.352	1E-07	3.3278	E-07	-8.179	9E-07
-9.	3507E-07	-1.1	66E-06	-4.413	9E-07	-6.363	5E-08	1.2635	E-07	1.466	4E-08
1.	9219E-05	1.8	082E-09	7.60	14E- 10	7.524	6E-10	7.9854	E-10	7-540	0E-10
8. 8	1584E-10	2.2	27(E-09	2.870	78-05 78-06	5 237	8E-08	1.7063	E-05	1.336	) 2-06 5 2-05
0.	04065-07	207	0372-07	1.0.74		J. 2. J /	3E- Ó I	J. U. Z. I 4	E-01	- Je JJ(	15-01
4D	107	1	1193	102	4	3	0	8	0	0	0
5 D	*RESPONSI	E IS	MUITIPL	CATIO	N FACTO	OR FOR	TRX-2	*			
7D	*EPRI SE	Ns. o	FKTO	AL CA	TURE				λ= -	-7.2670	E-03*
80	-9.09471	E-05	-6.0774]	E-05 -	1.2393	2-05 -1	-05171	E-06 -1.	0910	E-06	<b>FF A</b> (
- 1.	436 SE-05	-5.0	738E-06	-5.310	50E-06	-2.253	8E-05	-7-8249	E-06	-5-173	3E-06
-3.	.600 3E-06	-2.8	732E-06	-3.20	55E-C6	-3.748	2E-06	-4.3443	E-06	-4.728	2E-06
-1.	.0991E-06	-7.4	115E-08	-2.16	35E-07	-8.270	7E-08	-1.1299	E-07	-1.175	4E-07
-6.	-7974E-07	-1.0	433E-07	-2.03	05E-07	-1.822	2E-07	-1.9752	E-06	-1.238	4E-07
-1.	6796E-09	-7-1	13926-00	-7-17	105-L8 758-10	-7.186	05-08 6E-10	-7. 1930	E-08	-1.674	0E-09 1R-10
-2	.1812E-09	-2.1	149E-09	-6.12	50E-09	-9.666	8E-09	-4.5805	E-08	-5.652	8E-08
- 3.	8696E-08	-7_7	2521-08	-1-539	94E-C7	-1.155	8 <b>E</b> - C7	-2.5938	E-06	-4.750	8E-06
-3.	.7526E-07	-2.0	38CE-07	-1-10	598-C7	-6.820	5E-08	-5.7525	E-08	-3.813	8E-08
- 1.	. 1133E-08	-1-1	137 12-08 1860F-08	-3.34	148-09 108-09	-3-308	15-09	-3-0489	E-09	-3.392	02-09 27-09
-1.	.0088E-07	-9.0	803E-08	-1.28	04E-C7	-2.376	2E-07	-8.3862	E-06	-5.161	8E-07
-4.	4305E-07	-2.7	440E-07	-1_46	92E-07	-6.984	0E-08	-3.0515	E-08	-1. 123	5E-08
-1.	1368E-08	-3.0	573F-09	-3.03	83E-09	-3.075	9E-09	-3.0561	E-09	-3.094	4E-09
- 1. - 1	. +//5E-08 . 72468-07	1_2 1_8	2035E-08	-1-32	96F-07	-5.948	78-08	-9.2138	E-08	-1.663	1E-07
-2	4777E-C6	-1.3	327 1E-06	-5.77	18E-C7	-2.504	4E-07	-1,9425	E-07	-9.873	22-08
-1.	.856EE-08	-1_8	3550E-08	-7.95	35E-09	-7.870	4E-09	-8.0313	E-09	-6.354	5E-09
-6.	4228E-09	-1-5	224E-08	-1-540	04E-08	-8-433	6E-08	-2.6583	E-07	-4.327	6E-07
		F U		- 3- 97		- 1. // 4	112-114				

4D 107	1 1193	904	4	3	0	8	0	0	0
0									
5D RESPON	SE IS MULTIP	LICATION	FACTO	OR FOR	TRX-2	*			
7D *EPRI S	ENS. OF K TO	AL SCA	TTERI	ſG			A =	-1.1165	E-04 *
8D -91996	SE-05 -2.258	6E-05 -7	.2315	E-06 -6	-9523	E-06 5.	.7599	E-05	
2.0044E-0	5 1_2872E-0	5 3_020	3E-06	5.213	8E-06	-1.243	9E-06	4.662	9E-06
-1.806/E-C	/ 5-1112E-0	1 1-283	5E-06	3.083	7E-06	1.8082	2 E-06	2.231	3E-06
1.3015E-0	6 2.9342E-0	6 3.158	5E-06	1.597	7E~06	5.640	9 <b>E-0</b> 7	6.429	8E-06
5-9421E-0	/ -3.5711E-0	7 -1.867	7E-06	-5.095	2E-07	-8.1732	2E-07	1.458	7E-06
-7.0738E-0	6 -7.1043E-0	7 -6.070	98-08	1.467	4E-05	-3.3330	5 E-05	-1.969	6E-07
1. 435 3E- 0	6 5.3471E-0	6 3.467	8E-06	2.736	8E-06	2.080	ŧ E−06	2.942	7E-07
2.9453E-0	7 1.2577E-0	7 1.258	2 E- (7	1.258	7E-07	1.2609	5E-07	1.261	3E-07
3.8195E-0	7 3_6965E-0	7 1.066	6E-06	1.651	9E-06	5_6078	3 E-06	2.956	5E-06
1.5407E-0	6 2.7504E-0	6 3.038	4E-06	1.629	5E-06	-1-2320	DE-06	-5.188	0E-05
-9.8516E-0	6 -5.2210E-0	7 3_506	7E-06	5.265	5E-06	7.5124	<b>∔ E-0</b> 6	5.481	3E-06
1. 36 2 2 E - 0	6 1.3213E-0	6 3_846	3E-07	3.870	9E-07	3.8646	5E-07	3.898	1E-07
3.9013E-0	7 1.5955E-0	6 1.662	8E-06	2.357	98-06	3.1758	3E-06	7.911	6E-06
7.5759E-0	6 6.2769E-0	6 5.099	9E-06	2.090	8E-06	-4.4928	3E-05	-1.483	0E-05
-8.8127E-0	6 7.5138E-0	7 7_656	4E-06	8.948	6E-06	4.7150	) E-06	1.756	6E-06
1.7602E-0	6 4.7283E-0	7 4.696	9E-C7	4.753	4E-07	4,7257	7E-07	4.786	8E-07
1.8246E-0	6 1.8577E-0	6 2.020	9E-06	8.876	8E-06	1.1114	E-05	9.392	4E-06
4.2380E-0	6 4.7062E-0	6 6.131	9E-06	-2.391	4E- 08	3.7580	E-06	+2.575	6E-05
-3.5155E-0	5 -2.3983E-0	5 -3.377	8E-06	5.340	8E-06	1. 1674	E-05	8.336	2E-06
1.6207E-0	6 1.6324E-0	6 7.043	6E-07	6.997	6E-07	7.1633	E-07	7-000	5E-07
7.0873E-0	7 1.6865E-0	6 1.714	7E-06	9.647	5E-06	2.4327	e-05	1.735	0E-05
8.3257E-0	6 1.2011E-0	5 <b>1.</b> 815	0E-(5	7.855	4E-06	8.9218	BE-06	-1.852	7E-04
4D 107	1 1269	102	4	5	0	8	0	0	0
0									
5D *RESPONS	E IS MUITIPL	ICATION	FACTO	R FOR 1	r R X - 2	*			
7C *EPRI SE	NS. OF K TO	H CAPTU	JRE				A= -	1.5988	E-01*
8D -4.3788	E-07 -1.5743	E-06 -3.	0239E	-06 -3.	1832E	-06 -3.	06341	-06	
-3.1077E-06	-2.737CE-06	-2.9342	28-06	-3.3589	)E-06	-4-0881	P-06	-4.925	88-06
-6.2972E-06	-8-1775E-06	-1-0602	2E-05	-1.3836	E-05	-1-7950	E-05	-2-304	98-05
-2.9201F-05	-3.6977E-05	-4.7172	2E-05	-6-056	92-05	-7-7413	E-05	-9-620	78-05
-1.9744E-05	-1.5081E-06	-4-4119	-06 ·	-1-7024	E-06	-2.3131	F-06	-2.559	98-06
-1.3718E-05	-2.1292E-06	-4-1790	)E-06	-4-8689	E-06	-4.0192	E-05	-2.690	18-06
-1.8055E-06	-2-2327E-06	-9-1654	E-07	-6-6260	E-07	-5.0136	E-03	-7 055	58-00
-7.0653E-08	-3.0144F-08	-3_0149	-C8	- 3-0161	<b>12</b> -08	-3 0170	E-07	-7.035	3E-08
-9-1271E-08	-8_8217E-08	-2.5265	58-07	-3.8241	F-07	-1 2624	E-00 E-06	-1 154	12-00
-7-9199E-07	-1.7045F-06	-3.3907	F-06	-2 4736	8-06	- 1.2024	E-00 E-05	-0 450	75-06 75-06
-8-2055E-06	-4-89055+06	-3 0045	- C6	-2-4/30		-J.2400 -J.2707	E-0J	-9.0000	
-4-83338-07	-4 86305-07	-1 4220	NR-07.	- 1 4703	00-00	-2-2707	E-08	-1.002.	3E-06
-1 42848-07	-5 75788-07	-5 0346	2-07	- 1.4303	55-07 58-07	- 1- 4233	2-07	-1-434	1 E-07
-2 74508-06	-2 56368-06	-3 11202	10-01	-5 2004	5 - L/	-9-0032	E-07	-2. 3521	08-06
-9 96358-06	-2. JUJLE-00	-0 0605	10-00 ·	- 3.3400		- 1. /101	E-04	-1-099	12-05
-6 12168-07	-1 6309E-07	-1 6766	- 00 - <u>1</u>	-3-3300	DE-06	- 1.0020	8-06	-6.099.	38-07
-6 22702-07	-1.03900-07	-1-0200	15-17 ·	- 1.0434		- 1. 6296	E-07	-1.646	5E-07
-3 20105-07	-0.23/72-07	-1 1001		-2-/1/2	15-00	-3.5493	E-06	-5.042.	3E-06
-5 35008-05	-3 10935-05	-1 7370	16-00 ·	- J. J. J. Z. C	DE-04	-3.0400	£-05	-1.534:	SE-04
-1 17258-06	-3.130/E-U3	-1-7239	15-05 ·	-9-9970	1E-06	-1-05/6	E-05	-6.2110	5E-06
- 1. 1/JJE-00	-9 60058-07	- 3.0104	DE-07	- 4.90 IA	E-07	-5-05/8	E-0/	-4-0268	3E-07
-4.002225-07	-9.0000E-07	-9.0051	E-07 -	-5-21/3	1E-06	-1.5207	E-05	-1.6080	)E-05
- 1. 1933E-03	-2.0314E-03	-6-8035	E-05 -	-2-5068	E-03	-1.1552	E-03	-1.5438	3E-01
				_					
40 107	1 1269	904	4	5	0	8	0	0	0
		TCARTON							
JD TRESPONS	E IS HULLIPL	ICATION	FACTO	R FOR 7	RX-2	*			
00 - 52 KI SE	85. UF # TO 8-03 - 5 2070	n SCATT	LEBING	- 0 /	7620-	<u>.</u>	A=	1.83221	e-01*
1 03755 03	E-03 -3-30/0	5 7004	12895	-04 2.	1632E	-03 1.	00731	3-02	
1.03/5E-02	7. 1429E-03	5.7096	0E-03	5.4989	E-03	4.2949	E-03	4.144	5E-03
4. 18305-03	3.8427E-03	4-2061	IE-03	4.2565	E-03	4.7739	E-03	4.625	7E-03
4./5148-03	5.3668E-03	5.1763	SE-03	4-5616	E-03	5_3139	E-03	6.6999	9E-03
9-8559E-04	7.90548-05	1.6698	3E-04	8.0009	E-05	9.3522	E-05	3.198	DE-04
3-0790E-04	8-5264E-05	3-0133	3E-C4	1.451	SE-03	8_8641	E-04	3.004	1E-04
3- 308 1E- 04	1.0/75E-04	3.9631	E-04	2.9013	E-04	2.1444	E-04	3.004	2E-05
3.0029E-05	1.2803E-05	1.2797	E-05	1.2791	E-05	1.2796	E-05	1.279	3E-05
3.8667E-05	3.7328E-(5	1.0706	E-C4	1.6403	E-04	5.5905	E-04	3.0648	3 E-04
1-6202E-04	2.9285E-04	3.5698	E-04	1.9921	E-04	5.9479	E-04	1.505	3E-03
6.3840E-04	8.4180E-04	8.3403	E-04	8.4192	E-04	9.8262	E-04	6.7142	2E-04
1.7040E-04	1.6554E-04	4.7941	E-05	4-8102	2E-05	4.7864	E-05	4.8112	2E-05
4.7952E-05	1_941CE-04	1.9914	E-04	2.7626	E-04	3.6161	E-04	8.8507	7E-04
8.3465E-04	6_4885E-04	5.1278	E-04	2.8771	E-04	3.5024	E-03	5.792	3E-04
9.5877E-04	1.2318E-03	1.3970	E-03	1.1611	E-03	5.6250	E-04	2. 183	3E-04
2.1661E-04	5.7771E-05	5.7213	E-05	5.7723	E-05	5.7199	E-05	5.774	7E-05
2.1832E-04	2.1944E-04	2.3550	E-C4	9.9710	E-04	1. 2275	E-01	9 915	1E-04
4.4786E-04	4.946 SE-04	7.1208	E-04	3.8328	E-03	6-6913	E-04	1. 354	1E-01
2.34488-03	2.4511E-03	2_1985	E-01	1_8111	E-03	2. 2488	F-03	1, 340/	)F-07
2.508 1E-04	2-49578-08	1_0674	E-04	1_05#0	12-02	1 0743	5-0J	1 2064	12-V3
1.405PE-04	3_3170F-04	3 3339	2 04	1 7050	12-03	3 10143	B-04 B-03	1.373	15-04
1 17 188-03	1 73168-03	3 1920	10 47	1 8178	D 0 0 0	3 10 14	5-03	-0 520	22-03

4 D	107	1	127	6	102	4	3	0	8	0	0	0
500 80 	0 *RESPONSE *EPRI SEN -5.5263E 5165E-09 8013E-09 2936E-09 8516E-10 8516E-10 8964E-11 4497E-11 1242E-10 2012E-09 3018E-10 8464E-11 3865E-10 6804E-09 6482E-10 6765E-10 5765E-10 6765E-10 0779E-10 6482E-10 0866E-10 2011E-09	IS  S. 04 -1.4 -2.5 -4.0 -5.7 -5.9 -2.3 -1.3 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.5 -1.	MUIT F K -1.227 205 205 205 205 205 205 205 205 205 205	IPLI IO 886E -09 -09 -10 -10 -10 -10 -10 -10 -10 -10	$\begin{array}{c} CA 11 ( C \\ C \\ -0 \\ -3 \\ -3 \\ -3 \\ -3 \\ -3 \\ -3 \\ -1 \\ -2 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1 \\ -1$	CN FACTO PTURF -1.655CE 352E-CS 924E-CS 924E-CS 924E-CS 840E-C9 214E-05 611E-10 922E-12 806E-11 883E-10 234E-10 234E-10 234E-10 234E-10 557E-CS 788E-11 986E-10 557E-09 423E-10 372E-C8	R FOR -05 -1 -1.550 -3.834 -1.640 -4.570 -1.304 -1.778 -1.026 -6.631 -5.954 -5.954 -5.954 -4.435 -9.025 -4.435 -9.025 -4.435 -9.025 -4.435 -1.345 -1.394 -1.394 -6.765	TRX-2 .0030E 3E-09 0E-09 0E-09 99E-10 0E-09 99E-10 3E-10 3E-10 3E-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE-10 3FE	* -09 -1. -1.6614 -4.8378 -2.0927 -6.2112 -1.0792 -1.3458 -8.0976 -3.3871 -1.4098 -6.1376 -3.8382 -2.5853 -4.6090 -4.4761 -4.3871 -9.5455 -1.0366 -2.8367 -1.3532 -4.06000 -3.1188	$\lambda = -2235$ E = -03 E = -03 E = -10 E = -0.09 E = -0.9 E = -0.7	$\begin{array}{c} 1.9008\\ -09\\ -1.791\\ -2.597\\ -6.141\\ -2.597\\ -6.875\\ -7.232\\ -1.893\\ -3.095\\ -3.095\\ -3.695\\ -3.6861\\ -4.531\\ -3.861\\ -6.332\\ -2.953\\ -1.642\\ -4.432\\ -1.355\\ -4.119\\ -1.663\\ -4.160\\ -4.160\end{array}$	E - 03 * 5 E - 09 7 E - 08 9 E - 10 0 E - 10 6 E - 12 7 E - 10 8 E - 11 6 E - 12 7 E - 10 8 E - 01 8 E - 01 3 E - 10 3 E - 09 7 E - 09 9 E - 09 9 E - 05
4 D	107	1	127	6	904	4	3	0	8	0	0	0
5 C C 8 7 C C 8 3 6 4 1 - 5 1 2 3 6 4 1 - 5 1 2 3 6 - 1 1 3 6 - 1 1 3 6 - 1 1 3 6 - 1 1 3 6 - 1 1 - 3 1 - 3 1 - 1 9 8	*RE SPONSI *EPRI SEP -2.91321 8626E-04 1052E-C5 3141E-05 1324E-05 1324E-05 4632E-06 3138E-05 3138E-05 3138E-05 3138E-05 5257E-06 6897E-05 6547E-05 5337E-05 5337E-05 3761E-04 4089E-05 6965E-06 1172E-05	2 IS NS- 04 3 ( 3 - 0 4 5 - 1 5 - 1 2 - 1 3 - 1 3 - 1 5 - 1 1 - 1 5 - 1 1 - 1 2 - 1 1 - 1 2 - 1 1 - 1 1 - 1 2 - 1 1	MOIT DF K 0466 66916 66916 86017 99728 1945 1945 1945 1945 199728 86928 20415 86928 20415 86928 20415 86928 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 205768 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76E-05 85E-05 43E-05 74E-05 71E-06 47E-05 10E-06 77E-05 10E-06 27E-04 72E-04	* 5.8516 5.653( 3.2555 -1.9237 1.7479 1.0523 +8.164( 7.1213 3.5038 2.8194 -5.626 4.063( 4.063( 4.3059) 1.1155 6.1886 2.122 5.956	A= 495 6E-05 6E-05 6E-05 6E-05 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-05 8E-06 8E-06 8E-05 8E-06 8E-05 8E-06 8E-05 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06 8E-06	$1.8285 \\ = -04 \\ 5.984 \\ 4.969 \\ 7.469 \\ 7.469 \\ 1.817 \\ 1.052 \\ 2.461 \\ 1.052 \\ 2.523 \\ -5.500 \\ 4.932 \\ 3.529 \\ 7.057 \\ -4.920 \\ 1.618 \\ 4.355 \\ 7.898 \\ -5.956 \\ 7.334 \\ 9.588 \\ 1.605 \\ -7.734 \\ \end{array}$	E-03* 9E-05 1E-05 5E-05 4E-06 6E-06 6E-05 7E-05 7E-05 7E-05 9E-05 9E-05 9E-05 9E-05 9E-05 9E-05 9E-05 9E-05 9E-05 9E-05 3E-05 9E-05 3E-05 9E-05 3E-05 9E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 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3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05 3E-05
4 C	107 0	1	200	0	901	4	3	0	8	0	0	0
5 D D D D D D D D D D D D D D D D D D D	*RESPONS) *EPRI SI -3.3803) .9108E-03 .2112E-04 .2664E-04 .3610E-05 .3457E-05 .3056E-11 .1848E-11 .4977E-05 .9927E-06 .1143E-12 .4576E-13 .6116E-05 .3525E-06 .4159E-13 .2559E-05 .4121E-05 .4121E-05 .9137E-14	E IS. E NS. E -1. -3. -4. -2. -4. -9. -3. -9. -3. -9. -1. -2. -7. -9. -1. -2. -7. -9. -1. -2. -7. -9. -2. -2. -2. -2. -2. -2. -2. -2. -2. -2	NULT OF K 4981F 5135F 6273F 6273F 6273F 9459F 9459F 9459F 9459F 9459F 9459F 9459F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92268F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 92575F 9257575F 92575F 92575F 92575F 9257575F	IPL: TO 6981 -03 -04 -04 -05 -06 -12 -11 -11 -15 -07 -12 -12 -12 -04 -04 -05 -12 -12 -12 -14 -05 -04 -12 -04 -03 -12 -05 -12 -05 -12 -03 -14 -05 -14 -05 -106 -106 -12 -11 -15 -106 -12 -11 -15 -11 -15 -11 -15 -11 -11 -15 -11 -15 -11 -11	$\begin{bmatrix} CAT + & \\ B - & 3 & 0 \\ - & 3 & - & 9 \\ - & 3 & - & 9 \\ - & - & 2 & - & 4 \\ - & - & 7 & - & 2 \\ - & - & 7 & - & 2 \\ - & - & 7 & - & 2 \\ - & - & 7 & - & 2 \\ - & - & 2 & - & 2 \\ - & - & 2 & - & 2 \\ - & - & 2 & - & 2 \\ - & - & 2 & - & 2 \\ - & - & 2 & - & 2 \\ - & - & 2 & - & 2 \\ - & - & 2 & - & 2 \\ - & - & 2 & - & 2 \\ - & - & 2 & - & 2 \\ - & - & 2 & - & 2 \\ - & - & 2 & - & 2 \\ - & - & - & - & 2 \\ - & - & - & - & 2 \\ - & - & - & - & 2 \\ - & - & - & - & - \\ - & - & - & - & -$	ON PACTO 2 IN FL 2 IN FL 609E-03 252E-04 272E-04 272E-04 408E-05 097E-06 117E-07 247E-12 247E-12 247E-12 247E-13 1052E-04 471E-11 1052E-04 4880E-07 227E-14 1880E-07 1227E-14 1880E-05 081E-05 569E-14 1323E-13 1325-14 1323E-13 1325-14 1325-14 1325-14 1325-14 1355-14 1355-14 1355-14 1355-14 1355-14 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 1355-15 135	DR       FOR         POR       -7.000         -4.661       -3.300         -2.491       -2.491         -2.491       -2.453         -3.581       -9.366         -2.55       -4.933         -2.453       -2.133         -2.407       -3.333         -7.12       -7.45         -7.45       -3.47         -2.334       -2.32	TRX-2 2,43931 91E-04 62E-04 27E-04 81E-05 57E-08 38E-12 14E-09 95E-05 29E-08 20E-13 19E-10 91E-05 25E-09 82E-14 43E-10 35E-04 16E-07 04E-14 78E-11 78E-11	* -4.8446 -4.8446 -4.6946 -3.4642 -1.5725 -6.1824 -9.4546 -2.2313 -1.0145 -1.1591 -2.0827 -2.6307 -1.3624 -2.0670 -7.3477 -6.7890 -3.1205 -9.1774 -9.45600 -9.4593	A = - 04 E - 04 E - 04 E - 04 E - 04 E - 10 E - 12 E - 04 E - 10 E - 12 E - 04 E - 10 E - 12 E - 04 E - 05 E - 04 E - 04 E - 04 E - 04 E - 05 E - 04 E - 04 E - 04 E - 04 E - 05 E - 04 E -	-2.7038 -03 -5.249 -3.293 -3.153 -2.200 -3.624 -2.557 -9.715 -2.779 -9.286 -5.126 -5.126 -2.199 -1.173 -3.804 -6.661 -7.956 -7.046 -5.132 -1.562 -8.326 -1.318	E-02* 8E-04 1E-04 4E-05 1E-112 3E-05 5E-10 3E-105 5E-05 8E-10 7E-05 5E-05 8E-10 7E-05 5E-06 7E-13 8E-07 9E-06 3E-01 6E-14 3E-06

4 D	107	1	2000	903	4	3	0	8	0	0	0
5 D	*RESPONS	E IS	NULTIPL	ICATION	FACT	OR FOR	TRX-2	*			
7 D	*EPRI SI	ENS.	OF K TO	CB**2	IN V	OID			λ= ·	-2.4114	E-03*
8 D	-7.7187	E-05	-6.3903	E-05 -1	.8568	E-04 -1	.5073	E-04 -6.	. 1461	E-05	
-1.	2595E-04	-9-	1639E-05	-7.344	18E-05	-3.846	4E-05	-3.434	6E-05	~6.556	8E-05
-2-	1538-05	-3.	4304E-05	-0.827	38-05	-5.349	0E-05	-7.714	3E-05	-7.521	7E-05
-1_	20478-05	-7.	71408-07	-2.236	38-05	-8 469	88-07	-1 153	08-05	-5-409	18-05
-6.	8245E-06	-1.	0296E-06	-1-989	4E-06	-1_621	58-06	-1.833	58-08 58-05	-1.086	28-06
-6.	7205E-07	-6.1	9628E-07	-2.022	0E-07	-1.002	4E-07	-6.434	1E-08	-8.988	28-09
-9.	0301E-09	-3.8	960 CE-09	-3.866	48-09	-3.875	8E-09	-3.880	3E-09	-3.889	0E-09
-1-	1813E-08	-1-	1509E-08	-3_374	1E-C8	-5.676	0E-08	-3.726	0 E-07	~5.069	6E-07
-3.	4396E-07	-6-6	5181E-07	-1.306	5E-06	-9.824	1E-07	-2.130	4 E- 05	-3.457	2E-05
-2-	4/938-06 73888-08	-1-1	29335-06	-1 200	3E-07	-3.707	0E-07	-2.656	12-07	-1.469	1E-07
-1.	3363E-08	-5_1	5573E-08	-6-287	78-08	-1.067	92-07	-1.690	25-00	-1-332	28-08
-5.	9982E-07	-5.	2376E-07	-7.498	78-07	-1.470	2E-06	-6.166	3E-05	-3.365	52-06
-2.	8107E-06	-1.6	6430E-06	-7-606	8E-07	-2.507	4E-07	-7.521	3E-08	-2.748	9E-08
-2.	8300E-C8	-7.6	5822E-09	-7-670	2E-09	-7.804	2E-09	-7.790	7 B-09	-7.930	4 E-09
-3.	00052-08	-3.2	272 CE-08	-3_846	5E-08	-2.242	4E-07	-4.427	5E-07	-9.060	7E-07
-9-	40488-06	-1.	13688-06	-1 952	58-00	-9.10/	78-07	-0.234	58-06	-3-081	78-05
-1.	6270E-08	-1-1	5292E-08	-7_003	88-06	-6.944	18-09	-7.113	58-09	-5 789	7-08
-5.	8982E-09	-1.0	160E-08	-1.464	2E-C8	-8.664	1E-08	-4. 195	58-07	-1_164	98-06
- 1.	2527E-06	-3.3	3022E-06	-9.731	0E-06	-3.140	0E-05	-8.507	5E-06	-3.168	42-04
4 D	107	1	2000	902	4	3	0	8	0	0	0
	0										
5D 76	*RESPONSE	IS IS	MULTIPL	CATION	FACTO	DR FOR	TRX-2	*	-		
AD.	~1_48491	E-04	-4_39821	18442 2-04 -6	1 N C	LAU R-01 -7	075 #1	R-0/ -6	A= -	-8.1947 P-04	E-03*
-5.	4205E-04	-3.1	7966E-04	-1.317	38-04	-4-071	58-04	-9-8929	E-05	-04 -9.971	88-05
-6.	2727E-05	-5.8	882E-05	-1.634	6E-C4	-1.601	0E-04	-1.320	3E-04	-1.234	2E-04
-9.	6257E-05	-1_2	2685E-04	-1_611	9E-04	-2.313	3E-04	~2.115	)E-04	-6.888	7E-05
-3-	4927E-05	-2.3	015E-06	-6_674	9E-06	-2.534	0E-06	-3.447	3E-06	-3.567	7 E-06
- J.	3572E-05	-5-(	776E-06	-9-826	72-06	-8.733	0E-06	-1.442	3E-04	-8-693	6E-06
-1.	4/332-00	-1 0	06418-08	-1.940	92-09	-1. 103	95-00	- 0 076	)E-0/	-1.159	42-07
-1_	5092E-07	-1.4	631E-07	-4.236	1E-07	-6.678	98-07	-1.158	38-06	-3.887	28-08
-2.	6558E-06	-5.2	883E-06	-1-048	4E-C5	-7-825	7E-06	-5.378	/E-05	-1-078	28-00 98-04
-7.	9008E-06	-4.2	495E-06	-2.292	0E-06	-1.407	7E-06	-1.182	3E-06	-7.815	0E-07
-2-	2775E-07	-2.3	239E-07	-6.825	3E-C8	-6.878	0E-08	-6. 8661	7E-08	-6.924	9 <b>E-0</b> 8
-6.	9175E-08	-2.8	8267E-07	-2.997	1E-07	-4.473	1E-07	-6.196	E-07	-1.666	4E-06
-2-	03472-06	-1-2	2258-06	-2.55/	48-05	-4.714	22-06	~6_229	E-05	-3.437	3E-06
-7.	2904E-08	-1.9	501E-08	-1.947	28-07	-1.970	97-08	-1.9578	88-08	-1 981	0 P-08
-7_	5379F-08	-7.6	98EE-08	-8.491	0E-08	-3.794	3E-07	-5.8498	BE-07	-1.049	7E-06
-7.	6886E-07	-1.1	38 9E-06	-3.428	9E-06	-1.122	6E-04	-1.0112	2E-05	-6.470	9E-05
-4-	6919E-05	-2.4	443E-05	-1.045	32-05	-4.490	2E-06	-3.4506	6E-06	-1.741	0 <b>E-06</b>
-3.	2639E-07	-3-2	575E-07	-1-395	7E-07	-1.380	5E-07	-1.408	E-07	-1.113	78-07
- 1-	12325-07	-4.0	13018-05	-2.094	02-07	-1.4/0	JE-06	~4.5943	BE-06	-7.393	8E-06
- 6.6	9312E-00		201E-01	-4.500	06-03	- 1.002	OE-UW	- 1- 0 900	5E-04	-1-134	0E-03
4 D	107	1	2000	900	4	3	0	8	0	0	0
	0					-	•	·	•	v	v
50	*RESPONSE	IS	MULTIPLI	CATION	FACTO	DR FOR '	TRX-2	*			
712 - 19 m	- EPFI SE	INS.	UF K TO	LE##2	IN MC	DERATO	R 00 // 2-		A= -	1.0512	E-01*
-7	- 1.0724r 34535-03	-11 B	-5-01982	-3 721	-09271 UR-03	-7 533	•98431 68-03		64591	3-03	
-1.	95648-03	-1_4	3228-03	-1.342	4E-03	-1-070	0E-03	-1 4742	PE-03	-1-022	45-03
- 1.	3121E-03	-1.1	922E-03	-1.443	1E-03	-1.075	1E-03	+1.3780	E-03	-1-289	78-03
- 1_	6129E-04	-3.3	219E-05	-6.816	1E-05	-2.613	2E- 05	-2.9331	E-05	-8.493	8E-05
-1.	9514E-04	-2.9	81 9E-05	-1.057	8E-04	-2.732	6 <b>E-</b> 05	-2.9472	2-04	-1.895	7 E- 05
-1-	2666E-05	-3.0	747E-05	-3.369	7E-05	-2-431	6E-05	-1-8374	E-05	-2.583	9E-06
-2.	34028-06	-1-1	0372-06 2778-06	-1-103	38-04	-1.104	15-06	-1_1043	E-06	-1.104	3E-06
-2-	8774E-C5	-6-5	987E-05	-1,306	3E-04	-9.481	18-05	-6.7300	6-05 8-09	-4. 199	7 E-U5 8 E-04
-3.	7763E-05	-2.9	747E-05	-1.841	1E-05	-6.660	9E-05	-6.8366	E-05	-5.028	42-05
-1-	6967E-05	~1.7	055E-C5	-4-983	9E-06	-5-011	6E-06	-4.9925	B-06	-5.021	82-06
-5-1	0004E-06	-2.0	142E-05	-2.035	9E-05	-2.713	4E-05	-3.3457	E-05	-8_171	5E-05
-9.	4921E-05	-5.9	39CE-05	-2-175	0E-05	-5.942	3E-05	-1.0061	E-03	-6.389	5E-05
- 1-1	UI4/ビーU4 45378-15	-0.0	600F-06	-2.711	08-05	-1.820	0E-05	-8.9983	E-06	-2.447	1E-05
-2-	4909E-05	-2.5	0058-00	-2-667	35-UO 88-15	-1 092	12-04	-1 4071	12-06 12-04	-0.589	12-05
- 1.	7626E-05	-2.9	111E-05	-8-237	9E-05	-9.195	6E-04	-1,5356	8-04 R-01	-5.705	42-V3 58-04
-2.	6948E-04	-9.4	238E-05	-5.482	9E-05	-3.142	8E-05	-5.8148	E-05	-3.389	9 E-05
-6.	3834E-06	-6.3	634E-06	-2.724	0E-C6	-2-692	9E-06	-2.7441	E-06	-6.140	78-05
-6-	1920E-05	-1.4	6232-04	-1.470	7E-04	-7.913	2E-04	-5.6509	E-05	-3-507	9E-05
-3.1	1822E-05	-3.5	237E-05	-2.075	6E-04	-4.0818	8E-03	-1.1324	E-03	-1.444	4E-02

0		134 1	30	/ 0	0 0
5D *RESPONSE	E IS REACTIO	IN BATE BHC 28	FOR TRX-2*		
7D *EPRI SEN	NS. OF 2380	CAP EPI/THE T	0 2380 NUBAI	R A=-	- 1. 7 1 40 E- 05*
8D -1.7305B	E-06 -3_6672	E-06 -6.4737E	-06 -4.92941	8-06 -3.1939	E-07
-1.4997E-08	-1.065 EE-09	-3.8852E-10	-2.4025E-10	-1.7319E-10	-1.42522-10
-2.3942E-10	-2.6857E-10	-2.4285E-10	-7.1459E-12	-1.2051E-16	-1.3165E-15
-1.0642E-13	-3_6413E-10	-2.1440E-09	- 4. 348 1E- 14	-2.8865E-14	-2.7778E-14
-4.4694E-15	-3-565FE-16	-1-05188-15	-4.1145E-16	-5-5577E-16	-6. 52377-16
- 3. 237 18-15	-5-0281F-16	-9-89658-16	-1.44772-15	-9.18488-15	-6-43082-16
-4 56698-16	-6. 43548-16	-3 1666F-16	-1.72128-16	-1.0268F-17	-2.45317-18
-2 3//218-18	-0 93988-10	-0 78517-10	-0 91957-10	-9 99839-19	-1 00332-19
- 2. 342 15-10	-3.03046-13		- 3.010.0	-5.00435-13	- 3 04018-16
- 3+ 100 JE- 10	-3-37105-10	-1.34236-1/ 	- 34 314 36-17	-1-10-10-10	-3.34016-10
-2.33/1E-10	-4_4//UE-10	-/.9430E-10	- 3.09316-10	-1.13105-14	-2.0231E-14
-1-8/235-13	-1-23548-13	0 -8-/8335-10	-/-31318-10	-/-8050E-16	-2. 90//E-10
-1.6500E-17	-9.0052E-18	-2.1295E-18	-2-0740E-18	-2.0483E-18	-2.1034E-18
-2.2175E-18	-1.250 CE-17	-2.9586E-17	-1.28798-16	-3.62342-16	-1.04842-15
-9.3460E-16	-7.0510E-16	-8.7864E-16	-1.1663E-15	-3.4005E-14	-2.2561E-15
-2.16948-15	-1.7596E-15	-1_5229E-15	-1.0329E-15	-1.4642E-16	-1.6677E-17
- 1. 1524E- 17	-2.7063E-18	3 -2.6242E-18	-2.6363E-18	-2.6483E-18	-2 <b>.75178-1</b> 8
-1.2117E-17	-1.8101E-17	/ -3.5515E-17	-7.45192-16	-1.2293E-15	-1.2792E-15
-7.4066E-16	-9.9251E-16	5 -2.7796E-15	-6.7106E-14	-7.1891E-15	-2.8718E-14
-1.0418E-14	-6.9181E-15	-4-5136E-15	-3.0859E-15	-2.9525E-15	-3.8313E-16
-2.26858-17	-1_8908E-17	-7.4738E-18	-7.1865E-18	-7.2233E-18	-6.44598-18
-6.6435E-18	-1.6952E-17	-2-02868-17	-3.5597E-16	-4.4987E-15	-4- 4039E-15
-2.8150F-15	-5.567 CF- 15	-1.2990E-14	-4.35398-19	-1-42548-13	0_0
100.001 10	agaary <u>t</u> 1a				
4D 107	4 1262	18 4	30	70	0 6
0					
5D *RESPONSE	IS REACTIO	N BATE RHC 28	FOR TRX-2*		
7D *EPRI SEN	IS. OF 2380	CAP EPI/TER TO	) 2380 FISSI	ON A=-	-1.3765E-04*
8D 7.5582E	-06 2.8679	E-06 -3.9346E	-05 -1.02081	-04 -7.23681	5-06
1.9337E-07	5.7267E-08	2.5247E-08	1.6149E-08	1.1371E-08	5.4302E-09
6-8524E-09	7-0216F-09	5-7290E-09	1-9373E-10	3-9149E-15	3.7853E-14
8.2039F-12	2-33305-08	2-3759E-(7	9-1843E-12	5-3876E-12	1_8661E-12
1.74997-12	1.9816F-13	6-7890E-13	1.95838-11	2.95948-13	-2.39068-13
2 1925-12	2.220 0 - 13	1.13708-13	-2.93429-12	5 58968-12	-3-54378-13
-6 70368-12	-1 61639-13	_7 31128_12	-2.53420-12 -2.0150P-12	-2 22999-18	-1 76857-15
-0-/930E-13	-1-0103E-12		- 01018- 16	-2.33005-14	-6 90107-16
-1.00026-13	-0-9093E-10	-0.033/E-10	2 20202 44	-0-03205-10	-6 51048-13
-2.15/45-15	-2-20/32-13	-8-920/2-15	-3./U38E-14	-1. 1831E-12	4 30107-13
-2.0939E-13	-1,4874E-13	1. 3129E-13	1.5768E-13	8.3073E-12	1.30198-11
-1.1530E-12	-2.4513E-12	-2.5283E-12	-2.0994E-12	-1.5862E-12	-3.4155E-13
-1.3830E-14	-6.8229E-15	-1.5427E-15	-1.4732E-15	-1.4332E-15	-1.4552E-15
– 1. 5143E– 15	-8_267 1E-15	-1.8516E-14	-8.5263E-14	-3.3495E-13	-1.78128-12
-1.6973E-12	-8.2612F-13	-5.1723E-13	- 3 <b>.</b> 744 38- 13	2.1977 <b>E-</b> 11	-1_7069E-13
-2.1104E-12	-4.1098E-12	-4.2672E-12	-1.68918-12	-1.3388E-13	-1.27728-14
-0 46550.45	-1.8652P-15		4 9075- 45	-1 78068-15	-1 83598-15
-0-10335-13		-1.79328-15 ·	-1./8058-15	12/00/02 13	
-7.9453E-15	-1.1577E-14	-1.79328-15 -2.2510E-14	-1./8655-15 -7.04468-13	-2.9172E-12	-2.9267E-12
-7.9453E-15 -1.1353E-12	-1.1577E-14 -9.8101E-13	-1.79328-15 -2.2510E-14 -8.6168E-13	-1.7865E-15 -7.0446E-13 6.3403E-11	-2.9172E-12 4.8426E-12	-2.9267E-12 2.1606E-11
-7.9453E-15 -1.1353E-12 -7.7615E-13	-1.1577E-14 -9.8101E-13 -9.3856E-12	-1.7932E-15 -2.2510E-14 -8.6168E-13 -1.0238E-11	-1.7865E-15 -7.0446E-13 6.3403E-11 -7.0283E-12	-2.9172E-12 4.8426E-12 -3.7482E-12	-2.9267E-12 2.1606E-11 -2.7475E-13
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-7.9453E-15 -1.1353E-12 -7.7615E-13 -1.4552E-14 -4.0151E-15	-1.1577E-14 -9.8101E-13 -9.3856E-12 -1.1881E-14 -1.0242E-14	-1.7932E-15 -2.2510E-14 -8.6168E-13 -1.0238E-11 -4.6307E-15 -1.2280E-14	-1./865E-15 -7.0446E-13 6.3403E-11 -7.0283E-12 -4.4158E-15 -2.3656E-13	-2.9172E-12 4.8426E-12 -3.7482E-12 -4.3992E-15 -6.6411E-12	-2.9267E-12 2.1606E-11 -2.7475E-13 -3.9010E-15 -9.1597E-12
-7.9453E-15 -7.9453E-15 -1.1353E-12 -7.7615E-13 -1.4552E-14 -4.0151E-15 -5.4089E-12	-1.1577E-14 -9.8101E-13 -9.3856E-12 -1.1881E-14 -1.0242E-14 -7.0542*-12	-1.7932B-15 $-2.2510E-14$ $-8.6168E-13$ $-1.0238E-11$ $-4.6307E-15$ $-1.2280E-14$ $-1.7916E-12$	-1./865E-15 -7.0446E-13 6.3403E-11 -7.0283E-12 -4.4158E-15 -2.3656E-13 5.8016E-10	-2.9172E-12 4.8426E-12 -3.7482E-12 -4.3992E-15 -6.6411E-12 1.9496E-10	-2.9267E-12 2.1606E-11 -2.7475E-13 -3.9010E-15 -9.1597E-12 0.0
-7. 105 52-15 -7. 945 32-15 -1. 135 32-12 -7. 76 152-13 -1. 455 22-14 -4. 015 12-15 -5. 408 92-12	-1.1577E-14 -9.8101E-13 -9.3856E-12 -1.1881E-14 -1.0242E-14 -7.0542E-12	-1.7932E-15 -2.2510E-14 -8.6168E-13 -1.0238E-11 -4.6307E-15 -1.2280E-14 -1.7916E-12	-1.7865E-15 -7.0446E-13 6.3403E-11 -7.0283E-12 -4.4158E-15 -2.3656E-13 5.8016E-10	-2.9172E-12 4.8426E-12 -3.7482E-12 -4.3992E-15 -6.6411E-12 1.9496E-10	-2.9267E-12 2.1606E-11 -2.7475E-13 -3.9010E-15 -9.1597E-12 0.0
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-7.9453E-15 -7.9453E-15 -1.1353E-12 -7.7615E-13 -1.4552E-14 -4.0151E-15 -5.4089E-12	-1.1577E-14 -9.8101E-13 -9.3856E-12 -1.1881E-14 -1.0242E-14 -7.0542E-12	-1.79328-15 -2.25108-14 -8.6168E-13 -1.0238E-11 -4.6307E-15 -1.2280E-14 -1.7916E-12	-1. /865E-15 -7.0446E-13 6.3403E-11 -7.0283E-12 -4.4158E-15 -2.3656E-13 5.8016E-10	-2.9172E-12 4.8426E-12 -3.7482E-12 -4.3992E-15 -6.6411E-12 1.9496E-10	-2.9267E-12 2.1606E-11 -2.7475E-13 -3.9010E-15 -9.1597E-12 0.0
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	-1.1577E-14 -9.8101E-13 -9.3856E-14 -1.1881E-14 -1.0242E-14 -7.0542E-12 4 1262 3 IS REACTIO REI SENS. OF 2-05 8.7673 1.2915E-02 3.1577E-02 2.0386E-04 2.7464E-04 1.5593E-03 6.5438E-05 2.0248E-04 1.5593E-03 6.5438E-03 2.644E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04 8.3496E-04		-1.7865E-13 6.3403E-11 -7.0283E-12 -4.4150E-15 -2.3656E-13 5.8016E-10 3 0 FOR TRI-2* TRR TO 2380C -03 1.16491 1.0880E-02 2.7270E-02 2.2028E-04 9.8230E-03 1.015E-03 6.6322E-05 9.3611E-04 7.3289E-04 1.4949E-03 1.9174E-04 1.1428E-03 2.6689E-03 1.673E-02 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03 1.675E-03	-2.9172E-12 4.8426E-12 -3.7482E-12 -4.3992E-15 -6.6411E-12 1.9496E-10 7 0 AP A= - -02 1.95441 1.1108E-02 2.3973E-02 3.2801E-02 8.0313E-05 2.1993E-03 9.8072E-03 1.3365E-03 1.3365E-03 1.9504E-04 1.3241E-03 1.8004E-02 4.364E-04	-2.9267E-12 2.1606E-11 -2.7475E-13 -3.9010E-15 -9.1597E-12 0.0 0 6 -2.3697E-02+ -02 1.4252E-02 2.7223E-02 4.2988E-02 2.183E-03 6.7068E-04 1.4900E-04 6.7138E-05 2.2246E-03 5.8254E-03 1.9858E-04 3.6678E-03 2.8552E-03 2.660E-04
	-1.1577E-14 -9.8101E-13 -9.3856E-14 -1.1881E-14 -1.0242E-14 -7.0542E-12 4 1262 5 IS REACTIO RI SENS. OP -05 8.7673 1.2915E-02 1.7905E-02 2.0386E-04 2.7464E-04 1.5593E-03 2.0248E-04 1.1839E-03 2.0248E-04 1.1839E-03 3.821E-04 8.3496E-04 2.7112E-03 4.8881E-03 3.67085E-02		-1.7805E-15 -7.0446E-13 6.3403E-11 -7.0283E-12 -4.4158E-15 -2.3656E-13 5.8016E-10 3 0 FOR TRI-2* TRI-2* TRI-28 FOR TRI-2* TRI-28 COS 1.16491 1.0880E-02 2.7270E-02 2.2028E-04 9.8230E-03 1.015E-03 6.6322E-05 9.3611E-04 7.3289E-04 1.4949E-03 1.9174E-04 1.428E-03 2.6689E-03 1.763E-02 2.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.000E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05 5.0470E-05	-2.9172E-12 4.8426E-12 -3.7482E-12 -4.3992E-15 -6.6411E-12 1.9496E-10 7 0 -02 1.95441 1.1108E-02 2.3973E-02 3.2801E-02 8.0313E-05 2.1993E-03 9.8072E-04 6.6769E-05 3.4667E-03 2.2087E-03 1.3265E-03 1.9504E-04 1.3241E-03 1.8004E-02 4.3634E-04 7.1221E-05	-2.9267E-12 2.1606E-11 -2.7475E-13 -3.9010E-15 -9.1597E-12 0.0 0 6 -2.3697E-02* -02 1.4252E-02 2.7223E-02 2.1183E-03 6.7068E-04 1.4900E-04 6.7138E-05 2.2246E-03 5.8254E-03 1.9858E-04 3.6678E-03 2.8552E-03 2.8552E-03 2.0600E-04 7.3266E-05
-C. 105 3E-15 -7. 945 3E-15 -1. 135 3E-12 -7. 76 15E-13 -1. 455 2E-14 -4. 015 1E-15 -5. 408 9E-12 4D 107 0 5D *RESPONSE 7D *FORSS EP 8D 8.53 CBE 1. 878 2E-02 1. 603 0E-02 2. 63 28E-02 7. 877 3E-03 3. 511 2E-04 7. 219 2E-04 1. 516 5E-04 2. 065 2E-04 4. 353 4E-03 3. 418 8E-03 2. 353 5E-04 2. 853 5E-04 2. 853 5E-04 2. 853 5E-04 3. 851 2E-04 3. 551 2E-04 3. 551 2E-04 3. 551 2E-04 3. 553 5E-04 3. 552 04 3. 552 04 5. 552	-1.1577E-14 -9.8101E-13 -9.8356E-14 -1.1881E-14 -1.0242E-14 -7.0542E-12 4 1262 5 S REACTIO RI SENS. OP 5-05 8.7673 1.2915E-02 1.7905E-02 3.1577E-02 2.0386E-04 2.7464E-04 1.5593E-03 6.5436E-05 2.0248E-04 1.1839E-03 5.6821E-04 8.3496E-04 2.7112E-03 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9823E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.9825E-07 4.8381E-03 6.7085E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985E-05 2.985		-1.7865E-13 6.3403E-11 -7.0283E-12 -4.4156E-15 -2.3656E13 5.8016E-10 3 0 FOR TRI-2* TRE TO 2388C 03 1.16491 1.0880E-02 2.7270E-02 2.2028E-04 1.0015E-03 6.6322E-05 9.3611E-04 7.3289E-04 1.4949E-03 1.9174E-04 1.428E-03 2.6689E-03 1.1763E-03 7.0470E-05 7.3747E-04 7.37270E-02 2.6689E-03 1.1763E-03 7.0470E-05 7.3747E-04 7.3747E-04 7.3747E-04 7.3747E-04 7.3747E-04 7.3747E-04 7.3747E-04 7.3747E-04 7.3747E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E-05 7.3477E	-2.9172E-12 4.8426E-12 -3.7482E-12 -4.3992E-15 -6.6411E-12 1.9496E-10 7 0 2.95441 1.1108E-02 2.3973E-02 3.2801E-02 8.0313E-05 2.1993E-03 9.8072E-04 6.6769E-03 3.2087E-03 1.3365E-03 1.3241E-03 3.8004E-02 4.3634E-04 7.1221E-05 3.0962E-04	-2.9267E-12 2.1606E-11 -2.7475E-13 -3.9010E-15 -9.1597E-12 0.0 0 6 -2.3697E-02* -02 1.4252E-02 2.7223E-02 4.2988E-02 2.1183E-03 6.7068E-04 1.4900E-04 6.7138E-05 2.2246E-03 1.1789E-03 1.9858E-04 3.6678E-03 2.8552E-03 2.8552E-03 2.0600E-04 7.3266E-05 5.1515E-03
-C. 1655E-15 -7.9453E-15 -7.7615E-13 -1.4552E-14 -4.0151E-15 -5.4089E-12 4D 107 0 5D *RESPONSE 7D *FORSS EP 8D 8.53C8E 1.8782E-02 1.6030E-02 2.6328E-02 7.8773E-03 3.5112E-04 4.5165E-04 2.0583E-04 2.3535E-04 2.3535E-04 2.8603E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.653E-04 2.652E-04 2.653E-04 2.652E-04 2.652E-04 2.653E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.652E-04 2.752E-04 2.652E-04 2.652E-04 2.652E-04 2.752E-04 2.752E-04 2.752E-04 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- 3.	638	SOE-	09	-2.	024	1E-	09	-8-9	9886	5E-0	9	-7.8	334	1E-08	-3.	5843	B-08	-9.992	5E-10
-3.	837	9E-	10	~6.	704	5E-	11	-5.8	3680	) e - 1	1	-5.3	368	8E-11	-4.	9592	B-11	-4.758	0E-11
- 1.	794	1E-	10	-2.	246	3E-	10	-4.(	0897	7e-1	0	-1.9	911	4E-08	-2.	2971	E-08	-1.514	88-08
-1.	160	)6E-	80	-1.	296	28-	08	-3-5	5154	1E-0	7	-1-4	125	28-06	-7-	1663	R-08	-1-308	07-06
- 1_	426	58-	80	-1.	620	TE-	0.8	-1.3	706	5 F - 1	7	-3.0	144	#F-08	-9	1774	P-00	-9 507	68-10
-4	67 0	08-	11	~ 1	955	FE-	11	-1	979	19-1	1	-1.9	5.0.0	78-11	- 1	5607	P_11	-1 417	08-10
-1	183	178-	11	- 3	997	28-		_ 1 0	2636	5 P_ 1	4	_ 1	101	28-00		7656	3 00	-1.41/	5-11
-5	503	)]p_		_4	007	2 E -						- 14		25-03	-0.	7330	5-00	-1.099	55-07
- J.	101		vo	-0.	0.30	42-	00	-/-(	1013	- U	0	-2.4	223	08-00	- 1.	5394	R-00	-3.395	7E-04
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5 P -	- - -	cne	¥ 6 5						- 10		~~		· -						
יעכי דר	- # 2	240	a 28	12	- H E	ACT]	UN	841	15 B	ULC .	28	FOL	L T	#X-2*			_		
10,	- E P	RI	SEN	5.	ີ້	191	J C	AP E	PI/	TBB	T	ວຸ23	150	FISS	101		A=	5.4885	B-01*
sn Us	1	. 79	/9E	-07	. 9	-770	DZE-	-08	-1-	133	9Ë	-06	-4	-0835	E-06	-4.	00281	5-06	_
2.	052	2 <b>E</b> -	06	6.	671	0E-(	26	7.1	523	E-0	6	6.6	46	8E-06	6.	1407	E-06	3.328	5 <b>E-06</b>
2.	58 1	4E-	C 6	2.	429	5E-(	06	2.5	i435	6E-0	6	3_4	21	7E-06	5.2	2344	2-06	5.549	1E-06
1.	949	2E-	05	1_1	966	7E-(	)5	5.2	836	E-C	5	1.0	27	58-04	1.	3446	B- 04	5.207	88-05
4_ (	539	4E-	05	5.	599	SE-4	)6	1_9	536	B-0	5	5.7	28	3E-06	8.	450	E-06	-7. 160	08-06
6-1	808	8E-	05	7.	132	21-1	) 6	3.4	657	R-0	6.	-6.5	56	3E-05	2.4	1503	R-04	-2.010	68-06
-1.	329	88-	06	-5-	912	57-1	6	- 3 - 1	520	8-0	ē.	-3 4	84	18-04	_3	1987		-0 351	12_00
_7	126	08-	00	_2	, 12 6 1 H	C =	10		120	0-0	ö		200	10-00			B-01	-0.332	15-07
	1.J) 1.J	75-	03	_0	014	52**( 67	, 7 . 	- 4 - 1	120	0-4	2.	- 2.0		15-09	-2.	105	5-09	-2-600	18-09
q., (	020	5-	50		4/9 05-	20-0		-3-7	400	E-C	e ·	-4-9	12	25-07	-1-1	0776	B-05	-2-091	45-06
-2-3	5/0	2E-	0/	-2-	221	38-(	11	2-8	231	B 0	6	4.6	00	68-06	4.(	1631	E~04	5.294	95-04
- 8.	\$75	9E-	05	-4.	729	1E-(	)5 ·	-3.7	412	E-0	5	-1.9	53	0E-05	-1.3	808	<b>E-05</b>	-2.612	8 <b>E-0</b> 6
-1.(	076	0E-	07	-5. !	570	9E-(	)8 ·	- 1. 3	023	Z-0	<b>8</b> -	-1.2	64	2E- 08	- 1. 2	2528	<b>E-0</b> 8	-1.297	58-08
- 1. :	376	6E-	33	-7.	876	9B-0	38 ·	-1_9	036	E-0	7	-9.4	27	1E-07	-4_0	772	8-06	-2.703	28-05
-4-2	233	8 <b>8</b> -	05	-4-	533	48-0	)5 -	-1.1	679	B-0	4	-6.1	37	4E- 05	7	1682	R-04	-8. 101	68-06
-3.	92 Ñ	58-	06	-5.4	0.81	78-1	6 .	-2.5	910	R-0	5.	-1.2	70	18-04	_ 1	2004	1-0s	_7	18_07
-24	556	QP-	07		591	6 F	18	_3 0	124	10 - 10 11 - 11	õ	_ 2 6	6 7	15-04 01-00		1070 1664	B-93	-3 000	0.8-07
- 60 1	110	25-	01 67	_		CE-(	, U '	- 3. 7	131	5-V	с <sup>.</sup>	-1.5	34	05~08	- 3.	:221	a-08	-3.098	78-08
- <u> -</u> ]	440	38-	ι/ 85	-1.	402	UE-C	11 -	-2-5	296	R-0	1	- 1.7	/1	1E-05	-5.5	190	<b>z-</b> 05	-3.656	> <b>3−0</b> 5
- 1. 9	119	YE-	05	-1.	198	UE-C	15 -	-1.1	860	8-0	4	1.5	33	4E-03	5.6	416	B-05	1.111	32-03
- 1. '	193	1B	06	-2.	399	9E-(	)5 ·	-3.0	088	E-0	<b>4</b> -	-7.0	03	38-05	-1.1	845	<b>B</b> -05	-6.016	58-07
-2.9	920	4 E -	68	-2.	122	8E-(	)8 -	-9.5	885	E-0	g .	-9.2	47	1E-09	-9-3	1161	B-09	-8.357	92-09
-8-	736	OE-	09	-2-	288	SE-0	38 -	-2_8	630	E-0	8 -	-7-1	36	58-07	-1.	767	R-0.4	-3-612	38-04
. • ·	116	0	<u>م</u> بّ		272		. e		0.75		-								77 77
- 1-		<b>up</b> -	U 4	-0-	6 I E	0 2 - 1	/ > -	-1_0	817	R-0	5		3.5	48-114	A	1/10	8-114	5.800	67-01

4D	107	4	126	1 1	02	4	ļ.	3	0	7	0	0	6
5 D	0 *RESPONSE	: IS	REAC	TION	BATE	RHC	: 28	FOR 1	RX-2*				
7 D	*EPBI SEN	IS. 0	F 23	8U CA	PEF	I/TH	B T	0 2350	CAPTU	RE	<b>A=</b>	9.6092	E-02*
23	1.6663E	1 1	3.3	835E- -06	1 52	·2.99	1805	- 08 -1	1.96991 208-06	1 76	5.4281E 66 P-06	1 096	17-06
9.	4980E-07	9.9	2762	-07	1.08	133g-	06	1.519	97E-06	1.842	23E-06	2.105	42-06
7.	5797E-06	1.0	206E	-05	1.88	63E-	05	4.512	228-05	6.72	68-05	2.963	2E-05
3.	7120E-05	3.9	111E	-06	1.30	798-	05	3.683	10E-06	5.473	36E-06	-4.325	4E-06
-5.	0615E-07	-3-8	4642	-06 -	2.51	96E-	-06	-3.572	28E-06	-3.330	)1E-07	-6.789	7E-07
-5.	6474E-09	-2.1	921E	- 09 -	2.09	52E-	-09	-2.033	37E-09	-1.99	09E-09	-1.974	8E-09
-6.	0697E-09	-6-4	362E	- 09 -	2.56	85E-	• 68	-4-932	238-07	-1-550	088-05	-1.203	1E-06
-2.	45928-07	-3.1	598E 5868	-07 -06 -	5 62	10/E- )778-	-06	-2.471	122-07	1.68	438-04	2.049	105-04
-1_	5811E-08	-8.0	703E	-09 -	1.86	57E-	-09	-1.799	95E-09	-1.77	20E-09	-1.823	9E-09
- 1-	9237E-09	-1.0	854E	- 68 -	2.57	92E-	69	-1.294	458-07	-5.67	35 E-07	-3.924	2E-06
-6-	480 3E-06	-8.0	967E	-06 -	5.0:	61E-	-05	-2.512	222-05	4.54	382-04	-3-084	28-06
-3.	6288E-07	-6.4	414E	-08 -	-5.70	)33E-	-08	-5.240	58E-08	-4-86	38E-08	-4-684	0E-08
-1.	776EE-07	-2-2	110E	-07 -	3.77	77E-	-07	-1.692	228-05	-3.99	59E-05	-1.905	2E-05
-6.	48578-06	-5.4	096E	-06 -	-6.58	366 E-	-05	1.38	06E-03	2.28	278-05	3.893	14E-04
-4.	4723E-08	-3.8	052E	-03 -	1.53	35E-	-08	-1.49	52E-08	-1.52	24E-08	-1.380	112-08
- 1_	4589E-08	-3.8	92 0 E	- 08 -	-5.01	198E-	-08	-1-53	71E-06	-3.87	298-04	-9.438	32E-04
-6.	7160E-05	-3.0	356E	-05 -	-2.59	943E-	-06	1.60	33E-03	2.51	18E-04	9.370	09E-02
40	107	a	126	1 (	204	1	1	٦	0	7	0	a	6
	0	•		•			•	3	•		•	•	•
5 D	*RESPONSE	EIS	REAC	TION	BATI	E RHO	28	B FCR 1	FRX-2*				
70 8n	+2,2124	NS. 0 R-07	-1.0	8982-	-06 -	-2.19	21/3 9843	гня то 2-06 -	2300 : 3-53641	2-06 -1	KI AF " 8.34243	·2.4040 -06	16-05+
-4.	3884E-06	-5.4	46 1E	-07	2.56	508E-	-07	4.72	61E-07	8.08	55E-07	2.856	7E-07
6.	8470E-09	-9.2	748E	- 68 -	-2-5	889E-	-07	-3.55	22E-07	-3.91	81E-07	-9.302	28E-07
-5.	4276E-07	-9-3	1274E	-07 - -07	-1.40	998. 1918.	-06	-4.16	18E-07	-1.22	698-07 708-06	-5.283	58-06 738-06
2.	2744E-06	1.7	834E	-06	2.30	)8 1E-	- (5	-2.02	15E-05	8.62	66E-06	9.700	)2E-06
1.	0366E-05	1.2	233 9E	-05	3,54	404E-	-07	-7.64	16E-07	-1.20	70 E- 07	-1.087	74E-08
-1.	0580E-08	-4.5	079E	-09 -	-4-5	159E-	-09	-4.56	35E-09	-4-63	45E-09	-4.734	1E-09
-2	5306E-06	-2.6	133 CE 149 EE	-06 -	-1.20	589E-	-06	-2.09	228-06	5.45	80 E-07	1.018	39E-05
8.	4636E-06	1.1	56 1E	-05	7.22	266E-	-06	3.10	36E-06	3.11	43E-07	-4.123	33E-07
-3.	6057E-08	-2-1	005E	- 68 -	-5.10	550E-	-09	-5-08	60E-09	-5.08	29E-09	-5.278	36E-09
- 1.	17938-05	-7.0	10036 19338	-08 -	-8-4	592E.	-06	-6-23	078-06	3.83	118-06	-1.100	152-05
1.	1739E-05	1.4	543E	-05	7_6	377E	- 06	8.48	79E-07	-2.61	37E-07	-1. 595	53E-08
-1.	2978E-08	-3.4	25 CE	-09 -	-3_41	567E-	-09	-3.61	58E-09	-3.76	09E-09	-4.035	5E-09
- 1.	1535E-08	-3.1 -4 F	1112E	-08 -	-0-0'	487E 1592-	-08	-2-35	988-06	-9.35	14E-06	-9.176	078-06
7.	9374E-06	9.7	928E	-06	3.6	335E-	-06	5.14	57E-07	-1.03	83E-06	-1.288	37E-07
- 1.	7627E-08	-1-6	660P	-08 -	-7.0	16 3 E-	-09	-6-94	79E-09	-7.30	51E-09	-6.797	78E-09
-7.	2733E-09	-1.5	353 SE	-08 -	-2.4	739 E- 1 30 E.	-08	-5-05	27E-07	-1.42	298-05	-1.006	55E-05
-0.	.70352-00	-0.1	/J42E	-00 -	-0.0	0.0 9 5	- 00	-2.70	105-00	J. UZ	<b>335-00</b>	3.77	12-03
4 D	107	4	119	33	102		4	з	0	7	0	0	6
	0						<u> </u>						
20 70	*EPRI SF	E IS NS. 3	DE 23	1110N	HAT AP P	2 88 91/1	C 2 BR	TO AL	CAPTUR	P	1=	7.942	5 R-03+
6 D	3,9336	E-07	1.5	5578E	-07	-2.4	408	E-09 -	2.0865	- E-09	2.5288	E-09	
5	- 126 2E-08	1.	73831	2-07	1.7	962E	- (7	4.21	85E-07	3.80	01E-07	2.36	38E-07
5	-98/8E-07	3. 4.	907CI 60801	s-07 R-07	4.5	314E 229F	-07	2.18	328-07	8.68	848-07 198-06	6.25	302-07
3	8222E-07	3.	22391	3-08	1.0	354E	- (7	3.43	84E-08	4 95	37E-08	8.54	20E-10
3	. 32 30E-07	4_	11811	E-08	5.5	860E	-08	-2.85	77E-07	9.35	21E-07	2.08	11E-09
-4	-0379E-08	-1.	44291 27651	5-07 6-09	-9.2	422B	-08	-7.31	928-08	-5.49	50 K-08	-7.69	942-09 878-09
	.8716E-05	-9.	512 91	3-09	-2.7	215E	-03	-4-13	61E-08	-1.27	35 <u>8-07</u>	-4_06	878-08
-8	.8209E-09	2.	75751	E-09	4.5	986E	-08	4-08	64E-08	1.39	93E-06	2.40	29 <b>5-06</b>
~ 5	.4427E-09	-1.	76721	2-07	-2-3	880E	-07	-2.59	32E-07	-3.28	568-07	-2.30	438-07
- 0	-/ibee-08 -5912e-08	-5.	9 18 1) 428 81	5-08 3-08	-6-5	7408 340 R	-08	-8-88	07E-08	-1.58	748-07	-2-59	005-08 738-07
- 1	.8702E-07	-8.	52341	E-08	-4.0	167E	-08	8.69	69E-09	4.57	57E-06	1.32	39E-07
- 8	.5257E-CE	-3.	777 81	2-07	-5-8	849E	-07	-5.50	10E-07	-2.74	63 <b>B-</b> 07	-9.89	672-08
-9	.8058E-08	-2.	6143) 91031	2-08 -09	-2.5	885E	-(8	-2.61	11E-C8	-2.58	72E-08	-2-61	182-08
- 3	- 2014E-07	-7.	47491	E-08	4.7	4268	-08	-4-44	048-05	1.17	59E-06	4.90	202-06
i	.5847E-C7	-6.	45351	E-07	-1.2	584E	-06	- 1.30	42E-06	-1.77	208-06	-1.09	81E-06
-2	-0573E-07	-2-	04841	E-07	-8.7	653E	- 08	-8.66	47E-08	-8.82	75B-08	-7.76	698-08
-6	.4369E-07	-5.	22841	E-07	1.0	353E	-06	1.19	09E-04	-2.50	738-05	7.74	25E-03

4 D	107	4	1 193	904	4	3	0	7	0	0	6
5 D	*RESPONSI	E IS	REACTION	N RATE	RHC 28	FCR	TRX-2*				
70 80	*EPRI SEL 1.38001	NS. 0 R-06	F 2380 ( 4_3233)	CAPTURI E-06 -1	E EPI/TI	HR TO	AL SCA	TTERIN	IG A = -	-5.218 F-05	7E-04 *
<u>3</u> .	3118E-06	1.4	71CE-05	1.293	17E-05	1.51	53E-05	1.792	21E-05	-2.46	52E-06
3.	5947E-C6	-2.7	459E-06	-5.572	22E-06 -	-1.45	72E-05	-6.449	2E-06	-1-484	+6E-05
-8.	3212E-05	-1-5	4108-06	-2.462	288-05 - 198-05	-8.37 5.72	68E-06 96E-06	-1.398	178-06	-5.950	018-05
5.	8945F-05	5.9	390E-06	2.36	1E-06 -	- 1. 19	37E-04	2.430	4E-04	3.120	)3E-06
-1-	1064E-05	-4.3	325E-05	-2-810	)7E-05 -	-2.23	12E-05	-1-697	1E-05	-2.399	0E-06
-3.	1100E-06	-3.0	075E-06	-8-664	12E-06 -	-1-02	578-05 738-05	-1-024	08-06	-1.02	/5E-06 51E-05
-8.	8670E-06	-1.1	878E-05	-1.145	4E-C5 -	-6.94	17E-06	9.795	4E-06	3.975	59E-04
- 6-	6979E-05	-1.3	51 SE-06	-3.187	58-05 -	-4.41	41E-05	-6.181	98-05	-4.503	33E-05
-3.	2246E-06	-1.3	171E-05	-1.366	598-05 -	-1.92	11E-05	-2.559	0E-06	-6.200	)4E-05
-5.	0663E-05	-2.9	26 1E-05	-2.399	8E-05 -	-2.59	56E-05	3.507	7 E-04	1.172	21E-04
-1.	1902E-05	-0.9	4148-06	-6-348	198-05 - 38-06 -	-7_23	69E-05	-3.794	12-05	-1.391	10E-05
-1.	4438E-05	-1-4	70CE-05	-1.598	98-05 -	-7.02	35B-05	-8.845	4E-05	-7.722	28E-05
-3.	1714E-05	-3.1	89 1E-05	-5-578	9E-05	1.65	812-05	-8.550	6E-06	1.495	2E-04
- 1.	30212-05	-1.3	106E-05	-5-653	14E-06 -	- 5_61	428-05 568-06	-9.553	18E-05	-5-085	08-05
-5.	1490E-06	-1.2	254E-05	-1-246	1E-05 -	-7.00	73E-05	-1.932	0E-04	-1. 322	29E-04
-6.	9274E-05	-9-9	992E-05	-1, 391	18E-C4 -	-4_04	07E-05	-4_634	1E-05	2.132	20E-04
4 D	107	4	1269	102	4	5	0	7	0	0	6
5 D	*RESPONS	E IS	REACTIO	N BATE	RHC 28	FCR 1	<b>r</b> RX-2*				
7 D	*EPRI SE	NS. C	DF 2380	CAP EPI	THE TO	нсі	APTURE		A=	1.8172	E-01*
03 9	1.9490 1729E-08	E-09 1-4	4-6736 1065F-07	E-09 2	2.5834E- 138-07	-09 I 2.491	4.3482E 008-07	-092 3416	-4516E	-08	007
6	. 3793E-07	9	3837E-07	1_384	0E-C6	2.05	95E-06	3.033	9E-06	4.368	12-06
6.	4288E-06	8.9	231E-06	1.298	7E-05	1.91	748-05	2.604	9B-05	3.366	1E-05
6.	.4445E-06	9	1728E-07	1.600	98-06 -	7.01	21E-07	1.041	38-06 48-05	7.594	0E-07 7E-07
2	. 1921E-07	-4.3	3756E-07	-3.983	9E-07 -	-3.00	8E-07	-2.151	78-07	-2.988	3E-08
-2.	.9764E-08	-1_2	2668E-08	-1.264	48-C8 -	1.26	16E-08	-1.261	8E-08	-1.259	9E-08
1	.8353E-07	-5.9	969 1E-07	1.505	0E-C6	1_14	11E-06	2.768	38-05	4.916	3E-08 3E-05
2.	-5359E-C6	1.6	193E-07	-8.505	9E-07 -	1.208	39E-06	-1.598	4 E-06	-1.002	02-06
-2	.0844E-07 .3428E-08	-2-1	1727E-07	-2-262	198-08 - 178-07 -	-3.32	/0E-08 24E-07	-5.349 -4_689	4E-08	-5.360	5E-08 87-06
- 3.	. 1893E-07	4.5	519CE-07	1.163	2E-06	2.21	88E-06	1.010	7 E-04	5,232	5E-06
3.	230 CE-C6	-2.8	3751E-08	-2.296	0E-C6 -	2.44	14E-06	-1.144	5E-06	-3.898	02-07
- 3.	.7645E-07	-3.7	1802E-07	-4.079	42-02 - 42-07 -	-1_812	22E-06	-9.894	9E-08	-9.975	28-08 28-07
7.	5912E-07	1.7	273E-06	6.798	8E-06	2.67	52E-04	2.745	0E-05	1.107	1E-04
6	.1552E-(5 .7198F-07	1.1	121 1E-05	-1.273	18E-C7 -	-3.859	598-06 ·	-6.134 -2 828	5 E-06	-3-702	9E-06
- 2	2457E-07	-5.2	2771E-07	-5.273	1E-07 -	2.826	57E-06	-7.281	0E-06	9.007	4E-08
3.	.4833E-06	1_4	067E-05	5.357	3E-05	2.578	30E-03	1_261	2 E-03	1.770	4E-01
4 D	107	4	1269	904	4	5	0	7	0	0	6
<b>6</b> n	0		DELCETO								•
70	*EPBI SE	E 15 NS. (	F 2380	N BATE CAPIURI	BHC 28 E EFI/TH	FCR 1 FR TO	FRI÷2≢ ∃ SCAT	TERING	A= -	1.0346	R 0.0*
8 D	-5.8531	E-05	-7.0126	E-04 -	.5814E-	03-1	8.1949E	-03 -1	. 3714E	-02	
- 1.	.4945E-02 .6029F-02	-1.0	180CE-02	-1.034	17E-C2 -	-1.03	13E-02	-1.092	7E-02	-1.409	1E-02
- 2	736 1E-02	-3.2	2333E-02	-3.245	57E-02 -	2.85	38E-02	-3.459	28-02	-4.654	2E-02
-6.	5793E-03	-2.5	5349E-04	-4.367	9E-C4 -	3.27	73E-04 -	-3.693	5E-04	-1.949	5E-03
-2	.4288E-03	-5-4	123E-04	-1./4:	98-C3 -	·1-150 ·2-184	36E-02	-5-309	7E-03	-1-982	8E-03 2E-04
-2.	2553E-04	-9.6	131E-05	-9,606	8E-05 -	9.600	03E-05	-9.603	2E-05	-9.599	1E-05
-2. - A	.9004E-04 .6011F-04	-2.7	981E-04	-8.019	0E-04 -	1.22	768-03 ·	-4.184	1E-03	-2.004	38-03
-5.	4378E-03	-6.7	317E-03	-6.690	)1E-03 -	6.416	56E-03	-7.530	3E-03	-5.116	28-02
- 1.	2708E-03	-1-2	308E-03	-3-560	1E-04 -	3.57	05B-04	-3.551	6 E-04	-3.569	0E-04
-3.	. 330 cE-04 . 2534F-03	-1.4	1397E-03	-1.470	92-03 - 22-03 -	2.904	188-03 · 598-03 ·	-2.691 -2.592	7E-03	-6.429	3E-03 7E-03
-7.	0333E-03	-9.6	182E-03	-1.123	6E-02 -	9.353	32E-03	-4.522	3E-03	-1.616	7E-03
- 1.	6020E-03	-4.2	71CE-04	-4-229	1E-04 -	4-266	54E-04 ·	-4.227	5E-04	-4-268	0E-04
- 1.	.0137E-03	-3.3	2232-03	-5-876	6E-03 -	-7.406	52E-03 · 10E-02 ·	-9.051 -4.790	/E-03 7e-03	-7.936	UE-03 1P-07
- 1,	5958E-02	-1.8	75 1E-02	-1.738	5E-02 -	1.448	33E-02	- 1. 778	8E-02	-1.062	5E-02
-1.	9820E+03	-1.9	717E-03	-8-432	2E-04 -	8.332	26E-04 ·	-8_486	5E-04	-7.246	3E-04
-9	34828-03	-1.3	2512-03	-1.823	9E-02 -	- <b>5.</b> 346 8. 346	5F-02	-2.440	0E−U2 6₽−02	-1.758	/ E-02

4D 107	4 1276	102	4	3	0	7	0	0	6
0 5d *response	E IS REACT	ION BATE	RHO 28	FOR T	RX-2*				
7D *EPRI SEN 8D 2.45981	IS. OF 238	U CAP EPI 54e-06 1	/188 T	0 0 CA	PTURE .37001	- 12 9-	λ= 79195	5.52801	B-05*
4.4762E-11 2.1313E-10	7.6707E-	11 9.790 10 4.037	6E-11	1.149	3E-10	1.3883	E-10	1.5993	3E-10
1.7175E-09	2-4132E-	09 3.516	5E-09	5.193	6E-09	7.0419	E-09	9.088	BE-09
1.7323E-09	2_4647E-	10 4_311	48-10 3E-10	-1.877	46-10 58-10	5.1082	E-10 E-09	2.1707	7E-10
5-8906E-11 -7.9891E-12	-1. 1753E- -3.4001E-	10 -1.069 12 -3.393	7E-10	-8.067 -3.386	1E-11 1E-12	-5.7760	E-11 E-12	-8.0212	28-12 58-12
-1.0201E-11 4-9224E-11	-9.8100E- 1.6006E-	12 -2.810 10 4.034	3E-11	-4.349	8E-11 3E-10	-1.5146	E-10 E-09	1.0449	98-11 98-08
6.8027E-10	4.8887E-	11 -2.287	9E-10	-3.253	9E-10	-4.3053	E-10 E-11	-2.6990	08-10
-1.43882-11	-5-8505E-	11 -6.105	9E-11	-8.944	9E-11	-1.2624	E-10	-2.8740	DE-10
8.6893E-10	-7.7439E-	12 -6.188	9E-10	-6.577	8E-10	-3.0825	E-10	-1.0496	5E-10
-1.0229E-10	-2.7085E- -1.0175E-	11 - 2.675 10 - 1.097	1E-11 9E-10	-2.692 -4.876	5E-11 0E-10	-2.6638	E-11 E-10	-2.6854	4E-11 DE-11
2.0393E-10 8_4843E-09	4.6383E- 3.0218E-	10 1.824 09 -3.430	0E-09	7.194 -1.036	0E-08 1E-09	7.3936	E-09 E-09	2.972	4E-08 9E-10
-1.7987E-10	-1.7756E-	10 -7.557 10 -1.410	8E-11	-7-449	78-11 18-10	-7.5665	E-11	-5-9809	9E-11
9.3427E-10	3.7833E-	09 1_446	6E-08	6.957	6E-07	3.4049	E-07	4.771	98-05
4E 107	4 1276	904	4	3	0	7	0	0	6
5E *RESPONSI 7D *EPRT SEI	E IS BEACT NS. OF 238	ION BATE II CAPTURE	BHC 28	FOR T	RX-2*	TTERING	<b>)</b> = -	-1- 0870	R-02*
8D -3.46061	E-06 2.47	50E-05 -1	- 1913E	-06 -1	.4863	E-04 -9.	2648	-04 -1 599	38-04
-1.6456E-04	-1.8193E-	04 -2.04	19E-C4	-2.198	4E-04	-2.2344	E-04	-3.256	9E-04
9.2333E-05	2.2628E-	05 9.313	7E-05	2.127	5E-04	3.5443	E-04	-1.041	2E-04
4_4830E-04 -1_4980E-04	8_8032E- -4_1325E-	$05 1_0072$ $04 - 2_0420$	21E-04	-1.824	7E-04	-1.3499	E-03	-6_904	58-05 28-05
-1_8998E-05 -2_4531E-05	-8.1050E- -2.3702E-	06 -8.103 05 -6.814	8E-06	-8_102	3E-06 9E-04	-8.1094	E-06	-8.110	0E-06 1E-04
-6-9968E-05 1.0419E-04	-9.2253E- -2.6892E-	05 -8.652 04 -4.063	24E-05 35E-04	-5.018	08-05 48-04	1.6468	88-04 88-04	4.002	0E-03 1E-04
-9.4523E-05	-9.1516E-	05 - 2.654 04 - 1.129	3E-05	-2.666	4E-05	-2.657	2E-05	-2.675	4E-05
-4-1850E-04	-2.3675E-	04 - 1.903 04 - 7.234	39E-04	-1.969	5E-04	4.337	5E-03	3.834	4E-04
-1.1935E-04	-3.1949E-	05 -3.16	91E-05	-3.202	9E-05	-3.1798	E-05	-3.216	5E-05
-2.6164E-04	-2.6161E-	04 -4.495	55E-C4	2.283	5E-04	-1.590	E-05	3.943	2E-04 1E-03
2.6279E-03 -1.1768E-04	7.4165E- -1.1814E-	04 -2.978 04 -5.088	38E-C4 54E-05	-6.122	8E-04 7E-05	-9.4018	BE-04	-6.135	7E-04 5E-05
-4-4021E-05 -6-6055E-04	-1.0461E- -9.7641E-	04 -1.06	15E-C4 32E-C3	-5.924	0E-04 0E-04	-1_692	E-03 BE-04	-1.231 8.792	5E-03 9E-04
4D 107	4 2000	901	4	3	0	7	0	0	6
5D *RESPONSE	E IS REACT	ION BATE	BHC 28	FCR T	8X-2*	81187	1-	h 1050	8_ 07 ÷
8D 1.28681	E-06 1.66	45E-06 -9	9.1125	2-06 -2	-2 IN .7900	E-05 -2.	5011	4-1958	+ + + + + +
9-0477E-06	6.2654E-	05 4.242	0E-06	3.090	78-05 88-06	2.187	E-05	7.360	4E-05 1E-06
1.9265E-05 1.5266E-05	2.1857E- 1.0184E-	05 2.029 05 3.408	88-05 828-05	5 <b>.1</b> 81 8 <b>.</b> 772	8E-05 3E-06	3.7629	E-05	1.816 -7.063	5E-05 5E-06
1.5839E-05 -2.6606E-05	1.3871E- -4.0732E-	06 7.018	37E-07	-8.586	7E-05 4E-07	6.8278	E-05	-1.760	8 2-05 7 8-10
-3.6993E-10	-1.504 CE-	10 -1.47	38-10	-1.469	2E-10	-1-4767	B-10	-1.507	3E-10
-3.5215E-05	-3.1838E-	05 1.099	98-05	1.114	62-05	5.1912	E-05	4.232	82-05
-1. 27 12E-10	-3.234 1E-	11 -5.656	4E-12	-5.129	25-06 6E-12	-3.953	E-0/	-2.182	02-08 58-12
-5.5625E-12 -4.8844E-04	-4_1916E- -4_7084E-	11 -2.270 04 -2.823	118-10 68-04	-4.045 -1.065	48-09 58-05	-5.6609	E-08	-1.724	5E-04 0E-07
-2.3082E-06 -2.7615E-11	-2.9177E-	06 -1.597 12 -5.122	4E-06	-2.184	4E-07 1E-12	-2.5050	E-09	-6.418	7 <b>E-11</b> 8E-12
-2.7110E-11	-5.990 SE-	11 -2.25	48-10	-6.138	5E-08	-1.4568	E-06	-3.515	38-06
-3.3035E-06	-2.636 SE-	05 -1.579	6E-05	-5-977	2E-06	-1.1691	E-06	-1.019	8E-08
-3.3588E-11	-9.2723E-	11 -1.332	7E-10	-9.172	4E-09	-3,3181	E-06	-1.301	48-05
- 1. 3/298-05	-2.JJU2E-	vo -0.935	05-06	1.727	UK→04	- 1.4376	E-04	4.432	5E-03

4 D	107	4	2000	903	4	3	0	7	0	0	6
5 D	*RESPONS	E IS	REACTIO	N BATE	BHC 2	B FCR T	RX-2*				<b>.</b>
7D 8D	*EPBI S 3.3058	ENS. E-07	OF 2380 1-5353	CAP EP E-07 -1	PI/TEB 1426	TO DB* E-07 -4	*2 IN •9363	VOID E-07 1	λ= .9184	5.6318 E-08	E-04 *
2.	6093E-06	3.9	055E-06	3_889	6E-06	2.291	0E-06	2.208	7E-06	3.795	1E-06
1.	3914E-06 8307E-06	2.2	2466E-06 1093E-05	4_868	68-06 58-05	5.133	5E-06 7E-05	7.175	38-06 78-05	7.529	4E-06 5E-06
3	9719E-06	3.	27128-07	1.061	0E-06	3.402	1E-07	4.942	1E-07	-9.693	5E-08
3_ -4_	3220E-06 8138F-07	3.9	9105E-07 5788F-06	4-824	78-07	-3.459	0E-06	8.550	0E-06 7R-07	-7.481	98-08 28-08
- 8_	8116E-C8	-3.7	1547E-08	-3.751	3E-08	-3.747	6E-08	-3.747	9E-08	-3.744	9E-08
-1.	1308E-C7	-1.0	)894E-07 5725R-08	-3.113	15E-07	-4.705	9E-07	-1.372	72-06 38-05	-4.487	28-07
-2.	9110E-07	-1_5	5276E-06	-1.958	6E-06	-2.108	4E-06	-2.696	6E-06	-1.937	9E-06
-4_	8946E-07	-4_7	7422E-07 522CE-07	-1-371	4E-07	-1.375	1E-07	-1.367	4 2-07 8 2-07	-1.373	3E-07
- 1.	5151E-06	-7.3	88 1E-07	-4.322	0E-07	-1.177	6E-07	3.244	7E-05	6.356	9E-07
-9_	9496E-07	-3_1	175E-06	-4.679	8E-06	-4.433	7E-06	-2.262	4 E- 06	-8-192	78-07 58-07
-8-	1730E-07	-8.	958E-07	-8.755	5E-07	-3.596	6E-06	-4.042	2E-06	-3.086	1E-06
-1.	0061E-06	-7.2	2249E- (7 5291E-06	-1.854	14E-07	6.475	2E-05	4.896	5E-06	1.933	8E-05
-9.	6397E-07	-9.5	593 EE-07	-4.103	6E-07	-4.055	4E-07	-4-130	5E-07	-3_628	6E-07
-3.	6555E-07	-8.6	5235E-07	-8-660	)3E-07	-4-656	98-06	-1.124	3E-05	-6.834	6E-06
2.	32005-00	2	JJ72E-00	2.007	00-00	2.507	05-03	0.045	06-00		26-04
	407				_	_		_			
40	0	4	2000	902	4	3	0	7	0	0	6
ים 510 יחד	*RESPONSI *EPRT SI	E IS	REACTION	N BATE	RHC 28	B FCR TI	RX-2*	CLAD	1=	1 9620	P-03*
8 D	6.4223	E-07	1.1274	E-06 -1	. 2726	E-07 -1.	<b>4</b> 0381	3-06 1.	40601	3-06	6-VJ+
1.	2500E-05	1.7	0298-05	7.350	5E-06	2.584	1E-05	6.8802	28-06	6.509	52-06
1.	4736E-05	2.0	343E-05	3.129	1E-05	5.834	2E-05	5.461	7E-05	1.534	4E-05
1_ : 1_ :	2146E-05	1.0	01 1E-06	3.194	4E-06	1.053	5E-06	1.511	3E-06	2.592	7E-08
- 2.	8236F-06	-1.0	0538-05	-6.420	6E-06	-5.076	6E-06	-3.8088	3E-06	-5. 330	7E-07
-5.	3229E-07	-2.2	68CE-07	-2.265	9E-C7	-2.263	5E-07	-2.2638	3E-07	-2.262	0E-07
-6-	0539E-07	1_8	875E-07	3,131	7E-06	2.766	8E-06	2.9018	3E-05	5.456	7E-05
- 1-	1459E-07	-3-6	848E-06	-4.949	4E-06	-5-352	1E-06	-6.755	5E-06	-4-7219	92-06
-3.3	247CE-07	-1.3	11 1E-06	-1.331	3E-06	-1.809	1E-07	-3.245	7E-07	-5.262	4 E-07 7 E-06
-3.	7719E-06	-1.7	111E-06	-8-023	0E-07	1.725	4E-07	3.398	78-05	8.816	28-07
-6.3	2888E-07	-1.6	7588-07	-1.658	18-06 98-07	-1.673	/E-06	-1.6574	12-00	-1.672	02-07 32-07
-6.	3194E-07	-6-3	395E-07	-6.780	2E-07	-2.837	7E-06	-3.300	E-06	-2.474	1E-06
1_1	4363E-05	-1.1	886E-05	-2.279	1E-05	-2.338	3E-05	-3.1478	3E-05	-1.936	3E-05 3E-05
-3.(	6163E-06	-3.5	970E-06	-1.538	1E-06	-1.5198	8E-06	-1-5477	E-06	-1.3612	2E-06
-1.	0887E-05	-3-2	223E-06	-3.247	62-06 12-05	-1./498	52-05 98-04	-4.3370	)B-05 78-04	-2.6190	52-05 48-03
4 D	107	u	2000	900	u	٦	0	7	0	0	6
5.0 3	O	e te	PRICTTO		<b>BRU 3</b> 8		- 		•	•	-
70 ·	*EPRI SI	ENS.	07 2380	CAF EP	I/TEE	TO DB**		HODERAT	λ=	2. 90281	3-02*
3B 2 -	7_44401 16918-04	2-06 2 4	1_4902:	E-05 9.	.3352E	2 6 1 9	.36391 5P_0#	-05 6.	9192E	-05	12-04
1.9	9819E-04	1.6	433E-04	1.753	0E-04	1.5932	2E-04	2_4917	E-04	1. 9383	1E-04
2.1	8887E-04	2.8	7702-04	3.972	8E-04	3.4033	3B-04	4.6370	E-04	4.5123	E-04
9	1676E-05	1.2	846E-05	4.066	8E-05	-3.9344	4E-06	1.3950	E-04	5.6901	E-06
1.1	5379E-06	-6.0	256E-06	-1.464	7E-05	-1.1027	78-05	-7.8856	E-06	-1.0944	12-06
-1.	3909E-06	-1.3	373E-06	-3.829	7E-06	-5.923	7E-06	-2.0592	2=05	1.4177	12-06
6-6	5679E-06	2.3	103E-05	5.798	4B-05	4.3739	98-05	3.5505	E-04	2.4413	32-04
-7_3	3172E-06	-6.6	813E-06	-1.896	1E-06	-1.8910	)B-05	-1.8738	E-05	-1.8771	E-06
-1-8	8704E-06	-7.6	006E-06	-7.923	8E-06	-1.1594	E-05	-1.6337	E-05	-3.7088	8E-05
3.2	2894E-05	-2.4	645E-C7	-1_255	1E-05	-1.3268	BE-05	-6. 1968	E-04	-1.5639	05-05
- 1. 5	5228E-05	-4-0	30 1E-06	-3.979	5E-06	-4.0045	5E-06	-3.9609	E-06	-3.9921	E-06
- 1	1280E-06	-1.5	102E-05	-1.628 4.348	5E-05	-/-216	)E-04	-0.0001	E-05	4.1170	12-06 )2-04
1.	5866E-04	3.3	C2 9E-05	-4-051	3E-07	-1.2122	2E-05	-3.3729	E-05	-2.0208	2-05
-3.6	554E-06	-3.6	053E-06 381E-05	-1.533	78-06 88-05	-1.5113	3E-06	-1.5344	E-06	-3.4093	E-05
1.	1039E-05	1.8	837E-05	1.634	4E-04	4.1978	3E-03	1.2363	E-03	1.6564	E-02

4 C	107	4	1262	452	4	3	0	8	0	0	7
<b>6</b> n	0										
2 L 7 L	*RESPONS	8 I S Ng 7	REACT	LON BATE U PIC PDI	DELTA	25 FOR	TRX-	•2 *		-1 33618	0E +
£D	-1-25741	E-06	-2-62	59E-06 -4	1-6573	10 2380 F-06 -3	. 4813	18 18-06 - 2	74 79 24 79	-1.22015 F-07	-05+
- 1_	0744E-08	-7.7	758 1E-	10 -2.923	9E-10	-1.854	8E-10	-1.3610	E-10	-1.1313	E-10
- 1.	9219E-10	-2-1	1647E-	10 -1.964	1E-10	-5.790	2E-12	9. 7822	E-17	-1.0704	B-15
-8.	6759E-14	-2.9	9575E-	10 -1_747	6E-C9	-3.542	7E-14	-2.3561	E-14	-2.3291	E-14
-3.	2939E-15	-2.8	3732E-	16 -8.535	2E-16	-3.362	1E-16	-4.5298	E-16	-5.4514	E-16
-2-	8700F-15	-4.(	1938E-	16 -8.045	07E-16 UB-16	-1.288	2E-15	-7.4932	E-15	-5.3469	E-16
-2.	345 FE-18	-9-6	35558-	10 -2-903	14 E - 10 19 V - 10	-9.836	08-10 Cr-10		8-1/ 8-10	-2.4000	E-10 F-19
- 3.	1727E-18	-3.3	3787E-	18 -1.344	9E-17	-5-313	6E-17	-5-5577	E-16	-3-4335	E-16
-2.	0208E-16	-3.8	3053F-	16 -6.653	4E-16	-4.733	6E-16	-9-2224	E-15	-1.6521	E-14
- 1_	5883E-15	-1.0	)763E-	15 -7.935	5 <b>E-1</b> 6	-6.849	2E-16	-7.5751	E-16	-2.9494	E- 16
- 1-	6523E-17	-9.(	)30€E-	18 -2.136	9E-18	-2.081	7E-18	-2.0564	E-18	-2.1119	E-18
-2-	2268E-18	-1-2	255 EE-	17 -2.972	7E-17	-1-291	3E-16	-3.6028	E- 16	-1.0132	E-15
-0.	0093E-10 84068-15	-0.3	548822-	16 -7.935	48-16	-9.976	2E-16	-2-7854	E-14	-1.8808	E-15
- 1-	16 10 - 17	-2.7	12745-	18 -2.644	19F-19	-2.657	38-19		5-10 F-18	-2 7742	6-1/ F-19
- 1.	22 18E- 17	-1.6	255E-	17 -3.580	7E-17	-7-447	28-16	-1.1755	E- 15	-1-1585	R-15
-6.	5087E-16	-8.5	5940E-	16 -2.414	6E-15	-5-487	3E-14	-5.8917	E- 15	-2.3749	E-14
-8.	6666E-15	-5.9	985 9E-	15 - 4.144	7E-15	-2.960	2E-15	-2.9315	E-15	-3.8613	E-16
- 2-	29 17E-17	-1.9	108E-	17 -7.554	1E-18	-7.264	6E-18	8 -7.3027	E-18	-6_5172	E18
-6-	7169E-18	-1-3	7135E-	17 -2.050	8E-17	-3.591	4E-16	-4-4455	E-15	-4.1595	E-15
-2.	546 IE- 15	-4- (	S/ 101-	15 -1.095	0 1 <u>B</u> 1 4	- 3.552	48-13	5 -1.1/92	8-13	0_0	
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5 D	*RESPONSI	EIS	REACT	ION FATE	DELTA	25 FOR	TRX-	·2 *			
70	*EPRI SE	NS. C	DE 235	U FIS EPI	/THE	TO 2380	FISS	SION	<b>A</b> = -	-7.6650B	- 04 *
6D	-1.77591	E-04	-2.39	92E-04 -3	.0899	E-04 -5	.0381	E-05 9.	2228	E-06	
9.	2100E-07	8.8	3938E-	08 3.623	10E-08	2.339	6E- 08	1.7408	E-08	1.4831	E-08
4.	3560F-UE	2.	19272-	08 2.586	28-08	7.418	88-10		E-14	1-1675	E-13
6.	529CE-14	-1.0	18058-	14 -4 252	) 7 E - U C ) A E - 1 B	-2 080	28-13	-2-0000	5-12 7-14	-1.39/3	8-12 9-14
-2.	8576E-13	-4.9	9103E-	14 -4.502	25E-14	7.531	8E-1f	-1-8045	E-12	2-4861	2-14 R-13
1.	5985E-13	1.2	2409E-	13 1.857	9E-14	2.666	0E-15	4.4962	E-16	3.6339	E-17
з.	4787E-17	1.4	4623E-	17 1.456	6 1E- 17	1.463	5e-17	1.4731	E-17	1.4957	E-17
4.	7314E-17	5-0	063EE-	17 2.032	27E-16	8.243	6E-16	2.5166	E-14	1.0868	E-13
7.	9982E-14	1-5	5616E-	13 6.080	)4E-14	-5,195	9E-14	-5.7217	E-12	-7.3436	E-12
	4/338-12	9.6	1091E-	13 0-25	102-14	2.941	18-14		E- 15	1.5723	E-15
2.	2021E-17	1.2	) 74 52-	16 2.838	78-16	1 082	98-14	2.02//	5-1/ P-15	2.0883	2-1/ P-15
- 3.	324 1E-14	-2.2	2088E-	13 -2.214	13E-12	-2.925	6E-12	-6-5250	E-12	2.7128	E-13
1.	2265E-12	5_5	532 SE-	13 4.083	6E-14	-7.179	5E-14	-2.4119	E-15	3.5512	Ē-17
з.	8050E-17	9.8	3474E-	18 9.818	18-18	1.008	8 <b>e- 1</b> 7	1.0291	E- 17	1.0834	E-17
4.	853CE-17	7.3	1732E-	17 1.385	5E-16	-4_268	7E-15	-2.4589	E-14	1.6129	E-13
У. С	49 37E-14	1.1	208E-	13 -6.481	2E-12	-6.212	0E-13	2.7532	E-12	-3.8700	E-11
-9	0420E+ 12 28038- 10	3.0	100 UE-	12 -9.018	538-13 108-16	5-884	18-14	1.0812	E-14	-9.6320	E-17
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-1.	5898E-13	1.4	1918E-	12 8.752	0E-12	3.299	78-10	-2-2190	E-13	0_0	E- 12
4 D	107	4	1262	102	4	3	0	8	0	0	7
5D -	*RESPONSE	TS	REACTI	ON RATE	DRITA	25 202	T P Y -	<b>)</b> *			
70	*EPFI SEN	is. o	F 235t	FIS EPI	ZTHE 7	2380	CAPT	2 - URE	λ=	2_0110E-	01+
8 D	-8.14148	-07	-4.496	7E-06 -1	. 560 1	-05 -7.	3339	E-06 3.6	53441	3-05	
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1.4	4455E-04	1.7	10 CE-0	1.876	9E-04	2.0155	E-04	2.01721	2-04	2. 18371	2-04
7.	70168-04	-4 0	U/4E-( 71378-1	14 -5.656	38-05	4.2703	8 - 05	-2.69821	-04	-2.16961	2-04
-2.	5920E-06	-2.3	1328-0	26 -8_628	48-07	2.8334	18-01	-3.7536	-07	-1-44191	5-05 -05
3.1	2642E-C5	6.3	82 8E-C	5 3.379	4E-05	2_8558	E-05	3,98171	2-05	6.25431	-06
6.	3723E-06	2.7	512E-0	6 2.770	3E-CE	2.7889	E-06	2.80641	-06	2.82071	-06
8.	6376E-06	8_4	771E-0	6 2.485	7E-C5	3.6774	E-05	8.27551	-05	9.78521	-05
4.	0717E-05	4-7	16 1E-0	5 8.847	8E-06	-6.3683	E-06	-9.4865E	-05	-1-82341	2-04
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3.(	0465E-04	3.0	931E-0	)4 6.189	28-05	-3_9307	E-04	-1.0722	1-04 1-04	9_67871	-05
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1_ (	5938E-05	1.7	042E-0	5 1.691	7E-05	-4.3085	E-05	-6.3934	-05	1.73681	-04
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1.(	0329E-03	1.0	617E-0	3 -6.056	3E-04	9.6408	E-05	6.8978E	<b>⊢</b> 05	1.35861	-05
3.5	0/58E-06	3.9	953E-0	1.804	UE-C6	1.8263	E-06	1.93701	-06	1.82291	-06
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and a state of the second s

4D 107	4 1262	904	4 3	0 8	0	07
$\begin{array}{c} 4D & 107 \\ 0 \\ 5E * RESPON \\ 7D * EPRIS \\ 8D - 6.021 \\ -1.1819P-0 \\ -4.7804E-0 \\ 1.3808E-0 \\ 1.7610E-0 \\ -4.4808E-0 \\ 8.65596E-0 \\ -6.4449P-0 \\ -8.6576E-0 \\ -6.4449P-0 \\ -8.6576E-0 \\ -1.1110E-0 \\ -2.4900E-0 \\ -2.4900E-0 \\ -2.4900E-0 \\ -2.4900E-0 \\ -1.6207E-0 \\ -1.6857E-0 \\ -3.8170E-0 \\ -3.9826E-0 \\ -3.9826E-0 \\ -5.0952E-0 \\ -5.0952E-0 \\ \end{array}$	$\begin{array}{r} 4 & 1262 \\ SE IS BEACTIMENS, OF 2350 \\ 4E-04 & -1.530 \\ 4-2.3920F-0 \\ 6-2.0355E-0 \\ 5-1.1047E-0 \\ 5-1.2636F-0 \\ 5-1.2636F-0 \\ 6-2.7763F-0 \\ 6-2.7763F-0 \\ 6-3.4683F-0 \\ 6-3.4683F-0 \\ 6-3.56995E-0 \\ 5-56995E-0 \\ 5-3.9671E-0 \\ 4-27061E-0 \\ 5-3.9671E-0 \\ 4-27061E-0 \\ 5-4.4396E-0 \\ 5-4.4396E-0 \\ 5-4.2606E-0 \\ 6-4.3406E-0 \\ 5-7.3183E-0 \\ 5-7.3182E-0 \\ 5-7.3182E-0 \\ 5-7.3183E-0 \\ 5-7.3182E-0 \\ 5-7.3182E$	904 PIS EPI/T 0E-03 -2.1 5 -5.2346E 6 -4.9766E 6 -2.7538E 5 -3.0986P 4 -5.0986P 4 -2.7921E 6 -2.4667E 5 -3.10986P 5 -3.210986P 5 -3.210986P 5 -3.21086P 5 -3.21	4 3 HR TO 238U 280E-03 -1 -06 -4.299 -06 -2.649 -05 3.473 -06 1.255 -05 3.325 -05 3.325 -05 -3.828 -06 -5.198 -05 -3.828 -05 -3.433 -05 -3.433 -05 -3.433 -05 -3.433 -05 -3.433 -05 -3.829 -04 -2.488 -04 -2.488 -05 -3.829 -04 -2.488 -05 -3.829 -05 -3.829 -05 -3.829 -04 -2.488 -05 -3.829 -05 -3.929 -05 -3.929 -05 -3.929 -05 -	0 8 TRX-2 SCATTERIN .9209E-03 0E-06 -6.0 6E-06 -8.1 2E-06 2.3 1E-05 -4.3 0E-05 -4.3 0E-05 -4.3 0E-05 -5.6 6E-06 -2.8 2E-05 -5.6 6E-06 -8.6 9E-05 -2.9 7E-05 -2.6 3E-05 -2.	0 * G A= - -9.04011 056B-06 290B-05 539B-05 923E-06 719E-04 892E-05 219E-06 748E-05 339BE-05 339BE-05 36E-05 378E-05 378E-05 378E-05 378E-05 378E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 363E-05 365E-05 365E-05 365E-05 365E-05 365E-05 365E-05 365E-05 365E-05 365E-05 365E-05 365E-05 365E-05 365E-05 365E-	$\begin{array}{c} 0 & 7 \\ \hline \\ -1. 3395 E-02* \\ \hline \\ -04 \\ 1. 138 4 E-06 \\ -1. 0489 E-05 \\ \hline \\ -6. 045 6 E-04 \\ 1. 685 0 E-06 \\ \hline \\ 2. 8758 E-05 \\ \hline \\ -6. 3495 E-06 \\ \hline \\ -2. 8332 E-06 \\ \hline \\ -3. 332 E-06 \\ \hline \\ -3. 3572 0 E-04 \\ \hline \\ -4. 784 4 E-05 \\ \hline \\ -8. 645 8 E-06 \\ \hline \\ 3. 0129 E-06 \\ \hline \\ -3. 363 4 E-04 \\ \hline \\ -1. 5437 E-05 \\ \hline \\ -4. 5027 E-06 \\ \hline \\ 1. 2878 E-03 \\ \hline \\ -1. 213 1 E-05 \\ \hline \\ -1. 273 0 E-06 \\ \hline \\ -4. 6526 E-05 \\ \hline \\ 1. 6122 E-03 \\ \hline \end{array}$
4D 107	4 1261	452 1	4 3	0 8	0	07
5D *RESPONS 7D *EPRI SE 6D 4.0631 1.7715E-07 4.5982E-C8 1.0595E-C7 1.1808E-07 4.4431E-08 1.6429E-10 -9.2376E-12 -1.0849E-11 7.5498E-12 -1.0849E-11 7.5498E-11 -1.8892E-11 -8.3713E-09 7.0740E-10 -3.5940E-10 -3.5940E-10 -1.6892E-09 -4.4467E-11 -1.4186E-11 -1.4051E-C8	E IS REACTIONS. OF 235U E-08 1.0651 1.3053E-(7 4.5132E-08 1.3552F-(7 4.9433E-09 6.8897E-09 -2.0107E-10 -3.6821E-12 -1.1624E-11 2.9594E-10 1.796(E-10) -6.8272E-11 -1.1192E-10 -8.0033E-09 -1.7845E-10 -6.2916E-11 -2.1175E-10 6.6846E-10 9.1721E-10 -3.7165E-11 -1.3106E-09	N RATE DE) PIS EPI/TE E-07 2.09 9.6434E- 5.0134E- 1.3534E- 1.2765E- -7.0508E- -3.5708E- -3.5708E- -2.9740E- -1.6765E- -2.8674E- -2.8674E- -5.2633E- -4.34967E- -5.863E- 1.0214E- -4.4815E- -1.6967E- 1.6967E-	$\begin{array}{c} \textbf{TA} \ 25 \ \textbf{FOR} \\ \textbf{HE} \ \textbf{TO} \ 235 \textbf{U} \\ \textbf{59E-07} \ 2, \\ \textbf{-C6} \ 7, 276 \textbf{C} \\ \textbf{08} \ 5, \textbf{7322} \\ \textbf{C7} \ 2, \textbf{0601} \\ \textbf{C7} \ 2, \textbf{0601} \\ \textbf{C8} \ 4, \textbf{8912} \\ \textbf{C6} \ -4, \textbf{1828} \\ \textbf{10} \ -2, \textbf{5977} \\ \textbf{12} \ -3, \textbf{5107} \\ \textbf{11} \ -6, \textbf{5090} \\ \textbf{09} \ 5, \textbf{0167} \\ \textbf{11} \ -6, \textbf{5090} \\ \textbf{09} \ 5, \textbf{0167} \\ \textbf{10} \ -1, \textbf{3297} \\ \textbf{08} \ 2, \textbf{3731} \\ \textbf{09} \ -6, \textbf{3078} \\ \textbf{11} \ -5, \textbf{0437} \\ \textbf{10} \ -1, \textbf{7248} \\ \textbf{08} \ 6, \textbf{5274} \\ \textbf{08} \ -1, \textbf{9612} \\ \textbf{11} \ -1, \textbf{4753} \\ \textbf{11} \ -1, \textbf{0709} \\ \textbf{11} \ -1, \textbf{0709} \\ \textbf{08} \ 1, \textbf{0709} \end{array}$	$\begin{array}{c} TRX-2 \\ NUBAR \\ 3674E-07 \\ 2E-08 \\ 5.93 \\ 2E-08 \\ 7.15 \\ 2E-09 \\ 6.90 \\ 2E-09 \\ 1.39 \\ 2E-09 \\ -4.08 \\ 2E-12 \\ -3.47 \\ 2E-09 \\ -4.28 \\ 2E-09 \\ -4.68 \\ 2E-11 \\ -4.24 \\ 2E-09 \\ -4.69 \\ -4.69 \\ 2E-11 \\ -4.24 \\ 2E-09 \\ -4.69 \\ -4.69 \\ -4.69 \\ -4.69 \\ -4.69 \\ -5.75 \\ 2E-08 \\ -5.75 \\ -5.75 \\ 2E-08 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ -5.75 \\ $	$A = 2$ $2 \cdot 1842 B$ $74 E - 08$ $66 E - 08$ $66 E - 08$ $66 E - 07$ $11 E - 09$ $71 E - 07$ $96 E - 10$ $42 E - 10$ $96 E - 07$ $96 E - 09$ $- 48 E - 09$ $- 48 E - 09$ $- 68 E - 07$ $91 E - 08$ $- 20 E - 08$ $17 E - 08$ $- 20 E - 08$ $56 E - 07$	3. 6104E-05* -07 5. 0271E-08 8. 3802E-08 1. 9274E-07 5. 2585E-09 1. 0989E-09 -1. 0641E-11 -3. 4845E-11 3. 3675E-07 -1. 9869E-09 -1. 7557E-11 3. 3675E-07 -1. 9869E-09 -1. 7557E-18 -1. 0972E-08 1. 5461E-08 -9. 2959E-10 -4. 4746E-19 -3. 9164E-09 4. 9209E-07 -8. 1022E-10 -1. 3553E-11 -9. 2076E-08 2. 9414E-05
40 107 0	4 1261	18 4	3	0 8	0	07
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4 C	107	4	12	61	102	4	3	0	8	0	0	7
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30	*RESPUNSE *FDDT SENG		RF F	101101 1001 1	1 881 15 D	E DELTA DTABUE M	23 208				0 34451	P- 03+
8D	-7 1633F-	.08	-1	22851	13 B	-2 77568	-07 -9	50967	-08 #	69197	-07	6-02+
1	26348-06	1 7	26	22031	2 1	-2.773CD	2 395	58-06	2 6940	00105	2 0201	5-2-05
	38288-06		27	12-06	4 7	2708-06	5 656	58-06	5 1980	P-06	6 3330	08-06
6	7884F-06	9.5	289	F-06	-3.3	8518-06	3 743	88-06	-7 2831	8-05	-2 149	78-05
1.	4512r-06 -	2.0	721	R-07	-8.0	1458-07	-3 840	78-07	-5 8285	B-03	-7 6651	68-07
-4	7982F-06 -	7.7	46	E-07	-6.2	4928-07	1.738	08-08	-2.1864	P-05	5.799	78-07
1.	19475-07	2.0	679	F-07	6.5	0838-08	5.030	37-08	6.8418	B-09	1. 494	9P-10
1.	26497-10	ũ q	590	F-11	1.7	718 - 11	4.665	5E-11	4.5876	R-11	4.580	5E-11
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-6.	29648-05	<u>u</u> .c	1784	F-07	1.4	0848-07	3.544	12-08	8.3745	8-09	2.045	1 F-09
1.	8030E-10	1_1	226	F-10	2.7	8208-11	2.754	98-11	2.7651	R-11	2.886	2 - 11
3.	0850E-11	1.7	890	F-10	4.3	695E-10	1_842	98-09	3. 3032	E-09	-5-8900	08-09
- 1.	2369E-07 -	-2	1604	F-06	-2.1	589E-C4	-1-968	48-04	-1.3427	E-04	5-001	8E-06
2.	2148E-06	1.0	258	E-06	2.5	445E-07	-6.222	7E-06	-6.8605	E-07	4.002	9E-09
2.	210CE-09	4.3	9490	E-10	3.9	699E-10	3.748	7E-10	3.5456	E-10	3.477	0E-10
1.	3604E-09	1.7	1595	E-09	2.9	307E-09	-8.473	8E-08	-3.2085	E-07	1.058	02-06
5.	4643E-07	9.5	546(	E-07	-4_9	684E-04	-1.231	9E-05	1.2986	B-05	-6.960	2E-04
1.	4699E-05	1.1	39	E-05	-3.1	720E-C5	6.848	0E-07	4.5573	E-08	8.518	0E-10
6.	7683E-11	6.5	586	1E-11	2.8	456E-11	2.872	9E-11	3.0820	E-11	2.9922	2E-11
3.	3518E-11	9.	5003	3E-11	1.3	025E-10	2.444	4E-09	-8.2474	E-06	-1.306	8E-04
- 1.	9434E-06	6.4	451	E-06	1.2	782E-C5	9.121	6E-04	-1.3387	'E- C7	9.371	1E-02
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5 D	*RESPONSE	IS	BE	CTIO	N BAT	E DELTA	25 FOR	TRX-2	*			
7 D	*EPBI SENS	5. (	T	2350	PIS E	PI/THE T	0 2350	SCATI	ERING	A= -	1.2129	E-04*
80	-3.6851E-	-06	-1.	4278	E-05	-1.66C4E	-05 -1	.03121	-05 -6.	97098	-06	
-2.	9497E-06 -	-8.	914(	DE-C7	-2.5	168E-(7	-9_659	6E-08	-3.2661	/E-08	2.969	9E-08
-6.	0179E-C8 -	-2.0	060	2E-C8	-5.8	767E-C8	-3.517	9E-08	-1.3072	2E-07	-8.262	4E-08
-2.	7399E-07	3.	347	1E-07	-9.1	136E-07	2.202	3E-07	-1.4579	9E-06	-4.012	8 E-06
8.	3767E-07	4!	540	4E-08	7.5	959E-08	3.311	2E-08	6.0309	)E-08	4.007	7E-08
-9.	4385E-08 -	-3.0	016	4E-07	-5-4	997E-07	6.149	6E-07	-4.320	IE-06	2.373	6E-07
5.	987CE-C7	6.(	070	3E-07	1.2	629E-C8	-4.493	1E-08	-5.293	5E-09	-4.638	2 E- 10
-4.	5073E-10 -	-1.	919	0E-10	-1.9	204E-10	-1.938	0E-10	-1.9663	3E-10	-2.007	1E-10
-6.	4296E-10 -	~6.'	980	6E-10	-2.9	234E-09	-1.408	3E-08	-6.205	5E-07	2.638	3E-07
4.	6720E-07	1.	520	3 <b>E-0</b> 6	1.5	600E-06	1.917	6E-06	-1.632	3e-06	2.881	7e-06
-5.	6416E-06 -	-2.	544	6E-07	-1.2	248E-C8	7.292	5E-08	-4.224	2E-09	-1.794	5E-08
-1.	6302E-09 -	-9.4	442	0E-10	-2.2	866B-10	-2.237	4E-1C	-2.217	08-10	-2.278	3E-10
-2-	4049E-10 ·	-1-	342	EE-09	-3-0	788E-09	-1_414	1E-08	-5.171	1E-08	1.619	3E-07
7.	7845E-06	1.	782	0E-05	-1.8	478E-05	-1.732	1E-05	-3-669	4E-06	-3.089	2E-06
9.	8103E-07	1-	797	3E-06	1.2	178E-06	-7.811	6E-07	-5-266	5E-08	-1.111	1E-09
-8-	6044E-10 ·	-2.	218	SE-10	-2-2	241E-10	-2.297	8E-10	-2.367	1E-10	-2-515	02-10
- ].	1583E-09 ·	-1-	819	4E-09	-3-/	201E-09	-1-516	28-07	-/.912.	SE-0/	-1.414	02-07
2.	3336E-06	1-	530	EE-05	-6.5	620E-05	-4.314	8E-06	1-051	58-05	-1-241	18-05
1.	2895E-06	4-	130	2E-00	-2-8	104E-00	-4.031	35-07	-1.335		-1.203	02-00
-1.	64 30E-09	- !- !	546	1E-09	-0-4	993E-10	-0.432	98-10	-0.011	96-10	-0.403	6 E- 10
-0.	8944E-10 ·	- :-	000	1E-09	-2-3	1010-17	-4.204	20-00	-1 706		2.747	02-00
- 1.	92028-06	-2.	010	22-06	-2.3	2012-17	9.213	53E-07	-1.700	4E-03	J./04	05-01
	*0.7				10-		2	•		•	~	-
41	0	4	•	193	10 2	4	5	v	o	v	U	'
5 D	*RESPONSE	IS	8F	ACTIO	N RAT	E DELTA	25 FOR	TRX-	2 *			
70	*EPRI SEN	S. (	DF	2350	FIS E	PI/THE T	OALC	APTUR	2	<b>A</b> =	7.8712	E-03*
80	-6.0424E	-06	-2	2689	E-06	-2-57378	-07 5	.2771	2-09 3.	.03281	3-08	
1.	0139E-07	2.	268	0E-07	2.2	005E-07	5.040	7E-07	4.491	4E-07	3. 182	7E-07
1.	3357E-06	4.	991	4E-07	5.3	628E-07	2.333	72-06	8.142	5E-07	5.546	5E-07
3.	7614E-07	3.	118	2E-07	2.6	452E-07	4.238	1E-07	3.608	4E-07	5.408	6E-07
2.	0130E-07	1.	021	1E-08	2.8	400E-C8	1.053	8E-08	1_416	8 E- 0 8	1.439	4E-08
7.	8918E-08	1.	212	5E-08	2.9	002E-C8	3.605	4E-08	1_604	3E-07	4.684	7E-08
3.	1455E-08	3.	269	6E-08	1_0	7378-08	6.331	0E-05	4.832	5E-09	6.824	3E-10
6.	8373E-10	2.	918	CE-10	2.9	194E-10	2.922	0E-10	2.922	9E-10	2.924	8E-10
8.	8548E-10	8.	573	7E-10	2.4	770E-09	3.839	5E-09	1.594	6E-08	2.273	6E-08
1.	5593E-08	2.	972	3E- C8	3.0	006E-08	1.268	4E-08	-1-183	4E-07	2.256	22-07
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1.0703E-09	1_4	1796E-09	1.930	3E-09	2.953	8E-09	3.956	3E-09 3E-10	6-006 1-778	3E-09 6E-10
9.3055E-10	1.4	608E-10	2.995	1E-10	3.943	7E-10	2.678	9E-09	2.676	0E-10
1.8332E-10 7.1621E-12	2_2	2331E-10 2553E-12	9.149	3E-11	6.614 3.056	4E-11 5E-12	5.078	2E-11	7.153	5E-12 5E-12
9-2455E-12	8.9	332E-12	2.556	6E-11	3.854	0E-11	1.219	2 2- 10	1.167	3E-10
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6.2147E-11	6.2	2536E-11	1.827	8E-11	1.837	7E-11	1.830	5 <b>E-11</b>	1_840	9E-11
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1.5512E-C9	1.0	926E-09	7-339	4E-10	4.602	0E-10	2.467	0E-10	9.512	4E-11
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4.4210E-10	6.1	402E-10	-1-849	0E-10	4.775	1E-08	6.259	1E-09	1.457	28-08
2_6074z-10	2_6	5014E-10	3_080	2E-10	2.135	1E-09 8E-10	2.343	62-09 28-10	1.381	0E-09 9R-11
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-7.2019E-05	-5.8	536E-05	-6.154	0E-05	-5.740	4E-05	-8-219	2E-05	-7.542	4E-05
-1.1939E-04 4-0817E-05	-4.8	8836E-05 3775E-07	-3.079	)3E-04 6E-C6	-1.108	2E-04	-4.447	6E-04	-3.275	8E-04
-4.8749E-05	-1.3	3585E-05	-1.779	6E-05	8.328	5E-06	-2.227	9E-04	8.313	6E-05
5-8563E-05	6.3	30722-05 31628-07	2.339	188-C5	1.676	0E-05	1.365	6E-05	1.942	5E-06
2.5240E-C6	2.	442 3E-06	6.999	6E-C6	1.048	6E-05	3.014	3E-05	3.913	22-05
2.8264E-05	5.9	9191E-05 8798E-05	6.099	978-05	2.358	8E-05	-5.537	0E-04	-2.405	5E-04
1.2027E-05	1.	2352E-05	3_633	BOE-06	3.658	6E-06	3.647	9E-06	3.671	5E-06
3_6541E-C6	1_1	469€E-05 6768E+05	1.468	348-CS	1_886	5E-05	2.136	5E-05	4.344	42-05
1.9507E-04	1.	1505E-04	4.062	21E-05	-3.319	7E-06	9.771	4E-06	5.907	0E-06
6.1634E-06	1.0	5693E-06 37858-06	1.660	)6E-06	1.681	6E-06	1.669	78-06	1.688	42-06
2.3761E-05	3.	753 SE-05	-1.065	59E-C3	3.003	5E-04	8.146	4E-04	-3.568	5E-03
4-8149E-04	1-1	846CE-04 268CE-06	-1.922	21E-04	-3.821	28-05	-4.019	28-05	-2.700	5E-05
-5.5401E-06	-1.	3165E-05	-1.33	72E-05	-7.483	7E-05	-1.429	4E-04	-3.362	1E-04
-1.6874E-04	-2.3	2296E-04	-2.690	)2E-C4	-5.216	1E-04	-2.865	0E-03	8.926	4E-04
					_	_				_
41C 107 0	4	2000	901	4	3	0	8	0	0	7
5D *RESPONS	E IS	BEACTIO	N RATE	DELTA	25 FOR	TRX-	2 *		3	
8D -2.4428	ENS. E-05	-6.0437	E-05 -8	21/TH6 3.4364	то рв <del>+</del> E-05 -1	-2 IN -3469	FUEL E-05 3	A= 41581	3.4374 2-05	E-03*
6-7040E-05	7.	1454E-05	6.043	7E-05	4.446	9E-05	3.324	6E-05	3.849	42-05
1.7254E-05	2.0	0407E-05	-3.642	26E-06	4.299	0E-05	-1.837	1E-05	-1-317	98-05
5.968CE-07	-5.2	395 EE-07	-2-088	35E-06	-9-147	9E-07	-1-427	8E-06	-1.251	8E-06
6_2797E-06	3.	1425E-06	2.177	19E-07	8.729	7E-09	2.143	08-10	9_174	1E-12
8.2857E-12	3.4	4024E-12	3.355	54 <b>8-1</b> 2	3-370	3E-12	3.402	6E-12	3.496	0E-12
1. 3500E-05	3.	360 SE-05	5.118	378-06	-3.626	3E-06		42-07 92-05	-2.378	3E-05
-2.2264E-06	1_3	2016E-07	4.800	6E-08	1.473	1E-08	1.965	7E-09	1.194	3E-10
8.9203E-14	6.	+985E-13 9106E-13	8.434 3.845	128-14 198-12	5.759	4E-11	7.644	/E-14 9E-10	8.027 -2.588	UE-14
-9.3230E-06	-1-	2563E-04	-1.210	5E-03	-8.348	0E-05	- 1. 864	8E-05	3.821	02-07
1. 3449E- C6 1. 68 18E- 13	3.9 3.0	9407E-07 6907E-14	1.582	275-C8 592-14	-9.159	UE-09	-4.243	8E-11 5E-14	2.631	6E-13
2.076 CE-13	4 -	7676E-13	1.749	78-12	-3.073	9E-10	-1.169	8E-08	1.952	0E-07
5.9543E-06 4.2411E-05	1.	38328-05 C939e-05	-4.054	19E-04 56E-06	-2.039	58-06	8.581	1E-06	-4.960	5E-05
2.3865E-13	1.	8641E-13	7.210	)1E-14	6.945	7E-14	7.217	4E-14	6.919	1E-14
7.7169E-14 -3.9728E-07	2.2	2633E-13 4150E-06	i 3.458 i 4.404	18-13 58-05	1.458	7E-11	-7.066	1E-08 9E-08	-1.801	9E-06

4 C	107	4	2000	903	4	Э	0	8	0	0	7
5 D	*RESPONS	E IS	REACTIO	N BATE	DELTA	25 POB	TRX-	2 *			
7D 8 n	*EPRI SI	ENS.	OF 2350	FIS EF	I/THE	TO DB*	*2 IN	VOID	<b>A</b> =	4.9873	E-04*
5.	5397E-06	5.1	2011E-06	4.868	8E-06	2.819	- 380 D 8E-06	2.722	- 6141 17-06	5-06 5-590	68-06
2.	1248E-06	3.2	2597E-06	6.593	5E-06	6.244	5E-06	7-504	8 E-06	7.450	2E-06
1-	9328E-06	7.	USJ4E-06 7897E-08	3.661	3E-06	5.475	28-06	2.986	4E-06	4.143	82-06
5.	1140E-07	7	5423E-08	2.053	6E-07	2.341	6E-07	5.743	1E-07	4.032	2g-07
2.	6798E-07	2.6	606 EE-07	7.459	0E-08	3.457	6E-08	2.521	9E-08	3.564	0E-09
4.	6542E-09	4	524 CE-09	1.321	9E-C8	2.164	1E-05	1.229	98-09 38-07	2.030	28-09
1_	3804E-07	2.	5135E-07	2.048	5E-C7	5.819	1E-08	-2.521	3E-06	-6.665	1E-07
-/.	1226E-08	2.	1923E-07 1920F-08	2-342	6E+C7	1.526	0E-07	1.132	3E-07	6.856	7E-08
6.	5102E-09	2.0	6785E-C8	2.949	8E-C8	4.849	8E-08	7.242	7E-08	1.788	8E-07
1.	1282F-07	-1.4	4095E-C7	-2.278	4E-C6	-2.491	1E-06	4.539	5E-06	9.022	6E-07
1.	8035E-08	4.9	9129E-09	4.898	4E-09	4.973	42-09	4.951	4E-09 2E-09	1.687	52-08 28-09
1.	9264E-08	2-0	0153E-C8	2.311	8E-08	9.844	7E-08	1.211	BE-07	3.391	4E-07
7.	5774E-06	3.4	32652-07 51298-06	-5-581	28-06 68-08	3 763	48-05 68-07	3.457	0E-06	-1-377	0E-05
1.	6120E-08	1.6	5140E-08	6 934	1E-09	6.871	4E-05	7.030	BE-09	5.697	7E-09
5.	7893E+09	1.3	3836E-08	1.419	3E+08	8.1610	6E-08	5.231	5E-08	-6.320	3E-07
2.	23526-07		5197E-00	0.0/3	/E-UC	2.038	18-05	3. /53	4 B 0 6	3.6341	¥E-04
• -											
4 C	107 0	4	2000	902	4	3	0	8	0	0	7
50	*RESPONSE	IS IS	REACTIO	N RATE	DEITA	25 FOR	T RX - 2	*			
7 E 8 E	*EPRI SE -9_8653E	ENS.	OF 2350	FIS EP	I/THE 3//10	TO DB*4 ₽-05 3	2 IN 5504₽	CLAD	A=	1.92511	<u>8</u> −03*
2.	4725F-05	2.2	218E-05	9.005	0E-C6	3.0877	7E-05	8.131	7E-06	8_7648	BE-06
5.	8311E-06	5.7	7926E-06	1.649	0E-05	1.657	7E-05	1.3744	E-05	1.3231	E-05
6.	3967E-05	3.1	708E-05	8_762	28-05	2-6156	5E-05	4-322	E-05	7.880° 4.3689	12-06 17-07
з.	8977E-C6	5.9	011E-07	1.403	6E-C6	1.7279	9E-06	1. 171	1E-05	3.2886	5E-06
2.	1996E-06	2.2	278 1E-06	7.459	1E-07	4.391	1E-07	3.3478	BE-07	4.7248	E-08
6	1268E-08	5.9	313E-08	1.712	9E-07	2.6528	3E-07	1.0999	5E-08	1-5635	1E-08
1.	0702E-06	2.0	347E-06	2.043	5E-06	8.5878	BE-07	-2.4540	)E-06	5-1230	5E-06
- 1. 1_	1567E-05	1.1	1096E-06 177fF-07	8.987	1E-07 6E-08	6.2350	)E-07	5.491	3E-07	3.8464	E-07
3.	4669E-08	1.4	084E-07	1.468	8E-(7	2.1359	9E-07	2.8148	BE-07	6.5676	5E-07
5.	2063E-07	-1.6	5705E-07	-5-841	2E-06	-6.3474	E-06	8.7862	2E-06	1.1011	E-06
4	5619E-08	1.2	279E-08	1.219	6E-08	1.2336	SE-08	1.2244	E-08	1.2382	2E-08
4-	6968E-08	4.7	635E-08	5.203	7E-08	2-0221	E-07	2.3208	BE-07	4.5620	DE-07
3.	8077E-05	4.2	28 CE-07	2_473	98-06 38-06	2.9688	2E-05	4.671	E-06	-1.7977	/E-05
2.	9003E-07	2.8	948E-07	1.240	2E-C7	1.2267	E-07	1.251	E-07	9.897	E-08
9.	9962E-08	2.3	662E-07	2.388	78-07	1.2961	E-06	2.7065	SE-06	-4-8832	E-07
	3407E QU	2. (	0012-00	3.401	26-03	1.2000	55-04	2-0101	E-03	1.3003	0 <b>E-0</b> 3
4.5	107	**	2000		14	-	•		•		-
40	0	4	2000	900	4	3	U	в	U	0	'
50 ·	*RESPONSE *FPRT SE	IS NS	REACTION	N BATE I FIS PD	DELTA	25 FOR	TRX-2	*	3-	2 00105	-02*
£0	-1.0755E	-04	-1.7530	E-04 -1.	88901	2-04 8.	9190E	-05 2.	7849E	-04	- 02 +
3.0	6838E-04	3.0	698E-04	2.772	2E-C4	2.9398	E-04	2.3925	E-04	1.9457	E-04
1.	8003E-04	1.7	64CE-04	2.180	3E-04	1.9356	E-04	2.6052	E-04	2.9819	E-04
4.	2533E-05	8.5	43 1E-06	1.742	DE-05	6.6730	E-06	7.4672	E-06	2.1970	E-05
4.	9245E-05 7860E-06	1_1	4491-05	2.825.	3E-05 7E-05	9.0415	E-06	7.3158	E-05	7_0144	E-06
9.	7704E-07	4.1	675E-07	4.167	5E-07	4.1686	E-07	4.1691	E-07	4. 1694	E-07
1.	2606E-06	1.2	1781-06	3.484	)E-06	5.2485	E-06	1.6576	E-05	1.5837	E-05
8	5550E-06	1.2	495E-05	8.188	)E-05	3.0738	B-05	3.1957	E-04	2,3813	E-05
8.	1003E-06	8.1	434E-06	2.378	7E-C6	2.3910	E-06	2.3809	E-06	2.3938	E-06
3.1	3822E-06 8266E-05	9.5 1.9	2342-06	9.651	28-06	1.2767	E-05	1.5492	E-05	3.6318	E-05
5.1	8720E-05	3.4	772E-05	1.488	4E-05	9.2826	E-06	4.9595	E-06	1.4173	E-05
1-	4238E-05	3.8	125E-06	3.780	E-06	3-8180	E-06	3.7849	E-06	3.8225	E-06
8_1	9489E-06	1.4	482£-05	-4_4079	48-05 98-06	0.1091 4_5448	E-04	1.5316 9.2718	2-05 E-05	1.4738	E-05 E-04
2.	1936E-04	7.5	113E-05	3.638	1E-05	2.4979	E-05	4.8039	E-05	2.8138	E-05
5.3	2987E-06	5.2	821E-06	2.261	18-06	2.2352	E-06	2.2777	E-06	5.0955	E-05
2.0	6364E-05	2.6	373E-05	1.641	18-04	3.3285	E-04	9.6165	E-05	2.2340	E-05 E-02

4 D		1	07			4	1	2	62		45	2		- 1	4		1	3			0		8			0		(	)		4	Ļ	
	0																																
5D	*R)	E SI	90	NSE	1	s	RE	1	C11	ON	R	AT I	E I	DE:	1 T	<b>X</b> .	28	P	0 R	Т	RX	-2		*									
7 C -	* 1	E P	RI	SE	NS.		OF	-	238	30	FI:	s7:	23	50	F	IS	TO	) (	23	8ប	N	UBA	R			Å	= -	8. 2	210	70	6— Q	4*	
<b>a</b> 3	- 1	8.	06	85E	-0	5	-1	۱.	75	57E	-0	4 -	- 3.	. 0	71	3E-	-04	4 -	-2.	. 4	16	0 E -	04	_	1.	57	931	B-0!	5				
-7.	16'	73	E	07	-4.	. 9	152	23	E-(	8(	- 1,	. 6	932	2 E ·	- 0	£ -	-9.	.9:	21	9E	-0	s -	6.	86	93	E-	09	-5.	.51	17	9 E -	09	
-9.	01	87	E	09	-1.	- 0	01	13	E-(	8(	-8.	. 9'	74	1 E	- 0	ç.	-2.	.63	28	0E	- 1	0 -	4.	41	18	E-	15	-4.	.79	98.	7 E	14	
-3.	85	15	F	12	-1.	. 3	131	0	E-(	8	-7.	.7	62	5 E -	- 0	8	- 1.	5	76	4E	-1	2 -	1.	04	13	Ē-	12	-9.	. 29	94	32-	13	
-2.	03(	0 1	R-	13	-1	. 3	130	) ¢	E- '	4	-3.	8	529	5R.	- 1	4	-1.	. 41	80	2 E	- 1	4 -	2.	0 1	14	Ē-	14	-2.	. 20	33	2 E-	14	
- 1.	18	29	- F →	13	-1	- 8	125	50		u	- 4	6	080	R.	- 1	ù.	- 1	9	67	28	-1	ù -	3.	31	59	R-	13	-2	. 20	13	4 2~	14	
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- 3	52	7 1		15	-1	 h	100	5	£	17	-1		71	, <u>.</u>	- 1	ī.	_ î'	. U	76	7 P.	- 1	- <sup>-</sup>	1	<i>u</i> 9	53	- -	17	-1	5/	5	9 P	.17	
- J.	75	10	E - P	15	_5	• 7		50	E			• •	101	) E.	- 1	6		· 7	16	20 29	_ 1	<u> </u>	4	20	31	P_	1 /	_1	. J.	100	05-	14	
- 4-	13	17	с— Е_	16	- 0	- L //	132	) () 7 ()	5		22	• U 4	100	ים כ שנוי	1	10	- 0.		50	0E. 810		- o	1	22	31	2- P-	14	- 1.			78-	4.2	
-;-	21.	20		10		- 7		22	E		- 2		200	+ E.		4	- !-		5.5	46	- :	4 -	-	<u> </u>	21		13		. 20	20	167	13	
-0-		0 I 7 7	<u> </u>	14	3.	- 5	202	) C	Ē.	14	- 2	• 41	07. E E I	5 M.	- !	4 .	- !-	.0	04	OE 4 T	-!			40	14		14	-4.	. 0.	30	4.5-	13	
-4-	471	00	E-	10	-1	- 3		22	£		~ 3.	• •	22:	2 E.	- !	1		.0	00	15	-!	! -	3-	02	00	E	17	~3.	. 10	יכו	4 E~	17	
- 3-	21	04	<u> </u>	11	-!	- 5	538	53	E-	10	-4	• 3	33	/ K·	- !	0	-1.	.8	91	18	-1	5 -	<u>.</u>	29	32	E-	15	-1.	· 9.	35	8 E-	14	
-2-	21	19	E-	14	-1	٠ t	944	11	E	14	-2.	• 2	71.	JE	- !	4 .	- 3.	. 61	68	6E	- ]	4 ~	1.	21	51	E	12	-7.	. 6	11	2 E-	14	
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- 1.	66	16	E -	16	- 3,	- 8	39:	35	F	17	- 3.	• 7	73	ZE	- 1	1	- 3.	.7	88	4E	-1	7 -	з.	80	34	E	17	-3,	. 91	19	8 E	17	
-1.	73	68	E-	16	-2	• 5	589	95	E	16	-5	<b>.</b> 0	74	ŧΕ	- 1	6	-1,	.1	07	3E	-1	4	2.	41	36	E-	14	-3.	. 20	58	9 E-	14	
-2.	12	68	E-	14	-3	• (	)0(	) 1	E - '	14	-8	• 3	10	5 E	- 1	4	-2.	.4	09	7E	- 1	2 -	2.	56	54	E	13	-9.	. 9!	93.	7 E-	13	
- 3.	56	58	E-	13	-2	- (	396	54	E - 1	13	-1	- 0	86	5 E	- 1	3	-5.	. 9	50	7E	-1	4 -	4.	57	66	E-	14	-5.	. 41	59	6 E-	15	
-3.	21	06	E-	16	-2	• 6	572	2 C	E 1	16	-1	. 0	55	) E	- 1	6	- 1.	.0	13	8E	- 1	6 -	1.	01	83	E-	16	-9.	.01	83	8 E-	-17	
-9.	36	19	E-	17	-2	- 3	389	9 C	<b>E</b> — '	16	-2	. 8	59	5 E	- 1	6	-5.	.0	48	5E	-1	5 -	7.	19	12	E	14	-9.	. 2	47	8 E-	-14	
-7.	20	68	E-	14	-1	• 6	522	29	E - 1	13	-4	. 2	75:	2 E	- 1	3	- 1.	.5	72	7 E	- 1	1 -	4.	95	61	E-	12	0.	. 0				
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4 C	~	1	57			4	1	2	6 Z		11	=		1	4		-	1			0		8			0		0	)		4		
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10	+ ]	E P I	KI.	SE	NS.		OF	1	238	9U	FI	5/2	235	00	F	IS	T	) 2	231	RŪ	F	ISS	10	N	~	<u>}</u>	-	9.7	51	41	8-0	1*	
80		7	24	73E	-0	2_	1	•	90	OE	-0	1	3.	. 6	55	CE-	-0.	ł.	3.	. 1	93	6E-	01		2.	23	761	8-02	2				
]-	03	54	E	03	1	• 2	20	00	E-(	25	2.	. 4	36(	)E-	-0	5	1.	. 4 (	)4	8 E	-0	5	9. !	59	07	E(	96	7.	63	159	) E	06	
1.	23.	32	E	05	1.	• 3	63	E	E - (	)5	1.	• 2	165	ΞE-	- C	5	3.	.5	55	3E	- 0	7	5.	95	63	<b>E</b> - 1	12	6.	46	86	6 E-	11	
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0.0		0.0		0.0		0.0		0.0		0.0	
4 D	107	4	1261	452	u	3	0	8	٥	0	ц.
0						-	-	-	•	·	•
50 *R	ESPCNSI	3 I S	REACTION	N BATE	DELTA	28 FOR	TRX-2	*			
70 *	EPRI SI	ENS.	OF 2380	FIS/23	SU FIS	TC 23	50 NUB	AR	A= -	-2.2617	E-04*
1 69	3.80031 517-06	1 2	146T-06	8 827	-0002E 88-07	-UC 2	-2001E	-06 2.	22-07	E-06 4 120	82-07
3_60	97E-07	3.4	7278-07	3.783	2E-C7	4.273	3E-07	5.277	5E-07	6.105	5E-07
7.57	26E-C7	9.9	491E-07	1.433	9E-C6	1.480	7E-06	2.104	DE-06	8.748	7E-07
1. 10	58E-06	3.8	115E-08	1.000	0E-07	3.440	6 <b>E-</b> 08	4.943	7 <b>E-</b> 08	2.643	1 E-08
3.26	73E-C7	4.9	754E-08	9.324	1E-CE	-9.766	2E-08	9.936	5E-07	6.191	6E-09
3.72	(//E-10	-5.9	662E-09	-9.926	6E-05	-3-367	7E-08	-5-259	5E-09	-1.367	6E-10
-1-18	348-10		5152-11 6278-10	-6.661	18-10	-8.340	18-00	- 4. 403	25-11 78-09	-4.475	v£~11 5₽_00
-2-51	528-10	3_8	121E-10	2_061	6E-CP	2_847	28-08	1.673	, 5-08 98-08	2, 377	78-05
4.67	41E-08	-3.6	110E-08	-5.338	0E-0E	-4.605	28-08	-6.213	DE-08	-2.558	28-08
-1.51	44E-09	-8.7	535E-10	-2.146	6E-10	-2.130	7E-10	-2.146	DE-10	-2.249	4E-10
-2.42	0 1E - 10	-1_4	331E-09	-3.668	5E-09	-1.699	5E-08	-5.007	4E-08	-1.459	3 <b>2-07</b>
-1-29	08E-C7	-1-4	95 EE- (7	-9-485	3E-C7	-4.509	2E-08	3.069	1E-06	8.280	4E-08
1.51	13/E-09		38/1-10	-0.251	15-05	-8.180	18-107	≁4.183) _5 nc#	5E-07	-1.188	5E-08
-2_15	738-09	-2.7	0375-09	-4,919	7E-09	-2,201	28+07	-1.943	58-10 88-07	-6-840	518-08
-2.65	20E-08	-1.5	2662-08	-4.996	7E-07	4.560	0E-06	2.228	6E-07	3.037	6E-06
2.66	97E-08	-1.8	273E-08	-7.036	0E-07	-2.644	1E-07	-1.050	BE-07	-1.032	9E-08
-5-67	716E-10	-4.8	12 CE-10	-1.933	6E-10	-1.881	6E-10	-1.913	BE-10	-1.728	5E-10
-1.80	9 1E-10	-4.7	402E-10	-5.916	0E-10	-1.330	3E-08	-9.427	7E-07	-1.287	9E-06
	1076-01	- 1. I	0012-01	0.003	70 - 0C	1.030	-D0-2C	3.330	+ ⊑ U B	-2.708	コピーリタ

4D 107	4	1261	18	4	3	0	8	0	0	4
4D 107 0 5D *RESPONSE 7D * EPRI SI ED -2.7576E -4.3385E-04 -1.7952E-04 -4.6940E-04 -2.9918E-04 -1.8012E-04 -1.8012E-04 -1.8054E-06 -2.9095E-09 -3.3148E-09 -1.1152E-06 -2.1920E-04 -3.8883E-08 -5.2615E-09 -2.7462E-05 -6.7663E-06 8.8727E-08 -3.805E-05 -2.755E-05 -2.755E-05 -9.3861E-09	4 2 IS 2 NS. 2 - 04 - 3.3 - 1.6 - 5.7 - 1.9 - 3.6 - 1.1 - 3.5 - 3.6 - 3.7 - 7.7 - 7.	1261 REACTION OF 238U -5.7632H 17CF-04 165F-04 105F-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 102E-05 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-2.8320E-09 -7.3939E-05	-9.5	1244E-09 5486E-05	-9.295	1E-09 8E-04	-4.2681	E-07 E-03	-2.6272	2E-05	-1.662 -4.344	5E-04 4E-01
4D 107 0	4	1261	102	4	3	0	8	0	0	4
5D *RESPCNSI 7E * EPRI SI 8E $-1.19531$ 3.8826E-05 4.7824E-05 1.3904E-04 4.9366E-04 8.5039E-05 3.3900E-07 3.8091E-10 4.2802E-10 2.6430E-07 9.1538E-05 5.5403E-10 9.2008E-11 1.3798E-06 4.1922E-06 4.8672E-09 3.2328E-06 2.0296E-05 8.9455E-11 4.3926E-11 1.9278E-05	E IS ENS. 2-06 3.5 2.2 2.2 1.C 1.C 1.C 1.C 1.C 1.C 1.C 1.C 3.5 5.2 3.5 5.4 4.6 1.1 3.6 3.7 2.5 4.6 5.4 5.4 5.4 5.4 5.4 5.4 5.4 5.4 5.4 5.4	RE #CTION OF 2380 -4.21331 3143E-05 3954F-05 2795E-04 9917E-05 2040E-05 2925F-07 9921E-10 956E-06 5523E-06 3138E-10 7276E-06 3053E-10 3053E-10 3053E-10 3055F-05 3055F-05 3056E-11 2583E-10 0480E-05	RATE FIS/23 2-06 - 412 6-419 2-438 3-089 2-052 2-396 1-435 2-1435 4-226 8-427 8-164 1-410 5-596 1-892 8-480 7-052 2-206 6-457 3-763 2-323	$\begin{array}{c} \textbf{DELTA}\\ \textbf{50}  \textbf{F1}\\ \textbf{50}  \textbf{F1}\\ \textbf{51}\\ \textbf{51}\\ \textbf{51}\\ \textbf{52}\\ \textbf{52}\\ \textbf{52}\\ \textbf{52}\\ \textbf{52}\\ \textbf{52}\\ \textbf{52}\\ \textbf{52}\\ \textbf{52}\\ \textbf{53}\\ 53$	28 POR 5 TC 235 5 TC 235 4.0674 7.8386 3.1117 1.1347 7.8389 2.2360 1.4028 3.7365 3.2793 1.6668 8.0965 7.17668 9.0973 2.4563 8.0138 2.2697 3.8228 3.7328 4.2130 1.9562	$\begin{array}{c} \mathbf{TR} \mathbf{X} - 2 \\ \mathbf{T} \mathbf{U} \mathbf{O} 345 \\ \mathbf{F} \mathbf{U} \mathbf{O} 345 \\ \mathbf{E} \mathbf{E} - 05 \\ \mathbf{E} \mathbf{E} - 05 \\ \mathbf{E} \mathbf{E} - 06 \\ \mathbf{E} \mathbf{E} - 06 \\ \mathbf{E} \mathbf{E} - 07 \\ \mathbf{E} \mathbf{E} - 06 \\ \mathbf{E} \mathbf{E} \mathbf{E} - 06 \\ \mathbf{E} \mathbf{E} \mathbf{E} - 06 \\ \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E} \\ \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E} \\ \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E} \\ \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E} \mathbf{E}$	2 ** 2 URE 2 - 07 2. 4. 2326 7. 9445 5. 2101 1. 5300 1. 6973 2. 1362 1. 3795 1. 3795 1. 3795 1. 3745 3. 4550 5. 3446 8. 1547 2. 8540 1. 0613 3. 6424 7. 6008 2. 0177 5. 1092 1. 0626 4. 0094 3. 2976 2. 9074	A= 83072 E=05 E=044 E=052 E=044 E=048 E=048 E=048 E=048 E=048 E=048 E=05 E=07 E=068 E=048 E=048 E=048 E=048 E=048 E=048 E=048 E=048 E=05 E=05 E=07 E=068 E=058 E=058 E=048 E=058 E=058 E=048 E=058 E=058 E=048 E=058 E=048 E=058 E=048 E=058 E=048 E=058 E=048 E=058 E=048 E=058 E=048 E=058 E=048 E=058 E=048 E=058 E=048 E=058 E=048 E=058 E=048 E=058 E=048 E=058 E=058 E=048 E=058 E=058 E=048 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=058 E=0	9.9783 E-05 4.336 1.019 5.565 1.458 1.833 4.509 1.377 5.728 6.288 9.507 8.560 2.890 5.388 1.098 7.486 4.133 7.788 1.331 3.902 1.033 8.826	E-02* 8E-05 2E-04 1E-05 4E-10 5E-10 0E-04 5E-10 0E-04 0E-04 0E-04 0E-04 0E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2E-05 2
4E 107 0	4	1261	904	4	3	0	8	0	0	4
DC **ESPONSJ 7C * EPRI SJ EL -1.2904H -4.7618E-06 -1.3075E-08 -7.1016F-06 -1.4364E-07 3.0090E-07 1.3365E-06 -1.3385E-09 -1.9170E-09 -3.4185E-07 1.2024E-06 4.5270E-06 -1.5270E-06 -1.6727E-09 -2.4579F-09 -5.5284F-07 1.0117E-06 -2.0723E-09 -8.8247E-10	E IS E = 04 = -1.3 1.4 = -1.6 = -7.5 1.2 1.2 = -7.5 1.2 1.2 -7.5 1.2 1.2 -7.5 1.2 1.2 -7.5 1.2 1.2 -7.5 1.2 1.2 -7.5 1.2 1.2 -7.5 1.2 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 1.2 -7.5 -7.5 1.2 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 -7.5 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202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 202-0772 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5C *RI	ESPONSE	IS	RE	CTIC	DN R	ATE D	BITA	28 PO	R TRX-	2 *			
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2.366	55E-09 75E-08	2_1	2947 3596	E-09	6.	.6470 .6658	E-09	1.04	88E-08 07e-07	4.964	78-08	6.117 5.141	22-08
4.06	14E-07	2.1	2055	E-07	1.	1968	E-07	7.39	64E-08	6.287	8E-08	4. 173	37E-08
1_212 3_684	28E-08 48E-09	1_2	2361 5066	E-08	33.	6323	E = 09	3.66	12E-09	3.656	18-09	3.687	9E-09
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1.325	53E-07	1.9	3720 1361	E-07	5.	,9 <b>974</b> .2494	E-C7	1.90	64E-05	2.021	8E-06	8.086	8E-06
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1.382	0E-05	-1.4 -5.6	528	E-05 E-07	-3.	3653 4224	E-C6 E-06	-5.738	33E-06	1.276	2E-06	-5.062	3E-06
- 1. 395	7E-06	-3.0	697	E-06	-3.	6366	E-06	- 1.744	8E-06	-6.264	3E-07	-6.965	3E-06
7.650	6E-06	7.6	813	E-07	6.	4165	Б-С6 Б-С6	5-510	) 3E-07 18E-05	8.838	58-07 88-05	-1.578	88-06 28-07
-1.558	1E-06 -	-5.7	917	E-06	-3.	7483	E-06	-2.948	1E-06	-2.239	8E-06	-3. 168	6E-07
-4.116	1E-07 -	-3.9	553 835	E-07	-1.	1492	E-07 E-06	-1.356	98-07	-1-358	4E-07	-1.359	2E-07
-1.667	7E-06 -	-2-9	773	F-06	-3.	2899	E-06	-1.764	7E-06	1.330	1E-06	5.585	2E-05
-1.459	3E-06 ·	-1.4	198	E-07 E-06	-4.	1330	E-06 E-07	-5.088	3E-06	-8.010	9E-06	-5-839	1E-06 4E-07
-4.191	9E-07 -	-1.7	144	E-06	-1.	7862	E-06	-2-527	8E-06	-3-394	5E-06	-8.504	3E-06
9.342	8E-06 ·	-9.5	080	E-03 E-07	-8.	2888	E-06	-9.457	0E-06	-4-975	JE-05	-1.856	/E-05
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3.749	0E-05	2.5	220	E-05 E-06	3.	2874	E-06	-5.789	4E-06	-1.229	1E-05	-8.700	5E-06
-7.459	6E-07 -	-1.7	752	E-06	-1.	8051	E-06	-1.016	0E-05	-2.561	2E-07	-1.860	0E-07
-9.002	4E-06 -	-1.2	993	E-05	- 1_	96491	8-05	-8,557	3E-06	-9.861	9E-06	2.042	3E-04
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e_879 5_230	∠E-06 6E-07	5-2	92C) 624	E-06 E-07	3. 1.	29441 53881	2-C6 8-(7	2.393	78-06	2.466	E-06	1.820	7E-06
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6.627	2E-07	1.7	752	F-07	1.	7608	B-07	1.778	9E-07	1.7642	2E-07	1.782	48-07
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4 D	107	4	126	ç	904		4	5		0	8	0	0	4	
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бD	-2.9013	2-02	-9.2	163E	-02	-2.2	2266	E-01	-1.9	340	E-01 -	-2.4926	E-02		
-1.	2029E-02	-7.7	7945E	-03	-6_2	0301	E-03	- 5-	96 1 3E	-03	-4.6	523E-03	-4.488	35E-03	
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-5.	1426E-03	~5-6	2825	-03	-5./	1201	8-03 -04	-4.	941/8	-0.3	-5-7:	975-03	-7.450	50E-03	
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- 3-	2498E-05	-1-3	1856F	-05	-1.3	849	E-05	-1.	3843E	-05	- 1. 3	348E-05	-1-384	45E-05	
-4-	1847E-05	-4_(	0396E	-05	-1.1	5861	E-04	-1.	7752E	-04	-6-0	507E-04	-3.31	33E-04	
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- 1_	8431E-04	-1.3	7914E	-04	-5.1	880	E-05	-5-	2053E	-05	-5.1	795E-05	-5-200	63E-05	
-5-	1888E-05	-2-1	1004E	-04	-2.1	548	E-04	-2.	9895E	-04	- 3_ 9	131E-04	-9.57	04E-04	
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-4-	8416E-04	-5.	3571F	-04	-7.7	139	E-04	-4	1756	-03	-7-2	307E-04	-1.48	29E-03	
-2-	5428E-C3	-2-	656 (E	-03	-2.3	804	E-C3	-1.	9593E	-03	-2.4	196E-03	-1.44	50E-03	
-2.	6990F-04	-2-0	6856E	-04	-1_1	486	E-04	-1.	1351E	3-04	-1.1	560E-04	-1.50	54E-04	
-1.	5169E-C4	-3.5	5795E	-04	-3.5	963	E – C 4	-1.	9380E	-03	-3.3	299E-03	-2.47	95E-03	
- 1.	2664E-03	-1.8	e741E	-03	-2.6	904	E – C 3	- 1.	5344E	-02	-2.2	622E-03	9.29	26 E-03	
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5D -	*RESPONSE	1 I S	REAC	TION	RAT	EDE	ELTA	28 1	OR T	RX-2	2 *	_			
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8	44058-09	1.0	1819F-	-08	1.3	8181	2-08	1.	7532	-08	2.26	458-08	2.810	9E-08	
5.	7281E-09	4.3	177 SE-	-10	1.2	812	3-09	4.	453E	-10	6.72	10E-10	7.440	2E-10	
З.	9900E-09	6.1	90 8 E-	-10	1.2	1351	2-09	1.	110E	-09	1.16	78E-08	7.825	56E-10	
5.	2498E-1C	6.4	1895E-	-10	2.6	6311	3-10	1.	9249E	- 10	1_45	63E-10	2.049	3 <b>E-11</b>	
2.	0521E-11	8_7	155 1E-	-12	8.7	5651	3-12	8.	7600E	-12	8.76	24E-12	8.764	5E-12	
2.	6508E-11	2.	62 1E	-11	7.3	3731	3-11	1.	1105E	-10	3.66	51E-10	3.350	)1E-10	
2.	2985E-10	4.9	1477E	-10	9.8	3421	5-10	4	1/588	-10	1.54	288-10	2.801	1/2-08	
	38135-05	1.0	1735.	-10	00 4 1	9   31      1   1	5- 10 2211	о., И	16838	-11	4 14	345-10	1 170	17-11	
0_	1623E-11	1.6	1778E-	-10	1_6	9771	- 10	2.	2654E	-10	2.7	76 E-10	6.853	32E-10	
7.	9939E-10	7.4	632E	-10	9.9	8141	3-10	1.	5535E	-09	4.98	74E-08	3.196	53E-09	
2.	9004E-CS	2.0	)625E-	-09	1.4	4721	2-09	9.	7762E	-10	4.84	78E-10	1.778	30E-10	
1.	7844E-10	4.7	795E	-11	4_7	4051	8-11	. 4.	7891E	-11	4.74	94E-11	4.798	34 <b>E-1</b> 1	
1.	8149E-10	1.8	3234E	-10	1.9	47C1	8-10	7.	9179E	-10	1.03	343E-09	1.467	72E-09	
9.	4239E-10	1.3	510EE	-09	3.7	3931	8-09	1.	1455E	-07	1.12	21/2-08	4.45	/3E-08	
1.	55938-08	9	329tE 2056t	-09	5-0	2431	5-05	2.	10/95	-09	3.0	61F-10	1 166	50E-09 598-10	
J. 1	17718-10	2	7815F	-10	2.7	9971	r- 10	1.	5103E	-09	<u>n</u> _1(	07E-09	4.658	398-09	
3.	46442-09	7.6	5581E	-09	1.9	880	E-C8	7.	3208E	-07	3.31	49E-07	4.502	27E-05	
4 D	107	4	127	6	904		4	3		0	8	0	0	4	
5 n	U NDFSDANS		DE AC	Φ <b>Τ</b> Ο <b>Σ</b>		<b>2</b> ח		20		DV	· ·	*			
70	* EPRT SI	ENS.	07 2	3807	715/2	3510	6118 815	70°0	SCAT	487. TER	TNG	A= ·	-4. 2612	28-02*	
8D	-4.92491	E-03	-7-2	51 JE	3-03	-6.	1146	E-03	-1.9	532	E-02 -	-2.8847	E-03		
-4-	6773E-04	-3.3	3349E	-04	-1.3	5201	E-04	-1.	3022E	-04	-6.3	388E-05	-6.468	84E-05	
-6.	6074E-05	-4.3	311 CE	-05	-5-2	9891	8-05	-4_	3154B	-05	-6.1	153E-05	-5.379	92E-05	
-4-	6380E-05	-6-6	5936E	-05	-7.7	272	E-05	-4-	1060E	-05	~3.5	378E-05	-8.070	60E-05	
<u>]</u> .	8209E-05	-5-6	5615E	-08	5-6	498	8-06	4_	//94E	-07	1.9	S7/E-06	-1.96	/1E-05	
	07368-05	-5.6	1007E	-05	-3 0	001	6-03 8-05	- 2.	5364m	-05	-1.89	3108-05	-2 661	7 VE-V3	
-2-	66508-06	-1.	13725	-05	-1.1	373	E-06	-1.	1373e	-06	-1.1	3858-06	-1.13	88F-06	
-3.	4459E-C6	-3.3	3318E	-06	-9.5	887	E-06	-1.	4797E	-05	-5.1	228E-05	-2.72	67E-05	
-1.	4216E-05	-2.	5637E	-05	-3.0	117	B-05	-1.	6661E	-05	8.8	45E-06	5.940	53E-04	
2.	6258E-C5	-3.	127 1E	-05	-5.1	373	E-05	-6.	1775E	-05	-7.6	910E-05	-5.33	04E-05	
-1.	3405E-05	-1-3	3027E	-05	-3.7	830	B-06	-3.	8020E	-06	-3.79	004E-06	-3-81	79E-06	
- 3.	8141E-06	-1-9	554 1E	-05	-1.6	134)	E-05	-2.	2788E	-05	-3.0	04E-05	-7.62	54E-05	
-7.	2311E-05	-5.6	0/07E 6364=	-05	-4.3	761	6-C5 8-05	-1.	85.J8E	-05	_0_01	112-04 7468-05	-1 7/4	002-05	
- 1	0370E-V0 7438E-05	-3-0	569CB	-05	-7-4	330	6-43 F-45	-0-	6829P	-05		1928-05	-1-740	118-06	
-1.	7868E-05	-1.5	91048	-05	-1-9	607	E-05	- 8_	5085	-05	-1-01	1498-04	-8-50	732-05	
-3.	8174E-05	-4	21338	-05	-5.6	464	E-05	-7.	146 8E	-06	-2.20	536E-05	6_428	87E-04	
З.	6333E-04	1.	1320E	-04	-2.9	595	E-05	-7.	4804E	-05	-1.1	973E-04	-7.86	1E-05	
-1.	5130E-05	-1.5	520 1E	-05	-6.5	478	E-06	-6.	4983E	-06	-6.64	55E-06	-1-034	458-05	
-1.	0461E-05	-2.1	4837E	-05	-2.5	169)	E-C5	-1.	3949E	-04	-2-2	44 E-04	-1.728	36E-04	

4 C	107	4	2000	901	4	з	0	8	0	0	4
50	0 *RESPONSE	27.5	REICTIO	N RATE I		29 808	70 D V _ )				
7 D	* EFRI SE	ENS.	OF 2380	FIS/23	50 FIS	TC DB <sup>2</sup>	**2 IN	FUEL	<b>A</b> =	1. 5813	E-02*
80	-9.2305E	-04	-2.0727	E-03 -2.	6376E	-03-9.	7776E	-05 2.	0653E	6-03	
<b>∠</b> • n	0603E+03	1.0	5202E-03	1.147	5E-03	7.5822	212-04	5.2410	E-04	5.679	3E-04
3.	5339E-04	4.1	4037E-04 8829E-04	2.623	3E-04 TR-04	3.573	4E-04 5E-04	4.5023 2.015µ	E-04	3.562	8E-04 78-04
7.	9644E-05	2.1	8426E-C5	8.0505	58-05	2.7027	7E-05	3.7480	E-04	2.381	12-04
3.	6197E-05	4_	7162E-06	8.8823	3E-06	2.695	€-05	1.7012	E-04	3.921	5E-05
1.	7819E-05	9.4	8404E-06	8.0199	DE-07	3.8804	E-08	6.6910	E-10	2.767	3e-11
3.	44668-11	4_(	02372-11 045¢F-11	2.2596		2 761	18-11	2 4145	E-11	1.051	4E-11 5p-05
3.	7848E-05	1_0	0125E-04	8.2328	BE-05	5.344	1E-05	1.0974	E-04	1.004	5E-05 6E-04
3.	2368E-06	1.(	076 (E-06	2.8726	E-07	6-9281	1E-08	1.2546	E-08	5.551	3E-10
4.	4544E-12	1.	3275E-12	2.4754	E-13	2.3080	)E-13	2.2546	E-13	2.380	8E-13
1.	0400E-04	2.	1678E-C4	3.1380	)E-04	3-8582	22-10	2.84//	E-09 E-04	1.270	1E-05 1E-06
2.	5456E-C6	8. (	0502E-07	1.1773	E-C7	3.6153	E-09	2.2531	E-11	7.224	3E-13
3.	7039E-13	7.8	396 SE-14	7.6174	E-14	7.7318	8E-14	7.9695	E-14	8.628	8E-14
4	52046-13	7.3	0/6CE-12 2472F-05	4.2108	8E-12	8.1219	JE-10	7.3563	E-08	7.625	6E-07
5.	8561E-05	1.	7525E-05	2.8209	DE-C6	2.9353	E-04	1_0002	F-03	1.684	/8-05 18-11
3.	1542E-13	2.1	4365E-13	9.3875	E-14	9.0322	2E-14	9.3891	E-14	9.024	5E-14
1_	0113E-13	2.9	9977E-13	4.6829	E-13	2.5141	E-11	2-8253	E-08	1.425	6E-06
J.	94 102-06	1.	/2001-05	8-0080	DE-05	9.4279	E-04	1-6640	E-04	4.175	0E-03
4.5	107	"	2000	0.0.7		•	•	0			
41	0	4	2000	903	4	3	0	8	0	0	4
5 D (	*RESPONSE	IS	RE ACTIO	N RATE D	ELTA 2	28 FOR	<b>TRX-2</b>	*			
70 :	* EPRI SE	NS.	OF 2380	FIS/235	U FIS	TC DB*	*2 IN	VOID	λ= 	1.69011	E-03*
CU 1.	-1.97268 35908-04	04 9.9	1158-05	2-05 -1. 7.9453	3645E- 8-05	-04 2. # 1611	0389E- R-05	05 6.	2856E 8-05	-05	58-05
2.	5774E-C5	3.7	176E-05	7,3862	E-05	6_8693	E-05	8.3464	E-05	8.138	1E-05
8.	0231E-05	8.0	16 CE-05	6.4764	E-05	6.4870	<b>e-0</b> 5	6.4247	B-05	5.918	5E-05
1	3037E-05	8.3	478E-07	2-4201	E-06	9.1657	E-07	1.2487	E-06	1.270	5E-06
7.	2723E-07	7_4	265E-07	2-1529	E-06 E-07	1.0883	E-06 E-07	7.0099	8-09 8-09	9.7816	15-06 58-09
9.	8198E-09	4.1	975E-09	4 2043	E-09	4.2145	E-09	4.2194	E-09	4.228	8E-09
1-	2845E-08	1.2	516E-08	3.6709	E-08	6.1744	E-08	4.0358	E-07	5.486	1E-07
3-	/221E-07	7.1	616E-07	1.4138	E-06 E-07	1.0631	E-06	2.3056	E-05	3.7414	4B-05
4 4	6525E-08	4.8	0837-08	1_4212	E-08	1.4362	E-07 E-08	1.4382	E-07 R-08	1.4550	28-07
1.	4600E-C8	6.0	701E-08	6.8700	E-08	1.1651	E-07	1.8386	E-07	5.3638	3E-07
6.	5000E-07	5.6	746E-07	8.1287	E-07	1_5920	E-06	6.6734	E-05	3.6422	2E-06
3.1	28728-08	8 9	1208-00	8.2457	8-0/ 8-0C	2.7954	E-07	8.7950	E-08	3.2014	4E-08
3	5406E-C8	3.7	637E-08	4_4028	E-08	2.5057	E-07	4-8296	E-03 E-07	9.8223	28-03
7.	6070E-07	1_1	545E-06	3.5448	E-06	9.9213	E-05	8.9113	E-06	3.3357	7E-05
1.	0177E-05	5.1	25EE-06	2.0065	E-06	7-2015	E-07	3.6785	E-07	1.1315	5E-07
7.	31418-09	1.7	517E-08	1_8043	8-05 8-05	8.6741	E-09 F-07	8.8779	E-09 F-07	7.1905	5E-09
1.	3561E-06	3.5	739E-06	1.0531	B-05	3,3981	E-05	9.2076	E-06	3.4330	)E-04
4.5						_					
4 ()	0	4	2000	902	4	3	0	8	0	0	4
50	RESPONSE	IS	REACTION	N BATE D	EITA 2	8 108	<b>T</b> R X – 2	*			
710 × 810	EPRI SE -3,7511=	NS.	OF 2380	FIS/235	U FIS	TO DB*	*2 IN	CLAD	A= 1	5.44061	2-03*
5.8	84921-04	4.1	0647-04	1.4250	3334 <u>6</u> - F-04	-04 1 <u>.</u> 1.4046	1003E- 8-04	1 0703	2180£~ R0#	-04 1 0749	5 <b>R-0</b> #
6.	786 1E-05	6.3	702E-05	1.7684	E-04	1.7321	E-04	1.4290	E-04	1.3353	3E-04
1.	0415E-04	1.3	723E-04	1.7432	E-04	2.5032	E-04	2.2886	E-04	7_4545	5E-05
. L.	//95E-05	2.4	905E-06	7.2232	E-06	2.7421	E-06	3.7304	B-06	3.8607	/ E-06
5.9	9249E-06	6.3	630E-06	2.1071	E-05 E-06	1-2629	5-00 E-06	1. 2007.	E-04 E-07	9.4074	12-05 5P-07
1.	2616E-C7	5.3	86 CE-C8	5.3900	E-08	5.3965	E-08	5.3996	E-08	5.4051	E-08
1.0	5374E-07	1.5	8752-07	4.5964	E-07	7.2462	E-07	3.4232	E-06	4.2066	E-06
2_↓ 	5511F-06	5.7	2268-06	1.1345	E-05	8.4685	E-06	5.8206	E-05	1.1675	E-04
2.1	4807E-07	2_5	2628-07	7_4194	5-08 2-08	1.5205	5-08 5-08	1.2928] 7.4644:	6-06 8-08	7.5274	58-09 58-09
7.	5195E-08	3.0	7261-07	3.2579	E-07	4.8657	E-07	6.7481	E-07	1.8093	E-06
2-2	2059E-06	1.9	743E-06	2_7704	E-06	5.1033	E-06	6.7409	8-05	3.7197	E-06
י אנ. אי פ	13682-06	1.9	3/1E-06	2 1500	E-06	4.9792	E-07	2.1785	E-07	8.0006	E-08
8.1	3529E-08	8.5	263E-08	9_3963	8-08 8-08	4.1960	E-07	2. 1703) 6.39621	8-08 8-07	1, 1380	)E-08
8.	3210E-07	1.2	325E-06	3.7122	E-06	1.2149	E-04	1.0942	8-05	7.0033	E-05
5.(	0771E-05	2.6	451E-05	1.1318	E-05	4-8980	E-06	3.83381	E-06	1.9604	E-06
3.) 1.1	26578-07	3.6 2.0	6768-07	3 0200	8-C7 8-07	1.5542	E-07 E-04	1.5852	E-07	1.2530	)E-07
7	5022E-06	1.8	723E-05	5-3099	E-U/ R-05	2.0156	E-00 R-04	3.11/0	5-00 F-0/1	1 2336	E-05

4 D	107	4	2000	900	4	3	0	8	0	0	4
	0						_				
5D -	*RE SPONSE	IS	REACTIC	N RATE D	EITA	28 FOF	TRX-2	· *			
7 D '	* EPRI SE	NS.	CF 2380	FIS/235	U FIS	TO DB	**2 IN	HODER	A A=	6.8844	E-02*
<b>C</b> 3	-4.0971E	-03	-6.2283	E-03 -6-	6672E	-03 2	.4155E-	-03 8	.9221E	-03	
7.1	9294E-03	5.1	1982E-03	4.0258	E-03	3.822	8E-03	2.855	6E-03	2. 158	7E-03
2.	1165E-03	1_!	5494E-03	1_4528	E-C3	1.158	1E-03	1.595	0E-03	1.106	6 E-0 3
1.	4197E-03	1-2	2895E-03	1.5611	E-03	1.163	3E-03	1.491	1E-03	1-395	5E-03
1_1	74538-04	3.	59458-05	7. 1755	R-05	2.827	6R-05	3. 173	88-05	9.190	98-05
	1115E_04	2	12668-05	1 1 1 1 1 1 7	2.00	2 957	02-05	3 190	12-04	2 051	38-05
2.	370(8 05		22006-01	2 2 2 4 4 7	5-04	2.331	20-05	3-107	12-04	2.001	36-03
	37005-03		327UE-US	3.0403	E-05	2-031	35-03	1.300	25-05	2. /90	12-06
_ Z+	1995E-06	1.	1942E-06	1.1944	8-06	1.194	/E-06	1, 195	0E-06	1.195	2E-06
3.1	6144E - 06	3.4	4927E-06	9.9989	E-06	1.512	3E-05	4.983	3E-05	4.545	2 E-05
3.	1136E-05	7.1	1403E-05	1.4135	E-04	1.025	9E-04	7.283	2E-04	5.189	5E-04
4.	0863E-05	3.4	219CE-05	1.9923	E-05	7.207	9E-05	7.400	1E-05	5.442	3E-05
1.	8362E-05	1.8	845€E-C5	5.3932	E-06	5.423	3E-06	5.402	6E-06	5.434	3E-06
5.	4111E-06	2.	1797E-05	2.2032	E-05	2.936	3E-05	3.620	5E-05	8.843	7E-05
1_	0273E-04	6-6	1275F-05	2. 1537	E-(5	6-430	0E-05	1-088	7 E-03	6.914	1E-05
1	09805-04	6.9	56305-05	2.9349	R-05	1 971	98-05	9.745	58-06	2.649	28-05
	656 #8-05	7	11158-06	7 0519	P-06	7 122	62-06	7 062	05-06	7 173	38-06
2.	69668-05	<u>.</u> .	706 68-08		D-00	1 171	08-00	1 5 7 4	72-00	2 003	08-06
	09001-05	4.		2.0000	E-()	1.1/1	55-04	1.324	/E-04	2- 903	0E-05
1.	90766-05	3.	1501E-05	8.9141	8-05	9.950	58-04	1.001	6E-04	6.1/3	88-04
- 4+'	9160E-04	1.0	U197E-04	5.9333	E-05	3.402	0E-05	6.300	4E-05	3.673	7E-05
6.	9163E-06	6.1	8946F-06	2.9514	E-06	2.917	7E-06	2.973	1E-06	6.651	9E-05
6.	7075E-05	1.	584 1E-04	1.5931	E-04	8.571	8E-04	6.125	1E-05	3.798	1E-05
4_	0933E-05	3.8	8 <b>130E-</b> 05	2.2460	E-04	4.417	0E-03	1.225	4 E- 03	1.563	0E-02
4 D	107	4	1262	452	4	3	0	7	0	0	3
	0										
5 D	*RESPONSE	IS	REACTIO	N RATE C	B FCB	TEX-2	*				
70	* EPRT SE	NS.	07 2381	CAP/235	IT WIS	TO 23		R	1= -	1. 9987	8-05+
6 n	-1.96838	-06	-4 2712	- CRE/233	1790p	-06 -5	06337	-06 -2	92021	-07	
-1	7/1392-09	-1		-4 1614	P- 10	-00-5		-1 707	6 0 6 7 J I 6 10 - 10	-1 275	98-10
- 1.	74336~00	_ <u>!</u>	20032-03		B- 10	-2.434	115-10 -	- 1. /0/	0.5-10	-1.3/3	0E-10
- 4-	2000E-10	-2-	56878-10	-2.2511	E-10	-6.595	/E-12 -	-1.10/	9E-10	-1_205	88-15
-9-	6869E-14	-3.	3432E-10	-1.9523	E-09	-3.964	12-14 -	-2.620	2E-14	-2.363	42-14
-4_	9669E-15	-3.3	3341E-16	-9.6745	E-16	-3.726	4E-16 -	-5.059	58-16	-5.595	4 E- 16
-2.	97 18E- 15	-4-	5887E-16	-9_0664	E-16	-1.041	0E-15 -	-8.343	7 <b>E-1</b> 5	-5.584	5E-16
- 3.	7818E-16	-4.	7262E-16	-1.8507	E-16	-8.215	3E-17 ·	-1.361	2E-17	-1.095	3E-18
- 1.	0447E-18	-4.	385 EE- 19	-4-3602	E-19	- 4 - 373	6E-19 -	-4-401	5E-19	-4-465	98-19
- 1-	4086E-18	-1-6	4990F-18	-5-9663	E-18	-2.378	97-17	- 1. 381	18-16	-3.022	38-16
-1.	89338-16	-3.1	678 4 8-16	-6 7780	P-16	- 1 950	28-16	-1 030	07-18	-1.934	28-10
- 1	5/618-15	_0.4	17168-16	-0.7700	D-10 D-16	- 4.330	57-10	- 1.030	78-14	-1-345	45-14 08-14
	24075-10	- 2 - 1	9/102-10		E-10 ·	- 4. 300	SE-10 -	-4.013	25-10	-1.303	3E-10
-/-	34926-18	-2-3	98222-18	-9-3882	2-15	-9.131	08-15 -	-9-010	28-19	-9.24/	UE-19
-9-	7408E-19	-5-4	4798E-18	-1.2938	E-17	-5.667	7E-17 -	-1.653	9E-16	-5.494	7 <b>E-1</b> 6
- 5-	9730E-16	-4-8	8798E-16	-6_0209	E-16	-9.415	4E-16 -	- 3. 06 1	6 <b>E 1</b> 4	-1.947	7 E-15
-1.	7902E-15	-1.2	2942E-15	i -9 <b>.143</b> 2	B-16	-4.974	8E-16 -	-6.457	6 E- 17	-7.241	1E-18
-4_	9764E-18	-1.	1666E-18	-1.1306	E-18	- 1. 135	3E-18 -	-1.140	0E-18	-1.184	0E-18
-5.	2084E-18	-7.	77098-18	-1.5242	E-17	-3.310	0E-16 -	-6.758	0E-16	-8.683	0E-16
-5.	5371E-16	-7-	746 SE-16	-2-1497	E-15	-6-067	28-14 -	-6-465	48-15	-2-527	48-14
-9	0390E-15	-5-1	4108E-19	-2-9182	E-15	-1-672	98-15 -	-1.354	78-15	-1-644	78-16
-9-	65758-18	-8.0	13888-18	-7.1745	P-18	-3 050	8F-18 -	- 1 064	78-18	-2 734	12-18
-2	81788-18	-7	10112-10	-9 6079	P-10	-1.520	19-16 -	- 3 - 1 1 3	18-10	-2 - 7 - 5 - 7	15-10
- 1	0139P-15	_ 10 - 1	13112-10		5-1C ·		- 61-21	- 4 - 76 - 7	45-13	~2.552	46-15
- 14	91366-13	- 4- 4	21432-13	-1-0898	E-14	-3-95/	0E-13 -	- 1. 203	26-13	0.0	
4 C	107	4	1262	18	11	3	0	7	0	0	3
	0										
5 D -	*RESPONSE	IS	REACTIC	N PATE C	B FCR	T FX-2	*				
70	* EFRT SE	NS_	OF 2381	CAP/235	U FIS	TO 23	80 PISS	SION	A= -	2.7516	E-05*
80	1.24675	-05	1.2516	E-05 -7-	74758	-06 -4	-08177-	-05 +4	1295#	-06	
2	64925-08	21	796-19	9_4150	E-(9	6.027	58-09	4.194	1 R-0 C	1.601	98-09
4 .	63835-00	4 4	0, 9 0 E - 0 C	1 06 04	B-00	5 8 9 2 /	60-44	4 4 1 7	45-UJ Ap_46	1 001	55-03 68-14
	24010 10		1911202	1 1 1 1 1 1	5 67	4 2 4	68-11	1.11/	C D - 4 3	1.030	02-14
3.	340 1E+ 12	9-4	+14JE-09	1.1185	E-C/	4.202	6E-12	2.039	68-12	9.338	82-13
6-	0588E-13	9.2	2455E-14	3.1716	E-13	9.191	8E-14	1.389	7E-13	-1.088	7E-13
1. (	0328E-12	1_(	)568E-13	5.4910	E-14	-1.363	1E-12	2.693	8 <b>E-12</b>	-1.789	8E-13
- 3-	2476E-13	-7. 9	5782E-13	-3.4064	E-13 ·	-9.377	9E-14 -	-1.088	8 E- 1 4	-8.215	6E-16
-7.	7304E-16	-3.2	2174E-16	-3.1821	E-16	- 3_ 174	9E-16 -	-3.181	8 <b>E - 16</b>	-3.209	4 E- 16
- 1-	0047E-15	-1.0	0559E-15	-4.1548	E-15	-1.724	9E-14 -	-5.509	4E-13	-3.086	6 E- 13
-1-	0187E-13	-7.9	3132F-14	5.7168	E-14	7.592	12-14	4.177	4E-12	6.453	58-12
- 4.	52478-11	-1-1	44 98-17	-1.1779	E-12 -	-9.767	28-11 -	7. 171	18-17	-1. 587	28-13
-6	43148-15	· = ·	17365-16	-7 1767	F- 16	-6 257	78-16 -	6 667	01-16	-6. 770	38-16
-0.		_ 7 _ 6	11562-13		10 - 10 - P_ 46	-3 0CC	07-10 -	1 554	50-10 67-13	_0.170	55-10 52-13
	04032-10	- 3- 6	34002#13 3406# 43	-0.0130	10 - 10 ·	008°C	VD-14 *	1 054	05-13	-0-2/0	JE-13 JE-14
- /- !	00021-13	- 3.	1452-13	-1-1460	E-13 ·	-0-094	35-15	1.056	UE-11	~>	25-14
-1-1	U5U6E-12	-1-9	405E~12	-1-9842	E-12	-/_804	UE-13 -	-6-204	UE-14	-5.933	5E-15
-3.	7943E-15	-8.6	5677E-16	-8.3336	E- 16	-8-302	7E-16 -	-8_275	1E-16	-8.532	5 <b>E-16</b>
-3.	6928E-15	-5.3	380 SE-15	-1-0462	E-14	-3.269	2E-13 -	-1.353	4 E-12	-1.368	6E-12
-5.	328 1E- 13	-4_6	5570E-13	-3.2870	E-14	2.944	6E-11	2.089	0E-12	1.222	0E-11
-9_	2305E-13	-4_5	5816F-12	-4.7042	E-12	-3-267	6E-12 -	-1.741	4E-12	-1. 275	9E-13
-6-	75838-15	-5.4	51788-15	-2-1506	E-15	-2.050	88-15 -	2.043	1E-15	-1.811	82-15
1	86485-15	_1	75712-15	-5 7030	R-16	-1 000	67-12 -	1.074	0 - 12		1F-12
141	50705-13	- 44 /	13716-13 26260 41	1 3340	10 - 10 ·	2 5 6 1	68-10 "	J. V. V	2 E - 14		
- 4- 3	JUJ42-12	- Ja J	JUZ4E*12	1.3349	<u>c</u> − 12	2.004	05-10	7-040	6 E- I I	V U	

4 D	107	- 4	1262	102	4	3	0	7	0	0	3
5 D	*RESPONSE	IS	REACTIO	N BATE	CR FCI	TFX-2	*				
70	* EPRI SE	NS.	OF 2380	CAE/23	50 FIS	5 TO 23	80 CA	TURE	A =	9.7758E	-01*
ed a	3.9663E	-05	4.0740	E-04 2.	. 10521	3-03 5	4111	8-03 9	.07401	E-03	
· 7.	436CE-03	8.3	3053E-03	9.229	5E-03	1.009	5E-02	1.112	1E-02	1. 2630	E-03
1.	2217E-02	1.4	4654E-02	1.456	2E-02	1.266	2B-02	1.524	8E-02	1.9975	E-02
3.	6577E-03	9.4	1707E-05	8.283	3E-05	1.023	58-04	3.731	9E-05	9.8455	E-04
3.	3340E-04	7_2	27672-04	4-529	98-04 88-04	4.501	58-03	4.531	5E-03 88-04	5.0991	E-04
.7.	0061E-05	3.0	232E-05	3.043	7E-05	3.064	1E-05	3.084	7E-05	3.1017	E-05
<u>9</u> .	5098E-05	9-3	3547E-C5	2.758	1E-C4	4.326	2E-04	1.605	2E-03	1.0275	E-03
4.	32/9E-04	5.4	1/10E-04 225 FF- (3	5.277	9E-04	3.407	1B-04	1.031	1E-03	2.7156	E-03
2.	3768E-04	2.7	173E-04	8.535	1E-05	8.857	6E-05	9.010	1E-05	9.1739	E-04
9.	2699E-05	3.8	8575E-04	4.051	3E-04	5.286	5 <b>E-0</b> 4	6. 138	3E-04	1.7038	2-03
2-	02428-03	2.5	2084E-03 22928-03	1.628	98-03 68-03	1.284	3E-03	8.377	9E-03	1.3240	E-03
1	0852E-04	3.0	933E-05	3.144	6E-05	3.248	2E-05	3.283	5E-05	3.3775	E-05
1.	3186E-04	1_3	3752E-04	1.456	1E-C4	4.082	3E-04	1.441	5E-03	2.3824	E-03
1.	2312E-03	1.3	3595E-03	2.538	7E-03	9.147	2E-03	2.052	42-03	4.7929	E-03
1.	79521-05	1.9	3944E-05	8.981	DE-06	9.079	9E-06	9,579	12-04	9.1614	E-05
9.	7218E-06	2.4	318E-05	2.610	DE-05	1.101	8E-04	8.883	6E-04	4.0428	E-03
2.	9964E-03	5.3	3006E-03	7.952	4E-03	3.188	2E-02	6.774	4E-03	6.1628	E-01
<i>h</i> n	107	4	1262	004	ń	•	0	7	0	0	•
40	0	-	1202	304	4	. 3	U		U	0	3
5 D	*RESPONSE	IS	REACTIO	N BATE	CB FCE	TRX-2	*				
7 D 9 D	* EPRI SE	NS.	OF 2380	CAP/235	OFIS 1 65001	0 2380	SCAT	CERING	A=	2.82971	2-03*
-7.	1949E-05	-2.6	5096E-06	1.160	5E-05	1.484	-0492. 7E-05	4.069	1E-05	1.2406	5E-05
- 5.	0956E-07	-3.5	548 SE-06	-9.767	0E-06	-1.356	7E-05	-1.552	4E-05	-3.1663	BE-05
- 1_	3693E-05	-2.2	2395E-05	-3.097	7E-C5	-1.404	3E-05	-2.076	9E-05	-6.2902	2E-04
	32998-05	4_1	4433E-00 4677F-05	6-057	42-04	-5-599	38-05	8. /20	95-03 28-04	-1.2040	3E-04
6.	8302E-04	1.	186 SE-03	6.449	4E-05	-4.078	1E-04	-4.529	2E-04	-6. 8879	E-05
-7.	0005E-05	-3.0	0177E-05	-3.036	2E-05	-3.054	4E-05	-3.072	6E-05	-3.0872	2E-05
	5945E-06	-4-1	20522-05	-1-242	48-04	-4.073	5E-04	-4.080	98-04	2.2095	78-04
9	0515E-04	1.2	2379E-03	1_042	6E-03	6.271	1E-04	1.220	1E-04	-5.0673	3E-04
-2-	5410E-04	-2.8	8125E-04	-8.714	5E-05	-8.989	4E-05	-9.091	1E-05	-9.2001	E-05
-9.	97438-05	-3. 9_f	11258-04 50868-06	-3.771	28-04	-4-540	8E-04	-4.560	6 E-04	-4.788(	)E-04
6.	6278E-04	1.0	0029E-03	7.082	8E-04	1.153	5B-04	-1.698	1E-04	-1.0200	)E-04
- 1_	1270E-04	-3.	1482E-05	-3.171	3E-05	-3.247	0E-05	-3.252	6E-05	-3.3153	E-05
- 1.	20432-04	-1.2	25468-04 16838-05	-1-247	4E-(4	-2-627	1E-04	1.967	08-04	3.7603	3E-05
3.	2655E-04	4	268 SE-04	3.045	1E-C4	5,197	9E-05	-1.026	7E-04	-5. 7465	5E-05
-1.	9616E-05	-2.	1080E-05	-9.255	1E-C6	-9.205	5E-06	-9.482	9E-06	-8-5591	E-06
-8.	97698-06	-2-0	094 TE-05 11/28-04	-2.098	92-05	-7.791	9E-05	1_715	28-04	-7-0693	32-05
		•••	J 74CE 04	-12703	46-04	- 1- 303	05-04	-1.091	26-04	0.094	12-04
	107			45 Q		-	_	_			
4 B	0	4	1261	452	4	3	0	7	0	0	3
5 D	*RESPONSE	IS	REACTIO	N BATE	CR FCI	TFX-2	*				
70	* EFRI SE	NS.	OF 2380	CAF/23	50 FIS	5 TO 23	50 NU	BAR	A= -	-3.2140E	-04*
- 1_	8621E-07	-1_4	4425E-07	~1_213	0E-07	-1.041	- 500 S	-9.513	- 17 11) 512-08	-8.6918	E-08
-8.	7565E-0E	-8.9	9392E-08	-1.028	8E-07	-1.200	1E-07	-1.527	5 E-07	-1.8229	E-07
- 2_	3786E-07	-2-9	9115E-07	-4.489	4E-07	-4-588	2E-07	-6.765	4E-07	-6.8170	E-07
-9	5523E-08	-1.5	5252E-08	-2.773	2E-C8	-2-407	2E-08	-3.168	4E-08	-1. / 354	E-08
-7.	6637E-10	-1.	7897E-09	-8.259	1E-10	-1.554	2E-09	-2.097	8 E-10	-5.3636	E-12
-4.	6446E-12	-1-8	3482E-12	-1.790	5E-12	-1.759	1E-12	-1.739	5E-12	-1-7429	E-12
-5.	5964E-10	-1_!	524 1E-09	-1.507	0E-0P	-1.494	0E-10 7E-08	-4.005	78-09 98-07	-1.0051	2-09
- 1.	1629E-07	-1_8	9916E-08	-9-207	9E-09	-4-225	1E-09	-3.485	9E-09	-1.0810	E-09
-5.	9149E-11	-3.3	3635E-11	-8.198	5E-12	-8.106	5E-12	-8.147	8E-12	-8.5293	E-12
- y. - 1	54218-08	-2-1	+UUSE-11 77198-09	-1-5/5	38-10	-0-482	5E-10	-2-082	/E-09	-8.6291	E-09
- 3	4431E-05	-1_6	5565E-09	-5.745	4E-09	-3.870	5E-08	-1.601	5E-08	-4_3862	E-10
- 1.	6743E-10	-2.9	9190E-11	-2.553	5 <b>E-1</b> 1	-2.335	0E-11	-2.155	8E-11	-2.0673	E-11
-7.	7864E-11	-9.	7346E-11 1426E-09	-1.771	8E-10	-8-609	1E-09	-1.323	1E-08	-1. 1229	E-08
- 1_	4405E-08	-1.4	4323E-08	-8_876	1E-08	-1-725	0E-08	-4_429	0E-08	-1-3455	E-06 R-10
-2.	0046E-11	-1.6	5955E-11	-6.799	1E-12	-6.608	3E- 12	-6.713	2E-12	-6.0590	B-12
-6.	3417E-12	-1. ( -5	6615E-11	-2-075	78-11	-4.743	5E-10	-4-203	4E-08	-1-0417	E-07
		3.		-0.002	20-25	-2.424	ZE-00	- 1- 202	12-00	-3.04/9	Z-04

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4 D

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4 D		1	07			-4		12	26	1		1	6			4			3			(	)			7		0	)		0			3	
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5 D	*R	ΕS	PC	N S	E	IS	₿	El	1C	II	ON	R	ЛŤ	Е	CE	1	FC	R	T F	X-	•2		,	*											
7 D	*	ΕP	RI	S	E N:	S 🕳	0	F	2	38	U	CA	P/	23	151	1	FI	S	TC	2	23	5ช	P:	IS	SI	ON		1	l= -	-7.	75	583	E- (	01*	
8 D	-	1.	24	97	E-	04	~	3.	6	33	8E	-0	4	-7	- 9	935	5 6	E-	04	- 1	•9	.0!	54	4 E	-0	4	-8.	. 53	865	E-0	4	1			
-7.	34	25	E-	04		5.	66	6 1	1 E	-0	4	- 4	. 6	45	55 E	9-1	C 4	-	3.	89	90!	5B-	- 0 /	4	- 3	- 4	841	4 E-	-04	- 3	- 1	154	7 E-	-04	
-3.	13	16	E	C4	-	3.	17	91	4 E	-0	4	-3	-,6	40	171	5 <b>-</b> (	04	-	4.	23	32:	2E	-0	4	- 5	. 3	6.6	5 E-	-04	-6	- 3	389	2 E-	-04	•
-8.	23	85	E-	04	-	1.	01	7	1E	-0	3	-1	- 5	45	61	- (	0 3	-	1.	55	59	58-	- 0	3	- 2	- 2	95	2 E-	•03	-2	- 7	230	12	-03	i –
-5.	21	48	E-	04	-	3.	21	8 (	δE	-0	5	-9	• 2	45	81	s→(	05	-	3.	66	51	4E	-0	5	-5	•.0	02	) E-	-05	-6	· <b>-</b> 1	109	8 E-	-05	F
- 3.	04	18	F-	04	-	5.	00	58	ÊĒ	-0	5	-9	.5	84	101	S - (	0 5	-	9.	74	15	2E-	- 0 !	5	- 1	. 0	07	5 E-	-03	-1	- 2	212	0E-	-05	
-3.	11	16	E-	06	-	7.	87	93	ΞE	-0	6	-3	. 1	19	)6I	3-(	06		з.	36	52	5E-	- 01	6	- 3	- 1	91	7 E-	-07	-7	!_€	597	2E	-09	F
-6.	59	37	E-	09	-	2.	60	5 (	ÉE	-0	9	-2	. 5	14	101	3-1	09	-	2.	45	59	9 E-	- 0	9	~ 2	. 4	24	3 E -	-09	-2		+17	7 E	-09	F
-7.	47	80	E	09	-	7.	93	0;	2 E	-0	9	- 3	. 5	14	151	3-1	80	-	4.	70	)0	8E	-0	7	- 1	. 6	37.	3 E-	-05	-4	- (	)02	6 E ·	-06	)
-2.	04	78	E-	06	-	5.	20	1	1 E	-0	6	-4	. 8	79	01	3 (	05	-	4.	81	6	4 E-	- 0 !	5 ·	- 1	. 6	21	9 E-	-03	-2		129	7 E-	-03	)
-4.	07	58	E-	04	-	7.	87	2 '	1E	-0	5	-4	_1	46	581	3-(	05	-	1.	79	9	3E	-0	5	- 1	. 1	16	6 E-	-05	- 2	! !	155	3E-	-06	j i
-9:	11	72	E-	08	-	4.	79	9	3 E	-0	8	- 1	. 1	30	)21	3 (	0 E	-	1.	10	0 (	9E-	- 0	8	- 1	- 0	94	1 E-	-08	- 1	• *	136	0 E	-08	ļ.
- 1.	20	8 2	2E-	• <b>0</b> 8	-	6.	95	01	3 E	- 0	8	- 1	.7	03	301	3 1	C 7	-	8.	45	58.	3E	-0'	7	-3	. 6	13	4 E-	-06	-2		564	18	-05	j
-5.	59	63	8 E -	05	-	9.	38	2(	6E	-0	5	-4	- 6	12	291	3-0	04	-	5.	05	54	2E-	- 0	4	- 3	. 3	30	3 E-	-03	-1	- (	548	9E	-04	,
- 1.	30	39	Е-	05	-	7.	13	5(	0E	-0	6	-2	- 4	17	701	3 - 1	C5	-	1.	01	14	7E-	-0-	4	- 2	. 5	13	7 E -	-05	5	i., 9	906	9E-	-07	,
-2.	11	11	E-	07	-	з.	59	7:	2 E	-0	8	-3	. 1	25	531	2-1	<b>د</b> ٤	-	2.	83	38	9E-	- C	8	- 2		04	2 E-	-08	-2	. 1	181	8 E-	-08	1
-9.	.21	50	)E	• <b>c</b> 8	-	1.	12	93	3Ē	- C	7	-2	- 0	41	61	3-0	07	-	1.	.40	)5	6E-	-0	5	- 4	. 8	55	4 E-	-05	-4	. 1	507	8 E-	-05	j i
- 3.	72	43	F-	05	-	4.	15	0	2 2	-0	5	-9	. 3	02	241	3-1	04	-	4.	.51	12	5E-	- 0	3	- 2	- 4	57	9 E-	-04	-3	1.	953	4 E-	-03	ļ.
-4.	99	00	)E-	05		5_	55	0	1F	-0	5	-3	5	13	331	3 - 4	C 4	-	6.	13	39	5E	-0	5	- 9	- 2	80	4 E-	-06	-4		516	7 E-	-07	1
-2	24	40	) E-	- 68	-	1_	86	3.	3 P	-0	8	-7	. 3	77	781	E 1	0 S	-	7.	1	17	1E-	- 0	9	-7	. 1	72	9 E-	-09	-6		440	1 E-	-09	)
-6.	73	10	- F	. 0 9	_	1	76	5	4 E	-0	8	-2	_2	10	121	- 1	сe	_	5.	49	95	6E	- 0	7	- 1	_ 0	01	8 E-	-04	-3	1.	694	SE	-04	Į.
-1.	57	37	18-	-04	-	1.	90	ŝ.	7 F	-0	ŭ.	-2	. 3	2	121	R 1	Č4	_	6.	98	35	6E-	- 0	3	- 4		80	8 E-	-03	-7	1.1	232	4 E	-01	
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0 5D \*RESPONSE IS REACTION BATE CB FCR TFX-2 TC \* EFFI SENS. OF 236U CAF/235U FIS TC 235U CAPTURE A= 3.9 ED 2.5896E-09 8.6914E-09 -2.4498E-10 -7.0873E-08 -1.8567E-07 A= 3.9372E-02\* 5.9567E+08 4.233CE-07 5.8313E-07 6.3456E-07 6.6803E-07 3.4215E-07 2.4909E-07 2.324CE-07 2.3487E-07 3.8464E-07 5.6054E-07 6.1875E-07 3.1348E-06 4.1991E-C6 8.9543E-06 2.0743E-05 3.3096E-05 1.4982E-05 1.7156E-C5 1.8280E-06 6.1193E-06 1.7321E-06 2.5749E-06 -1.9651E-06 1.7553E-05 1.6885E-06 7.8873E-07 -1.1596E-05 3.2876E-05 -4.1533E-07 1.7555E-05 1.6885E-06 7.8873E-07 -1.1596E-05 3.2876E-05 -4.1533E-07 -2.4184E-07 -1.8031E-06 -1.1738E-06 -1.6620E-06 -1.5503E-07 -3.1615E-09 -2.6298E-05 -1.020EE-09 -9.7572E-10 -9.4709E-10 -9.2718E-10 -9.1969E-10 -2.8267E-05 -2.9977E-09 -1.3827E-06 -2.2972E-07 -7.2210E-06 -5.7019E-07 -1.1955E-07 -1.9716E-07 2.4730E-06 3.3026E-07 8.2274E-05 1.3151E-04 -1.9292E-05 -4.320EF-06 -2.6191E-C6 -1.1497E-06 -7.8265E-07 -1.7371E-07 -7.3525E-09 -3.7541E-09 -8.6800E-10 -8.3721E-10 -8.2444E-10 -8.4864E-10 -7.3525E-09 -3.7541E-09 -8.6800E-10 -8.3721E-10 -8.2444E-10 -8.4864E+10 -8.9510E-10 -5.0506E-09 -1.2002E-08 -6.0217E-08 -2.6366E+07 -1.8220E-06 -3.0023E-06 -3.6373E-06 -1.1118E-05 -4.8143E+07 2.1887E+04 -1.7165E+06 -1.8911E+06 -3.5854E+06 -1.1941E+05 -6.8567E+05 -1.8771E+05 -4.5363E+07 -1.6864E+07 -2.9937E+08 -2.6508E+0E -2.4387E+08 -2.2607E+08 -2.1771E+08 -8.2579E+08 -1.0276E+07 -1.7560E+07 -7.8534E+06 -1.8538E+06 -2.8079E+08 -3.0427E+06 -2.5663E+06 -2.3558E+06 6.4183E+04 9.8631E+06 2.2036E+04 -1.3666E+06 -1.3403E+05 -1.6612E+04 -3.6189E+05 -5.7701E+06 -3.7453E+07 -2.0733E+69 -1.7674E+09 -7.1320E+07 -6.9449E+09 -7.718E+06 -6.04189E+07 -2.0773E-C8 -1.7674E-08 -7.1229E-05 -6.9449E-09 -7.0714E-09 -6.4109E-09 -6.7767E-05 -1.8075E-08 -2.3319E-C8 -7.1393E-07 -1.7938E-04 -4.3087E-04 -3. 1077E-05 -1. 4463E-05 -1. 9312E-06 6.9271E-04 1. 1665E-04 3.8192E-02

4 1261 904 4 3 0 7 0 0 3 4 D 107 n

5D \*RESPONSE IS REACTION BATE CR FCR TFX-2 7E \* EPRI SENS. OF 238UCAP/235UFIS TO 235U SCATTERING A= -4.2 ED 1.0337E-07 2.9415E-07 -2.86C0E-07 -7.8540E-07 -3.4778E-06 A= -4.2127E-06\*

-1.8702E-06	-2.0230E-07	1.3317E-07	2.2494E-07	3.7733E-07	1.3095E-07
6.6150E-09	-4.1922E-08	-1_1685E-C7	-1.6297E-07	-1_7457E-07	-4.2726E-07
-2.3648E-07	-4.522CE-07	-6.3078E-07	-2.0577E-07	2.5872E-08	-2_2256E-06
-1.3342E-06	-2.272 SE-07	4.6899E-07	4.7152E-07	2.1499E-06	-2.9731E-06
1.0616E-06	8.4536E-07	1.0750E-05	-9.4227E-06	4.2516E-06	4.4911E-06
4.7798E-06	5.695(E-06	1.6371E-17	-3_5230E-07	-5.5749E-08	-5.0231E-09
-4.8874E-09	-2.0825E-09	-2.0862E-09	-2.1082E-09	-2.1410E-09	-2.1871E-09
-7.0201E-05	-7-6395E-09	-3.2145E-08	-1.5027E-07	-4.9314E-06	-3.0770E-06
-1.2017E-06	-1.316 SE-06	-6.7791E-07	-1.0806E-06	3.4623E-07	4.5677E-06
4.251CE-06	5.3831E-06	3.3567E-06	1_4372E-06	1.4478E-07	-1.9046E-07
-1.6653E-08	-9.7005E-09	-2.3856E-C9	-2.3491E-09	-2.3478E-09	-2.4385E-09
-2.5978E-09	-1.5158E-08	-3.7854E-C8	-1.9426E-07	-8.4265E-07	-5.1200E-06
-5_9188E-06	-4.306 SE-06	-2.87228-06	-1.9092E-06	1.9876E-06	2.7081E-06
5.3955E-06	6.6518E-06	3.4778E-06	4.3833E-07	-1.1838E-07	-7.3449E-09
-5.9776E-09	-1.5781E-09	-1.5973E-09	-1.6661E-09	-1.7330E-09	-1.8597E-09
-8.7845E-09	-1.4347E-08	-3.0664E-08	-1.0872E-06	-4.2976E-06	-4.2538E-06
-2.0613E-06	-3.0428E-06	-9.4409E-06	7.7755E-07	-9.6269E-07	2.5904E-06
3.6128E-06	4.2787E-06	1.8508E-06	2.6197E-07	-4.7462E-07	-5.9129E-08
-8.0924E-09	-7.6483E-09	-3.2212E-05	-3.1899E-09	-3.3536E-09	-3.1205E-09
-3.3386E-C9	-8.968CE-09	-1.1355E-08	-2.3222E-07	-6.5704E-06	-4.5063E-06
-3.00682-06	-3.6162F-06	-3-97908-06	-1-3443E-06	-7-64128-07	1-5400E-05

4D	107	4	11	193	102	4	3	0	7	0	0	3
0												
50 ¥R	ESPONS	EIS	REA	ACTIO	N BATE	CR FC	R TEX-	2 *				
70 T	6 2033	END.	UP 2	2360	CAE/23	50 FI	S TO A	L CAPT	URE	A=	3.2412	E-03*
1 80	538-08	6 .	2 4 7 9 5 1	-0417	5-0/ 1	-3000 19-00	- 80-3	1.0991	E-09 -5	4611	8-10	
3.88	008-00	1	5310	15-07	1 700	15-UC 08-07	1.07	298~07	1.509	8E-07	9.1/0	08-08
2.34	598-07	1	9626	88-07	2 730	70-07	0.0V	115-07	3.0/2	SE-07	2. 389	32-07
1.66	068-07	1	130	12-09	4 646	/B-0/	4.14	935-07	2.003	0E-07	4.583	5E-07
1_10	838-07	1	- 139 8434	58-08	2 8 2 9	35-10	-1 26	768-07	4-215	00-03	-4.211	12-10
-2-05	398-08	-6-	886	2F-08	-4.353	08-08	- 1.34	105-01	-2 590	55-07	-1.090	38-09
-3.60	96E-09	-1.	538	28-09	-1.536	97-00	-1 53	496-00 5hv_00		78-00	-3-014	22-09
-4-63	458-09		466	58-09	-1 278	08-03	-1 04	345-03		68-00	-2 010	0E-09
-4-98	228-09	-4_6	0.86	CF~10	1 965	02-00	1 97	205-00	-0-004	78-07	-2-010	75-08
1.10	748-09	-8.	5901	47-08	-1.133	68-07	-1 22	182-00	-1 5#1	02-07	-1 000	05-08
-2-68	65E-08	-2-	595	80-8	~7.500	98-09	-7 52	158-00	- 1	0E-0/	-7 512	05-07
-7.48	562-09	-3-0	024	7E-08	-3.075	28-08	-4.18	718-09	-5 360	79-09	-1 224	42-03
-8.83	14E-08	-3.9	9110	)F-08	-2-033	08-09	2.22	208-08	2.057	78-06	5 209	78-09
-5.45	81E-08	-1.	845	1E-C7	-2.773	0E-07	-2.56	22E-07	-1-282	68-07	-4 635	38-08
-4.59	40E-08	-1-2	2249	E-08	-1-212	9E-08	-1-22	358-08	-1-212	38-08	-1.223	92-08
-4.62	58E-08	-4-1	6446	5E-08	-4-972	3E-08	-2.08	41E-07	-2.434	6E-07	-1.861	58-07
-5-82	89E-08	° <b>−3</b> ∎8	8555	5E-C8	6.334	6E-C8	5.63	50E-06	4.970	7E-07	2.394	48-06
2.37	99E-07	-3-!	570	1E-07	-5.921	4E-07	-6.15	36E-07	-8.322	48-07	-5-149	18-07
-9.64	77E-08	-9.1	6058	EE-08	-4.110	6E-C8	-4.06	34E-08	-4.139	9E-08	-3-639	08-08
- 3_ 66	7 1E-C8	-8-6	6562	2E-08	-8.701	80-30	-4-70	30E-07	-1.174	2E-06	-7.103	9E-07
-3.06	80E-07	-2.	7584	4E-07	3.593	4E-07	5.04	99E-05	2.540	48-05	3,155	5E-03
4D	107	ц	1 .	193	60 a	ш	7	٥	7	^	•	3
0			•		204	•	J	U	,	v	U	3
50 *R	ESFONS	E IS	RE	CTIO	N RATE	CR FC	R TRX-	2 *				
7C *	EPRI S	ENS.	0 F	238U	CAP/235	UFIS	TO AL	SCATTE	RING	¥= -	·1.9321	E-04*
8D	3.3875	E-06	7.	5433	E-06 6.	8875	E-07 -	2.9299	E-06 -1	. 2847)	E-05	
1.11	00E-06	6.	370	1E-06	5.673	0E-C6	6.67	02E-06	7.967	7E-06	-8.342	9E-07
1.61	97E-06	-1.2	2253	3E-06	-2.496	8E-06	-6.64	78E-06	-2.856	2E-06	-6.805	0E-06
-3.48	29E-06	-7.6	5409	SE-06	-1_055	6B-05	-3.99	52E-06	6.133	2E-07	-2.573	3E-05
-7.20	63E-06	2.	1559	E-06	9.192	5E-06	2.67	06E-06	4.062	4E-06	-4.457	2E-06
2.74	19E-05	2.	7547	7E-06	9-829	7E-07	-5.56	87E-05	1.155	5E-04	9.656	3E-07
-5,49	29E-06	-2.0	0482	2E-05	-1.316	4E-05	-1.04	21E-05	-7-929	7E-06	-1.121	1 <b>2</b> -06
-1.12	26E-06	-4-	7924	4E-07	-4_793	5 <b>E-07</b>	-4.79	44B-07	-4.800	5E-07	-4-802	6E-07
- 1- 45	37E-06	-1.1	4060	CE-06	-4_051	0E-06	-6.25	46E-06	- 2. 104	3E-05	-1.013	4E-05
-4.36	63E-06	-6-0	0020	)E-06	-5.851	8E-06	-3.49	25E-06	6.536	8E-06	1.859	6E-04
3.19	25E-05	-1-4	454	7E-06	-1_536	2E-05	-2.09	08E-05	-2.909	8E-05	-2.120	7E-05
-5.31	74E-06	-5.	177.2	E-06	-1.506	8E-06	-1.51	60E-06	-1.513	1E-06	-1.525	7E-06
-1.52	63E-06	-6.	2353	E-06	-6.473	1E-06	-9-10	32E-06	-1-212	7E-05	-2.937	6E-05
-2.40	058-05	-1-	3702	E-05	-7.703	/E-C6	-7.90	86E-06	1.681	8E-04	5.440	3E-05
J. 10	11E-05	-4-	3493	12-06	-2-990	2E-05	-3-35	83E-05	-1.767	4E-05	-6.503	0E-06
-6 75	678-06		000	28-06	-1./36	28-00	-1./5	96E-06	-1.749	4E-06	-1.772	22-06
-1-51	198-05	-0-0	5003	25-05	-1 051	38-66	-3.20	205-02	-4-135	12-05	-3-649	22-05
1 30	828-04	- 1.	0424	2E-05	1 053	36703 78-05	7.90	305-00	~ 1.083	28-05	8-653	98-05
-6 01	638-06	-6 0	156	18-06	-2 612	10-05	-2.14	20E-03	-4-412	75-05	- 3. 102	81-05
-2.37	64E-06	-5-6	6557	12-00	-5-751	46-66	-1 23	315-UD 192-05	-2.000	28-05	-2.347	08-06
-3.11	44E-05	-4.9	5227	78-05	-6- 398	6E-05	-1-90	962-05	-9.861	88-06	- 20 727	08-05
						01 01		)0 <u>6</u> -0J	- 3.00 :	0.0-0.0	0.000	96-05
4 D	107	4	12	69	102	4	5	0	7	0	0	7
0							-	•	•	•	. •	-
50 *RI	ESPCNSE	IS IS	REA	CTIO	N BATE C	B FCF	? TFX-2	2 *				
70 * 1	EPRI SI	ENS.	OF	2380	CAP/235	50 FIS	тс н	CAPTU	RE	λ=	7.4115	E-02*
80 <u>2</u> 9	2.52301	s-05	5.	36951	5-05 4.	47261	5-09	1.21001	E-10 5	.7920E	-09	
3_3/3	548-08	5.5	394	E-08	7.4492	2E-08	9.976	57E-08	1.376	1E-07	1.769	2E-07
2-592	2 /E-07	3.8	515	E-07	5.7433	SE-07	8-63(	U/E-07	1.282	8 E-06	1.857	38-06
2.75	79E-06	3.8	330	E-06	5.626	1E-06	8.28	48E-06	1.126	6E-05	1.436	8E-05
3.43		2.9	201	E-07	8.9066	DE-07	3.240	50E-07	4.501	1E-07	3.150	42-07
6 201	015-00		205	1-07	0.8208	SE-U/	-4.092	228-07	8.26/	7E-06	3.184	22-07
-1 53	302.00	-2.0	043	E-1/	-2.043	DE-07	-1.53	54E-07	-1.106	/E-07	-1-539	1E-08
-1.04	102-08 068-08	-0-5	290	E-09	-5.4041	02-09	-0.505	35E-09	-0.506	08-09	-0.498	UE-09
- 1. 70 6 00	100-00 100-00	-1±8	1000	5-00 F-07		E-18	-0.343	5 0F 07	-2.879	58-07	-0.039	0 E-09
1 07	205-00	_2 - 4	122	2-07	0.3995	10-07	4.91	DOR-07	7.221	15-05	2.130	98-05 (n. 0-
-1 000	112-07	^	164	E-U0 E_17	-2 0070	05-07	-2 40		-0.028	JE~U/	-5.105	02-07 07 07
-7 86	778-00	-1-0	6 10 0	2-07	-1 2100	50-00 10-00	-1 764	905-08 368-07	-2-8/0	45-UU	-2.8/7	05-05
-2 100	978-00	1 4	466	E-07	6 050/	10-07	1 074	105-07	-2.430	4 E-U/	-3.352	024V/ 17-07
1 17	202-04	-2 "	1100	2-07	-1 2240	10-01	-1 22	425-00	4.323	J 5 - U 3 4 9 - 0 7	2-133	00-07
-1_96	618-07	-5 2	122	F-09	-5 1604	52-00	-1.23	64P-00	-5 120	75-07	-2.010	75-U/ 19_00
-1-95	34E-07	-1-9	61 A	2 00	-2-1120	)R-00	-9 261	738-07	-1 045	45-V0 07-04	-3 000	15-V8 59-07
2, 59/	048-07	6_7	223	F-07	3, 104	58-07	1 14	148-04	1 183	78-00	-3-080	35-V/ 08-05
1_21	74E-05	3.7	576	E-06	-7,0905	5E-07	-2.24	208-04	- 3. 3 8 5	10-03	-2 611	58-05 58-04
-3-674	41E-07	-3_6	331	E-07	-1_5480	28-17	-1.524	698-03	-3.343	00-00	-1 220	JE-UD 19-07
-1_23	44E-07	-2-9	032	E-07	-2_90#3	BE-07	-1-550	347-06	- 10 331	58-01	-1.420	18-07
1. 14	50E-06	5.4	138	E-06	2. 1822	2E-05	1.08	10E-03	5.299	2E-04	7.215	6E-02

4 D	107	4	1269	904	4	5	0 7	0	0	3
5D 7D 8D -6. -7. -1. -2.	0         *RESPONS         *EFRIS         1.9733         3350E-03         1122E-03         1831E-02         6083E-03         1928E-04	SE IS SENS. DE-05 0 -4.5 0 -8.0 2 -1.3 0 -8.1 1 -1.8	REACTIO OF 2380 -1.4325 5320E-03 5320E-03 5944E-03 1928E-05 8004E-04	DN RATE CH JCAP/23501 5E-04 - 1.1 3 - 4.37861 3 - 9.00751 2 - 1.34601 5 - 9.75641 4 - 7.11831	FCR 7 FIS TO 1414E-( 2-03 -4 3-03 -9 3-02 -1 3-05 -1 3-05 -1	ERX-2 H SCAT 3 - 3.2 4083E 8670E 1.1583E 1.101E 5.2695E	* TERING 292E-03 -03 -4.7 -03 -1.0 -02 -1.3 -04 -1.1 -03 -1.3	A = - -5,7624E 228E-03 826E-02 651E-02 523E-04 642E-03	4.2160E -03 -6.2159 -1.2249 -1.9143 -8.4085 -8.9875	-01* E-03 E-02 E-02 E-04 E-04
-1. -1. -3. -2. -5. -1. -2. -3. -7.	$\begin{array}{c} 1129 \pm -03\\ 0387 \pm -04\\ 3358 \pm -04\\ 9189 \pm -04\\ 2000 \pm -03\\ 8418 \pm -04\\ 6344 \pm -04\\ 3794 \pm -03\\ 2091 \pm -03\\ 2091 \pm -03\\ 3561 \pm -04\\ \end{array}$	-2.4 -4.4 -1.2 -5.3 -5.6 -6.6 -1.3 -4.4 -1.9	1274E-03 1274E-09 2886E-04 1382E-04 1382E-04 1479E-03 1557E-04 1557E-04 1557E-03 1042E-03 1611E-04	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	2-03 -1 2-05 -4 2-04 -5 2-04 -2 2-04 -1 2-04 -9 2-04 -8 2-04 -9 2-04 -9 2-0	-00522 -4214E -65188 -85728 -94452 -94452 -94452 -94452 -95908 -95908	-03 -7.4 +05 -4.4 -04 -1.9 -04 -1.9 -03 -3.4 -04 -1.2 -04 -1.2 -04 -8.2 -04 -1.9	2598-04 2288-05 2158-03 3458-04 5988-03 3238-04 3508-03 1328-03 1328-03 7348-03	-1.0396 -4.4209 -9.1792 -3.1432 -2.3518 -1.6402 -2.9425 -1.8497 -7.4230	E-04 E-05 E-03 E-03 E-03 E-03 E-03 E-03 E-03 E-04
-7. -7. -7. -9. -3. -4.	4091E-04 4843E-03 2351E-03 0815E-04 3226E-04 1891E-03	-7.4 -1.4 -8.5 -9.0 -7.8	1490E-04 1949E-03 1208E-03 1341E-04 1410E-04 1085E-03	8.007E 1.8677E 1.8677E 3.8635E 3.8635E 7.8793E 8.1278E	2-04 -3 2-03 -6 3-03 -6 3-04 -3 3-04 -4 3-03 -2	- 3963E - 0278E - 6153E - 8179E - 2539E - 9297E	$\begin{array}{r} -03 & -4.1 \\ -03 & -1.8 \\ -03 & -1.8 \\ -03 & -8.1 \\ -04 & -3.8 \\ -03 & -1.1 \\ -02 & -3.7 \end{array}$	4112-04 387E-03 293E-03 478E-03 884E-04 177E-02 091E-03	- 1. 95971 -3. 61801 -3. 71401 -4. 86841 -3. 29761 -7. 87791 3. 96161	E-04 B-03 E-03 E-04 E-04 E-03 E-03
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13408-05\\-055-99\\-055-99\\-055-99\\-055-99\\-055-42\\-055-42\\-055-42\\-055-42\\-055-22\\-055-22\\-055-31\\-055-22\\-055-31\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-22\\-055-2$	C 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4 D	107	4	2000	901	4	3	0	7	0	0	3
E 12	0						· •				
วย 7 ต	* EPRI SH	ENS.	OF 2380	CAE/23	CR FUR	TRA-2	2 + 3**2 IN	FUEL	λ=	1.7548	E-03*
80	1.99981	E-06	4.27571	E-06 -7	.446CE	-08 -1	.00382	-05 -1.	. 35461	8-05	
З.	1609E-06	1.1	7521E-05	1.627	0E-05	1.182	29E-05	8.271	7 E-06	4_480	6E-06
2.	3728E-06	1_	4667E-06	1.553	6E-06	2.477	72E-06	3.176	7 E-06	2.163	0E-06
7.	9675E-06	8.	9930E-06	9.635	5B-06	2.382	22E-05	1.852	0E-05	9.184	2E-06
	US5/E-06	4.	1000E-06	1.594	08-05 18-07	4.12:	00E-05	3 205	38-05	-3.209	9F-06
- 1	27128-05	-1.5	90948-05	-3-927	88-06	-2_888	13E-07 ·	-4-855	92-09	-1.940	28-10
- 1.	7226E-10	-7.	0039E-11	-6.860	9E-11	-6.84	17E-11	-6.876	9E-11	-7.019	6E-11
-2.	2762E-10	-2.	6215E-10	-1.430	3E-09	-1.691	75E-08 ·	-9_749	2 E-06	-2.993	7E-05
- 1.	7120E-05	-1_(	6696E-05	4.816	9E-06	5.382	21E-06	2.613	3E-05	2.100	8E-05
-6.	8215E-07	-1-1	273CE-C6	-8.927	1E-07	-4.778	38E-07 ·	-1.837	1E-07	-1.014	4E-08
- 2	58828-12	-1.1	95058-11	-1-056	48-10	-1-88	19E-12 ·	-2-2/9	8E-08	-8.006	6F-05
-2.	2629E-04	-2-	1152E-04	-6.233	7E-05	-2.04	18E-07	3.039	8E-05	-1.311	3E-07
- 1.	1483E-C6	-1.	3773E-06	-7.427	4E-07	-1-009	92E-07	- 1., 16 1	2 E 0 9	-2.982	2E-11
-1.	2834E-11	-2.	5406E-12	-2.381	0E-12	-2.352	29E-12	-2.370	3E-12	-2.509	4E-12
- 1.	2002E-11	-2.	71952-05	-1 022	45-10	-2-840	898-08 · 268-04	-0./38	38-06	1 570	52-05
- 3.	94328-06	-1.	28678-05	-7-256	58-06	-2-778	378-06 ·	-5-431	7E-07	-4.736	5E-09
-7.	3244E-11	-5.	0022E-11	-1.804	8E-11	-1.67	91E-11	-1.656	0E-11	-1.482	4E-11
- 1.	.5602E-11	-4_	3072E-11	-6.191	0E-11	-4.26	03E-09	-1.536	8 E-06	-5_941	3E-06
-6.	.3530E-06	-1-	2150E-05	-6.655	0E-C6	3.33	85E-04	6-676	6 <b>E-</b> 05	1.806	5E-03
<i></i>	10.7		2000	007		-	0	-	~	~	2
41	0	4	2000	903	4	3	0	'	U	U	3
50	*RESPONS	E IS	REACTIC	N BATE	CR FC	TRX-	2 *				
70	* EFRI S	ENS.	OF 238U	CAE/23	50 FIS	5 TC D	B**2 IN	VOID	λ=	2. 3324	ŧE−04*
03	4.5168	E-07	2.1324	E-07 1	1.76251	8-07 -	2.2049E	-07 -8	.2505	E-08	08-06
С. Б	- 2552E-07	8.	5821E-07	1_886	5E-06	2.02	948-06	2.906	0 - 0 /	3-073	002-06 882-06
4.	1717E-06	4.	28681-06	4.512	8E-06	6_13	37E-06	6_247	2E-06	4.373	34E-06
1.	.7348E-06	1.	4748E-C7	4_808	17E-07	1.53	77E-07	2.238	9 E- 07	-5.009	7E-08
1.	.5136E-06	1.	77321-07	2.123	9E-07	-1.61	97E-06	3.937	9E-06	-5.76	55E-08
- 2	.38//E-0/	-/.	4/988-0/	-4.740	158-07	-1 74	45E-07	-2.93/	9E-07	-4.11	/6E-08
	- 11232-02 - 27768-02	-5.	1323E-08	-1.453	148-07	-2.19	778-07	- 16 / 4 7 -6.444	5-00	-2_199	128-07
-6	.1197E-08	-3.	1343E-C8	1.408	1E-(7	1.41	37E-07	5.424	6E-06	7.996	52E-06
- 9	. 3231E-C8	-7.	307 CE- C7	-9-228	34E-07	-9.87	77E-07	-1.258	7 E- 06	-9_038	34E-07
-2	.2851E-07	-2.	2147E-07	-6.405	52E-CE	-6.42	26E-08	-6-386	7E-08	-6.414	16E-08
-0.	- 3902E-UE	-2-	350 CE-07	-2.013	518-07	-3.52	498-07	-4.421	2 E- U/	-9.80	01E-07
-5	-5636E-C7	-1.	5012E-06	-2,191	13E-06	-2-05	46E-06	-1-050	52-06	-3.814	42E-07
- 3	.7830E-07	-1.	0087E-C7	-9-988	90E-08	-1.00	75E-07	-9.981	7E-08	-1.00	76E-07
- 3	.8064E-07	-3.	8175E-07	-4-079	0E-07	-1.67	58E-06	-1.884	0E-06	-1.45	24E-06
-4	-7897E-07	-3.	5475E-07	2.310	)4E-C7	2.90	34E-05	2_077	5E-06	9.76	31E-06
	-30258-01	-1-	46428+07	-1.909	16E-C7	-1.88	325-00 718-07	-1.922	18-07	-1-688	272-00
-1	-7009E-C7	-4	0127E-07	-4-029	8E-07	-2.16	72E-06	-5.224	02-06	-3.13	80E-06
- 1	.3867E-06	-1-	4095E-06	5.895	56E-07	1_27	13e-05	3.801	6 E- 0 6	1.48	12E-04
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40	0	4	2000	342	-	J	0	'	v		J
5D	*RESPONSI	EIS	REACTIO	N BATE	CB FCF	TEX-2	2 *				
70	* EPRI S	ENS. P-07	0F 2380	CAP/23	100 FIS	5 TO DI	6772 IN 730000	CLAD -07 -3	A= .036#	8.0192 8-07	:E-04*
ец Ц.	4024F-06	6.	64718-06	2_902	38-06	1.02	8E-05	2.733	52-06	2,525	53E-06
1.	6938E-06	1.	7767E-06	5.534	42-06	6.25	18E-06	6.030	2E-06	6.176	7E-06
6.	2721E-06	8.	6655E-06	1.377	6E-05	2.56	09E-05	2.436	6 E- 0 5	6.678	0E-06
5.	.2769E-06	4.	469CE-07	1.433	17E-06	4-70	86E-07	6.772	7E-07	-1.278	2E-08
- 1	4002E-06	_u _u	9721E-07 7980E-06	1.1/5	08-06	-2 39	845-08 248-06	3.104 -1 787	8 E- US	-1_190	)15-07 )3 <b>8-07</b>
-2	4988E-07	-1.	7580E-00 0647E-07	-1-063	78-07	-1-06	262-07	-1.062	8E-07	-1-062	20E-07
- 3.	2067E-07	-3.	0895E-07	-8.837	0E-C7	-1.34	22E-06	-4.140	3E-06	-1.388	2E-06
- 3.	.4193E-07	-2-	7971E-C8	1.338	2E-06	1.23	61E-06	1.361	5E-05	2. 504	9E-05
2.	.3315E-C8	-1-	7912E-06	-2.349	5E-CE	-2.52	09E-06	-3.168	4E-06	-2.210	6E-06
- 5.	-4949E-07 -5275p-07	-5.	16875-07	-1-532	12-07	-1-53	188-07	-1-526	95-07 57-06	-2-49	34E-0/ 12F-06
- 1	-7812E-06	-7.	8512E-07	-4.060	7E-CP	4_40	83E-07	1.528	42-05	3.468	352-07
- 3.	.5938E-07	-1.	2037E-06	-1.796	8E-06	-1.65	19E-06	-8.243	7E-07	-2.97	51E-07
- 2	9463E-07	-7.	8517E-08	-7.773	1E-C8	-7.83	96E-08	-7.766	3E-08	-7-838	87E-08
-2	.9613E-07	-2-	9711E-07	-3.178	2E-07	-1-32	93E-06	-1.545	78-06	-1.174	9E-06
- J. U	-03975-07 -5068F-06	-2-	40912-01 57541-06	-1.072	/JE+U/ /48-05	-1-10	338-05	2.090 -1.479	3 E-06	-9-070	005-03 958-06
- 1	.6958E-06	-1-	6868E-06	-7.213	2E-07	-7-12	75E-07	-7.258	52-07	-6-37	76E-07
-6	4243E-07	-1.	5154E-06	-1.521	17E-06	-8.19	92E-06	-2.029	4E-05	-1.21	37 E-05
- 5	.1888E-06	-4_	6016E-06	5.821	2E-06	7.64	93E-05	4.929	5E-05	5.324	15E-04

4 D	107	4	2000	900	4	3	0	7	0	0	3
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25	* TESPUNSI	1 1 D E	12 AC 1101	CALC C				*****	•	4 4000	
/ U 6 m	- CERT 31	2N3. U 2-06	1 71211	CAE/23:	61600	-05 3	70545	HODERA	. A=	-1. 1833 T-05	E-02*
2	07005.05	3-00 0.71	14/12/1	5-0J 14	0 1C2E	-00 34	. 7734E		534/	E-05	
	97802-05	2.12	150F 05	9.4470		1.0490	DE-04	8.8850	E-05	/. 100	/E-05
	03462-05	0.14		1.2/44	2E~UC	0-0/0	9E-05	1-0536	E-04	8.241	12-05
1-	23926-04	1.23	555E-04	1./21	12-04	1.4/05	SE-04	2-0054	E-04	1.926	DE-04
	8050E-05	0.44	10 11-00	1.3760	E-05	4.982	E-06	5.7076	E-06	1.045	3E-05
	9775E-05	5.53	330E-06	1_7281	E-05	-2.2967	E-06	6.0625	E-05	2.243	9E-06
4-	4227E-07	-3.44	186E-06	-7-5135	E-06	-5.6345	5E-06	-4.0558	E-06	-5.636	7E-07
- 5-	6163E-07	-2.39	90 E - 07	-2-3864	E-C7	-2-3815	5E-07	-2.3817	E-07	-2.378	4E-07
-7.	1751E-07	-6.90	326E-07	-1.9765	E-C6	-3.0491	IE-06	-1.0505	E-05	-2.416	5 <b>E-07</b>
2.	4789E-C6	9.33	36(E-06	2.4655	5 <b>E−C</b> 5	1.8839	)E-05	1.5661	E-04	1.058	1E-04
4.	9336E-06	-1.96	519E-07	-2.8540	)E-06	-1_8651	IE-05	-2-4087	E-05	-1.526	1 E-05
- 3.	8583E-C6	-3.56	53E-06	-1.0157	E-06	-1_0140	)E-06	-1.0054	E-06	-1.007	7 E-06
- 1_	0035E-06	-4.07	142E-06	-4-2280	E-06	-6.1091	E-06	-8.4673	E-06	-1.9280	5E-05
-7.	2952E-06	3.81	22E-06	3.8419	E-06	1.1952	2E-05	2.5329	E-04	1.239	42-05
1.	1939E-05	-2.09	01E-06	-6.6741	E-0€ -	-6.6891	E-06	-3.1594	E-06	-8.067	7E-06
-7.	8807E-06	-2.08	380E-06	-2.0628	E-06	-2.0766	5E-06	-2-0544	E-06	-2.071	1E-06
-7.	8129E-06	-7.83	375E-06	-8.4388	E-06	-3_6983	E-05	-4.1430	E-05	-1.683	3E-06
1.	4086E-06	4.33	80E-06	2.0443	E-05	2.9215	5E-04	4.5594	E-05	1.797	2E-04
6.	1217E-05	1_10	70E-05	-2.2551	E-C6 -	-7-0484	E-06	-1.8393	E-05	-1-098	R-05
-1.	9986E-C6	-1.97	43E-06	-8.4068	E-07	-8.2879	E-07	-8.4196	E-07	-1-872	3E-05
- 1_	8816E-05	-4.42	221E-05	-4-4194	E-05	-2.3636	5E-04	-1-5104	E-05	-1-178	1E-06
3.	6286E-06	7.24	96E-06	6 6573	E-05	1.7603	BE-03	5.1946	E-04	6.751	DE-03

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