

**ENDF/B PROCESSING CODES  
FOR THE RESONANCE REGION**

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**NATIONAL NEUTRON CROSS SECTION CENTER**

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Availability of Computer Programs

The computer programs described in this report have been sent to the Argonne Code Center for distribution. For further information write or call

Argonne Code Center, Building 203 Room C-230  
Argonne National Laboratory  
9700 South Cass Avenue  
Argonne, Illinois 60439

Phone: Area 312 739-7711 Extension 4366

## Introduction

In this report we describe some six programs written for calculating point-wise cross-sections in the resolved and unresolved resonance region. These programs have been written specifically to read in the resonance parameters in the ENDF/B files. However, the smooth cross-sections from File 3 have to be added to the output of these programs to obtain the final cross-section.

Out of the six codes described in this report, the first four calculate the cross-sections in the resolved resonance region and the last two in the unresolved resonance region. The first program SIGPLOT calculates cross-sections for scattering, capture and fission using the single level Breit-Wigner parameters of ENDF/B Version I data. It also calculates multilevel scattering cross-sections. The cross-sections may be Doppler broadened if necessary. The second program SIGMA2 is essentially a modified version of SIGPLOT written for ENDF/B Version II data. The third program RAMP1 calculates scattering, capture and fission cross-sections using the Reich-Moore approximation, with or without Doppler broadening. The next program ADLER calculates cross-sections from the Adler-Adler parameters. Doppler broadening is done using the  $\psi$  and  $\chi$  functions. AVRAGE3 and AVRAGE4 calculate cross-sections in the unresolved region using energy independent parameters and energy dependent parameters of ENDF/B Version II respectively. Width-fluctuation corrections are applied by numerical integration. Also, there is no provision made for allowing any inelastic effects in AVRAGE3 whereas they are taken into account in the latter program. After describing the programs, we have given the program listings with sample input data and

results of the test problems.

The main purpose of writing these codes has been to have a set of codes which (i) would serve as a standard reference set against which the results of other codes could be compared and (ii) could be used in neutron cross-sections evaluation and (iii) from which automated plots of cross-sections could be obtained for author proofs. As such, every effort has been made to obtain accurate results from the codes avoiding the usual computer time-saving approximations such as taking only a small number of resonances in a particular energy region. Also, these codes have been checked against existing codes to trace down any errors of programming. However, the author would appreciate it if the users could communicate any errors they might find in using these codes.

My grateful thanks are due to D. E. Cullen for writing the subroutines used in calculating the Doppler broadened cross sections by the trapezoidal rule. I have also benefited from useful discussions with M. S. Moore.

Copies of these programs have been sent to the Argonne Code Center. (See Availability of Computer Codes)

Any further details regarding these programs may be obtained from the author at the National Neutron Cross Section Center.





Description of the Programs



## PROGRAM SIGPLOT

This is a program to calculate scattering, capture, fission, and total cross sections from resonance parameters of Version I data from File 2 of ENDF/B. Provision is also made to allow for level-level interference effects in the scattering cross section. The formulae used are essentially the same as given in the report of Gregson, et al.,<sup>(1)</sup> but are modified to include fission. Modified versions of the three subroutines, ORDER, FACTS, and SIGMA, described in this report are used in the current program. Further details of these formulae are given in the Data Formats and Procedures Manual<sup>(2)</sup>.

### Formulae:

#### 1. Elastic Scattering

$$\begin{aligned}
 \sigma_{nn}^{\ell}(m) &= (2\ell+1) \frac{4\pi}{k_m^2} \sin^2 \varphi_{\ell} \\
 &+ \frac{\pi}{k_m^2} \sum_J g_J \sum_{r=1}^{N_{res}(\ell,J)} \frac{\Gamma_{nr}^2 \cos 2\varphi - 2\Gamma_{nr} (\Gamma_{\gamma r} + \Gamma_{fr}) \sin^2 \varphi_{\ell}}{(E-E_r')^2 + \left(\frac{\Gamma_r}{2}\right)^2} \\
 &+ \frac{2(E-E_r') \Gamma_{nr} \sin 2\varphi_{\ell}}{(E-E_r')^2 + \left(\frac{\Gamma_r}{2}\right)^2} \tag{1}
 \end{aligned}$$

## 2. Capture

$$\sigma_{ny}^{\ell}(m) = \frac{\pi}{k_m^2} \sum_J g_J \sum_{r=1}^{N_{res}(\ell, J)} \frac{\Gamma_{nr} \Gamma_{fr}}{(E-E_r')^2 + \left(\frac{\Gamma_r}{2}\right)^2} . \quad (2)$$

## 3. Fission

$$\sigma_{nf}^{\ell}(m) = \frac{\pi}{k_m^2} \sum_J g_J \sum_{r=1}^{N_{res}(\ell, J)} \frac{\Gamma_{nr} \Gamma_{fr}}{(E-E_r')^2 + \left(\frac{\Gamma_r}{2}\right)^2} . \quad (3)$$

## 4. Elastic Scattering with Level-Level Interference

In addition to the expression given in Eq. (1), we have the following level-level interference term:

$$\frac{\pi}{k_m^2} \sum_J g_J \sum_{r=2}^{N_{res}(\ell, J)} \sum_{s=1}^{r-1} \frac{2\Gamma_{nr} \Gamma_{ns} \left[ (E-E_r')(E-E_s') + \frac{\Gamma_r \Gamma_s}{4} \right]}{\left[ (E-E_r')^2 + \left(\frac{\Gamma_r}{2}\right)^2 \right] \left[ (E-E_s')^2 + \left(\frac{\Gamma_s}{2}\right)^2 \right]} , \quad (4)$$

where  $m$  is the  $m^{\text{th}}$  isotope,

$N_{\text{res}}(\ell, J)$  are the number of resonances for a given  $\ell$  and  $J$ ,

$$\Gamma_{nr}(E) = \frac{P_{\ell}(E)\Gamma_{nr}(|E_r|)}{P_{\ell}(|E_r|)},$$

$$\Gamma_r = \Gamma_{nr}(E) + \Gamma_{\gamma r} + \Gamma_{fr},$$

$$E_r' = E_r + \left[ \frac{S_{\ell}(|E_r|) - S_{\ell}(E)}{2P_{\ell}(|E_r|)} \right] \Gamma_{nr}(|E_r|) \quad (E \text{ in eV}),$$

$$k_m = 2.196771 \times 10^{-3} \left( \frac{\text{AWR}}{\text{AWR} + 1.0} \right) \sqrt{E(\text{eV})} \quad (\text{barns})^{-1/2},$$

AWR = mass of the element in units of the neutron mass,

$E$  = neutron energy in eV in the Laboratory System,

$S_{\ell}$  = shift factor,

$P_{\ell}$  = penetration factor,

$\phi_{\ell}$  = phase shift,

$\rho$  =  $ka$ ,

$a$  = channel radius.

#### Storage Capacity of the Program

1. Maximum number of isotopes: 10.
2. Maximum number of  $\ell$  values per isotope per energy range: 5.
3. Maximum number of resonances over all isotope energy ranges and  $\ell$  values: 500.
4. Total memory for the program: 37K octal.

5. Time: approximately 14 secs C.P. time/ 25 res/ isotope on the CDC-6600.
6. This program assumes that the resolved resonance parameters are given for one energy range which is the same for all isotopes.

Procedure:

1. After all the data for one element are read in, the resonance energies over all isotopes are arranged in increasing order.
2. For each pair of levels which lie within the limits of the energy range in the input data, a variable number ( $8 = 4$  MM as it stands now) of energy points which lie between these two levels are generated, and the scattering, capture, fission, and total cross section are calculated and printed out for all the resonances of a given isotope as well as for all the isotopes of a given element. A finer mesh may be obtained by setting MM (card SIGP246) to a higher value.
3. To avoid having huge core storage, the cross sections are not stored in memory but are printed out as they are generated.
4. The resonances in each isotope are arranged in increasing order of  $l$  and for a given increasing order of J before the cross sections are calculated.
5. For a given isotope, the measured resonance spins are, for example, 3 and 4. In File 2 the spins of some low energy resonances where they have been experimentally measured will have one of these two values. For the rest of the resonances where this data is lacking, the

spins would be given as 3.5. In such a case, in calculating the cross section with level-level interference, we let spin-3 resonances interfere with one another. Similarly, spin-4 resonances that interfere with each other are treated as a group. The rest of the resonances (spin 3.5) do not interfere among themselves unless this is indicated on the title card in Col. 65 (see p. 8).

6. To Doppler-broaden cross sections, we write the Doppler-broadened cross section as

$$\sigma_{\Delta}(E') = \frac{1}{\Delta\sqrt{\pi}} \int_0^{\infty} \sigma(E'') e^{-[(E'-E'')/\Delta]^2} dE'' , \quad (5)$$

where

$$\Delta \text{ (eV)} = 0.3177 \left( \frac{T_{eff}^0}{293.0} \right)^{1/2} \left( \frac{E' \text{ (eV)}}{AWR} \right)^{1/2}$$

$T_{eff}^0$  = effective temperature in degrees Kelvin.

AWR = nuclear mass

The above expression is obtained as a good approximation for the more accurate expression for Doppler-broadened cross section (see Solbrig<sup>(3)</sup>) when  $E/\Delta \gg 1$ . It is known that this approximation is good except at very low energies where the more accurate expression has to be used. Therefore, in this program Doppler-broadening of the cross section is by-passed for neutron energies less than 0.025 eV. The above expression



can be written as

$$\sigma_{\Delta}(E') = \frac{1}{\sqrt{\pi}} \int_{-E'/\Delta}^{\infty} \sigma(E' + x \cdot \Delta) e^{-x^2} dx, \quad (6)$$

where since  $E'/\Delta$  is large, the integral is written as

$$\sigma_{\Delta}(E') = \frac{1}{\sqrt{\pi}} \int_{-\infty}^{+\infty} \sigma(E' + x \cdot \Delta) e^{-x^2} dx. \quad (7)$$

#### A. Gauss-Hermite Quadrature

This integral can be evaluated using a 9-point Gauss-Hermite quadrature formula, provided the structure in the cross section is not small compared with the Doppler width  $\Delta$ . Comparison of a test case which is Doppler broadened using  $\psi$  and  $\chi$  functions, the trapezoidal rule, and Gauss-Hermite quadrature formula gives accurate results, provided the width of the resonances  $\Gamma \geq 5\Delta$ . If this condition is not satisfied, we have recourse to using the trapezoidal rule for evaluating the integral as described below. In most of the cases we use the quadrature formula for calculating the integral, as it has been found that the trapezoidal rule method requires a large amount of computer time. However, the trapezoidal method should be used if the resonances are very narrow and/or are very closely spaced. This may be done by setting all FLAG(I) = 1 in the subroutine SIEVE.

#### B. Trapezoidal Method

The above integrals can also be evaluated numerically by using the

trapezoidal rule. To start with, a certain number of pivot points (NTAB which is an odd integer) equal to, say, 11 are specified at each energy  $E'$  where we wish to evaluate the Doppler-broadened cross section. Pivot points are then specified at eleven energy values given by  $E'' = E'$  and  $E'' = E' \pm \Delta \dots E' \pm 5\Delta$ . The cross section to be Doppler-broadened is explicitly evaluated at each pivot point at every iteration. The integral will give negligible contribution beyond this energy interval due to the  $e^{-(E' - E'')^2/\Delta^2}$  factor. If, however,  $E'$  is very small so that the energy at one of the above pivot points is less than or equal to zero, we set  $E'' = 10^{-3}$  eV as the lowest energy and set the energy of the pivot points at  $E'' = 10^{-3} + \Delta \dots, 10^{-3} + 10\Delta$ . In addition, we have to specify an ERROR (say of the order of  $10^{-4}$ ). The above integral is then evaluated at these points, and if the relative value in each subinterval is less than  $\text{ERROR}/(\text{NTAB}-1)$ , the program assumes that the integral has converged in that interval; if not, at every iteration the number of steps is doubled until the integral converges. This method has been checked against results obtained by using  $\psi$  and  $\chi$  functions in test cases and found to converge rapidly.

Use of these two numerical methods to evaluate the Doppler-broadened cross sections enables us to treat resonances due to higher  $l$ -values where expressions for the Doppler-broadened cross sections in terms of the  $\psi$  and  $\chi$  functions become very involved.

## Input Data

The first card of the input is a **TITLE** card with the format (7A4,2X,I5,F5.1, 2I5, E10.4, I5). One can punch an appropriate title in Cols. 1-28. If Doppler-broadened cross sections are desired, punch 1 in Col. 35, or else punch 0. In Cols. 36-40 give the effective temperature  $T_{\text{eff}}$  in degrees Kelvin, and in Cols. 41-45 punch **NTAB**, which is equal to the odd number of pivot points for the integration for Doppler-broadening; **NTAB** > 13 seems highly unlikely. In Cols. 46-50 punch an integer between 1 and 6 which specifies the particular cross section to be Doppler-broadened. The following list indicates these:

- 1 - scattering cross section with no level-level interference
- 2 - capture cross section with no level-level interference
- 3 - fission cross section with no level-level interference
- 4 - sum of the above three
- 5 - scattering cross section with level-level interference
- 6 - sum of 5, 2, and 3.

In Cols. 51-60 punch **ERROR**, which has been described above. If level-level interference in the scattering cross sections among those resonances which are assigned an average spin is desired, punch 1 in Col. 65, or else punch 0. The rest of the data cards are from **ENDF/B File 2** beginning with the **HEAD** Card and these give the resonance parameters. These are described in the **Data Formats and Procedures Manual**(2).

## REACTOR CODE ABSTRACT

1. Name of Code: SIGPLOT.
2. Computer for which Code is designed: CDC-6600.
3. Nature of problem solved: This code calculates the scattering, capture, fission, and total cross sections from resolved resonance parameter data. Scattering cross sections may be calculated with or without level-level interference. Provision is also made to numerically Doppler-broaden any of the cross sections.
4. Method of solution: Multi-level Breit-Wigner formula. Details of formulae to be found in Gregson, et al.<sup>(1)</sup>
5. Restrictions on the complexity of the problem: This program can handle resonance data up to a maximum of 10 different isotopes with a total number of 500 resonances and an  $l$  value not exceeding 5. It further assumes that the resolved resonance parameters are given for one energy range which is the same for all the isotopes of an element. The mesh points at which the cross sections are calculated can be varied. Since the calculated data are not stored, an increase in the number of mesh points does not conflict with any storage requirements.
6. Typical running time: Calculations of the cross sections of mono-isotopic manganese from its resonance data with 27 resonances, with 20 mesh points between the positive energy resonance, takes 14 secs of central processor time on the CDC-6600.
7. Unusual features of the program:
  - a) In calculating scattering cross sections with level-level interference, resonances are grouped according to their spins for the same  $l$  value. Thus for s-wave resonances, for example, the spins are 3 and 4. It is possible that there are a number of resonances whose spins have not been measured, and these are

given an average spin of 3.5. The program normally calculates scattering cross sections with level-level interference among the spin-3 group and the spin-4 group. Contributions of the spin-3.5 resonances are calculated as a sum of single-level Breit-Wigner terms. If, however, it is desired to include the level-level interference terms among these resonances, this may be indicated on the control card.

b) The method of numerical integration used to Doppler-broaden cross sections is very general and is designed to take care of situations where the fine structure of the cross section is rapidly varying.

8. Related auxiliary programs: This program has been patterned after the MLBW program<sup>(1)</sup> with certain corrections and changes in the sub-routines ORDER, FACTS, and SIGMA.
9. References: K. Gregson, M. F. James, and D. S. Norton, "MLBW - A Multi-level Breit-Wigner Computer Program," U.K. Atomic Energy Establishment Report AEEW-M517 (1965).
10. Machine requirements: This needs a 37k octal memory.
11. Programming language: FORTRAN IV.
12. Operating system or monitor: Brookhaven National Laboratory version of CDC Scope 2.0 operating system.
13. Other programming or operating information: None.
14. Name and establishment: M. R. Bhat and D. Cullen, National Neutron Cross Section Center, Brookhaven National Laboratory, Upton, N.Y.
15. Material available: Fortran deck with sample output.
16. Category:

## PROGRAM SIGMA2

This program is a modified version of SIGPLOT described in the preceding pages. The modifications enable it to handle ENDF/B Version II data. These modifications are described in the Data Formats and Procedures Manual<sup>(2)</sup> in great detail and are briefly the following:

(1) provision is made to give the individual isotopic masses AWRI

(2) channel radius "a" (in units of  $10^{-12}$  cm) and defined by

$$a = \left[ 1.23(AWRI * 1.008665)^{1/3} + 0.8 \right] \times 10^{-1}$$

is used to calculate the penetrabilities  $P_\ell(ka)$  and the shift factors  $S_\ell(ka)$  whereas the effective scattering radius  $\hat{a}$  is used to calculate  $\phi_\ell(k\hat{a})$ , the phase shift.

For details regarding the input data, Doppler broadening and other details of the program please see the write-up on SIGPLOT (p. 12) as they are common to the two programs.



## PROGRAM RAMP1

Program RAMP1 (Reich And Moore Program Version 1) calculates scattering, capture, fission and total cross sections in the resolved resonance region using the Reich-Moore formalism<sup>(4)</sup>. The resonance parameters are assumed to be in the ENDF/B Version-II data format<sup>(2)</sup>. The cross sections may also be Doppler broadened if so desired.

### Formulae:

The cross section for a neutron reaction with the exit channel  $c$  is:

$$\sigma_{nc} = \pi \lambda_n^2 \sum_J g_J \left| \delta_{nc} - U_{nc}^J \right|^2 \quad (1)$$

where  $\lambda_n$  is the reduced neutron wave length;  $g_J$  is the statistical weight factor for resonances of spin  $J$  and  $U_{nc}^J$  is the collision matrix.

In the Reich-Moore approximation, the collision matrix is expressed in terms of a matrix (I-K), with dimensions  $(m+1) \times (m+1)$  where  $m$  is the number of fission channels, used in the cross section analysis; ( $m=2$  in the ENDF/B format) and it is assumed that there is only one neutron channel (though there may be two channel spins for p-wave neutrons). Thus we define,

$$(I-K)_{cc'} = \delta_{cc'} - \frac{i}{2} \sum_{\lambda} \frac{\Gamma_{\lambda c}^{1/2} \Gamma_{\lambda c'}^{1/2}}{E_{\lambda} - E - \frac{i}{2} \Gamma_{\lambda \gamma}} \quad (2)$$

where  $E_{\lambda}$  is the resonance energy and  $\Gamma_{\lambda \gamma}$  the corresponding capture width of the  $\lambda$ -th resonance and  $\Gamma_{\lambda c}$  and  $\Gamma_{\lambda c'}$  are the partial widths corresponding to the channels  $c$  and  $c'$ . Here it is also further assumed that the shift factor  $\Delta_{\lambda}$  is zero. The collision matrix  $U_{nc}^J$  can be expressed in terms



of the matrix defined in equation (2) as

$$U_{nc}^J = e^{-i(\varphi_n + \varphi_c)} [2(I-K)_{nc}^{-1} - \delta_{nc}] \quad (3)$$

where  $\varphi_n$  and  $\varphi_c$  are the hard-sphere phase-shifts. The different cross sections can now be written as

$$\sigma_{Total} = \sum_J \sigma_{nT}^J = 2\pi \chi_n^2 \sum_J g_J \operatorname{Re}(1 - U_{nn}^J) \quad (4)$$

$$= 2\pi \chi_n^2 \sum_J g_J \left[ (1 - \cos 2\varphi_n^l) + 2 \operatorname{Re}(e^{-2i\varphi_n^l} \rho_{nn}^J) \right]$$

$$\sigma_{Fission} = \sum_J \sigma_{nf}^J = \pi \chi_n^2 \sum_J g_J \left( |U_{nf_1}^J|^2 + |U_{nf_2}^J|^2 \right) \quad (5)$$

$$= 4\pi \chi_n^2 \sum_J g_J \left( |\rho_{nf_1}^J|^2 + |\rho_{nf_2}^J|^2 \right)$$

$$\sigma_{Scattering} = \sum_J \sigma_{nn}^J = \pi \chi_n^2 \sum_J g_J |1 - U_{nn}^J|^2 \quad (6)$$

$$= \pi \chi_n^2 \sum_J g_J \left[ 2(1 - \cos 2\varphi_n^l) + 4 \operatorname{Re}(e^{-2i\varphi_n^l} \rho_{nn}^J) - 4 \operatorname{Re}(\rho_{nn}^J) + 4 |\rho_{nn}^J|^2 \right]$$

$$\sigma_{capture} = 4\pi \chi_n^2 \sum_J g_J \sum_{a,b} (I-K)_{na}^{-1} (I-K)_{nb}^{-1*} \operatorname{Re}[(I-K)_{ab} - \delta_{ab}] \quad (7)$$

where  $a, b = 1, 2, 3$ , and 1 = neutron channel and 2, 3 are fission channels.

The total, fission and capture cross-sections are obtained by direct calculation and the scattering cross-section is obtained by subtraction from these.



### Storage Capacity of the Program

1. Maximum number of isotopes: 10.
2. Maximum number of  $l$  values per isotope per energy range: 5.
3. Maximum number of resonances over all isotope energy ranges and  $l$  values: 500.
4. Total memory for the program: 40 K octal.
5. Time: approximately 11 secs/100 energy points for a nucleus with 4 isotopes and 294 s- and p-wave resonances.
6. This program assumes that the resolved resonance parameters are given for one energy range which is the same for all isotopes.

### Procedure:

1. After all the data for one element are read in, the resonance energies over all isotopes are arranged in increasing order.
2. For each pair of levels which lie within the limits of the energy range in the input data, a variable number of energy points (4 MM = 8 as it stands now) which lie between these two levels are generated, and the scattering, capture, fission, and total cross section are calculated and printed out for all the resonances of a given isotope as well as for all the isotopes of a given element. One can get a finer mesh by setting MM (card RMP1228) to a higher value.
3. To avoid having huge core storage, the cross sections are not stored in memory but are printed out as they are generated.
4. The resonances in each isotope are arranged in increasing order of  $l$  and for a given increasing order of J before the cross sections are calculated.
5. To Doppler-broaden cross sections, the same procedure using Gauss-Hermite Quadrature or the Trapezoidal Method as described in SIGPLOT (p.10) is used.

### Input Data

The first card of the input is a TITLE card with the format (7A4,2X,I5,F.1, 2I5, E10.4, I5). One can punch an appropriate title in Cols. 1-28. If Doppler-broadened cross sections are desired, punch 1 in Col. 35, or else punch 0. In Cols. 36-40 give the effective temperature  $T_{\text{eff}}$  in degrees Kelvin, and in Cols. 41-45 punch NTAB, which is equal to the odd number of pivot points for the integration for Doppler-broadening; NTAB > 13 seems highly unlikely. In Cols. 46-50 punch an integer between 1 and 4 which specifies the particular cross section to be Doppler-broadened. The following list indicates these:

- 1 - scattering cross section
- 2 - capture cross section
- 3 - fission cross section
- 4 - total cross section.

In Cols. 51-60 punch ERROR, which has been described above. The rest of the data cards are from ENDF/B File 2 beginning with the HEAD Card and these give the resonance parameters<sup>(2)</sup>.

## REACTOR CODE ABSTRACT

1. Name of Code: RAMP1
2. Computer for which code is designed: CDC-6600
3. Nature of problem solved: This code calculates scattering, capture, fission and total cross sections from Reich-Moore resolved resonance parameters. Cross sections may be Doppler broadened if so desired.
4. Method of solution: Reich-Moore approximation. Details may be found in the reference given.
5. Restrictions on the complexity of the problem: This program can handle resonance data up to a maximum of 10 different isotopes with a total number of 500 resonances and an  $l$  value not exceeding 5. The mesh points at which the cross sections are calculated can be varied. Further, since the calculated data are not stored, an increase in the number of mesh points does not conflict with any storage requirements.
6. Typical running time: Calculations of 4 isotopes involving a total of 294 s and p-wave resonances took 11 sec. of central processor time per 100 energy points on the CDC-6600.
7. Unusual features of the program: The Doppler broadening is done using numerical methods and can handle p-wave and resonances corresponding to higher partial waves.
8. Related auxiliary programs: None
9. References: C. W. Reich and M. S. Moore, Phys. Rev. 111, 929, 1958.
10. Machine Requirements: This program needs 40K octal memory.
11. Programming language: FORTRAN IV

13. Operating System or monitor: Brookhaven National Laboratory  
version of CDC Scope 3.0 operating system.
14. Name and establishment: M. R. Bhat, National Neutron Cross Section  
Center, Brookhaven National Laboratory, Upton, N. Y. 11973.
15. Material available: FORTRAN deck with sample output.
16. Category:



PROGRAM ADLER

This is a program to calculate total, capture or fission cross-sections according to the Adler-Adler formalism using the corresponding parameters from File 2 of ENDF/B Version II data.

Formulae

The Adler-Adler formulae have been discussed in the reports given in the references<sup>(5,6)</sup>. The formulae are:

$$\begin{aligned} \sigma^{(x)}(E) = & \frac{2C}{E} (1 - \cos \omega) \\ & + \frac{C}{\sqrt{E}} \sum_k \frac{\nu_k (G_k^{(x)} \cos \omega + H_k^{(x)} \sin \omega) + (\mu_k - E)(H_k^{(x)} \cos \omega - G_k^{(x)} \sin \omega)}{(\mu_k - E)^2 + \nu_k^2} \\ & + \frac{C}{\sqrt{E}} (A_1^{(x)} + \frac{A_2^{(x)}}{E} + \frac{A_3^{(x)}}{E^2} + \frac{A_4^{(x)}}{E^3} + B_1^{(x)}E + B_2^{(x)}E^2) \end{aligned} \quad (1)$$

$$\text{and } B.G = \frac{C}{\sqrt{E}} (A_1^{(x)} + \frac{A_2^{(x)}}{E} + \frac{A_3^{(x)}}{E^2} + \frac{A_4^{(x)}}{E^3} + B_1^{(x)}E + B_2^{(x)}E^2);$$

$$\text{where } \frac{C}{E} = \pi \lambda^2; \text{ where } \frac{1}{\lambda} = k = 2.196771 \times 10^{-3} \times \left( \frac{AWRI}{AWRI+1.0} \right) \sqrt{E(\text{eV})}$$

where k is the wave number of the incident neutron in the center-of-mass system and AWRI is the isotopic mass in units of the neutron mass.

$\frac{2C}{E} (1 - \cos \omega)$  = potential scattering cross section; this term is non-zero only for scattering and total cross sections.



Procedure (con't)

(3) Cross-sections are not stored in memory so that an increase in mesh points does not conflict with any memory requirements.

(4) Only s-wave resonances are handled by the program.

(5) The Doppler broadened cross-section is written as:

$$\sigma_{\Delta}(E) = \frac{1}{\Delta\sqrt{\pi}} \int_0^{\infty} \sigma(E') e^{-\frac{(E-E')^2}{\Delta^2}} dE' \quad (2)$$

where  $\Delta(\text{eV}) = 0.3177 \left( \frac{T_{\text{eff}}^{\circ}}{293.0} \right)^{\frac{1}{2}} \left( \frac{E(\text{eV})}{\text{AWRI}} \right)^{\frac{1}{2}}$

where  $T_{\text{eff}}^{\circ}$  = effective temperature in degrees Kelvin

AWRI = mass of the isotope. This expression is quite good

except for resonances of very small energies.<sup>(7)</sup> We use the

real and imaginary parts of the complex probability integral

which are proportional to the  $\Psi$  and  $\Phi$  functions to obtain

expressions for Doppler broadened cross-sections.

We define.

$$U = \text{Im} \left( \frac{i}{\pi} \int_{-\infty}^{+\infty} \frac{e^{-t^2}}{z-t} dt \right) ; \quad V = \text{Re} \left( \frac{i}{\pi} \int_{-\infty}^{+\infty} \frac{e^{-t^2}}{z-t} dt \right) \quad (3)$$

where  $z = \xi + i\eta$ ,  $\xi$  and  $\eta$  real. Further,

$$\Psi(s, \theta) = \frac{1}{2} \sqrt{\frac{\pi}{\theta}} U(\xi, \eta) = \frac{1}{(4\pi\theta)^{\frac{1}{2}}} \int_{-\infty}^{+\infty} \frac{e^{-(s-r)^2/4\theta}}{1+r^2} dr$$

$$\text{and } \Phi(s, \theta) = \frac{1}{2} \sqrt{\frac{\pi}{\theta}} V(\xi, \eta) = \frac{1}{(4\pi\theta)^{\frac{1}{2}}} \int_{-\infty}^{+\infty} \frac{e^{-(s-r)^2/4\theta}}{1+r^2} r dr$$

where  $\eta = \frac{1}{2\sqrt{\theta}}$  and  $\xi = s\eta$ . If we further set  $\xi = \frac{\mu-E}{\Delta}$  and  $\eta = \frac{\nu}{\Delta}$ ,

$$\omega = 2k\hat{a}$$

$$= 2WN \sqrt{E(\text{eV})}$$

Where  $\hat{a}$  corresponds to the effective scattering radius in units of  $10^{-13}$  cm;

$$\text{and } WN = 2.196771 \left( \frac{AWRI}{AWRI + 1.0} \right) \times 10^{-3} \times \hat{a},$$

$$A_1^{(x)}, A_2^{(x)}, A_3^{(x)}, A_4^{(x)}$$

$$\text{and } B_1^{(x)}, B_2^{(x)}$$

are background parameters which give contributions due to "tails" of resonances lying outside of the energy range under consideration. They are associated with the type of reaction "x".

$$G_k^{(x)}, H_k^{(x)}$$

Are Adler-Adler parameters, characteristic of the k-th resonance and the type of reaction indicated by "x".

### Procedure

(1) After all the data for one element are read in, the resonance energies of all the isotopes are arranged in increasing order.

(2) For each pair of resonances which lie within the limits of the energy range in the input data, a variable number of energy points (20 = 4 MM as it stands now) which lie between these two resonances are generated, and the total, capture and fission cross sections are calculated and printed out. This is done for all the resonances in an element. A finer mesh may be obtained by setting MM (card ADLR278) to a higher value.

we obtain the Doppler broadened cross section as

$$\sigma_{\Delta}^{(x)}(E) = \frac{2C}{E} (1 - \cos \omega) + \frac{C\sqrt{\pi}}{\Delta} \sum_k \frac{U_k^{(x)}}{E_k^{\frac{1}{2}}} (G_k^{(x)} \cos \omega + H_k^{(x)} \sin \omega) + \frac{C\sqrt{\pi}}{\Delta} \sum_k \frac{V_k^{(x)}}{E_k^{\frac{1}{2}}} (H_k^{(x)} \cos \omega - G_k^{(x)} \sin \omega) \quad (4)$$

The potential scattering term (non-zero only for scattering and total cross-sections) and the background terms are not Doppler broadened, as they are slowly varying and not affected by Doppler broadening. The functions  $U_k^{(x)}$  and  $V_k^{(x)}$  are characteristic of the k-th resonance of the type of cross-section "x", and its parameters are evaluated using a subroutine-PFCN<sup>(8)</sup>.

#### Input Data

First Data Card: Format (7A4, 2X, I5, F5.1)

Reads in TITLE(1), ..... , TITLE(7), IDPL, TEFF

TITLE(1), ....., TITLE(7), = any suitable title for the program.

IDPL = 1 if Doppler broadened cross-sections are desired or else = 0

TEFF = Effective temperature of the sample in degrees kelvin.

Rest of the Data Cards: Follow the ENDF/B File 2 format for Adler-Adler parameters. This is described in detail in Reference 2.

## REACTOR CODE ABSTRACT

1. Name of Code: ADLER
2. Computer for which code is designed: CDC-6600
3. Nature of problem solved: This code calculates total, capture and fission cross-sections from the corresponding Adler-Adler parameters in the ENDF/B File 2 and also Doppler broadens cross-sections.
4. Method of solution: Adler-Adler formalism. Details of formulae are to be found in the report given in references.
5. Restrictions on the complexity of the problem: This program can handle resonance data up to a maximum of 10 isotopes with a total number of 500 resonances. It further assumes that the resolved resonance parameters are given for one energy range which is the same for all the isotopes of an element. The mesh points at which the cross-sections are calculated can be varied. Since the calculated data are not stored, an increase in the number of mesh points does not conflict with any storage requirement.
6. Typical running time: Calculations of cross-sections of one isotope with 37 resonances and 20 mesh points between resonances takes:
  - (a) without Doppler broadening, 21 secs
  - (b) with Doppler broadening, 209 secs.
7. Unusual features of the program: None
8. Related auxiliary program: None
9. References: D. B. Adler and F. T. Adler, Analysis of Neutron Resonances in Fissile Elements: Programs CØDILLI, CURVEPLØT and SIGMA, Report COO-1546-3 (Sept. 1966), Dept. of Physics, University of Illinois, Urbana, Illinois.
10. Machine requirements: This needs a 37K octal memory.
11. Programming language: FORTRAN IV
12. Operating system or monitor: Brookhaven National Laboratory version of CDC Scope 3 operating system.

13. Other programming or operating information: None
14. Name and establishment: M. R. Bhat, National Neutron Cross-Section Center, Brookhaven National Laboratory, Upton, New York.
15. Material available: FORTRAN Deck with sample output.
16. Category:

PROGRAM AVRAGE 3

This is a program to calculate scattering, capture, and fission cross sections in the unresolved resonance region from the energy independent parameters given in ENDF/B, File 2.

Method

The method follows the paper of Lane and Lynn<sup>(9)</sup> and we write the average scattering, fission, and capture cross section respectively as

$$\langle \sigma_{n,n} \rangle = \frac{K}{E} \sum_J \frac{g_J}{\langle D_J \rangle} \left[ \left\langle \frac{\Gamma_n \Gamma_n}{\Gamma_n + \Gamma_f + \Gamma_\gamma} \right\rangle - 2\Gamma_n \sin^2 \varphi_\lambda \right] + \sigma_p \quad (1)$$

$$\langle \sigma_{n,f} \rangle = \frac{K}{E} \sum_J \frac{g_J}{\langle D_J \rangle} \left\langle \frac{\Gamma_n \Gamma_f}{\Gamma_n + \Gamma_f + \Gamma_\gamma} \right\rangle, \quad (2)$$

and

$$\langle \sigma_{n,\gamma} \rangle = \frac{K}{E} \sum_J \frac{g_J}{\langle D_J \rangle} \left\langle \frac{\Gamma_n \Gamma_\gamma}{\Gamma_n + \Gamma_f + \Gamma_\gamma} \right\rangle, \quad (3)$$

where  $K = (2\pi^2/k^2)E(\text{ev})$ , where  $k = \frac{1}{\lambda} = 2.196771 \times 10^{-3} * \left( \frac{\text{AWRI}}{\text{AWRI}+1.0} \right) \sqrt{E}$  and

AWRI is the isotopic mass,

E = neutron energy in eV,

$g_J = \frac{(2J+1)}{2(2I+1)}$ , where I is the target nucleus spin and J is the compound nucleus spin,

$\langle D_J \rangle$  = mean level spacing in eV for spin J resonances,

$\sigma_p = \sum_l \sigma_{pl}$  = potential scattering cross section,

$\sigma_{pl} = 4\pi(2l+1) \frac{\sin^2 \varphi_l}{k^2}$  where l is the angular momentum and

$\varphi_0 = k\hat{a}$  where  $\hat{a}$  is the scattering radius (A)

$\varphi_l = k\hat{a} - \tan^{-1}(k\hat{a})$  and etc.

and the rest of the quantities are different partial widths in eV. The quantities in equation (1) refer to one particular  $l$ -value. The brackets indicate averaging over the neutron and fission width fluctuations assumed to follow a  $\chi^2$  distribution of different degrees of freedom as given in the ENDF/B data. We would like to point here that the fluctuation correction factors  $R_{nl,J}$ ,  $R_{\gamma l,J}$ , or  $R_{fl,J}$  are not calculated separately as the fluctuation corrections are applied by direct averaging as indicated in equations 1-3. The summation is over the different spin states. The averaging is done by the method of Greebler and Hutchins<sup>(10)</sup> and corresponds to evaluating the double integrals on a 10x10 grid, and  $\nu$  can vary from 1 to 4. The gamma width  $\Gamma_\gamma$  is assumed to follow a  $\delta$ -function type of distribution corresponding to a large number degrees of freedom in the  $\chi^2$  distribution.

Incidentally, we note here that this program (1) takes into account only s- and p-wave contributions to the cross sections and (2) does not take into account inelastic scattering. This program uses the channel radius  $a = (1.23 \times (\text{AWRI} \times 1.008668))^{1/3} + 0.8$  in units of  $10^{-12}$  cm to calculate nuclear penetrabilities.

This program needs 21K octal memory for execution.

The data input is explained in great detail in the FORTRAN listing of the program and follows the ENDF/B format except for the first data card which is the title card.

Title Card Format (I10,7A4,2X,3E10.4)

This reads in IRUN, RUN(1), ....., RUN(7), EO, EN, ESTEP.

IRUN = Any run number. If this is zero the program exists, otherwise this card indicates the beginning of a new calculation and one can stack any number of these one behind another.

RUN(1), ....., RUN(7) = Any alphanumeric information.

EO = Beginning energy for calculations in eV.

EN = Ending energy for calculations in eV.

ESTEP = Step interval in eV for calculations in eV.

This information is needed only for non-fissile nuclei.



## REACTOR CODE ABSTRACT

1. Name of Code: AVRAGE3
2. Computer for which Code is designed: CDC-6600
3. Nature of problem solved: This Code calculates average scattering, capture, and fission cross sections from s- and p-wave data of the unresolved parameters of File 2 of ENDF/B.
4. Method of calculation: Theory of average cross section due to Lane and Lynn.<sup>(9)</sup>
5. Restrictions on the complexity of the problem: This program calculates average cross sections up to 100 energy values in the unresolved region. It does not allow for inelastic scattering and calculates only s- and p-wave contributions. Maximum  $\nu = 4$ .
6. Typical running time: Test run calculating s- and p-wave contributions to average scattering, capture, and fission cross sections of Pu-239 at 16 energy points and s- and p-wave contributions to average scattering at capture cross section of U-238 at 100 energy points took 5 secs of central processor time on the CDC-6600.
7. Unusual feature of the program: This program can allow for different degrees of freedom for fission width distribution of resonances of different spins.
8. Related auxiliary programs: None.
9. References: A. M. Lane and J. E. Lynn, Proc. Phys. Soc. A70, 557 (1957).
10. Machine requirements: Needs 21K octal memory.
11. Programming language: FORTRAN IV.
12. Operating system or monitor: Brookhaven National Laboratory version of CDC Scope 3.0 operating system.
13. Other programming or operating information: None.

14. Name and establishment: M. R. Bhat, National Neutron Cross Section Center, Brookhaven National Laboratory, Upton, New York.
15. Material available: Fortran deck with sample output.
16. Category:



PROGRAM AVRAGE4

This is a program to calculate scattering capture, and fission cross sections in the unresolved resonance region, with the ENDF/B Version II data for the unresolved parameters of File 2 which gives the average neutron, gamma and fission widths and widths for any competing inelastic processes as a function of energy.

Method

The method follows the paper of Lane and Lynn<sup>(9)</sup> and we write the average scattering, fission, and capture cross section respectively as

$$\langle \sigma_n \rangle = \frac{K}{E} \sum_J \frac{g_J}{\langle D_J \rangle} \left[ \left\langle \frac{\Gamma_n \Gamma_n}{\Gamma_n + \Gamma_f + \Gamma_\gamma + \Gamma_x} \right\rangle - 2 \Gamma_n \sin^2 \phi_\lambda \right] + \sigma_p \quad (1)$$

$$\langle \sigma_f \rangle = \frac{K}{E} \sum_J \frac{g_J}{\langle D_J \rangle} \left\langle \frac{\Gamma_n \Gamma_f}{\Gamma_n + \Gamma_f + \Gamma_\gamma + \Gamma_x} \right\rangle, \quad (2)$$

and

$$\langle \sigma_\gamma \rangle = \frac{K}{E} \sum_J \frac{g_J}{\langle D_J \rangle} \left\langle \frac{\Gamma_n \Gamma_\gamma}{\Gamma_n + \Gamma_f + \Gamma_\gamma + \Gamma_x} \right\rangle, \quad (3)$$

where  $K = (2 \pi^2 / k^2) E$  (eV) where  $k$  is defined below,

$E$  = neutron energy in eV,

$g_J = \frac{(2J+1)}{2(2I+1)}$ , where  $I$  is the target nucleus spin and  $J$  is the compound nucleus spin,

$\langle D_J \rangle$  = mean level spacing in eV spin  $J$  resonances,

$\sigma_p = \sum \sigma_{p\ell}$  = potential scattering cross section.

$$\sigma_{p\ell} = 4\pi(2\ell+1) \frac{\sin^2 \varphi_\ell}{k^2} \quad \text{Where } \ell \text{ is the angular momentum and}$$

$$\varphi_0 = k\hat{a} \text{ where } \hat{a} \text{ is the scattering radius (A)}$$

$$\varphi_1 = k\hat{a} - \tan^{-1}(k\hat{a})$$

$$\varphi_2 = k\hat{a} - \tan^{-1}\left(\frac{3k\hat{a}}{3-k^2\hat{a}^2}\right) \text{ where}$$

$$k = 2.196771 \times 10^{-3} \left(\frac{\text{AWRI}}{\text{AWRI}+1.0}\right) \sqrt{E(\text{eV})}$$

and AWRI is the isotopic mass in units of neutron mass.

$\Gamma_x$  = is a width in eV to allow for any competing inelastic processes, and the rest of the quantities are different partial widths in eV.

$\Gamma_n = \Gamma_n^0 \sqrt{E} V_\ell \mu_{\ell,J}$  where  $\Gamma_n^0$  is the reduced neutron width (GNO(I)),  $\mu_{\ell,J}$  is the number of degrees of freedom in the neutron width distribution (AMUN), E the neutron energy and  $V_\ell$  is the penetration factor defined as:

$$V_\ell = 1 \text{ for } \ell = 0$$

$$= \rho^2 / (1+\rho^2) \text{ for } \ell = 1$$

$$= \rho^4 / (9+3\rho^2+\rho^4) \text{ for } \ell = 2$$

where  $\rho = ka$  where k is the wave-number of the neutron in the center-of-mass system (see above) and  $a = (1.23(\text{AWRI} \times 1.008665)^{1/3} + 0.8) \times 0.1$  is the channel radius in units of  $10^{-12}$  cm. The brackets indicate averaging over the neutron, fission, and any inelastic width fluctuations assumed to follow a  $\chi^2$  distribution of different degrees of freedom as given in the ENDF/B data. The summation is over the different spin states J. Hence, allowance is made for possible different degrees of freedom of the fission width distribution corresponding to different spin states. The averaging is done by a method similar to that of Grebler and Hutchins,<sup>(10)</sup> and corresponds to evaluating the double integrals on a  $10 \times 10$  grid, and  $\nu$  can vary from 1 to 4. The gamma width  $\Gamma_\gamma$  is assumed to follow a  $\delta$ -function type of distribution corresponding to a large number of degrees of freedom in the  $\chi^2$  distribution.

Incidentally, we note here that this program (1) takes into account only s-, p-, and d-wave contributions to the cross sections and (2) does take into account inelastic scattering. The scattering radius A in the

unresolved resonance region of ENDF/B File 2 is used to calculate potential scattering while the nuclear radius  $a$  defined above is used to calculate nuclear penetrabilities as suggested in the new procedural modifications at the April 1970 CSEWG Meeting.

This program needs 58K (octal) memory for execution.

The data input is explained in great detail in the FORTRAN listing of the program and follows the ENDF/B format except for the first data card which is the title card.

Title Card Format (I10, 7A4)

Read in IRUN, RUN(1), ..... , RUN(7)

IRUN = Any run number. If it is zero the program exits if non-zero it indicates the beginning of a new calculation. One can stack any number of these cases one behind the other.

RUN(1), ..... , RUN(7) = Any alphanumeric in formation.

## REACTOR CODE ABSTRACT

1. Name of Code: AVRAGE4
2. Computer for which Code is designed: CDC-6600
3. Nature of problem solved: This Code calculates average scattering, capture, and fission cross sections from s-, p-, and d-wave data of the unresolved parameters of File 2 of ENDF/B. The parameter corresponds to ENDF/B Version II data with energy dependent neutron, gamma, fission, and inelastic widths.
4. Method of calculation: Theory of average cross section due to Lane and Lynn.<sup>(9)</sup>
5. Restrictions on the complexity of the problem: This program calculates average cross sections up to 100 energy values in the unresolved region. It allows for inelastic scattering and its width fluctuation and calculates only s-, p-, and d-wave contributions. Maximum  $\nu = 4$ .
6. Typical running time: Test run calculating s- and p-wave contributions to average scattering, capture, and fission cross sections of Pu-239 at 16 energy points and s- and p-wave contributions to average scattering and capture cross section of U-238 at 19 energy points took 3.5 secs of central processor time on the CDC-6600.
7. Unusual feature of the program: This program can allow for different degrees of freedom for fission width distribution of resonances of different spins.
8. Related auxiliary programs: None.
9. References: A. M. Lane and J. E. Lynn, Proc Phys. Soc. A70, 557 (1957).
10. Machine requirements: Needs 58K octal memory.
11. Programming language: FORTRAN IV.
12. Operating system or monitor: Brookhaven National Laboratory version of CDC Scope 3.0 operating system.
13. Other programming or operating information: None.

14. Name and establishment: M. R. Bhat, National Neutron Cross Section Center, Brookhaven National Laboratory, Upton, New York 11973.
15. Material available: FORTRAN deck with sample output.
16. Category:



## References

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7. G. W. Hinman, G. F. Kuncir, J. B. Sampson and G. B. West, Nucl. Sci. Eng. 16, 202 (1963).
8. M. R. Bhat and G. E. Lee-Whiting, Nucl. Instruments and Methods 47, 277 (1967).
9. A. M. Lane and J. E. Lynn, Proc. Phys. Soc. A 70, 557 (1957).
10. P. Greebler and B. A. Hutchins, Proc. of the Seminar on Physics of Fast and Intermediate Reactors, IAEA, Vienna 1962, Vol. 3, p. 121.





ERAY(2,J)=AP(I)	SIGP121
102 CONTINUE	SIGP122
J1=J1+NRS	SIGP123
JL=JL+1	SIGP124
IF(NMOM-NLS(I,J2))104,104,103	SIGP125
103 NRANGE=NRANGE+1	SIGP126
J2=J2+1	SIGP127
IF(NRANGE-NERI)106,106,1010	SIGP128
1010 NRES(I)=J1-JFID	SIGP129
JFID=J1	SIGP130
101 CONTINUE	SIGP131
NTOTAL=J1-1	SIGP132
SCALE=1.0E+00	SIGP133
PHI=3.14159265	SIGP134
3 FORMAT(2E11,4,4I11)	SIGP135
4 FORMAT(6E11,4)	SIGP136
5 FORMAT(8E11,4,3I10)	SIGP137
6 FORMAT(2X,2E11,4)	SIGP138
7 FORMAT(107H NEUTRON ENERGY( EV) SIGNN SIGCAP	SSIGP139
1IGF SIGT SIGNNMULT SIGTMULT )	SIGP140
8 FORMAT(2X,7E15,6)	SIGP141
9 FORMAT(10X,2E20,6)	SIGP142
10 FORMAT(20H ERROR IN INPUT DATA)	SIGP143
11 FORMAT(10X,2I10)	SIGP144
12 FORMAT(10X,6I10)	SIGP145
16 FORMAT(15H NEUTRON ENERGYE15,6)	SIGP146
14 FORMAT(53H CROSS-SECTIONS CALCULATED WITHOUT DOPPLER BROADENING)	SIGP147
15 FORMAT(50H CROSS-SECTIONS CALCULATED WITH DOPPLER BROADENING)	SIGP148
17 FORMAT(33H (Z,A) DESIGNATION OF THE ELEMENTE11,4,22H AT,WT/MASS OFS	SIGP149
1 NEUTRONE11,4,15H NO OF ISOTOPES I5)	SIGP150
18 FORMAT(24H DATA FOR ISOTOPE NUMBER I5)	SIGP151
19 FORMAT(33H (Z,A) DESIGNATION OF THE ISOTOPEE11,4,21H FRACTIONAL ABS	SIGP152
1 UNDANCEE11,4,20H NO OF ENERGY RANGES I5)	SIGP153
20 FORMAT(36H LOWER LIMIT OF THE ENERGY RANGE(EV)E11,4,18H UPPER L	SIGP154
1 MIT(EV)E11,4,6H LRU=15,6H LRF=15)	SIGP155
21 FORMAT(13H NUCLEAR SPINE11,4,18H SCATTERING LENGTHE11,4,15H NO OF	SIGP156
1 L-VALUES I5,6H LIS=I5)	SIGP157
22 FORMAT(41H CONSTANT USED TO CALCULATE PENETRABILITYE11,4,22H SCATT	SIGP158
1 ERING LENGTH(A-)E11,4,17H ANGULAR MOMENTUM I5,17H NO OF RESONANCES	SIGP159
25)	SIGP160
23 FORMAT(85H ERES SPIN GTOT GN	SIGP161
1 GGAMMA GF )	SIGP162
24 FORMAT(11H I TITLE 7A4)	SIGP163
25 FORMAT(//)	SIGP164
26 FORMAT(6(2X,E11,4,2X))	SIGP165
27 FORMAT(33H CROSS-SECTIONS AT THERMAL ENERGY)	SIGP166
28 FORMAT(2X,2E20,6,I10)	SIGP167
29 FORMAT(2X,4E11,4)	SIGP168
30 FORMAT(22H EFFECTIVE TEMPERATUREF5,1,41H IN DEGREES KELVIN, NO	SIGP169
10F PIVOT POINTS I5,18H CONVERGENCE ERROR E10,4,13H AND INCROSS=15)	SIGP170
31 FORMAT(53H THE INTEGRAL FOR DOPPLER BROADENING DID NOT CONVERGE)	SIGP171
C---c-THIS IS WHERE RESONANCES OF EACH ISOTOPE ARE ARRANGED IN INCREASING	SIGP172
C---c-#G ORDER IN L AND FOR EACH L IN INCREASING ORDER IN J,	SIGP173
DO 133 I=1,NIS	SIGP174
NRESI=NRES(I)	SIGP175
CALL ORDER(I,NRESI)	SIGP176
133 CONTINUE	SIGP177
13 FORMAT(10(1X,I10))	SIGP178
DO 135 I=1,NTOTAL	SIGP179
ARAY(1,I)=ARAY(1,I)*SCALE	SIGP180
ARAY(3,I)=ARAY(3,I)*SCALE	SIGP181

	ARAY(4,I)=ARAY(4,I)*SCALE	SIGP182
	ARAY(5,I)=ARAY(5,I)*SCALE	SIGP183
	ARAY(6,I)=ARAY(6,I)*SCALE	SIGP184
135	CONTINUE	SIGP185
	NCOUNT=1	SIGP186
	DO 1330 I=1,NIS	SIGP187
	APX=AP(I)	SIGP188
	NRESI=NRES(I)	SIGP189
	NLMT=NCOUNT+NRFSI-1	SIGP190
	DO 1331 J=NCOUNT,NLMT	SIGP191
	CALL FACTS(ARAY(1,J),IRAY(1,J),PENFAR(J),SHIFAR(J),PS,CUNST,AWR,	SIGP192
	1APX,1.0)	SIGP193
1331	CONTINUE	SIGP194
	NCOUNT=NCOUNT+NRESI	SIGP195
1330	CONTINUE	SIGP196
	DO 108 I=1,NTOTAL	SIGP197
	ERAN(1,I)=ARAY(1,I)	SIGP198
	ERAN(2,I)=ARAY(3,I)	SIGP199
108	CONTINUE	SIGP200
	CALL QIKS(1,NTOTAL,MOV,KOM)	SIGP201
C-----	HERE RESONANCE IN AN ELEMENT ARE ARRANGED IN INCREASING ORDER IN	SIGP202
C-----	ENERGY ALONG WITH THEIR TOTAL GAMMAS TO CALCULATE THE ENERGY MESH	SIGP203
C-----	AT WHICH THE CROSS-SECTIONS ARE CALCULATED,	SIGP204
146	PRINT27	SIGP205
	PRINT25	SIGP206
	PRINT7	SIGP207
	E=ETHERM	SIGP208
	CALL SIGMA(ETHERM,AWR,1)	SIGP209
	PRINT25	SIGP210
	ELO=EL(1,1)*SCALE	SIGP211
	JFLAG(1)=1	SIGP212
	IRANGE=1	SIGP213
C-----	WE HAVE ARBITRARILY SET ELO=1.0E-11 MEV HERE TO BE ABLE TO DOPPLERS	SIGP214
C-----	BROADEN THERMAL CROSS-SECTIONS,LATER ON IN THE PROGRAM ELO IS READ	SIGP215
C-----	IN FROM THE DATA AND COULD VARY FROM 1.0E-11 TO 1.0E+09MEV,	SIGP216
	PRINT8,ETHERM,(AREF(LL),LL=1,6)	SIGP217
	IF(IDPL.EQ,1)GO TO 147	SIGP218
	GO TO 148	SIGP2181
147	TEF=TEFF/293.0	SIGP219
	DELTA=0.3177*SQRT ((TEF*ETHERM)/AWR)	SIGP220
C	CONTINUE	SIGP221
	CALL GRID(ETHERM,DELTA,NTAB,XTAB)	SIGP222
	CALL GREAT2(DOPPLER,FINT,XTAB,NTAB,ERROR,IERR)	SIGP223
	PRINT28,ETHERM,FINT,JFLAG(1)	SIGP224
	IF(IERR.EQ,1)PRINT31	SIGP225
148	PRINT25	SIGP226
	PRINT7	SIGP227
	PRINT25	SIGP228
	DO 124 JJ=1,NIS	SIGP229
	NERJJ=NER(JJ)	SIGP230
	DO 125 KK=1,NERJJ	SIGP231
	IRANGE=KK	SIGP232
	LRUJK=LRU(JJ,KK)	SIGP233
	IF(LRUJK-1)131,1321,125	SIGP234
131	PRINT10	SIGP235
	GO TO 130	SIGP236
1321	IF(JJ.EQ,1)GO TO 1320	SIGP237
	GO TO 132	SIGP2371
1320	ELOREF=EL(JJ,KK)*SCALE	SIGP238
	EHIREF=EH(JJ,KK)*SCALE	SIGP239
	ELO=ELOREF	SIGP240

EH1=EH1REF	SIGP241
GO TO 1240	SIGP242
132 ELO=EL(JJ, KK)*SCALE	SIGP243
EH1=EH(JJ, KK)*SCALE	SIGP244
IF(ELO, EQ, ELORF, AND, EH1, EQ, EH1REF)GO TO 124	SIGP245
GO TO 1240	SIGP2451
1240 MM=MAXPTS/(8*MAXRES)	SIGP246
NN=MM	SIGP247
IFLAG=1	SIGP248
NLSKK=NLS(JJ, KK)	SIGP249
J4=1	SIGP250
ISTART=1	SIGP251
IEND=1	SIGP252
117 IF(IEND EQ, 0)GO TO 125	SIGP253
J5=J4+1	SIGP254
E1=ERAN(1, J4)	SIGP255
G1=ERAN(2, J4)	SIGP256
E2=ERAN(1, J5)	SIGP257
G2=ERAN(2, J5)	SIGP258
IF(E1, LT, ELO, AND, E2, LT, ELO)GO TO 1120	SIGP259
GO TO 1105	SIGP2591
1105 IF(E1, LE, ELO, AND, E2, GT, ELO)GO TO 1110	SIGP260
GO TO 1111	SIGP2601
1110 E1=ELO	SIGP261
G1=G2	SIGP262
ISTART=0	SIGP263
GO TO 1114	SIGP264
1111 IF(E1, GT, ELO, AND, E2, LE, EH1)GO TO 1112	SIGP265
GO TO 1113	SIGP2651
1112 IF(J4, EQ, 1, AND, ISTART, EQ, 1)GO TO 1106	SIGP266
GO TO 1114	SIGP2661
1106 E2=E1	SIGP267
G2=G1	SIGP268
E1=ELO	SIGP269
J4=J4-1	SIGP270
ISTART=0	SIGP271
GO TO 1114	SIGP272
1116 E2=EH1+G1/FLOAT (MM)	SIGP273
G2=G1	SIGP274
IFLAG=0	SIGP275
GO TO 1114	SIGP276
1113 IF(E1, LT, EH1, AND, E2, GE, EH1)GO TO 1123	SIGP277
GO TO 1124	SIGP2771
1123 E2=EH1	SIGP278
G2=G1	SIGP279
IEND=0	SIGP280
GO TO 1114	SIGP281
1124 IF(E1, GE, EH1, AND, E2, GT, EH1)GO TO 125	SIGP282
GO TO 1125	SIGP2821
1125 IF(IFLAG)1120, 125, 1120	SIGP283
1114 IF(E1, EQ, E2)GO TO 1120	SIGP284
GO TO 1118	SIGP2841
1118 CONTINUE	SIGP285
CALL SIEVE(E1, G1, E2, G2, MM, NN, NX, TEFF, AWR)	SIGP286
CALL QIKS(1, NX, MOVE, KOME)	SIGP287
GO TO 116	SIGP288
1120 IF(IEND EQ, 0)GO TO 125	SIGP289
J4=J4+1	SIGP290
GO TO 117	SIGP291
116 DO 109 I=1, NX	SIGP292
E=EX(I)	SIGP293

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JFLAGI=JFLAG(I)
CALL SIGMA(E,AWR,KK)
PRINT8,E,(AREF(LL),LL=1,6)
IF(IDPL.EQ.1)GO TO 141
GO TO 109
141 IF(E.LT.ETHERM)GO TO 109
GO TO 1410
C-----IF THE NEUTRON ENERGY IS LESS THAN 0.0253 EV DOPPLER BROADENING IS
C-----PASSED AS A DIFFERENT KERNEL SHOULD BE USED TO CALCULATE DOPPLER
C-----BROADENED CROSS-SECTIONS,
1410 TEF=TEFF/293.0
DELTA=0.3177*SQRT ((TEF*E)/AWR)
C CONTINUE
GO TO (1121,1122),JFLAGI
1121 CALL GRID(E,DELTA,NTAB,XTAB)
32 FORMAT(2X,11E11,4)
CALL GREAT2(DOPPLER,FINT,XTAB,NTAB,ERROR,IERR)
PRINT28,E,FINT,JFLAG(I)
IF(IERR.EQ.1)PRINT31
GO TO 109
1122 CALL GAUSS(E,DELTA,DOPE)
PRINT28,E,DOPE,JFLAG(I)
109 CONTINUE
IF(IFLAG)1117,125,1117
1117 J4=J4+1
IF(NTOTAL=J4)125,1250,117
1250 E1=ERAN(1,J4)
G1=ERAN(2,J4)
GO TO 1116
125 CONTINUE
124 CONTINUE
120 CONTINUE
130 CALL EXIT
END
SUBROUTINE ORDER(K,N1)
COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU, LRF,LANG,NLS,
1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,LIS,C,AM,DREF,AREF,IRANGE,NIS,
3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR
DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),
1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),
2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),SHIFAR
3(500),SPI(10),AP(10),LIS(10),C(10),AM(10),DREF(6),AREF(6)
IF(K-1)2,2,3
2 NTR=0
NUML=0
NUMJ=0
NN=0
MM=0
JJ=0
NC=0
MC=0
3 NT=NTR+1
NTR=NTR+N1
OL=-0.9
8 OL=OL+1.0
DO 101 N=NT,NTR
TERM=FLOAT (IRAY(1,N))
IF(OL=TERM)101,101,9
9 NN=NN+1
DO 100 J=1,6
A=ARAY(J,N)

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SIGP294
SIGP295
SIGP296
SIGP297
SIGP2971
SIGP298
SIGP2981
ISSIGP299
SIGP300
SIGP301
SIGP302
SIGP303
SIGP304
SIGP305
SIGP306
SIGP307
SIGP308
SIGP309
SIGP310
SIGP311
SIGP312
SIGP313
SIGP314
SIGP315
SIGP316
SIGP317
SIGP318
SIGP319
SIGP320
SIGP321
SIGP322
SIGP323
SIGP324
SIGP325
ORDR001
ORDR002
ORDR003
ORDR004
ORDR005
ORDR006
ORDR007
ORDR008
ORDR009
ORDR010
ORDR011
ORDR012
ORDR013
ORDR014
ORDR015
ORDR016
ORDR017
ORDR018
ORDR019
ORDR020
ORDR021
ORDR022
ORDR023
ORDR024
ORDR025
ORDR026
ORDR027

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	ARAY(J,N)=ARAY(J,NN)	ORDR028
	ARAY(J,NN)=A	ORDR029
100	CONTINUE	ORDR030
	DO 1001 J=1,3	ORDR031
	IA=IRAY(J,N)	ORDR032
	IRAY(J,N)=IRAY(J,NN)	ORDR033
	IRAY(J,NN)=IA	ORDR034
1001	CONTINUE	ORDR035
	DO 1002 J=1,2	ORDR036
	EA=ERAY(J,N)	ORDR037
	ERAY(J,N)=ERAY(J,NN)	ORDR038
	ERAY(J,NN)=EA	ORDR039
1002	CONTINUE	ORDR040
101	CONTINUE	ORDR041
	IF(NN=NC)8,8,11	ORDR042
11	NUML=NUML+1	ORDR043
	LN(NUML)=NN-NC	ORDR044
	NC=NN	ORDR045
	NU=NT+LN(NUML)-1	ORDR046
	OM=0.25	ORDR047
14	OM=OM+0.5	ORDR048
	DO 205 M=NT,NU	ORDR049
	TERMJ=ARAY(2,M)	ORDR050
	IF(OM-TERMJ)205,205,15	ORDR051
15	MM=MM+1	ORDR052
	DO 204 J=1,6	ORDR053
	A=ARAY(J,M)	ORDR054
	ARAY(J,M)=ARAY(J,MM)	ORDR055
	ARAY(J,MM)=A	ORDR056
204	CONTINUE	ORDR057
	DO 2041 J=1,3	ORDR058
	IA=IRAY(J,M)	ORDR059
	IRAY(J,M)=IRAY(J,MM)	ORDR060
	IRAY(J,MM)=IA	ORDR061
2041	CONTINUE	ORDR062
	DO 2042 J=1,2	ORDR063
	EA=ERAY(J,M)	ORDR064
	ERAY(J,M)=ERAY(J,MM)	ORDR065
	ERAY(J,MM)=EA	ORDR066
2042	CONTINUE	ORDR067
205	CONTINUE	ORDR068
	IF(MM=MC)14,14,16	ORDR069
16	NUMJ=NUMJ+1	ORDR070
	JN(NUMJ)=MM-MC	ORDR071
	MC=MM	ORDR072
	NT=NT+JN(NUMJ)	ORDR073
	IF(NN-MM)17,17,14	ORDR074
17	IF(NTR-NN)18,18,8	ORDR075
18	RETURN	ORDR076
	END	ORDR077
	SUBROUTINE SIGMA(O,BWR,KK)	SIGM001
	COMMON/E/XMIN(6),XMAX(6),XREF(6)	SIGM002
	COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU, LRF,LANG,NLS,	SIGM003
	1NRES, LN, JN, PENFAR, SHIFAR, SPI, AP, LIS, C, AM, DREF, AREF, IRANGE, NIS,	SIGM004
	3INCROSS, IVSPIN, ELO, TEFF, DELTA, E, AWR	SIGM005
	DIMENSION ARAY(6,500), IRAY(3,500), ERAY(2,500), NOT(20), ZAI(10),	SIGM006
	1ABN(10), NER(10), LFW(10), EL(10,10), EH(10,10), LRU(10,10), LRF(10,10),	SIGM007
	2LANG(10,5,5), NLS(10,10), NRES(10), LN(50), JN(150), PENFAR(500), SHIFAR	SIGM008
	3(500), SPI(10), AP(10), LIS(10), C(10), AM(10), DREF(6), AREF(6)	SIGM009
	PI=3.14159265359	SIGM010
	DO 4 J=1,6	SIGM011



AREF(J)=0,0	SIGM012
4 CONTINUE	SIGM013
TERROR=1.0E-03	SIGM014
L2=0	SIGM015
N2=0	SIGM016
LA=0	SIGM017
JA=0	SIGM018
NTR=0	SIGM019
DO 112 I=1,NIS	SIGM020
NRESI=NRES(I)	SIGM021
API=AP(I)	SIGM022
3 NTR=NTR+NRESI	SIGM023
IF(NRESI)110,110,100	SIGM024
100 LA=LA+1	SIGM025
102 L2=L2+LN(LA)	SIGM026
CALL FACTS(Q,IRAY(1,L2),PF,SF,PS,CONSTE,BWR,API,3,0)	SIGM027
SNGLN=0.0	SIGM028
SNGLG=0.0	SIGM029
SNGLF=0.0	SIGM030
SNNL2=0.0	SIGM031
103 JA=JA+1	SIGM032
104 N1=N2+1	SIGM033
N2=N2+JN(JA)	SIGM034
GJ=2.0*(2.0*SPI(I)+1.0)	SIGM035
GJ=(2.0*ARAY(2,N1)+1.0)/GJ	SIGM036
X=1.0	SIGM037
SPIN=ARAY(2,N1)	SIGM038
SPII=SPI(I)	SIGM039
CALL SPINOR(SPII,IRAY(1,L2),XSPIN)	SIGM040
ABDIF=ABS(XSPIN-SPIN)	SIGM041
IF(IVSPIN,EQ,1)GO TO 115	SIGM042
GO TO 116	SIGM0421
116 IF(ABDIF,LT,TERROR)GO TO 117	SIGM043
GO TO 115	SIGM0431
117 X=0.0	SIGM044
115 SNNK23=0.0	SIGM045
DO 108 K=N1,N2	SIGM046
GNK=PF*ARAY(4,K)/PENFAR(K)	SIGM047
GK=GNK+ARAY(5,K)+ARAY(6,K)	SIGM048
ERDK=ARAY(1,K)+((SHIFAR(K)-SF)*ARAY(4,K))/(2.0*PENFAR(K))	SIGM049
ED=Q-ERDK	SIGM050
DK=ED*ED+0.25*GK*GK	SIGM051
SNNK2=GNK*GNK*COS(2.0*PS)	SIGM052
SNNK2=SNNK2-2.0*GNK*(ARAY(5,K)+ARAY(6,K))*SIN(PS)*SIN(PS)	SIGM053
SNNK2=SNNK2+2.0*GNK*ED*SIN(2.0*PS)	SIGM054
SNNK2=SNNK2/DK	SIGM055
SNGK=GNK*ARAY(5,K)/DK	SIGM056
SNFK=GNK*ARAY(6,K)/DK	SIGM057
SNGLN=SNGLN+SNNK2*GJ	SIGM058
SNGLG=SNGLG+SNGK*GJ	SIGM059
SNGLF=SNGLF+SNFK*GJ	SIGM060
SNNK3=0.0	SIGM061
IF(K=N1)107,107,105	SIGM062
105 M1=K-1	SIGM063
DO 106 M=N1,M1	SIGM064
GNM=PF*ARAY(4,M)/PENFAR(M)	SIGM065
GM=GNM+ARAY(5,M)+ARAY(6,M)	SIGM066
ERDM=ARAY(1,M)+((SHIFAR(M)-SF)*ARAY(4,M))/(2.0*PENFAR(M))	SIGM067
EDD=Q-ERDM	SIGM068
DM=EDD*EDD+0.25*GM*GM	SIGM069
SNNM3=EDD*EDD+0.25*GK*GM	SIGM070

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SNNM3=SNNM3*2,0*GNK*GNM/(DM*DK)
SNNK3=SNNK3+SNNM3
106 CONTINUE
107 CONTINUE
SNNK23=SNNK23+SNNK2+SNNK3*X
108 CONTINUE
SNNL2=SNNL2+SNNK23*GJ
IF(L2=N2)109,109,103
109 BETA=PI*ABN(1)/(CONSTE*CONSTE)
AREF(1)=AREF(1)+SNGLN*BETA
AREF(2)=AREF(2)+SNGLG*BETA
AREF(3)=AREF(3)+SNGLF*BETA
AREF(4)=AREF(4)+BETA*(SNGLN+SNGLG+SNGLF)
AREF(5)=AREF(5)+SNNL2*BETA
AREF(6)=AREF(6)+BETA*(SNGLG+SNGLF+SNNL2)
IF(L2=NTR)100,110,110
110 SIGP=0,0
LRUJK=LHU(I,KK)
IF(LRUJK-1)1250,1250,125
1250 NLSKK=NLS(I,KK)
DO 126 LL=1,NLSKK
LURE=LANG(I,KK,LL)
SS=FLOAT(LURE)
CALL FACTS(Q,LURE,PF,SF,PS,CONSTA,BWR,API,3,0)
TRM=(2,0*SS+1,0)*4,0*PI
TRM=TRM*SIN(PS)*SIN(PS)/(CONSTA*CONSTA)
SIGP=SIGP+TRM
126 CONTINUE
125 AREF(1)=AREF(1)+SIGP*ABN(I)
AREF(4)=AREF(4)+SIGP*ABN(I)
AREF(5)=AREF(5)+SIGP*ABN(I)
AREF(6)=AREF(6)+SIGP*ABN(I)
112 CONTINUE
RETURN
END
SUBROUTINE FACTS(Q,L,PF,SF,PS,CONSTE,BWR,BP,PL0D)
C
C SUBROUTINE TO CALCULATE PENETRATION AND
C SHIFT FACTORS
C Q IS THE ENERGY L IS THE ANGULAR MOMENTUM PF PENETRATION FACTOR
C SF THE SHIFT FACTOR AND PS THE PHASE SHIFT AP IS R CONSTE IS KM
C FOR DETAILS OF FORMULAE SEE GREGSON ET AL AEEW-M517(MLBW)1965
C
DATA WNEUT/1,008665/
EAB=ABS(Q)
CONHLD=2,196771E+03*BWR*SQRT(EAB)
CONSTE=CONHLD/(BWR+1,0)
C-----SINCE AWR IS GIVEN WITH THE NEUTRON MASS AS UNITY WE ADD ONE ABOVE
C-----TO CONVERT TO THE CENTER-OF-MASS SYSTEM
ROE=BP*CONSTE
S=FLOAT(L)
IF(L,LE-0)GO TO 100
GO TO(110,120,130,140,150),L
100 PF=ROE
SF=0,0
IF(PL0D-LT,2,0) GO TO 160
PS=ROE
GO TO 170
110 ROE2=ROE*ROE
DENOM=1-0+ROE2
PF=ROE2*ROE/DENOM

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SIGM071
SIGM072
SIGM073
SIGM074
SIGM075
SIGM076
SIGM077
SIGM078
SIGM079
SIGM080
SIGM081
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SIGM084
SIGM085
SIGM086
SIGM087
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SIGM099
SIGM100
SIGM101
SIGM102
SIGM103
SIGM104
SIGM105
FACT001
FACT002
FACT003
FACT004
FACT005
FACT006
FACT007
FACT008
FACT009
FACT010
FACT011
FACT012
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FACT023
FACT024
FACT025
FACT026

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SF=-1.0/DENOM	FACT027
IF(PL0D.LT,2,0) GO TO 160	FACT028
PS=ROE-ATAN (ROE)	FACT029
IF(PS/ROE=0,000001)160,170,170	FACT030
120 ROE2=ROE*ROE	FACT031
ROE4=ROE2*ROE2	FACT032
DENOM=3.0*ROE2+ROE4+9,0	FACT033
PF=ROE4*ROE/DENOM	FACT034
SF=- (18.0+3,0*ROE2)/DENOM	FACT035
IF(PL0D.LT,2,0) GO TO 160	FACT036
PS=ROE-ATAN (3,0*ROE/(3,0-ROE2))	FACT037
IF(PS/ROE=0,000001)160,170,170	FACT038
130 ROE2=ROE*ROE	FACT039
ROE4=ROE2*ROE2	FACT040
ROE6=ROE4*ROE2	FACT041
DENOM=225,0+45,0*ROE2+6,0*ROE4+ROE6	FACT042
PF=ROE6*ROE/DENOM	FACT043
SF=- (675,0+90,0*ROE2+6,0*ROE4)/DENOM	FACT044
IF(PL0D.LT,2,0) GO TO 160	FACT045
PS=ROE-ATAN ((15,0*ROE-ROE2*ROE)/(15,0-6,0*ROE2))	FACT046
IF(PS/ROE=0,000001)160,170,170	FACT047
140 ROE2=ROE*ROE	FACT048
ROE4=ROE2*ROE2	FACT049
ROE6=ROE4*ROE2	FACT050
ROE8=ROE4*ROE4	FACT051
DENOM=11025,0+1575,0*ROE2+135,0*ROE4+10,0*ROE6+ROE8	FACT052
PF=ROE8*ROE/DENOM	FACT053
IF(PL0D.LT,2,0) GO TO 160	FACT054
SF=- (44100,0+4725,0*ROE2+270,0*ROE4+10,0*ROE6)/DENOM	FACT055
PS=ROE-ATAN ((105,0*ROE-10,0*ROE2*ROE)/(105,0-45,0	FACT056
1*ROE2+ROE4))	FACT057
IF(PS/ROE=0,000001)160,170,170	FACT058
150 ROE2=ROE*ROE	FACT059
ROE4=ROE2*ROE2	FACT060
ROE6=ROE4*ROE2	FACT061
ROE8=ROE4*ROE4	FACT062
ROE10=ROE6*ROE4	FACT063
DENOM=893025,0+99225,0*ROE2+6300,0*ROE4+315,0*ROE6	FACT064
1*15,0*ROE8+ROE10	FACT065
PF=ROE10*ROE/DENOM	FACT066
SF=4465125,0+396900,0*ROE2+18900,0*ROE4	FACT067
1*630,0*ROE6+15,0*ROE8	FACT068
SF=-SF/DENOM	FACT069
IF(PL0D.LT,2,0) GO TO 160	FACT070
PS=ROE-ATAN ((945,0*ROE-ROE*(105,0*ROE2-ROE4))/(945,0-420,0*ROE2+	FACT071
115,0*ROE4))	FACT072
IF(PS/ROE.GE,0,000001) GO TO 170	FACT073
160 PS=0,0	FACT074
170 RETURN	FACT075
END	FACT076
SUBROUTINE MOV(I,J)	MOV 001
COMMON/D/ERAN(2,501)	MOV 002
I1=I	MOV 003
J1=J	MOV 004
IF(I1.EQ,0)I1=501	MOV 005
IF(J1.EQ,0)J1=501	MOV 006
ERAN(1,J1)=ERAN(1,I1)	MOV 007
ERAN(2,J1)=ERAN(2,I1)	MOV 008
RETURN	MOV 009
END	MOV 010
SUBROUTINE MOVE(I,J)	MOVE001

COMMON/C/EX(101),JFLAG(101)	MOVE002
I1=I	MOVE003
J1=J	MOVE004
IF(I1.EQ.0)I1=101	MOVE005
IF(J1.EQ.0)J1=101	MOVE006
EX(J1)=EX(I1)	MOVE007
JFLAG(J1)=JFLAG(I1)	MOVE008
RETURN	MOVE009
END	MOVE010
FUNCTION KOM(I,J)	KOM 001
COMMON/D/ERAN(2,501)	KOM 002
I1=I	KOM 003
J1=J	KOM 004
IF(I1.EQ.0)I1=501	KOM 005
IF(J1.EQ.0)J1=501	KOM 006
EOM=ERAN(1,I1)-ERAN(1,J1)	KOM 007
IF(EOM)100,101,102	KOM 008
100 KOM=-1	KOM 009
GO TO 103	KOM 010
101 KOM=0	KOM 011
GO TO 103	KOM 012
102 KOM=1	KOM 013
103 RETURN	KOM 014
END	KOM 015
FUNCTION KOME(I,J)	KOME002
COMMON/C/EX(101),JFLAG(101)	KOME003
I1=I	KOME004
J1=J	KOME005
IF(I1.EQ.0)I1=101	KOME006
IF(J1.EQ.0)J1=101	KOME007
EOX=EX(I1)-EX(J1)	KOME008
IF(EOX)100,101,102	KOME009
100 KOME=-1	KOME010
GO TO 103	KOME011
101 KOME=0	KOME012
GO TO 103	KOME013
102 KOME=1	KOME014
103 RETURN	KOME015
END	KOME015
SUBROUTINE QIKS (MM,NN,MOVE,COMPAR)	QIKS0010
CGIKS ALL-IN-MEMORY SORT PROGRAM	QIKS0020
C MM = FIRST SUBSCRIPT	QIKS0030
C NN = LAST SUBSCRIPT (ARRAY IS IN COMMON)	QIKS0040
C MOVE AND COMPARE ARE USER SUPPLIED PROGRAMS	QIKS0050
DIMENSION MSAVE(20),NSAVE(20)	QIKS0060
KEYLOC(M,N)=(N+M)/2	QIKS0070
I=0	QIKS0080
J=0	QIKS0090
LEVEL = 0	QIKS0100
M=MM	QIKS0110
N=NN	QIKS0120
35 CONTINUE	QIKS0130
C TEST FOR ONE OR TWO ITEMS	QIKS0140
IF(N-M-1) 31,51,32	QIKS0150
C 32 CONTINUE	QIKS0160
C PARTITION AND SPREADER GO HERE, SEE BELOW. RETURN IS TO 8	QIKS0170
C PUSH DOWN	QIKS0180
8 LEVEL=LEVEL+1	QIKS0190
C WORK ON SMALLEST PORTION	QIKS0200
IF ((J-M) = (N-I)) 134, 134, 34	QIKS0210
134 MSAVE(LEVEL) = I	QIKS0220

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34 MSAVE(LEVEL)=M
   NSAVE(LEVEL)=J
   M=I
   GO TO 35
51 IF(COMP(M,N))31,31,131
   SWAP IF ONLY TWO ITEMS ARE OUT OF ORDER
C 131 CALL MOVE(M,0)
   CALL MOVE(N,M)
   CALL MOVE(0,N)
31 IF(LEVEL)151,150,151
150 RETURN
C 151 M = MSAVE(LEVEL)
   N=NSAVE(LEVEL)
   LEVEL=LEVEL-1
   GO TO 35
C END MAIN
C PARTITION
32 I=M
   J=N
   KEY=KEYLOC(M,N)
   CALL MOVE(KEY,0)
54 IF(N=KEY)17,1,17
17 CALL MOVE(N,KEY)
1 CONTINUE
C HOLE AT BOTTOM
   IF(COMP(0,I))3,2,2
2 I=I+1
   IF(I=J)1,4,1
3 CALL MOVE(I,J)
   GO TO 5
6 CONTINUE
C HOLE AT TOP
   IF(COMP(0,J))5,5,7
5 J=J-1
   IF(I=J)6,4,6
7 CALL MOVE(J,I)
   GO TO 2
C 4 CONTINUE
   SPREADER GOES HERE
C END PARTITION
C SPREADER
4 CALL MOVE(0,I)
12 IF(I=N)110,10,110
110 I=I+1
   IF(COMP(0,I))10,12,10
10 IF(J=M)108,8,108
108 J=J-1
   IF(COMP(0,J))8,10,8
C 8 CONTINUE
   RETURN TO MAIN PROGRAM
C END
SUBROUTINE SPINOR(S,L,XJ)
   TERM=0.0
   DENOM=0.0
   IF(S.EQ.0.,AND.L.EQ.0)GO TO 100
   GO TO 101
C-----FOR S=0 AND S-WAVE RESONANCES SPINS ARE ALL KNOWN HENCE ONE NEEDS

```

QIKS0260  
QIKS0270  
QIKS0280  
QIKS0290  
QIKS0300  
QIKS0310  
QIKS0320  
QIKS0330  
QIKS0340  
QIKS0350  
QIKS0360  
QIKS0370  
QIKS0380  
QIKS0390  
QIKS0400  
QIKS0410  
QIKS0420  
QIKS0430  
QIKS0440  
QIKS0450  
QIKS0460  
QIKS0470  
QIKS0480  
QIKS0490  
QIKS0500  
QIKS0510  
QIKS0520  
QIKS0530  
QIKS0540  
QIKS0550  
QIKS0560  
QIKS0570  
QIKS0580  
QIKS0590  
QIKS0600  
QIKS0610  
QIKS0620  
QIKS0630  
QIKS0640  
QIKS0650  
QIKS0660  
QIKS0670  
QIKS0680  
QIKS0690  
QIKS0700  
QIKS0710  
QIKS0720  
QIKS0730  
QIKS0740  
QIKS0750  
QIKS0760  
QIKS0770  
SPNR001  
SPNR002  
SPNR003  
SPNR004  
SPNR0051  
SPNR005

```

C-----LEVEL=LEVEL INTERFERENCE,
101 IF(S.EQ.0.)GO TO 102
    GO TO 103
102 XJ=FLOAT (L)
    GO TO 110
103 XJ1=S*0.5
    XJ2=S*0.5
111 XL=FLOAT (L)
    IF(XJ1.GT.XL)GO TO 104
    GO TO 105
104 TERM=TERM+XJ1*(2.0*XL+1.0)
    DENOM=DENOM+(2.0*XL+1.0)
    GO TO 106
105 TERM=TERM+XL*(2.0*XJ1+1.0)
    DENOM=DENOM+(2.0*XJ1+1.0)
106 IF(XJ2.GT.XL)GO TO 107
    GO TO 108
107 TERM=TERM+XJ2*(2.0*XL+1.0)
    DENOM=DENOM+(2.0*XL+1.0)
    GO TO 109
108 TERM=TERM+XL*(2.0*XJ2+1.0)
    DENOM=DENOM+(2.0*XJ2+1.0)
109 XJ=TERM/DENOM
    GO TO 110
100 XJ=0.0
110 RETURN
    END
    SUBROUTINE GAUSS(Q,BELTA,DOPE)
    COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU, LRF,LANG,NLS,
1NRRES,LN,JN,PENFAR,SHIFAR,SPI,AP,LIS,C,AM,DREF,AREF,IRANGE,NIS,
3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR
    DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),
1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),
2LANG(10,5,5),NLS(10,10),NRRES(10),LN(50),JN(150),PENFAR(500),
3SHIFAR(500),SPI(10),AP(10),LIS(10),C(10),AM(10),DREF(6),AREF(6)
    DIMENSION ABC(9),WET(9)
    DATA ABC/-3.19099320178153,-2.26658058453184,-1.46855328921667,-0.8485010
172355101875284,0,0,0,72355101875284,1.46855328921667,2.26658058453184,3.19099320178153/
2184,3.19099320178153/
    DATA WET/0.3960697726326E-04,0.4943624275537E-02,0.8847452739438E-04,0.4326515570026E+00,0.7202352156061E+00,0.4326515570026E+00,0.8485010
2847452739438E-01,0.4943624275537E-02,0.3960697726326E-04/
    DATA PHIRT/1.772454/
    TERM=0.0
    X=BELTA*ABC(9)
    IF(E-X)100,100,101
101 DO 102 I=1,9
    ABCI=ABC(I)
    WETI=WET(I)
    Z=E+ABCI*BELTA
    CALL SIGMA(Z,AWR,IRANGE)
    TERM=TERM+AREF(INCROSS)*WETI
102 CONTINUE
    DOPE=TERM/PHIRT
    GO TO 110
100 DOPE=0.0
110 RETURN
    END
    SUBROUTINE GREAT1(F,FINT,NTAB,JMAX,XTAB,PARTS,GOOF,INTER,ERROR,
1 IERR)
C-----CARRY OUT CONVERGENCE INTEGRATION SCHEME USING TRAPAZOIDAL RULE

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SPNR006
SPNR007
SPNR0071
SPNR008
SPNR009
SPNR010
SPNR011
SPNR012
SPNR013
SPNR0131
SPNR014
SPNR015
SPNR016
SPNR017
SPNR018
SPNR019
SPNR0191
SPNR020
SPNR021
SPNR022
SPNR023
SPNR024
SPNR025
SPNR026
SPNR027
SPNR028
SPNR029
GAUS001
GAUS002
GAUS003
GAUS004
GAUS005
GAUS006
GAUS007
GAUS008
GAUS009
GAUS010
GAUS011
GAUS012
GAUS013
GAUS014
GAUS015
GAUS016
GAUS017
GAUS018
GAUS019
GAUS020
GAUS021
GAUS022
GAUS023
GAUS024
GAUS025
GAUS026
GAUS027
GAUS028
GAUS029
GAUS030
GAUS031
GRT1001
GRT1002
GRT1003

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C-----AND DOUBLING THE NUMBER OF REGIONS PER SUBINTERVAL FOR EACH      GRT1004
C-----ITERATION, ONLY DOUBLE UP IN THOSE INTERVALS THAT HAVE NOT ALREADY GRT1005
C-----CONVERGED,                                                         GRT1006
C-----F      =SINGLE PRECISION FUNCTION TO BE INTEGRATED                 GRT1007
C-----FINT   =THE RESULTING INTEGRAL                                     GRT1008
C-----NTAB  =NUMBER OF ORDINATES SUPPLIED (THERE ARE N-1 INTERVALS)     GRT1009
C-----JMAX  =MAXIMUM ALLOWABLE NUMBER OF ITERATIONS                     GRT1010
C-----XTAB  =TABLE OF THE ORDINATE VALUES, RANGE OF INTEGRATION IS     GRT1011
C-----      FROM XTAB(1) TO XTAB(NTAB)                                  GRT1012
C-----PARTS =ARRAY OF DIMENSION NTAB, EQUAL TO THE PARTIAL INTEGRALS    GRT1013
C-----      OVER EACH OF THE NTAB-1 INTERVALS                          GRT1014
C-----GOOF  =ARRAY OF DIMENSION NTAB, EQUAL TO THE NORMAL ERROR IN EACH GRT1015
C-----      OF THE NTAB-1 INTERVAL,                                     GRT1016
C-----INTER =ARRAY OF DIMENSION NTAB, SEPECIFYING THE NUMBER OF        GRT1017
C-----      SUBINTERVALS IN EACH INTERVAL                               GRT1018
C-----ERROR =ACCEPTABLE NORMAL ERROR                                    GRT1019
C-----IERR  =ERROR INDICATOR, SET TO ZERO IF METHOD CONVERGES, SET TO    GRT1020
C-----      ONE IF METHOD DOES NOT CONVERGE                               GRT1021
C-----      DIMENSION XTAB(NTAB),PARTS(NTAB),INTER(NTAB),GOOF(NTAB)   GRT1022
C-----INITIALIZE VALUE OF THE INTEGRAL                                    GRT1023
C-----      FINT=0,0                                                    GRT1024
C-----CALCULATE THE NUMBER OF INTERVALS                                  GRT1025
C-----      NM1=NTAB-1                                                  GRT1026
C-----CALCULATE ALLOWABLE ERROR PER INTERVAL                            GRT1027
C-----      ERRN=ERROR/FLOAT(NM1)                                       GRT1028
C-----INITIALIZE APPROXIMATION TO INTEGRAL                              GRT1029
C-----      TOTAL=0,0                                                    GRT1030
C-----CALCULATE INITIAL APPROXIMATION                                   GRT1031
C-----      DO 10 I=1,NM1                                                GRT1032
C-----          INTER(I)=1                                               GRT1033
C-----          PARTS(I)=0,5*(XTAB(I+1)-XTAB(I))*(F(XTAB(I+1))+F(XTAB(I))) GRT1034
C-----          10 TOTAL=TOTAL+PARTS(I)                                   GRT1035
C-----CALCULATE INITIAL ERRORS                                         GRT1036
C-----      DO 15 I=1,NM1                                                GRT1037
C-----          15 GOOF(I)=PARTS(I)                                       GRT1038
C-----SET UP LOOP OVER ITERATIONS                                       GRT1039
C-----      DO 100 J=1,JMAX                                              GRT1040
C-----SAVE LAST APPROXIMATION                                           GRT1041
C-----      TOTAL1=TOTAL                                                 GRT1042
C-----SET UP LOOP OVER INTERVALS                                         GRT1043
C-----      DO 20 I=1,NM1                                                GRT1044
C-----CHECK FOR CONVERGENCE IN THIS INTERVAL                            GRT1045
C-----      IF(ABS(GOOF(I)/TOTAL),LT,ERRN) GO TO 20                      GRT1046
C-----CALCULATE DOUBLE INTERVAL                                         GRT1047
C-----      DX=(XTAB(I+1)-XTAB(I))/FLOAT(INTER(I))                     GRT1048
C-----DOUBLE NUMBER OF STEPS                                           GRT1049
C-----      INTER(I)=2*INTER(I)                                         GRT1050
C-----INITIALIZE CONTRIBUTION TO INTEGRAL                                GRT1051
C-----      REST=0,0                                                     GRT1052
C-----      II=INTER(I)                                                  GRT1053
C-----INITIALIZE ORDINATE                                               GRT1054
C-----      XNOW=XTAB(I)+0,5*DX                                          GRT1055
C-----SET UP LOOP OVER ORDINATES                                         GRT1056
C-----      DO 30 K=1,II,2                                               GRT1057
C-----          REST=REST+F(XNOW)                                         GRT1058
C-----          30 XNOW=XNOW+DX                                           GRT1059
C-----CALCULATE NEXT PARTIAL INTEGRAL                                    GRT1060
C-----      REST=0,5*(PARTS(I)+DX*REST)                                   GRT1061
C-----ADD NEW PARTIAL INTEGRAL AND SUBTRACT OLD PARTIAL INTEGRAL       GRT1062
C-----      TOTAL=TOTAL+REST-PARTS(I)                                    GRT1063
C-----CALCULATE NEW ERROR AND SET PARTIAL INTEGRAL TO NEW VALUE         GRT1064

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      GOOF(I)=REST-PARTS(I)
      PARTS(I)=REST
      20 CONTINUE
C-----CHECK FOR CONVERGENCE
      100 IF(ABS(1,-TOTAL1/TOTAL),LE,ERROR) GO TO 200
C-----THE METHOD HAS NOT CONVERGED
      FINT=TOTAL
      IERR=1
      RETURN
C-----THE METHOD HAS CONVERGED
      200 FINT=TOTAL
      IERR=0
      RETURN
      END
      SUBROUTINE GREAT2(F,FINT,XTAB,NTAB,ERROR,IERR)
C-----CARRY OUT CONVERGENCE INTEGRATION SCHEME USING UP TO 200 INTERVALS
C-----WHICH ARE THEN FURTHER SUBDIVIDED UNTIL CONVERGENCE OCCURS OR THE
C-----MAXIMUM ALLOWABLE NUMBER OF ITERATIONS IS EXCEEDED, THE SUBROUTINE
C-----ARGUMENTS ARE DEFINED AS FOLLOWS,.....
C-----F =FUNCTION TO BE INTEGRATED,
C-----FINT =THE RESULTING INTEGRAL
C-----XTAB =TABLE OF ORDINATES (INTEGRATION INTERVAL IS FROM XTAB(1) TO
C-----XTAB(NTAB))
C-----NTAB =THE LENGTH OF THE XTAB TABLE (NUMBER OF ORDINATES),
C-----ERROR =ALLOWABLE NORMAL ERROR,
C-----IERR =ERROR INDICATOR SET TO ZERO IF METHOD CONVERGES, SET TO
C-----ONE IF METHOD DOES NOT CONVERGE,
C-----ONE IF METHOD DOES NOT CONVERGE OR TABLE (XTAB) IS TOO LONG
      DIMENSION XTAB(33),PARTS(33),GOOF(33),INTER(33)
C-----DEFINE THE MAXIMUM ALLOWABLE NUMBER OF ITERATIONS AND THE MAXIMUM
C-----TABLE LENGTH,
      DATA JMAX,NTABMX/20,1000/
C-----DETERMINE IF TABLE IS TOO LONG
      IF(NTAB.GT,NTABMX) GO TO 100
C-----CALL GENERAL INTEGRATION SUBROUTINE,
      ZZZ=F(5.0)
      CALL GREAT1(F,FINT,NTAB,JMAX,XTAB,PARTS,GOOF,INTER,ERROR,IERR)
      RETURN
C-----TABLE IS TOO LONG.
      100 IERR=1
      FINT=0.0
      RETURN
      END
      FUNCTION DOPPLER(X)
      COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU,LRF,LANG,NLS,
      1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,LIS,C,AM,DREF,AREF,IRANGE,NIS,
      3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR
      DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),
      1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),
      2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),SHIFAR
      3(500),SPI(10),AP(10),LIS(10),C(10),AM(10),DREF(6),AREF(6)
      Z=(E-X)/DELTA
      Z2=Z*Z
      CALL SIGMA(X,AWR,IRANGE)
      DOPPLER =AREF(INCROSS)*EXP(-Z2)/(DELTA*1.772454)
      RETURN
      END
      SUBROUTINE GRID(Q,BELTA,NTAB,XTAB)
      COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU,LRF,LANG,NLS,
      1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,LIS,C,AM,DREF,AREF,IRANGE,NIS,
      3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR

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GRT1065
GRT1066
GRT1067
GRT1068
GRT1069
GRT1070
GRT1071
GRT1072
GRT1073
GRT1074
GRT1075
GRT1076
GRT1077
GRT1078
GRT2001
GRT2002
GRT2003
GRT2004
GRT2005
GRT2006
GRT2007
GRT2008
GRT2009
GRT2010
GRT2011
GRT2012
GRT2013
GRT2014
GRT2015
GRT2016
GRT2017
GRT2018
GRT2019
GRT2020
GRT2021
GRT20211
GRT2022
GRT2023
GRT2024
GRT2025
GRT2026
GRT2027
GRT2028
DOPL001
DOPL002
DOPL003
DOPL004
DOPL005
DOPL006
DOPL007
DOPL008
DOPL009
DOPL010
DOPL011
DOPL012
DOPL013
DOPL014
GRID001
GRID002
GRID003
GRID004

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DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),   GRID005
1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),GRID006
2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),   GRID007
3SHIFAR(500),SPI(10),AP(10),LIS(10),C(10),AM(10),DREF(6),AREF(6)  GRID008
DIMENSION XTAB(33)   GRID009
  IGNORE=1   GRID010
  N2=NTAB/2   GRID011
  N21=N2+1   GRID012
  N22=N2+2   GRID013
  N3=NTAB-1   GRID014
  XTAB(N21)=0   GRID015
  DO 1410 I=N22,NTAB   GRID016
  XTAB(I)=XTAB(I-1)+BELTA   GRID017
  II=NTAB+1-I   GRID018
  XTAB(II)=XTAB(II+1)-BELTA   GRID019
1410 CONTINUE   GRID020
  DO 1411 I=1,NTAB   GRID021
  XTABI=XTAB(I)   GRID022
  IF(XTABI)1412,1412,1411   GRID023
1412 IGNORE=0   GRID024
1411 CONTINUE   GRID025
  IF(IGNORE,EQ,0)GO TO 1413   GRID026
  GO TO 1414   GRID0261
1413 XTAB(1)=1,0E+03   GRID027
  DO 1415 I=1,N3   GRID028
  I1=I+1   GRID029
  XTAB(I1)=XTAB(1)+FLOAT(I)*BELTA   GRID030
1415 CONTINUE   GRID031
1414 RETURN   GRID032
  END   GRID033
SUBROUTINE SIEVE(E1,G1,E2,G2,M,N,NX,BEFF,BWR)   SIEV001
COMMON/C/EX(101),JFLAG(101)   SIEV002
IF(E2.LT,E1)GO TO 101   SIEV003
GO TO 300   SIEV0031
300 N2=2*N   SIEV004
DO 1000 I=1,100   SIEV005
JFLAG(I)=2   SIEV006
1000 CONTINUE   SIEV007
TEF=BEFF/293,0   SIEV008
DP=(1.5885E+00)*SQRT(TEF/BWR)   SIEV009
WHEN MULTIPLIED BY SQRT(E) DP GIVES 5 TIMES CORRESPONDING DELTA   SIEV010
DP1=DP*SQRT(E1)   SIEV011
DP2=DP*SQRT(E2)   SIEV012
DG1=G1/FLOAT(M)   SIEV013
DG2=G2/FLOAT(M)   SIEV014
EX(1)=E1   SIEV015
IF(G1.LT,DP1)GO TO 1001   SIEV016
GO TO 1002   SIEV0161
1001 JFLAG(1)=1   SIEV017
1002 ENDDIF=ABS(E2-E1)   SIEV018
NX=1   SIEV019
DO 100 I=1,N   SIEV020
XX=E1+DG1*FLOAT(I)   SIEV021
IF(XX.LT,E2)GO TO 107   SIEV022
GO TO 100   SIEV0221
107 NX=NX+1   SIEV023
EX(NX)=XX   SIEV024
IF(G1.LT,DP1)GO TO 1003   SIEV025
GO TO 100   SIEV0251
1003 JFLAG(NX)=1   SIEV026
100 CONTINUE   SIEV027

```

DO 200 I=1,N	SIEV028
XX=E2-DG2*FLOAT (I)	SIEV029
IF(XX.GT,E1)GO TO 108	SIEV030
GO TO 200	SIEV0301
108 NX=NX+1	SIEV031
EX(NX)=XX	SIEV032
IF(G2.LT,DP2)GO TO 1005	SIEV033
GO TO 200	SIEV0331
1005 JFLAG(NX)=1	SIEV034
200 CONTINUE	SIEV035
110 DIFF=(E2-E1)/FLOAT (N2)	SIEV036
IF(DIFF)101,102,102	SIEV037
101 PRINT103	SIEV038
PRINT2000,E1,E2,DIFF	SIEV039
GO TO 104	SIEV040
103 FORMAT(32H CALLING SEQUENCE OF SIEVE WRONG)	SIEV041
2000 FORMAT(4H E1=E13,6,4H E2=E13,6,6H DIFF=E13,6)	SIEV042
102 N21=NX+1	SIEV043
NN=NX	SIEV044
N22=N21*N2-2	SIEV045
NX=N22	SIEV046
E21=(E1+E2)/2.0	SIEV047
DP12=DP*SQRT (E21)	SIEV048
E43=E2-E1-((G1+G2)/2.0)	SIEV049
IF(E43.LT,DP12)GO TO 1006	SIEV050
GO TO 1007	SIEV0501
1006 DO 111 I=N21,N22	SIEV051
I2=I-NN	SIEV052
EX(I)=E1+DIFF*FLOAT (I2)	SIEV053
JFLAG(I)=1	SIEV054
111 CONTINUE	SIEV055
GO TO 1040	SIEV056
1007 DO 112 I=N21,N22	SIEV057
I2=I-NN	SIEV058
EX(I)=E1+DIFF*FLOAT (I2)	SIEV059
DPTEST=DP*SQRT (EX(I))	SIEV060
IF(EX(I).LE,E21)GO TO 1008	SIEV061
GO TO 1009	SIEV0611
1008 IF(G1.LT,DPTEST)GO TO 1010	SIEV062
GO TO 112	SIEV0621
1010 JFLAG(I)=1	SIEV063
GO TO 112	SIEV064
1009 IF(G2.LT,DPTEST)GO TO 1011	SIEV065
GO TO 112	SIEV0651
1011 JFLAG(I)=1	SIEV066
112 CONTINUE	SIEV067
1040 DO 113 I=1,NX	SIEV068
DPF=DP*SQRT (EX(I))	SIEV069
IF(DPF,E0.0,0)GO TO 113	SIEV0691
TERM=EX(I)/DPF	SIEV070
IF(TERM.LT,25.)GO TO 114	SIEV071
GO TO 113	SIEV0711
114 JFLAG(I)=1	SIEV072
113 CONTINUE	SIEV073
104 RETURN	SIEV074
END	SIEV075

SIGPLOT TEST, IRON DATA,

		0 350.	11	2	1.0E-4	
26056.E+0	55.36724E+0	0	0	4	0	0
26054.0	0.0584	0	0	1	0	0
4750.	100.E+3	1	2	0	0	0
0.	0.6	0	0	2	0	0
.001175	0.0	0	0	78	13	0
-15000.	.5E+0	5001.000	5000.	1.00		
7.83E+3	.5E+0	1202.16	1200.E+0	2.16		
52.1 E+3	.5E+0	2100.E+0	2100.E+0	.3E+0		
71.9 E+3	.5E+0	1600.E+0	1600.E+0	.3E+0		
98.5 E+3	.5E+0	400.E+0	400.E+0	.3E+0		
102.6 E+3	.5E+0	1375.E+0	1375.E+0	.3E+0		
132. E+3	.5E+0	1600.E+0	1600.E+0	.3E+0		
147. E+3	.5E+0	1950.E+0	1950.E+0	.3E+0		
173. E+3	.5E+0	4800.E+0	4800.E+0	.3E+0		
188.5 E+3	.5E+0	38000.E+0	38000.E+0	.3E+0		
245. E+3	.5E+0	13000.E+0	13000.E+0	.3E+0		
330. E+3	.5E+0	2750.E+0	2750.E+0	.3E+0		
370. E+3	.5E+0	3000.E+0	3000.E+0	.3E+0		
1.175E+3	0.	1	0	12		2
9480.	.5	2.04	1.04	1.0		
14400.	.5	2.13	1.13	1.0		
26056.E+0	.9168E+0	0	0	1		0
4750.	100.E+3	1	2	0		0
0.E+0	.60E+0	0	0	2		0
.001187	0.0	0	0	90		15
-4000.	.5	576.01	575.	1.01		
27700.	.5	1401.44	1400.	1.44		
74. E+3	.5E+0	425.E+0	425.E+0	1.E+0		
83.6 E+3	.5E+0	1000.E+0	1000.E+0	1.E+0		
123.5 E+3	.5E+0	150.E+0	150.E+0	1.E+0		
130. E+3	.5E+0	500.E+0	500.E+0	1.E+0		
141.3 E+3	.5E+0	2300.E+0	2300.E+0	1.E+0		
169. E+3	.5E+0	690.E+0	690.E+0	1.E+0		
186. E+3	.5E+0	3160.E+0	3160.E+0	1.E+0		
220. E+3	.5E+0	1300.E+0	1300.E+0	1.E+0		
243.5 E+3	.5E+0	300.E+0	300.E+0	1.E+0		
273. E+3	.5E+0	3500.E+0	3500.E+0	1.E+0		
315. E+3	.5E+0	5500.E+0	5500.E+0	1.E+0		
360. E+3	.5E+0	9300.E+0	9300.E+0	1.E+0		
382. E+3	.5E+0	10000.E+0	10000.E+0	1.E+0		
1.187E+3	0.0	1	0	72		12
1150.	.5	.616	.052	.564		
2350.	.5	1.0004	.0004	1.		
11200.	1.5	1.022	.022	1.		
22700.	1.5	1.1055	.1055	1.		
34100.	1.5	2.346	.346	2.		
36600.	.5	1.43	.43	1.		
38300.	1.5	1.298	.298	1.		
45800.	.5	2.381	.381	2.		
51900.	.5	2.685	.685	2.		
53300.	1.5	1.37	.37	1.		
55000.	.5	1.1625	.1625	1.		
59000.	.5	2.74	.74	2.		
26057.E+0	.021700E+0	0	0	1		0
4750.	100.E+3	1	2	0		0
0.	.6	0	0	2		0
.001193	0.0	0	0	30		5
3900.	0.0	241.5	240.	1.5		
6300.	1.0	463.73	460.	3.73		
28000.	1.	3005.	3000.	5.		

40500.	0.	2516.83	2516.	.83	
45500.	1.	269.83	269.	.83	
.001193	0.0		1	0	8
1630.	0.	1.08	.25	.83	
4750.	0.	1.086	.256	.83	
7220.	1.	1.753	.923	.83	
7900.	1.	1.146	.316	.83	
12800.	2.	1.336	.506	.83	
13900.	2.	2.426	.776	1.65	
18000.	1.	2.71	1.06	1.65	
21300.	1.	6.92	1.92	5.	
26050.E+0	.0031E+0		0	0	0
4750.	100.E+3		1	2	0
0.E+0	.60E+0		0	2	0
1.200E=3	0.0		0	6	1
-600.	.5	3.57	2.57	1.00	
1.200E=3	0.0		1	0	2
230.	.5	1.00654	.00654	1.	
359.	.5	1.0173	.0173	1.	

TITLE SIGPLOT TEST, IRON DATA,

(Z,A) DESIGNATION OF THE ELEMENT 2.6056E+04 AT.WT/MASS OF NEUTRON 5.5367E+01 NO OF ISOTOPES 4

DATA FOR ISOTOPE NUMBER 1

(Z,A) DESIGNATION OF THE ISOTOPE 2.6054E+04 FRACTIONAL ABUNDANCE 5.8400E-02 NO OF ENERGY RANGES 1  
LOWER LIMIT OF THE ENERGY RANGE(EV) 4.7500E+03 UPPER LIMIT(EV) 1.0000E+05 LRU= 1 LRP= 2  
NUCLEAR SPIN 0.0000E+00 SCATTERING LENGTH 6.0000E-01 NO OF L-VALUES 2 LIS= 0  
CONSTANT USED TO CALCULATE PENETRABILITY 1.1750E-03 SCATTERING LENGTH(A-) 0.0000E+00 ANGULAR MOMENTUM 0 NO OF RESONANCES 13

ERES	SPIN	GTOT	GN	GGAMMA	GF
-1.5000E+04	5.0000E-01	5.0010E+03	5.0000E+03	1.0000E+00	0.0000E+00
7.8300E+03	5.0000E-01	1.2022E+03	1.2000E+03	2.1600E+00	0.0000E+00
5.2100E+04	5.0000E-01	2.1000E+03	2.1000E+03	3.0000E+01	0.0000E+00
7.1900E+04	5.0000E-01	1.6000E+03	1.6000E+03	3.0000E+01	0.0000E+00
9.8500E+04	5.0000E-01	4.0000E+02	4.0000E+02	3.0000E-01	0.0000E+00
1.02260E+05	5.0000E-01	1.3750E+03	1.3750E+03	3.0000E-01	0.0000E+00
1.3200E+05	5.0000E-01	1.6000E+03	1.6000E+03	3.0000E-01	0.0000E+00
1.4700E+05	5.0000E-01	1.9500E+03	1.9500E+03	3.0000E-01	0.0000E+00
1.7300E+05	5.0000E-01	4.8000E+03	4.8000E+03	3.0000E-01	0.0000E+00
1.8850E+05	5.0000E-01	3.8000E+04	3.8000E+04	3.0000E+01	0.0000E+00
2.4500E+05	5.0000E-01	1.3000E+04	1.3000E+04	3.0000E+01	0.0000E+00
3.3000E+05	5.0000E-01	2.7500E+03	2.7500E+03	3.0000E+01	0.0000E+00
3.7000E+05	5.0000E-01	3.0000E+03	3.0000E+03	3.0000E+01	0.0000E+00

CONSTANT USED TO CALCULATE PENETRABILITY 1.1750E-03 SCATTERING LENGTH(A-) 0.0000E+00 ANGULAR MOMENTUM 0 NO OF RESONANCES 2

ERES	SPIN	GTOT	GN	GGAMMA	GF
9.4800E+03	5.0000E-01	2.0400E+00	1.0400E+00	1.0000E+00	0.0000E+00
1.4400E+04	5.0000E-01	2.11300E+00	1.1300E+00	1.0000E+00	0.0000E+00

DATA FOR ISOTOPE NUMBER 2

(Z,A) DESIGNATION OF THE ISOTOPE 2.6056E+04 FRACTIONAL ABUNDANCE 9.1680E-01 NO OF ENERGY RANGES 1  
LOWER LIMIT OF THE ENERGY RANGE(EV) 4.7500E+03 UPPER LIMIT(EV) 1.0000E+05 LRU= 1 LRP= 2  
NUCLEAR SPIN 0.0000E+00 SCATTERING LENGTH 6.0000E-01 NO OF L-VALUES 2 LIS= 0  
CONSTANT USED TO CALCULATE PENETRABILITY 1.1870E-03 SCATTERING LENGTH(A-) 0.0000E+00 ANGULAR MOMENTUM 0 NO OF RESONANCES 15

ERES	SPIN	GTOT	GN	GGAMMA	GF
-4.0000E+03	5.0000E-01	5.7601E+02	5.7500E+02	1.0110E+00	0.0000E+00
2.7700E+04	5.0000E-01	1.4014E+03	1.4000E+03	1.4400E+00	0.0000E+00
7.4000E+04	5.0000E-01	4.2500E+02	4.2500E+02	1.0000E+00	0.0000E+00
8.3600E+04	5.0000E-01	1.0000E+03	1.0000E+03	1.0000E+00	0.0000E+00
1.2350E+05	5.0000E-01	1.5000E+02	1.5000E+02	1.0000E+00	0.0000E+00
1.3000E+05	5.0000E-01	5.0000E+02	5.0000E+02	1.0000E+00	0.0000E+00
1.4130E+05	5.0000E-01	2.3000E+03	2.3000E+03	1.0000E+00	0.0000E+00
1.6900E+05	5.0000E-01	6.9000E+02	6.9000E+02	1.0000E+00	0.0000E+00
1.8800E+05	5.0000E-01	3.1600E+03	3.1600E+03	1.0000E+00	0.0000E+00
2.2000E+05	5.0000E-01	1.3000E+03	1.3000E+03	1.0000E+00	0.0000E+00
2.4350E+05	5.0000E-01	3.0000E+02	3.0000E+02	1.0000E+00	0.0000E+00
2.7300E+05	5.0000E-01	3.5000E+03	3.5000E+03	1.0000E+00	0.0000E+00
3.1500E+05	5.0000E-01	5.5000E+03	5.5000E+03	1.0000E+00	0.0000E+00
3.6000E+05	5.0000E-01	9.3000E+03	9.3000E+03	1.0000E+00	0.0000E+00
3.8200E+05	5.0000E-01	1.0000E+04	1.0000E+04	1.0000E+00	0.0000E+00

CONSTANT USED TO CALCULATE PENETRABILITY 1.1870E-03 SCATTERING LENGTH(A\*) 0.0000E+00 ANGULAR MOMENTUM 1 NO OF RESONANCES 12

ERES	SPIN	GTOT	GN	GGAMMA	GF
1.1500E+03	5.0000E-01	6.1600E+01	5.2000E-02	5.6400E-01	0.0000E+00
2.3500E+03	5.0000E-01	1.0004E+00	4.0000E-04	1.0000E+00	0.0000E+00
1.1200E+04	1.5000E+00	1.0220E+00	2.2000E-02	1.0000E+00	0.0000E+00
2.2700E+04	1.5000E+00	1.4055E+00	1.0550E-01	1.0000E+00	0.0000E+00
3.4100E+04	1.5000E+00	2.3460E+00	3.4600E-01	2.0000E+00	0.0000E+00
3.6600E+04	5.0000E-01	1.4300E+00	4.3000E-01	1.0000E+00	0.0000E+00
3.8300E+04	1.5000E+00	1.2980E+00	2.9800E-01	1.0000E+00	0.0000E+00
4.5800E+04	5.0000E-01	2.3810E+00	3.8100E-01	2.0000E+00	0.0000E+00
5.1900E+04	5.0000E-01	2.6850E+00	6.8500E-01	2.0000E+00	0.0000E+00
5.3300E+04	1.5000E+00	1.3700E+00	3.7000E-01	1.0000E+00	0.0000E+00
5.5000E+04	5.0000E-01	1.1625E+00	1.6250E-01	1.0000E+00	0.0000E+00
5.9000E+04	5.0000E-01	2.7400E+00	7.4000E-01	2.0000E+00	0.0000E+00

DATA FOR ISOTOPE NUMBER 3

(2,A) DESIGNATION OF THE ISOTOPE 2.6057E+04 FRACTIONAL ABUNDANCE 2.1700E-02 NO OF ENERGY RANGES 1  
 LOWER LIMIT OF THE ENERGY RANGE(EV) 4.7500E+03 UPPER LIMIT(EV) 1.0000E+05 LRU= 1 LRF= 2  
 NUCLEAR SPIN 5.0000E-01 SCATTERING LENGTH 6.0000E-01 NO OF L-VALUES 2. LIS= 0  
 CONSTANT USED TO CALCULATE PENETRABILITY 1.1933E-03 SCATTERING LENGTH(A\*) 0.0000E+00 ANGULAR MOMENTUM 0 NO OF RESONANCES 5

ERES	SPIN	GTOT	GN	GGAMMA	GF
3.9000E+03	0.0000E+00	2.4150E+02	2.4000E+02	1.5000E+00	0.0000E+00
6.3000E+03	1.0000E+00	4.6373E+02	4.6000E+02	3.7300E+00	0.0000E+00
2.8000E+04	1.0000E+00	3.0050E+03	3.0000E+03	5.0000E+00	0.0000E+00
4.0500E+04	0.0000E+00	2.5168E+03	2.5160E+03	8.3000E+01	0.0000E+00
4.5500E+04	1.0000E+00	2.6983E+02	2.6900E+02	8.3000E+01	0.0000E+00

ERES	SPIN	GTOT	GN	GGAMMA	GF
1.6300E+03	0.0000E+00	1.0800E+00	2.5000E+01	8.3000E-01	0.0000E+00
4.7500E+03	0.0000E+00	1.0860E+00	2.5600E+01	8.3000E-01	0.0000E+00
7.2200E+03	1.0000E+00	1.7530E+00	9.12300E+01	8.3000E-01	0.0000E+00
7.9000E+03	1.0000E+00	1.1460E+00	3.1600E+01	8.3000E-01	0.0000E+00
1.2800E+04	2.0000E+00	1.3360E+00	5.0600E+01	8.3000E-01	0.0000E+00
1.3900E+04	2.0000E+00	2.4260E+00	7.7600E+01	1.6500E+00	0.0000E+00
1.8000E+04	1.0000E+00	2.7100E+00	1.0600E+00	1.6500E+00	0.0000E+00
2.1300E+04	1.0000E+00	6.9200E+00	1.9200E+00	5.0000E+00	0.0000E+00

DATA FOR ISOTOPE NUMBER 4

(Z,A) DESIGNATION OF THE ISOTOPE 2.6058E+04 FRACTIONAL ABUNDANCE 3.100E-03 NO OF ENERGY RANGES 1  
 LOWER LIMIT OF THE ENERGY RANGE(EV) 4.7500E+03 UPPER LIMIT(EV) 1.0000E+05 LRU= 1 LRF= 2  
 NUCLEAR SPIN 0.0000E+00 SCATTERING LENGTH 6.0000E-01 NO OF L-VALUES 2 LIS= 0  
 CONSTANT USED TO CALCULATE PENETRABILITY 1.2000E+03 SCATTERING LENGTH(A-) 0.0000E+00 ANGULAR MOMENTUM 0 NO OF RESONANCES 1

ERES	SPIN	GTOT	GN	GGAMMA	GF
-6.0000E+02	5.0000E-01	3.5700E+00	2.5700E+00	1.0000E+00	0.0000E+00

CONSTANT USED TO CALCULATE PENETRABILITY 1.2000E-03 SCATTERING LENGTH(A-) 0.0000E+00 ANGULAR MOMENTUM 1 NO OF RESONANCES 2

ERES	SPIN	GTOT	GN	GGAMMA	GF
2.3000E+02	5.0000E-01	1.0065E+00	6.5400E+03	1.0000E+00	0.0000E+00
3.5900E+02	5.0000E-01	1.0173E+00	1.7300E+02	1.0000E+00	0.0000E+00

CROSS-SECTIONS AT THERMAL ENERGY

NEUTRON ENERGY ( EV)	SIGNN	SIGCAP	SIGF	SIGT	SIGNNMULT	SIGTMULT
2.530000E-02	1.336513E+01	2.523085E+00	0.000000E+00	1.588822E+01	1.137573E+01	1.389682E+01
NEUTRON ENERGY ( EV)	SIGNN	SIGCAP	SIGF	SIGT	SIGNNMULT	SIGTMULT

4,750000E+03	6,785771E+00	5,602725E-01	0,000000E+00	7,346044E+00	5,693696E+00	6,253968E+00
4,981865E+03	6,502255E+00	5,412982E-03	0,000000E+00	6,507667E+00	5,432315E+00	5,437728E+00
5,137500E+03	6,465403E+00	5,973383E-03	0,000000E+00	6,471377E+00	5,410551E+00	5,416524E+00
5,213730E+03	6,460483E+00	6,343325E-03	0,000000E+00	6,466826E+00	5,413359E+00	5,419702E+00
5,525000E+03	6,580239E+00	8,971672E-03	0,000000E+00	6,589210E+00	5,570369E+00	5,579341E+00
5,836270E+03	7,275194E+00	1,643329E-02	0,000000E+00	7,291627E+00	6,323456E+00	6,339890E+00
5,912500E+03	7,693594E+00	2,030699E-02	0,000000E+00	7,713901E+00	6,760468E+00	6,780773E+00
6,068135E+03	9,350730E+00	3,432255E-02	0,000000E+00	9,385053E+00	8,444930E+00	8,479252E+00
6,300000E+03	1,367890E+01	6,217415E-02	0,000000E+00	1,374108E+01	1,253046E+01	1,259264E+01
6,530000E+03	1,153816E+01	3,519009E-02	0,000000E+00	1,157335E+01	1,013255E+01	1,016774E+01
6,531865E+03	1,151748E+01	3,498538E-02	0,000000E+00	1,155247E+01	1,011163E+01	1,014663E+01
6,760000E+03	1,039641E+01	2,128743E-02	0,000000E+00	1,041770E+01	9,013376E+00	9,034663E+00
6,763730E+03	1,039735E+01	2,119639E-02	0,000000E+00	1,041855E+01	9,014939E+00	9,036135E+00
6,990000E+03	1,128880E+01	1,963277E-02	0,000000E+00	1,130843E+01	9,945808E+00	9,965440E+00
7,218247E+03	1,414936E+01	3,261779E-01	0,000000E+00	1,447554E+01	1,287594E+01	1,320212E+01
7,219123E+03	1,466805E+01	7,810764E-01	0,000000E+00	1,544913E+01	1,339505E+01	1,417612E+01
7,220000E+03	1,552657E+01	1,539844E+00	0,000000E+00	1,706642E+01	1,425398E+01	1,579382E+01
7,220876E+03	1,469754E+01	7,810644E-01	0,000000E+00	1,547860E+01	1,342535E+01	1,420642E+01
7,221753E+03	1,420473E+01	3,263050E-01	0,000000E+00	1,453104E+01	1,293296E+01	1,325927E+01
7,228920E+03	1,399226E+01	3,789944E-02	0,000000E+00	1,403016E+01	1,272393E+01	1,276183E+01
7,372500E+03	1,656123E+01	2,761971E-02	0,000000E+00	1,658885E+01	1,538890E+01	1,541652E+01
7,525000E+03	1,999688E+01	3,279241E-02	0,000000E+00	2,000160E+01	1,897588E+01	1,900867E+01
7,677500E+03	2,328673E+01	3,707367E-02	0,000000E+00	2,332380E+01	2,256588E+01	2,260295E+01
7,830000E+03	2,511229E+01	3,806536E-02	0,000000E+00	2,515035E+01	2,470823E+01	2,474630E+01
7,847500E+03	2,517165E+01	3,794436E-02	0,000000E+00	2,520960E+01	2,480225E+01	2,484019E+01
7,865000E+03	2,519768E+01	3,787235E-02	0,000000E+00	2,523555E+01	2,486198E+01	2,489986E+01
7,882500E+03	2,519088E+01	3,846959E-02	0,000000E+00	2,522935E+01	2,488779E+01	2,492626E+01
7,898854E+03	2,523834E+01	2,589722E-01	0,000000E+00	2,549731E+01	2,496461E+01	2,522358E+01
7,899427E+03	2,536322E+01	5,920254E-01	0,000000E+00	2,595524E+01	2,509050E+01	2,568252E+01
7,900000E+03	2,557363E+01	1,147331E+00	0,000000E+00	2,672097E+01	2,530192E+01	2,644925E+01
7,900573E+03	2,536117E+01	5,920071E-01	0,000000E+00	2,595318E+01	2,509046E+01	2,568247E+01
7,901146E+03	2,523234E+01	2,589441E-01	0,000000E+00	2,549129E+01	2,496264E+01	2,522158E+01
8,295000E+03	1,919762E+01	2,253041E-02	0,000000E+00	1,922015E+01	1,923586E+01	1,925839E+01
8,690000E+03	1,335408E+01	1,199169E-02	0,000000E+00	1,336607E+01	1,330078E+01	1,331278E+01
9,085000E+03	1,020244E+01	7,076996E-03	0,000000E+00	1,020951E+01	1,003792E+01	1,004499E+01
9,477960E+03	9,323108E+00	8,350098E-01	0,000000E+00	1,015812E+01	9,083403E+00	9,918413E+00
9,478980E+03	1,061444E+01	2,081131E+00	0,000000E+00	1,269557E+01	1,037469E+01	1,245582E+01
9,480000E+03	1,277854E+01	4,159574E+00	0,000000E+00	1,693811E+01	1,253810E+01	1,669768E+01
9,481020E+03	1,061935E+01	2,081001E+00	0,000000E+00	1,270035E+01	1,037823E+01	1,245924E+01
9,482040E+03	9,318955E+00	8,350569E-01	0,000000E+00	1,015401E+01	9,077790E+00	9,912847E+00
9,910000E+03	7,313152E+00	3,242707E-03	0,000000E+00	7,316394E+00	7,021110E+00	7,024352E+00
1,034000E+04	6,564929E+00	2,419987E-03	0,000000E+00	6,567349E+00	6,241760E+00	6,244180E+00
1,077000E+04	6,031694E+00	1,925410E-03	0,000000E+00	6,033619E+00	5,690138E+00	5,692064E+00
1,119898E+04	5,660840E+00	1,862921E+00	0,000000E+00	7,523761E+00	5,309128E+00	7,172049E+00
1,119949E+04	5,720218E+00	4,654958E+00	0,000000E+00	1,037518E+01	5,368506E+00	1,002346E+01
1,120000E+04	5,830226E+00	9,308277E+00	0,000000E+00	1,513850E+01	5,478464E+00	1,478674E+01
1,120051E+04	5,735508E+00	4,655149E+00	0,000000E+00	1,039066E+01	5,383695E+00	1,003884E+01
1,120102E+04	5,672045E+00	1,863079E+00	0,000000E+00	7,535124E+00	5,320232E+00	7,183311E+00
1,160000E+04	5,320346E+00	1,381587E-03	0,000000E+00	5,321728E+00	4,964007E+00	4,965388E+00
1,200000E+04	5,062646E+00	1,213998E-03	0,000000E+00	5,063860E+00	4,705030E+00	4,706244E+00
1,240000E+04	4,838706E+00	1,098311E-03	0,000000E+00	4,839804E+00	4,482188E+00	4,483286E+00
1,279866E+04	4,802337E+00	2,700907E-01	0,000000E+00	5,072428E+00	4,449188E+00	4,719278E+00
1,279933E+04	5,047677E+00	6,737919E-01	0,000000E+00	5,721469E+00	4,694669E+00	5,368461E+00
1,280000E+04	5,459894E+00	1,346754E+00	0,000000E+00	6,806648E+00	5,106218E+00	6,452972E+00
1,280067E+04	5,051586E+00	6,737859E-01	0,000000E+00	5,725372E+00	4,697238E+00	5,371024E+00
1,280134E+04	4,804717E+00	2,701045E-01	0,000000E+00	5,074822E+00	4,450510E+00	4,720614E+00
1,307500E+04	4,513546E+00	9,679320E-04	0,000000E+00	4,514514E+00	4,162595E+00	4,163563E+00
1,335000E+04	4,394794E+00	9,259876E-04	0,000000E+00	4,395720E+00	4,047085E+00	4,048011E+00









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      IRAY(3,J)=I
      ERAY(1,J)=SPI(I)
      ERAY(2,J)=AP(I)
102  CONTINUE
      J1=J1+NRS
      JL=JL+1
      IF(NMOM-NLS(I,J2))104,104,103
103  N RANGE=N RANGE+1
      J2=J2+1
      IF(N RANGE-NERI)106,106,1010
1010 NRES(I)=J1-JFID
      JFID=J1
101  CONTINUE
      NTOTAL=J1-1
      SCALE=1.0E+00
      PHI=3.14159265
      3  FORMAT(2E11,4,4I11)
      4  FORMAT(6E11,4)
      5  FORMAT(8E11,4,3I10)
      6  FORMAT(2X,2E11,4)
      7  FORMAT(107H NEUTRON ENERGY( EV)      SIGNN      SIGCAP
1IGF      SIGT      SIGNNMULT      SIGTMULT )
      8  FORMAT(2X,7E15,6)
      9  FORMAT(10X,2E20,6)
10   FORMAT(20H ERROR IN INPUT DATA)
11   FORMAT(10X,2I10)
12   FORMAT(10X,6I10)
14   FORMAT(53H CROSS-SECTIONS CALCULATED WITHOUT DOPPLER BROADENING)
15   FORMAT(49H CROSS-SECTIONS CALCULATED WITH DOPPLER BROADENING)
16   FORMAT(15H NEUTRON ENERGYE15,6)
17   FORMAT(33H (Z,A) DESIGNATION OF THE ELEMENTE11,4,22H AT,WT/MASS OF
1  NEUTRONE11,4,15H NO OF ISOTOPES I5)
18   FORMAT(24H DATA FOR ISOTOPE NUMBER I5)
19   FORMAT(33H (Z,A) DESIGNATION OF THE ISOTOPEE11,4,21H FRACTIONAL ABS
1UNDANCEE11,4,20H NO OF ENERGY RANGES I5)
20   FORMAT(36H LOWER LIMIT OF THE ENERGY RANGE(EV)E11,4,18H  UPPER L
1MIT(EV)E11,4,6H  LRU=I5,6H  LRF=I5)
21   FORMAT(13H NUCLEAR SPINE11,4,18H SCATTERING LENGTHE11,4,15H NO OF
1L-VALUES I5)
22   FORMAT(45H MASS OF THE ISOTOPE IN UNITS OF NEUTRON MASSE11,4,22H
1CATTERING LENGTH(A-)E11,4,17H ANGULAR MOMENTUM I5,17H NO OF RESONANS
2CES I5)
23   FORMAT(85H      ERES      SPIN      GTOT      GN
1      GGAMMA      GF )
24   FORMAT(11H TITLE      7A4)
25   FORMAT(//)
26   FORMAT(6(2X,E11,4,2X))
27   FORMAT(33H CROSS-SECTIONS AT THERMAL ENERGY)
28   FORMAT(2X,2E20,6,I10)
29   FORMAT(2X,4E11,4)
30   FORMAT(22H EFFECTIVE TEMPERATUREF7,1,41H  IN DEGREES KELVIN,  NO
10F PIVOT POINTS I5,18H CONVERGENCE ERRORE10,4,13H AND INCROSS=I5)
31   FORMAT(53H THE INTEGRAL FOR DOPPLER BROADENING DID NOT CONVERGE)
33   FORMAT(116H1 PROGRAM SIGMA2, PROGRAM TO CALCULATE SINGLE OR MULTIL
1EVEL BREIT-WIGNER CROSS-SECTIONS. USES ENDF/B VERSION II DATA)
C-----THIS IS WHERE RESONANCES OF EACH ISOTOPE ARE ARRANGED IN INCREASINSIG2176
C-----G ORDER IN L AND FOR EACH L IN INCREASING ORDER IN J,
      DO 133 I=1,NIS
      NRESI=NRES(I)
      CALL ORDER(I,NRESI)
133  CONTINUE

```

13	FORMAT(10(1X,I10))	SIG2182
	DO 135 I=1,NTOTAL	SIG2183
	ARRAY(1,I)=ARRAY(1,I)*SCALE	SIG2184
	ARRAY(3,I)=ARRAY(3,I)*SCALE	SIG2185
	ARRAY(4,I)=ARRAY(4,I)*SCALE	SIG2186
	ARRAY(5,I)=ARRAY(5,I)*SCALE	SIG2187
	ARRAY(6,I)=ARRAY(6,I)*SCALE	SIG2188
135	CONTINUE	SIG2189
	NCOUNT=1	SIG2190
	DO 1330 I=1,NIS	SIG2191
	XWR=AWRI(I)	SIG2192
	YWR=XWR*1.008665	SIG2193
	YWR=YWR**(1.0/3.0)	SIG2194
	APX=0.123*YWR+0.08	SIG2195
	NRESI=NRES(I)	SIG2196
	NLMT=NCOUNT+NRESI-1	SIG2197
	DO 1331 J=NCOUNT,NLMT	SIG2198
	CALL FACTS(ARRAY(1,J),IRAY(1,J),PENFAR(J),SHIFAR(J),PS,CONST,XWR,	SIG2199
	1APX,1.0)	SIG2200
1331	CONTINUE	SIG2201
	NCOUNT=NCOUNT+NRESI	SIG2202
1330	CONTINUE	SIG2203
	DO 108 I=1,NTOTAL	SIG2204
	ERAN(1,I)=ARRAY(1,I)	SIG2205
	ERAN(2,I)=ARRAY(3,I)	SIG2206
108	CONTINUE	SIG2207
	CALL QIKS(1,NTOTAL,MOV,KOM)	SIG2208
C----	HERE RESONANCE IN AN ELEMENT ARE ARRANGED IN INCREASING ORDER IN	SIG2209
C----	ENERGY ALONG WITH THEIR TOTAL GAMMAS TO CALCULATE THE ENERGY MESH	SIG2210
C----	AT WHICH THE CROSS-SECTIONS ARE CALCULATED.	SIG2211
146	PRINT27	SIG2212
	PRINT25	SIG2213
	PRINT7	SIG2214
	E=ETHERM	SIG2215
	CALL SIGMA(ETHERM,1)	SIG2216
	PRINT25	SIG2217
	ELO=EL(1,1)*SCALE	SIG2218
	JFLAG(1)=1	SIG2219
	IRANGE=1	SIG2220
C----	WE HAVE ARBITRARILY SET ELO=1.0E-11 MEV HERE TO BE ABLE TO DOPPLERS	SIG2221
C----	BROADEN THERMAL CROSS-SECTIONS,LATER ON IN THE PROGRAM ELO IS READS	SIG2222
C----	IN FROM THE DATA AND COULD VARY FROM 1.0E-11 TO 1.0E+09MEV,	SIG2223
	PRINT8,ETHERM,(AREF(LL),LL=1,6)	SIG2224
	IF(IDPL.EQ.1)GO TO 147	SIG2225
	GO TO 148	SIG22251
147	TEF=TEFF/293.0	SIG2226
	DELTA=0.3177*SQRT((TEF*ETHERM)/AWR)	SIG2227
C	CONTINUE	SIG2228
	CALL GRID(ETHERM,DELTA,NTAB,XTAB)	SIG2229
	CALL GREAT2(DOPPLER,FINT,XTAB,NTAB,ERROR,IERR)	SIG2230
	PRINT28,ETHERM,FINT,JFLAG(1)	SIG2231
	IF(IERR.EQ.1)PRINT31	SIG2232
148	PRINT25	SIG2233
	PRINT7	SIG2234
	PRINT25	SIG2235
	DO 124 JJ=1,NIS	SIG2236
	NERJJ=NER(JJ)	SIG2237
	DO 125 KK=1,NERJJ	SIG2238
	IRANGE=KK	SIG2239
	LRUJK=LRU(JJ,KK)	SIG2240
	IF(LRUJK=1)131,1321,125	SIG2241

131	PRINT10	SIG2242
	GO TO 130	SIG2243
1321	IF(JJ,EQ,1)GO TO 1320	SIG2244
	GO TO 132	SIG22441
1320	ELOREF=EL(JJ,KK)*SCALE	SIG2245
	EHIREF=EH(JJ,KK)*SCALE	SIG2246
	ELO=ELOREF	SIG2247
	EHI=EHIREF	SIG2248
	GO TO 1240	SIG2249
132	ELO=EL(JJ,KK)*SCALE	SIG2250
	EHI=EH(JJ,KK)*SCALE	SIG2251
	IF(ELO,EQ,ELORFF,AND,EHI,EQ,EHIREF)GO TO 124	SIG2252
	GO TO 1240	SIG22521
1240	MM=MAXPTS/(8*MAXRES)	SIG2253
	NN=MM	SIG2254
	IFLAG=1	SIG2255
	NLSKK=NLS(JJ,KK)	SIG2256
	J4=1	SIG2257
	ISTART=1	SIG2258
	IEND=1	SIG2259
117	IF(IEND.EQ,0)GO TO 125	SIG2260
	J5=J4+1	SIG2261
	E1=ERAN(1,J4)	SIG2262
	G1=ERAN(2,J4)	SIG2263
	E2=ERAN(1,J5)	SIG2264
	G2=ERAN(2,J5)	SIG2265
	IF(E1.LT,ELO,AND,E2.LT,ELO)GO TO 1120	SIG2266
	GO TO 1105	SIG22661
1105	IF(E1.LE,ELO,AND,E2.GT,ELO)GO TO 1110	SIG2267
	GO TO 1111	SIG22671
1110	E1=ELO	SIG2268
	G1=G2	SIG2269
	ISTART=0	SIG2270
	GO TO 1114	SIG2271
1111	IF(E1.GT,ELO,AND,E2.LE,EHI)GO TO 1112	SIG2272
	GO TO 1113	SIG22721
1112	IF(J4.EQ,1,AND,ISTART,EQ,1)GO TO 1106	SIG2273
	GO TO 1114	SIG22731
1106	E2=E1	SIG2274
	G2=G1	SIG2275
	E1=ELO	SIG2276
	J4=J4+1	SIG2277
	ISTART=0	SIG2278
	GO TO 1114	SIG2279
1116	E2=EWI+G1/FLOAT (MM)	SIG2280
	G2=G1	SIG2281
	IFLAG=0	SIG2282
	GO TO 1114	SIG2283
1113	IF(E1.LT,EHI,AND,E2.GE,EHI)GO TO 1123	SIG2284
	GO TO 1124	SIG22841
1123	E2=EWI	SIG2285
	G2=G1	SIG2286
	IEND=0	SIG2287
	GO TO 1114	SIG2288
1124	IF(E1.GE,EHI,AND,E2.GT,EHI)GO TO 125	SIG2289
	GO TO 1125	SIG22891
1125	IF(IFLAG)1120,125,1120	SIG2290
1114	IF(E1,EQ,E2)GO TO 1120	SIG2291
	GO TO 1118	SIG22911
1118	CONTINUE	SIG2292
	CALL SIEVE(E1,G1,E2,G2,MM,NN,NX,TEFF,AWR)	SIG2293

CALL QIKS(1,NX,MOVE,KOME)	SIG2294
GO TO 116	SIG2295
1120 IF(IEND.EQ,0)GO TO 125	SIG2296
J4=J4+1	SIG2297
GO TO 117	SIG2298
116 DO 109 I=1,NX	SIG2299
E=EX(I)	SIG2300
JFLAGI=JFLAG(I)	SIG2301
CALL SIGMA(E,KK)	SIG2302
PRINT8,E,(AREF(LL),LL=1,6)	SIG2303
IF(IDPL.EQ,1)GO TO 141	SIG2304
GO TO 109	SIG2304.1
141 IF(E.LT-ETHERM)GO TO 109	SIG2305
GO TO 1410	SIG2305.1
C-----IF THE NEUTRON ENERGY IS LESS THAN 0,0253 EV DOPPLER BROADENING IS	SIG2306
C-----PASSED AS A DIFFERENT KERNEL SHOULD BE USED TO CALCULATE DOPPLER	SIG2307
C-----BROADENED CROSS-SECTIONS,	SIG2308
1410 TEF=TEFF/293,0	SIG2309
DELTA=0.3177*SQRT ((TEF*E)/AWR)	SIG2310
C CONTINUE	SIG2311
GO TO (1121,1122),JFLAGI	SIG2312
1121 CALL GRID(E,DELTA,NTAB,XTAB)	SIG2313
32 FORMAT(2X,11E11,4)	SIG2314
CALL GREAT2(DOPPLER,FINT,XTAB,NTAB,ERROR,IERR)	SIG2315
PRINT28,E,FINT,JFLAG(I)	SIG2316
IF(IERR.EQ,1)PRINT31	SIG2317
GO TO 109	SIG2318
1122 CALL GAUSS(E,DELTA,DOPE)	SIG2319
PRINT28,E,DOPE,JFLAG(I)	SIG2320
109 CONTINUE	SIG2321
IF(IFLAG)1117,125,1117	SIG2322
1117 J4=J4+1	SIG2323
IF(NTOTAL=J4)125,1250,117	SIG2324
1250 E1=ERAN(1,J4)	SIG2325
G1=ERAN(2,J4)	SIG2326
GO TO 1116	SIG2327
125 CONTINUE	SIG2328
124 CONTINUE	SIG2329
120 CONTINUE	SIG2330
130 CALL EXIT	SIG2331
END	SIG2332
SUBROUTINE QIKS (MM,NN,MOVE,COMPAR)	QIKS0010
CQIKS ALL-IN-MEMORY SORT PROGRAM	QIKS0020
C MM = FIRST SUBSCRIPT	QIKS0030
C NN = LAST SUBSCRIPT (ARRAY IS IN COMMON)	QIKS0040
C MOVE AND COMPAR ARE USER SUPPLIED PROGRAMS	QIKS0050
DIMENSION MSAVE(20),NSAVE(20)	QIKS0060
KEYLOC(M,N)=(N+M)/2	QIKS0070
I=0	QIKS0080
J=0	QIKS0090
LEVEL = 0	QIKS0100
M=MM	QIKS0110
N=NN	QIKS0120
35 CONTINUE	QIKS0130
C TEST FOR ONE OR TWO ITEMS	QIKS0140
IF(N-M=1) 31,51,32	QIKS0150
C 32 CONTINUE	QIKS0160
C PARTITION AND SPREADER GO HERE, SEE BELOW, RETURN IS TO 8	QIKS0170
C PUSH DOWN	QIKS0180
8 LEVEL=LEVEL+1	QIKS0190
C WORK ON SMALLEST PORTION	QIKS0200

```

NSAVE(LEVEL)=N
N=J
GO TO 35
34 MSAVE(LEVEL)=M
NSAVE(LEVEL)=J
M=1
GO TO 35
51 IF(COMP(M,N))31,31,131
SWAP IF ONLY TWO ITEMS ARE OUT OF ORDER
131 CALL MOVE(M,0)
CALL MOVE(N,M)
31 IF(LEVEL) 151, 150, 151
150 RETURN
C
151 M = MSAVE(LEVEL)
NSAVE(LEVEL)
LEVEL=LEVEL+1
GO TO 35
C
END MAIN
PARTITION
32 I=M
J=N
KEY=KEYLOC(M,N)
CALL MOVE(KEY, 0)
54 IF (N - KEY) 17, 1, 17
17 CALL MOVE(N,KEY)
1 CONTINUE
HOLE AT BOTTOM
IF(COMP(0,1))3,2,2
2 I=I+1
IF (I - J) 1, 4, 1
3 CALL MOVE(I,J)
GO TO 5
6 CONTINUE
HOLE AT TOP
IF(COMP(0,J))5,5,7
5 J=J-1
IF (I - J) 6, 4, 6
7 CALL MOVE(J,I)
GO TO 2
4 CONTINUE
SPREADER GOES HERE
END PARTITION
C
SPREADER
4 CALL MOVE(0,I)
12 IF (I - N) 110, 10, 110
110 I = I + 1
IF(COMP(0,1))10,12,10
10 IF (J - M) 108, 8, 108
108 J = J - 1
IF(COMP(0,J))8,10,8
8 CONTINUE
RETURN TO MAIN PROGRAM
C
END
SUBROUTINE MOV(I,J)
COMMON/D/ERAN(2,501)
I=I
J1=J

```

```

01KS0240
01KS0240
01KS0250
01KS0260
01KS0270
01KS0280
01KS0290
01KS0300
01KS0310
01KS0320
01KS0330
01KS0340
01KS0350
01KS0360
01KS0370
01KS0380
01KS0390
01KS0400
01KS0410
01KS0420
01KS0430
01KS0440
01KS0450
01KS0460
01KS0470
01KS0480
01KS0490
01KS0500
01KS0510
01KS0520
01KS0530
01KS0540
01KS0550
01KS0560
01KS0570
01KS0580
01KS0590
01KS0600
01KS0610
01KS0620
01KS0630
01KS0640
01KS0650
01KS0660
01KS0670
01KS0680
01KS0690
01KS0700
01KS0710
01KS0720
01KS0730
01KS0740
01KS0750
01KS0760
01KS0770
MOV 001
MOV 002
MOV 003
MOV 004

```



```

IF(I1.EQ,0)I1=501
IF(J1.EQ,0)J1=501
ERAN(1,J1)=ERAN(1,I1)
ERAN(2,J1)=ERAN(2,I1)
RETURN
END
SUBROUTINE MOVE(I,J)
COMMON/C/EX(101),JFLAG(101)
I1=I
J1=J
IF(I1.EQ,0)I1=101
IF(J1.EQ,0)J1=101
EX(J1)=EX(I1)
JFLAG(J1)=JFLAG(I1)
RETURN
END
FUNCTION KOM(I,J)
COMMON/D/ERAN(2,501)
I1=I
J1=J
IF(I1.EQ,0)I1=501
IF(J1.EQ,0)J1=501
EOM=ERAN(1,I1)-ERAN(1,J1)
IF(EOM)100,101,102
100 KOM=-1
GO TO 103
101 KOM=0
GO TO 103
102 KOM=1
103 RETURN
END
FUNCTION KOME(I,J)
COMMON/C/EX(101),JFLAG(101)
I1=I
J1=J
IF(I1.EQ,0)I1=101
IF(J1.EQ,0)J1=101
EOX=EX(I1)-EX(J1)
IF(EOX)100,101,102
100 KOME=-1
GO TO 103
101 KOME=0
GO TO 103
102 KOME=1
103 RETURN
END
SUBROUTINE SPINOR(S,L,XJ)
TERM=0,0
DENOM=0,0
IF(S,EQ,0,AND,L,EQ,0)GO TO 100
GO TO 101
C-----FOR S=0 AND S-WAVE RESONANCES SPINS ARE ALL KNOWN HENCE ONE NEEDS
C-----LEVEL-LEVEL INTERFERENCE,
101 IF(S,EQ,0,)GO TO 102
GO TO 103
102 XJ=FLOAT(L)
GO TO 110
103 XJ1=S+0.5
XJ2=S-0.5
111 XL=FLOAT(L)
IF(XJ1,GT,XL)GO TO 104
MOV 005
MOV 006
MOV 007
MOV 008
MOV 009
MOV 010
MOVE001
MOVE002
MOVE003
MOVE004
MOVE005
MOVE006
MOVE007
MOVE008
MOVE009
MOVE010
KOM 001
KOM 002
KOM 003
KOM 004
KOM 005
KOM 006
KOM 007
KOM 008
KOM 009
KOM 010
KOM 011
KOM 012
KOM 013
KOM 014
KOM 015
KOME001
KOME002
KOME003
KOME004
KOME005
KOME006
KOME007
KOME008
KOME009
KOME010
KOME011
KOME012
KOME013
KOME014
KOME015
SPNR001
SPNR002
SPNR003
SPNR004
SPNR0041
SPNR005
SPNR006
SPNR007
SPNR0071
SPNR008
SPNR009
SPNR010
SPNR011
SPNR012
SPNR013

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GO TO 105
104 TERM=TERM+XJ1*(2.0*XL+1.0)
DENOM=DENOM+(2.0*XL+1.0)
GO TO 106
105 TERM=TERM+XL*(2.0*XJ1+1.0)
DENOM=DENOM+(2.0*XJ1+1.0)
106 IF(XJ2.GT.XL)GO TO 107
GO TO 108
107 TERM=TERM+XJ2*(2.0*XL+1.0)
DENOM=DENOM+(2.0*XL+1.0)
GO TO 109
108 TERM=TERM+XL*(2.0*XJ2+1.0)
DENOM=DENOM+(2.0*XJ2+1.0)
109 XJ=TERM/DENOM
GO TO 110
100 XJ=0.0
110 RETURN
END
SUBROUTINE GREAT2(F,FINT,XTAB,NTAB,ERROR,IERR)
C-----CARRY OUT CONVERGENCE INTEGRATION SCHEME USING UP TO 200 INTERVALS
C-----WHICH ARE THEN FURTHER SUBDIVIDED UNTIL CONVERGENCE OCCURS OR THE
C-----MAXIMUM ALLOWABLE NUMBER OF ITERATIONS IS EXCEEDED, THE SUBROUTINE
C-----ARGUMENTS ARE DEFINED AS FOLLOWS.....
C-----F =FUNCTION TO BE INTEGRATED.
C-----FINT =THE RESULTING INTEGRAL
C-----XTAB =TABLE OF ORDINATES (INTEGRATION INTERVAL IS FROM XTAB(1) TO
C-----XTAB(NTAB))
C-----NTAB =THE LENGTH OF THE XTAB TABLE (NUMBER OF ORDINATES).
C-----ERROR =ALLOWABLE NORMAL ERROR.
C-----IERR =ERROR INDICATOR SET TO ZERO IF METHOD CONVERGES, SET TO
C-----ONE IF METHOD DOES NOT CONVERGE,
C-----ONE IF METHOD DOES NOT CONVERGE OR TABLE (XTAB) IS TOO LONG
DIMENSION XTAB(33),PARTS(33),GOOF(33),INTER(33)
C-----DEFINE THE MAXIMUM ALLOWABLE NUMBER OF ITERATIONS AND THE MAXIMUM
C-----TABLE LENGTH,
DATA JMAX,NTABMX/20,1000/
C-----DETERMINE IF TABLE IS TOO LONG
IF(NTAB.GT.NTABMX) GO TO 100
C-----CALL GENERAL INTEGRATION SUBROUTINE.
ZZZ=F(5.0)
CALL GREAT1(F,FINT,NTAB,JMAX,XTAB,PARTS,GOOF,INTER,ERROR,IERR)
RETURN
C-----TABLE IS TOO LONG.
100 IERR=1
FINT=0.0
RETURN
END
SUBROUTINE GREAT1(F,FINT,NTAB,JMAX,XTAB,PARTS,GOOF,INTER,ERROR,
1 IERR)
C-----CARRY OUT CONVERGENCE INTEGRATION SCHEME USING TRAPAZOIDAL RULE
C-----AND DOUBLING THE NUMBER OF REGIONS PER SUBINTERVAL FOR EACH
C-----ITERATION, ONLY DOUBLE UP IN THOSE INTERVALS THAT HAVE NOT ALREADY
C-----CONVERGED,
C-----F =SINGLE PRECISION FUNCTION TO BE INTEGRATED
C-----FINT =THE RESULTING INTEGRAL
C-----NTAB =NUMBER OF ORDINATES SUPPLIED (THERE ARE N-1 INTERVALS)
C-----JMAX =MAXIMUM ALLOWABLE NUMBER OF ITERATIONS
C-----XTAB =TABLE OF THE ORDINATE VALUES, RANGE OF INTEGRATION IS
C-----FROM XTAB(1) TO XTAB(NTAB)
C-----PARTS =ARRAY OF DIMENSION NTAB, EQUAL TO THE PARTIAL INTEGRALS
C-----OVER EACH OF THE NTAB-1 INTERVALS

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SPNR0131
SPNR014
SPNR015
SPNR016
SPNR017
SPNR018
SPNR019
SPNR0191
SPNR021
SPNR022
SPNR023
SPNR024
SPNR025
SPNR026
SPNR027
SPNR028
SPNR029
GRT2001
GRT2002
GRT2003
GRT2004
GRT2005
GRT2006
GRT2007
GRT2008
GRT2009
GRT2010
GRT2011
GRT2012
GRT2013
GRT2014
GRT2015
GRT2016
GRT2017
GRT2018
GRT2019
GRT2020
GRT2021
GRT20211
GRT2022
GRT2023
GRT2024
GRT2025
GRT2026
GRT2027
GRT2028
GRT1001
GRT1002
GRT1003
GRT1004
GRT1005
GRT1006
GRT1007
GRT1008
GRT1009
GRT1010
GRT1011
GRT1012
GRT1013
GRT1014

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C-----GOOF  =ARRAY OF DIMENSION NTAB, EQUAL TO THE NORMAL ERROR IN EACH GRT1015
C-----      OF THE NTAB-1 INTERVAL. GRT1016
C-----INTER =ARRAY OF DIMENSION NTAB, SEPECIFYING THE NUMBER OF GRT1017
C-----      SUBINTERVALS IN EACH INTERVAL GRT1018
C-----ERROR  =ACCEPTABLE NORMAL ERROR GRT1019
C-----IERR   =ERROR INDICATOR, SET TO ZERO IF METHOD CONVERGES, SET TO GRT1020
C-----      ONE IF METHOD DOES NOT CONVERGE GRT1021
C-----      DIMENSION XTAB(NTAB),PARTS(NTAB),INTER(NTAB),GOOF(NTAB) GRT1022
C-----INITIALIZE VALUE OF THE INTEGRAL GRT1023
C-----      FINT=0.0 GRT1024
C-----CALCULATE THE NUMBER OF INTERVALS GRT1025
C-----      NM1=NTAB-1 GRT1026
C-----CALCULATE ALLOWABLE ERROR PER INTERVAL GRT1027
C-----      ERRN=ERROR/FLOAT(NM1) GRT1028
C-----INITIALIZE APPROXIMATION TO INTEGRAL GRT1029
C-----      TOTAL=0.0 GRT1030
C-----CALCULATE INITIAL APPROXIMATION GRT1031
C-----      DO 10 I=1,NM1 GRT1032
C-----          INTER(I)=1 GRT1033
C-----          PARTS(I)=0.5*(XTAB(I+1)-XTAB(I))*(F(XTAB(I+1))+F(XTAB(I))) GRT1034
C-----          10 TOTAL=TOTAL+PARTS(I) GRT1035
C-----CALCULATE INITIAL ERRORS GRT1036
C-----      DO 15 I=1,NM1 GRT1037
C-----          15 GOOF(I)=PARTS(I) GRT1038
C-----SET UP LOOP OVER ITERATIONS GRT1039
C-----      DO 100 J=1,JMAX GRT1040
C-----      SAVE LAST APPROXIMATION GRT1041
C-----          TOTAL1=TOTAL GRT1042
C-----      SET UP LOOP OVER INTERVALS GRT1043
C-----          DO 20 I=1,NM1 GRT1044
C-----          CHECK FOR CONVERGENCE IN THIS INTERVAL GRT1045
C-----          IF(ABS(GOOF(I)/TOTAL),LT,ERRN) GO TO 20 GRT1046
C-----          CALCULATE DOUBLE INTERVAL GRT1047
C-----          DX=(XTAB(I+1)-XTAB(I))/FLOAT(INTER(I)) GRT1048
C-----          DOUBLE NUMBER OF STEPS GRT1049
C-----          INTER(I)=2*INTER(I) GRT1050
C-----          INITIALIZE CONTRIBUTION TO INTEGRAL GRT1051
C-----          REST=0.0 GRT1052
C-----          II=INTER(I) GRT1053
C-----          INITIALIZE ORDINATE GRT1054
C-----          XNOW=XTAB(I)+0.5*DX GRT1055
C-----          SET UP LOOP OVER ORDINATES GRT1056
C-----          DO 30 K=1,II,2 GRT1057
C-----              REST=REST+F(XNOW) GRT1058
C-----              30 XNOW=XNOW+DX GRT1059
C-----          CALCULATE NEXT PARTIAL INTEGRAL GRT1060
C-----          REST=0.5*(PARTS(I)+DX*REST) GRT1061
C-----          ADD NEW PARTIAL INTEGRAL AND SUBTRACT OLD PARTIAL INTEGRAL GRT1062
C-----          TOTAL=TOTAL+REST-PARTS(I) GRT1063
C-----          CALCULATE NEW ERROR AND SET PARTIAL INTEGRAL TO NEW VALUE GRT1064
C-----          GOOF(I)=REST-PARTS(I) GRT1065
C-----          PARTS(I)=REST GRT1066
C-----          20 CONTINUE GRT1067
C-----          CHECK FOR CONVERGENCE GRT1068
C-----          100 IF(ABS(1.-TOTAL1/TOTAL),LE,ERROR) GO TO 200 GRT1069
C-----          THE METHOD HAS NOT CONVERGED GRT1070
C-----          FINT=TOTAL GRT1071
C-----          IERR=1 GRT1072
C-----          RETURN GRT1073
C-----          THE METHOD HAS CONVERGED GRT1074
C-----          200 FINT=TOTAL GRT1075

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IERR=0
RETURN
END
SUBROUTINE GRID(Q,BELTA,NTAB,XTAB)
COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU,LRF,LANG,NLS,
1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,AWRI,AM,DREF,AREF,BREF,IRANGE,NIS,
3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR
DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),
1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),
2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),
3SHIFAR(500),SPI(10),AP(10),AWRI(10),AM(10),DREF(6),AREF(6),BREF(6,
410)
DIMENSION XTAB(33)
IGNORE=1
N2=NTAB/2
N21=N2+1
N22=N2+2
N3=NTAB-1
XTAB(N21)=Q
DO 1410 I=N22,NTAB
XTAB(I)=XTAB(I-1)+BELTA
II=NTAB+1=I
XTAB(II)=XTAB(II+1)-BELTA
1410 CONTINUE
DO 1411 I=1,NTAB
XTAB I=XTAB(I)
IF(XTAB I)1412,1412,1411
1412 IGNORE=0
1411 CONTINUE
IF(IGNORE,EQ,0)GO TO 1413
GO TO 1414
1413 XTAB(1)=1,0E=03
DO 1415 I=1,N3
I1=I+1
XTAB(I1)=XTAB(1)+FLOAT(I)*BELTA
1415 CONTINUE
1414 RETURN
END
SUBROUTINE GAUSS(Q,BELTA,DOPE)
COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU,LRF,LANG,NLS,
1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,AWRI,AM,DREF,AREF,BREF,IRANGE,NIS,
3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR
DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),
1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),
2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),
3SHIFAR(500),SPI(10),AP(10),AWRI(10),AM(10),DREF(6),AREF(6),BREF(6,
410)
DIMENSION ABC(9),WET(9)
DATA ABC/=3,19099320178153,=2,26658058453184,=1,46855328921667,=0,GAUS011
172355101875284,0,0,0,72355101875284,1,46855328921667,2,26658058453GAUS012
2184,3,19099320178153/
DATA WET/0,3960697726326E-04,0,4943624275537E-02,0,8847452739438E-
101,0,4326515570026E+00,0,7202352156061E+00,0,4326515570026E+00,0,8GAUS015
2847452739438E-01,0,4943624275537E-02,0,5960697726326E-04/
DATA PHIRT/1,772454/
TEF=TEFF/293,0
TERM=0,0
DO 200 K=1,NIS
T1=0,0
XWR=AWRI(K)
BELTA=(0,3177E+00)*SQRT((Q*TEF)/XWR)

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	X=BELTA*ABC(9)	GAUS024
	IF(E-X)100,100,101	GAUS025
101	DO 102 I=1,9	GAUS026
	ABCI=ABC(I)	GAUS027
	WETI=WET(I)	GAUS028
	Z=E+ABCI*BELTA	GAUS029
	CALL SIGMA(Z,IRANGE)	GAUS030
	T1=T1+BREF(INCROSS,K)*WETI	GAUS031
102	CONTINUE	GAUS032
	GO TO 110	GAUS033
100	T1=0,0	GAUS034
110	TERM=TERM+T1	GAUS035
200	CONTINUE	GAUS036
	DOPE=TERM/PHIRT	GAUS037
	RETURN	GAUS038
	END	GAUS039
	SUBROUTINE FACTS(Q,L,PF,SF,PS,CONSTE,BWR,BP,PL0D)	FACT001
C		FACT002
C	SUBROUTINE TO CALCULATE PENETRATION AND	FACT003
C	SHIFT FACTORS	FACT004
C	Q IS THE ENERGY L IS THE ANGULAR MOMENTUM PF PENETRATION FACTOR	FACT005
C	SF THE SHIFT FACTOR AND PS THE PHASE SHIFT AP IS R CONSTE IS KM	FACT006
C	FOR DETAILS OF FORMULAE SEE GREGSON ET AL AEEW-M517(MLBW)1965	FACT007
C		FACT008
	DATA WNEUT/1,008665/	FACT009
	EAB=ABS(Q)	FACT010
	CONHLD=2.196771E-03*BWR*SQRT(EAB)	FACT011
	CONSTE=CONHLD/(BWR+1,0)	FACT012
C---=	SINCE AWR IS GIVEN WITH THE NEUTRON MASS AS UNITY WE ADD ONE ABOVE	FACT013
C---=	TO CONVERT TO THE CENTER-OF-MASS SYSTEM	FACT014
	ROE=BP*CONSTE	FACT015
	S=FLOAT(L)	FACT016
	IF(L,LE,0)GO TO 100	FACT017
	GO TO(110,120,130,140,150),L	FACT018
100	PF=ROE	FACT019
	SF=0,0	FACT020
	IF(PL0D-LT,2,0) GO TO 160	FACT021
	PS=ROE	FACT022
	GO TO 170	FACT023
110	ROE2=ROE*ROE	FACT024
	DENOM=1.0+ROE2	FACT025
	PF=ROE2*ROE/DENOM	FACT026
	SF=-1.0/DENOM	FACT027
	IF(PL0D-LT,2,0) GO TO 160	FACT028
	PS=ROE-ATAN(ROE)	FACT029
	IF(PS/ROE-0,000001)160,170,170	FACT030
120	ROE2=ROE*ROE	FACT031
	ROE4=ROE2*ROE2	FACT032
	DENOM=3.0*ROE2+ROE4+9,0	FACT033
	PF=ROE4*ROE/DENOM	FACT034
	SF=- (18.0+3.0*ROE2)/DENOM	FACT035
	IF(PL0D-LT,2,0) GO TO 160	FACT036
	PS=ROE-ATAN(3.0*ROE/(3.0+ROE2))	FACT037
	IF(PS/ROE-0,000001)160,170,170	FACT038
130	ROE2=ROE*ROE	FACT039
	ROE4=ROE2*ROE2	FACT040
	ROE6=ROE4*ROE2	FACT041
	DENOM=225,0+45,0*ROE2+6,0*ROE4+ROE6	FACT042
	PF=ROE6*ROE/DENOM	FACT043
	SF=- (675,0+90,0*ROE2+6,0*ROE4)/DENOM	FACT044
	IF(PL0D-LT,2,0) GO TO 160	FACT045

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      PS=ROE-ATAN ((15,0*ROE-ROE2*ROE)/(15,0-6,0*ROE2))
      IF(PS/ROE<0,000001)160,170,170
140  ROE2=ROE*ROE
      ROE4=ROE2*ROE2
      ROE6=ROE4*ROE2
      ROE8=ROE4*ROE4
      DENOM=11025,0+1575,0*ROE2+135,0*ROE4+10,0*ROE6+ROE8
      PF=ROE8*ROE/DENOM
      IF(PLDD.LT,2,0) GO TO 160
      SF=-{44100,0+4725,0*ROE2+270,0*ROE4+10,0*ROE6)/DENOM
      PS=ROE-ATAN ((105,0*ROE-10,0*ROE2*ROE)/(105,0-45,0
1*ROE2+ROE4))
      IF(PS/ROE<0,000001)160,170,170
150  ROE2=ROE*ROE
      ROE4=ROE2*ROE2
      ROE6=ROE4*ROE2
      ROE8=ROE4*ROE4
      ROE10=ROE6*ROE4
      DENOM=893025,0+99225,0*ROE2+6300,0*ROE4+315,0*ROE6
1+15,0*ROE8+ROE10
      PF=ROE10*ROE/DENOM
      SF=4465125,0+396900,0*ROE2+18900,0*ROE4
1+630,0*ROE6+15,0*ROE8
      SF=-SF/DENOM
      IF(PLDD.LT,2,0) GO TO 160
      PS=ROE-ATAN ((945,0*ROE=ROE*(105,0*ROE2-ROE4))/(945,0-420,0*ROE2+
115,0*ROE4))
      IF(PS/ROE.GE,0,000001) GO TO 170
160  PS=0,0
170  RETURN
      END
      SUBROUTINE ORDER(K,N1)
      COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LEW,EL,EH,LRU,LEF,LANG,NLS,
1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,AWRI,AM,DREF,AREF,BREF,IRANGE,NIS,
3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR
      DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),
1ABN(10),NER(10),LEW(10),EL(10,10),EH(10,10),LRU(10,10),LEF(10,10),
2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),
3SHIFAR(500),SPI(10),AP(10),AWRI(10),AM(10),DREF(6),AREF(6),BREF(6,
410)
      IF(K-1)2,2,3
2  NTR=0
      NUML=0
      NUMJ=0
      NN=0
      MM=0
      JJ=0
      NC=0
      MC=0
3  NT=NTR+1
      NTR=NTR+N1
      OL=-0,9
8  OL=OL+1-0
      DO 101 N=NT,NTR
      TERM=FLOAT (IRAY(1,N))
      IF(OL-TERM)101,101,9
9  NN=NN+1
      DO 100J=1,6
      A=ARAY(J,N)
      ARAY(J,N)=ARAY(J,NN)
      ARAY(J,NN)=A

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FACT046
FACT047
FACT048
FACT049
FACT050
FACT051
FACT052
FACT053
FACT054
FACT055
FACT056
FACT057
FACT058
FACT059
FACT060
FACT061
FACT062
FACT063
FACT064
FACT065
FACT066
FACT067
FACT068
FACT069
FACT070
FACT071
FACT072
FACT073
FACT074
FACT075
FACT076
ORDR001
ORDR002
ORDR003
ORDR004
ORDR005
ORDR006
ORDR007
ORDR008
ORDR009
ORDR010
ORDR011
ORDR012
ORDR013
ORDR014
ORDR015
ORDR016
ORDR017
ORDR018
ORDR019
ORDR020
ORDR021
ORDR022
ORDR023
ORDR024
ORDR025
ORDR026
ORDR027
ORDR028
ORDR029
ORDR030

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100	CONTINUE	ORDR031
	DO 1001 J=1,3	ORDR032
	IA=IRAY(J,N)	ORDR033
	IRAY(J,N)=IRAY(J,NN)	ORDR034
	IRAY(J,NN)=IA	ORDR035
1001	CONTINUE	ORDR036
	DO 1002 J=1,2	ORDR037
	EA=ERAY(J,N)	ORDR038
	ERAY(J,N)=ERAY(J,NN)	ORDR039
	ERAY(J,NN)=EA	ORDR040
1002	CONTINUE	ORDR041
101	CONTINUE	ORDR042
	IF(NN=NC)8,8,11	ORDR043
11	NUML=NUML+1	ORDR044
	LN(NUML)=NN=NC	ORDR045
	NC=NN	ORDR046
	NU=NT+LN(NUML)-1	ORDR047
	OM=0.25	ORDR048
14	OM=OM+0.5	ORDR049
	DO 205 M=NT,NU	ORDR050
	TERMJ=ARAY(2,M)	ORDR051
	IF(OM=TERMJ)205,205,15	ORDR052
15	MM=MM+1	ORDR053
	DO 204 J=1,6	ORDR054
	A=ARAY(J,M)	ORDR055
	ARAY(J,M)=ARAY(J,MM)	ORDR056
	ARAY(J,MM)=A	ORDR057
204	CONTINUE	ORDR058
	DO 2041 J=1,3	ORDR059
	IA=IRAY(J,M)	ORDR060
	IRAY(J,M)=IRAY(J,MM)	ORDR061
	IRAY(J,MM)=IA	ORDR062
2041	CONTINUE	ORDR063
	DO 2042 J=1,2	ORDR064
	EA=ERAY(J,M)	ORDR065
	ERAY(J,M)=ERAY(J,MM)	ORDR066
	ERAY(J,MM)=EA	ORDR067
2042	CONTINUE	ORDR068
205	CONTINUE	ORDR069
	IF(MM=MC)14,14,16	ORDR070
16	NUMJ=NUMJ+1	ORDR071
	JN(NUMJ)=MM=MC	ORDR072
	MC=MM	ORDR073
	NT=NT+JN(NUMJ)	ORDR074
	IF(NN=MM)17,17,14	ORDR075
17	IF(NTR=NN)18,18,8	ORDR076
18	RETURN	ORDR077
	END	ORDR078
	FUNCTION DOPPLER(X)	DOPL001
	COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU,LRF,LANG,NLS,	DOPL002
	1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,AWRI,AM,DREF,AREF,BREF,IRANGE,NIS,	DOPL003
	3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR	DOPL004
	DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),	DOPL005
	1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),	DOPL006
	2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),	DOPL007
	3SHIFAR(500),SPI(10),AP(10),AWRI(10),AM(10),DREF(6),AREF(6),BREF(6,	DOPL008
	410)	DOPL009
	TEF=TEFF/293,0	DOPL010
	TERM=0,0	DOPL011
	CALL SIGMA(X,IRANGE)	DOPL012
	DO 100 I=1,NIS	DOPL013

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XWR=AWRI(I)
CELTA=(0,3177E+00)*SQRT((TEF*E)/XWR)
Z=(E-X)/CELTA
Z2=Z*Z
T1=BREF(INCROSS,I)*EXP(-Z2)/(CELTA*1,772454)
TERM=TERM+T1
100 CONTINUE
DOPPLER=TERM
RETURN
END
SUBROUTINE SIGMA(Q,KK)
COMMON/E/XMIN(6),XMAX(6),XREF(6)
COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU, LRF,LANG,NLS,
1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,AWRI,AM,DREF,AREF,BREF,IRANGE,NIS,
3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR
DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),
1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),
2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),
3SHIFAR(500),SPI(10),AP(10),AWRI(10),AM(10),DREF(6),AREF(6),BREF(6,
410)
PI=3,14159265359
DO 4 J=1,6
AREF(J)=0,0
DO 5 K=1,10
BREF(J,K)=0,0
5 CONTINUE
4 CONTINUE
TERROR=1,0E-03
L2=0
N2=0
LA=0
JA=0
NTR=0
DO 112 I=1,NIS
NRESI=NRES(I)
API=AP(I)
XWR=AWRI(I)
YWR=XWR*1,008665
YWR=YWR*(1,0/3,0)
APX=0,123*YWR+0,08
3 NTR=NTR+NRESI
IF(NRESI)110,110,100
100 LA=LA+1
102 L2=L2+LN(LA)
CALL FACTS(Q,IRAY(1,L2),PF,SF,PX,CONSTE,XWR,APX,3,0)
CALL FACTS(Q,IRAY(1,L2),PX,SX,PS,CONSTE,XWR,API,3,0)
SNGLN=0,0
SNGLG=0,0
SNGLF=0,0
SNNL2=0,0
103 JA=JA+1
104 N1=N2+1
N2=N2+JN(JA)
GJ=2,0*(2,0*SPI(I)+1,0)
GJ=(2,0*ARAY(2,N1)+1,0)/GJ
X=1,0
SPIN=ARAY(2,N1)
SPII=SPI(I)
CALL SPINOR(SPII,IRAY(1,L2),XSPIN)
ABDIF=ABS(XSPIN-SPIN)
IF(IVSPIN,EQ,1)GO TO 115
DOPL014
DOPL015
DOPL016
DOPL017
DOPL018
DOPL019
DOPL020
DOPL021
DOPL022
DOPL023
SIGM001
SIGM002
SIGM003
SIGM004
SIGM005
SIGM006
SIGM007
SIGM008
SIGM009
SIGM010
SIGM011
SIGM012
SIGM013
SIGM014
SIGM015
SIGM016
SIGM017
SIGM018
SIGM019
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SIGM027
SIGM028
SIGM029
SIGM030
SIGM031
SIGM032
SIGM033
SIGM034
SIGM035
SIGM036
SIGM037
SIGM038
SIGM039
SIGM040
SIGM041
SIGM042
SIGM043
SIGM044
SIGM045
SIGM046
SIGM047
SIGM048
SIGM049
SIGM050
SIGM051

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GO TO 116	SIGM0511
116 IF(ABDIF,LT,TERROR)GO TO 117	SIGM0512
GO TO 115	SIGM0521
117 X=0.0	SIGM053
115 SNNK23=0.0	SIGM054
DO 108 K=N1,N2	SIGM055
GNK=PF*ARAY(4,K)/PENFAR(K)	SIGM056
GK=GNK+ARAY(5,K)+ARAY(6,K)	SIGM057
ERDK=ARAY(1,K)+((SHIFAR(K)-SF)*ARAY(4,K))/(2.0*PENFAR(K))	SIGM058
ED=Q-ERDK	SIGM059
DK=ED*ED+0.25*GK*GK	SIGM060
SNNK2=GNK*GNK*COS(2.0*PS)	SIGM061
SNNK2=SNNK2+2.0*GNK*(ARAY(5,K)+ARAY(6,K))*SIN(PS)*SIN(PS)	SIGM062
SNNK2=SNNK2+2.0*GNK*ED*SIN(2.0*PS)	SIGM063
SNNK2=SNNK2/DK	SIGM064
SNGK=GNK*ARAY(5,K)/DK	SIGM065
SNFK=GNK*ARAY(6,K)/DK	SIGM066
SNGLN=SNGLN+SNNK2*GJ	SIGM067
SNGLG=SNGLG+SNGK*GJ	SIGM068
SNGLF=SNGLF+SNFK*GJ	SIGM069
SNNK3=0.0	SIGM070
IF(K=N1)107,107,105	SIGM071
105 M1=K-1	SIGM072
DO 106 M=N1,M1	SIGM073
GNM=PF*ARAY(4,M)/PENFAR(M)	SIGM074
GM=GNM+ARAY(5,M)+ARAY(6,M)	SIGM075
ERDM=ARAY(1,M)+((SHIFAR(M)-SF)*ARAY(4,M))/(2.0*PENFAR(M))	SIGM076
EDD=Q-ERDM	SIGM077
DM=EDD*EDD+0.25*GM*GM	SIGM078
SNNM3=ED*EDD+0.25*GK*GM	SIGM079
SNNM3=SNNM3+2.0*GNK*GNM/(DM*DK)	SIGM080
SNNK3=SNNK3+SNNM3	SIGM081
106 CONTINUE	SIGM082
107 CONTINUE	SIGM083
SNNK23=SNNK23+SNNK2+SNNK3*X	SIGM084
108 CONTINUE	SIGM085
SNNL2=SNNL2+SNNK23*GJ	SIGM086
IF(L2=N2)109,109,103	SIGM087
109 BETA=PI*ABN(I)/(CONSTE*CONSTE)	SIGM088
AREF(1)=AREF(1)+SNGLN*BETA	SIGM089
AREF(2)=AREF(2)+SNGLG*BETA	SIGM090
AREF(3)=AREF(3)+SNGLF*BETA	SIGM091
AREF(4)=AREF(4)+BETA*(SNGLN+SNGLG+SNGLF)	SIGM092
AREF(5)=AREF(5)+SNNL2*BETA	SIGM093
AREF(6)=AREF(6)+BETA*(SNGLG+SNGLF+SNNL2)	SIGM094
BREF(1,I)=SNGLN*BETA+BREF(1,I)	SIGM095
BREF(2,I)=SNGLG*BETA+BREF(2,I)	SIGM096
BREF(3,I)=SNGLF*BETA+BREF(3,I)	SIGM097
BREF(4,I)=BETA*(SNGLN+SNGLG+SNGLF)+BREF(4,I)	SIGM098
BREF(5,I)=SNNL2*BETA+BREF(5,I)	SIGM099
BREF(6,I)=BETA*(SNGLG+SNGLF+SNNL2)+BREF(6,I)	SIGM110
IF(L2=NTR)110,110,110	SIGM111
110 SIGP=0.0	SIGM112
LRUJK=LRU(I,KK)	SIGM113
IF(LRUJK=1)1250,1250,125	SIGM114
1250 NLSKK=NLS(I,KK)	SIGM115
DO 126 LL=1,NLSKK	SIGM116
LURE=LANG(I,KK,LL)	SIGM117
SS=FLOAT(LURE)	SIGM118
CALL FACTS(Q,LURE,PF,SF,PS,CONSTA,XWR,API,3,0)	SIGM119
TRM=(2.0*SS+1.0)*4.0*PI	SIGM120

	TRM=TRM*SIN(PS)*SIN(PS)/(CONSTA*CONSTA)	SIGM121
	SIGP=SIGP+TRM	SIGM122
126	CONTINUE	SIGM123
125	AREF(1)=AREF(1)+SIGP*ABN(I)	SIGM124
	AREF(4)=AREF(4)+SIGP*ABN(I)	SIGM125
	AREF(5)=AREF(5)+SIGP*ABN(I)	SIGM126
	AREF(6)=AREF(6)+SIGP*ABN(I)	SIGM127
	BREF(1,I)=BREF(1,I)+SIGP*ABN(I)	SIGM128
	BREF(4,I)=BREF(4,I)+SIGP*ABN(I)	SIGM129
	BREF(5,I)=BREF(5,I)+SIGP*ABN(I)	SIGM130
	BREF(6,I)=BREF(6,I)+SIGP*ABN(I)	SIGM131
112	CONTINUE	SIGM132
	RETURN	SIGM133
	END	SIGM134
	SUBROUTINE SIEVE(E1,G1,E2,G2,M,N,NX,BEFF,BWR)	SIEV001
	COMMON/C/EX(101),JFLAG(101)	SIEV002
	IF(E2.LT,E1)GO TO 101	SIEV003
	GO TO 300	SIEV0031
300	N2=2*N	SIEV004
	DO 1000 I=1,100	SIEV005
	JFLAG(I)=2	SIEV006
1000	CONTINUE	SIEV007
	TEF=BEFF/293.0	SIEV008
	DP=(1.5885E+00)*SQRT (TEF/BWR)	SIEV009
C	WHEN MULTIPLIED BY SQRT(E) DP GIVES 5 TIMES CORRESPONDING DELTA	SIEV010
	DP1=DP*SQRT(E1)	SIEV011
	DP2=DP*SQRT (E2)	SIEV012
	DG1=G1/FLOAT (M)	SIEV013
	DG2=G2/FLOAT (M)	SIEV014
	EX(1)=E1	SIEV015
	IF(G1.LT,DP1)GO TO 1001	SIEV016
	GO TO 1002	SIEV0161
1001	JFLAG(1)=1	SIEV017
1002	ENDIF=ABS (E2-E1)	SIEV018
	NX=1	SIEV019
	DO 100 I=1,N	SIEV020
	XX=E1+DG1*FLOAT (I)	SIEV021
	IF(XX.LT,E2)GO TO 107	SIEV022
	GO TO 100	SIEV0221
107	NX=NX+1	SIEV023
	EX(NX)=XX	SIEV024
	IF(G1.LT,DP1)GO TO 1003	SIEV025
	GO TO 100	SIEV0251
1003	JFLAG(NX)=1	SIEV026
100	CONTINUE	SIEV027
	DO 200 I=1,N	SIEV028
	XX=E2-DG2*FLOAT (I)	SIEV029
	IF(XX.GT,E1)GO TO 108	SIEV030
	GO TO 200	SIEV0301
108	NX=NX+1	SIEV031
	EX(NX)=XX	SIEV032
	IF(G2.LT,DP2)GO TO 1005	SIEV033
	GO TO 200	SIEV0331
1005	JFLAG(NX)=1	SIEV034
200	CONTINUE	SIEV035
110	DIFF=(E2-E1)/FLOAT (N2)	SIEV036
	IF(DIFF)101,102,102	SIEV037
101	PRINT103	SIEV038
	PRINT2000,E1,E2,DIFF	SIEV039
	GO TO 104	SIEV040
103	FORMAT(32H CALLING SEQUENCE OF SIEVE WRONG)	SIEV041

2000	FORMAT(4H E1=E13,6,4H E2=E13,6,6H DIFF=E13,6)	SIEV042
102	N21=NX+1	SIEV043
	NN=NX	SIEV044
	N22=N21*N2-2	SIEV045
	NX=N22	SIEV046
	E21=(E1+E2)/2,0	SIEV047
	DP12=DP*SQRT (E21)	SIEV048
	E43=E2-E1-((G1+G2)/2,0)	SIEV049
	IF(E43,LT,DP12)GO TO 1006	SIEV050
	GO TO 1007	SIEV0501
1006	DO 111 I=N21,N22	SIEV051
	I2=I-NN	SIEV052
	EX(I)=E1+DIFF*FLOAT (I2)	SIEV053
	JFLAG(I)=1	SIEV054
111	CONTINUE	SIEV055
	GO TO 1040	SIEV056
1007	DO 112 I=N21,N22	SIEV057
	I2=I-NN	SIEV058
	EX(I)=E1+DIFF*FLOAT (I2)	SIEV059
	DPTTEST=DP*SQRT (EX(I))	SIEV060
	IF(EX(I).LE,E21)GO TO 1008	SIEV061
	GO TO 1009	SIEV0611
1008	IF(G1.LT,DPTTEST)GO TO 1010	SIEV062
	GO TO 112	SIEV0621
1010	JFLAG(I)=1	SIEV063
	GO TO 112	SIEV064
1009	IF(G2.LT,DPTTEST)GO TO 1011	SIEV065
	GO TO 112	SIEV0651
1011	JFLAG(I)=1	SIEV066
112	CONTINUE	SIEV067
1040	DO 113 I=1,NX	SIEV068
	DPF=DP*SQRT (EX(I))	SIEV069
	IF(DPF,EQ,0,0)GO TO 113	SIEV0691
	TERM=EX(I)/DPF	SIEV070
	IF(TERM.LT,25,)GO TO 114	SIEV071
	GO TO 113	SIEV0711
114	JFLAG(I)=1	SIEV072
113	CONTINUE	SIEV073
104	RETURN	SIEV074
	END	SIEV075

SIGMA2 TEST, IRON DATA,				0 350.	11	2	1.0E-4	
26056.E+0	55.36724E+0	0	0	0	0	4	0	0
26054.E+0	.0584E+0	0	0	0	0	1	0	0
4750.	100.E+3	1	2	0	0	2	0	0
53.4762	0.0	0	0	0	0	78	13	0
-15000.	.5E+0	5001.000	5000.	1.00				
7.83E+3	.5E+0	1202.16	1200.E+0	2.16				
52.1 E+3	.5E+0	2100.E+0	2100.E+0			.3E+0		
71.9 E+3	.5E+0	1600.E+0	1600.E+0			.3E+0		
98.5 E+3	.5E+0	400.E+0	400.E+0			.3E+0		
102.6 E+3	.5E+0	1375.E+0	1375.E+0			.3E+0		
132. E+3	.5E+0	1600.E+0	1600.E+0			.3E+0		
147. E+3	.5E+0	1950.E+0	1950.E+0			.3E+0		
173. E+3	.5E+0	4800.E+0	4800.E+0			.3E+0		
188.5 E+3	.5E+0	38000.E+0	38000.E+0			.3E+0		
245. E+3	.5E+0	13000.E+0	13000.E+0			.3E+0		
330. E+3	.5E+0	2750.E+0	2750.E+0			.3E+0		
370. E+3	.5E+0	3000.E+0	3000.E+0			.3E+0		
53.4762	0.	1	0	12			2	
9480.	.5	2.04	1.04	1.0				
14400.	.5	2.13	1.13	1.0				
26056.E+0	.9168E+0	0	0	1			0	
4750.	100.E+3	1	2	0			0	
55.4544	.60E+0	0	0	2			0	
-4000.	0.0	0	0	90			15	
27700.	.5	576.01	575.	1.01				
74. E+3	.5E+0	1401.44	1400.	1.44				
83.6 E+3	.5E+0	425.E+0	425.E+0	1.E+0				
123.5 E+3	.5E+0	1000.E+0	1000.E+0	1.E+0				
130. E+3	.5E+0	150.E+0	150.E+0	1.E+0				
141.3 E+3	.5E+0	500.E+0	500.E+0	1.E+0				
169. E+3	.5E+0	2300.E+0	2300.E+0	1.E+0				
188. E+3	.5E+0	690.E+0	690.E+0	1.E+0				
220. E+3	.5E+0	3160.E+0	3160.E+0	1.E+0				
243.5 E+3	.5E+0	1300.E+0	1300.E+0	1.E+0				
273. E+3	.5E+0	300.E+0	300.E+0	1.E+0				
315. E+3	.5E+0	3500.E+0	3500.E+0	1.E+0				
360. E+3	.5E+0	5500.E+0	5500.E+0	1.E+0				
382. E+3	.5E+0	9300.E+0	9300.E+0	1.E+0				
55.4544	0.0	10000.E+0	10000.E+0	1.E+0				
1150.	.5	1	0	72			12	
2350.	.5	.616	.052	.564				
11200.	1.5	1.0004	.0004	1.				
22700.	1.5	1.022	.022	1.				
34100.	1.5	1.1055	.1055	1.				
36600.	.5	2.346	.346	2.				
38300.	.5	1.43	.43	1.				
45800.	1.5	1.298	.298	1.				
51900.	.5	2.381	.381	2.				
53300.	.5	2.685	.685	2.				
55000.	1.5	1.37	.37	1.				
59000.	.5	1.1625	.1625	1.				
59000.	.5	2.74	.74	2.				
26057.E+0	.021700E+0	0	0	1			0	
4750.	100.E+3	1	2	0			0	
56.4463	.5	0	0	2			0	
3900.	0.0	0	0	30			5	
6300.	1.0	241.5	240.	1.5				
28000.	1.	463.73	460.	3.73				
		3005.	3000.	5.				

40500.	0.	2516.83	2516.	.83	
45500.	1.	269.83	269.	.83	
56.4463	0.0		1	0	8
1630.	0.	1.08	.25	.83	
4750.	0.	1.086	.256	.83	
7220.	1.	1.753	.923	.83	
7900.	1.	1.146	.316	.83	
12800.	2.	1.336	.506	.83	
13900.	2.	2.426	.776	1.65	
18000.	1.	2.71	1.06	1.65	
21300.	1.	6.92	1.92	5.	
26058.E+0	.0031E+0		0	0	0
4750.	100.E+3		1	2	0
0.E+0	.60E+0		0	0	0
57.4356	0.0		0	0	1
-600.	.5	3.57	2.57	1.00	
57.4356	0.0	1	0	12	2
230.	.5	1.00654	.00654	1.	
359.	.5	1.0173	.0173	1.	

PROGRAM SIGMA2, PROGRAM TO CALCULATE SINGLE OR MULTILEVEL BREIT-WIGNER CROSS-SECTIONS, USES ENDF/B VERSION II DATA

TITLE SIGMA2 TEST, IRON DATA.

(Z,A) DESIGNATION OF THE ELEMENT 2,60556E+04 AT,WT/MASS OF NEUTRON 5,5367E+01 NO OF ISOTOPES 4

DATA FOR ISOTOPE NUMBER 1

(Z,A) DESIGNATION OF THE ISOTOPE 2,6054E+04 FRACTIONAL ABUNDANCE 5,8400E+02 NO OF ENERGY RANGES 1  
 LOWER LIMIT OF THE ENERGY RANGE (EV) 4,7500E+03 UPPER LIMIT (EV) 1,0000E+05 LRU# 1 LRF# 2  
 NUCLEAR SPIN 0,0000E+00 SCATTERING LENGTH 6,0000E-01 NO OF L-VALUES 2  
 MASS OF THE ISOTOPE IN UNITS OF NEUTRON MASS 5,3476E+01 SCATTERING LENGTH(A-) 0,0000E+00 ANGULAR MOMENTUM 0 NO OF RESONANCES 13

ERES	SPIN	GTOT	GN	GGAMMA	GF
-1,5000E+04	5,0000E-01	5,0010E+03	5,0000E+03	1,0000E+00	0,0000E+00
7,8300E+03	5,0000E-01	1,5022E+03	1,2000E+03	2,1600E+00	0,0000E+00
5,2400E+04	5,0000E-01	2,4000E+03	2,1000E+03	3,0000E+01	0,0000E+00
7,1900E+04	5,0000E-01	1,6000E+03	1,6000E+03	3,0000E+01	0,0000E+00
9,8500E+04	5,0000E-01	4,0000E+02	4,0000E+02	3,0000E+01	0,0000E+00
1,0260E+05	5,0000E-01	1,3750E+03	1,3750E+03	3,0000E+01	0,0000E+00
1,3200E+05	5,0000E-01	1,6000E+03	1,6000E+03	3,0000E+01	0,0000E+00
1,4700E+05	5,0000E-01	1,9500E+03	1,9500E+03	3,0000E+01	0,0000E+00
1,7300E+05	5,0000E-01	4,8000E+03	4,8000E+03	3,0000E+01	0,0000E+00
1,8050E+05	5,0000E-01	3,8000E+04	3,8000E+04	3,0000E+01	0,0000E+00
2,4500E+05	5,0000E-01	1,3000E+04	1,3000E+04	3,0000E+01	0,0000E+00
3,3000E+05	5,0000E-01	2,7500E+03	2,7500E+03	3,0000E+01	0,0000E+00
3,7000E+05	5,0000E-01	3,0000E+03	3,0000E+03	3,0000E+01	0,0000E+00

MASS OF THE ISOTOPE IN UNITS OF NEUTRON MASS 5,3476E+01 SCATTERING LENGTH(A-) 0,0000E+00 ANGULAR MOMENTUM 0 NO OF RESONANCES 2

ERES	SPIN	GTOT	GN	GGAMMA	GF
9,4800E+03	5,0000E-01	2,0400E+00	1,0400E+00	1,0000E+00	0,0000E+00
1,4400E+04	5,0000E-01	2,1300E+00	1,1300E+00	1,0000E+00	0,0000E+00

DATA FOR ISOTOPE NUMBER 2

(Z,A) DESIGNATION OF THE ISOTOPE 2,60556E+04 FRACTIONAL ABUNDANCE 9,1680E+01 NO OF ENERGY RANGES 1

LOWER LIMIT OF THE ENERGY RANGE(KEV) 4.7500E+03 UPPER LIMIT(KEV) 1.0000E+05 LRU= 1 LRF= 2  
 NUCLEAR SPIN 0.0000E+00 SCATTERING LENGTH 6.0000E-01 NO OF L-VALUES 2  
 MASS OF THE ISOTOPE IN UNITS OF NEUTRON MASS 5.5454E+01 SCATTERING LENGTH(A=) 0.0000E+00 ANGULAR MOMENTUM 0 NO OF RESONANCES 15

ERES	SPIN	GTOT	GN	GGAMMA	GF
-4.0000E+03	5.0000E-01	5.7601E+02	5.7500E+02	1.0100E+00	0.0000E+00
2.7700E+04	5.0000E-01	1.4014E+03	1.4000E+03	1.4400E+00	0.0000E+00
7.4000E+04	5.0000E-01	4.2500E+02	4.2500E+02	1.0000E+00	0.0000E+00
8.3600E+04	5.0000E-01	1.0000E+03	1.0000E+03	1.0000E+00	0.0000E+00
1.2350E+05	5.0000E-01	1.5000E+02	1.5000E+02	1.0000E+00	0.0000E+00
1.3000E+05	5.0000E-01	5.0000E+02	5.0000E+02	1.0000E+00	0.0000E+00
1.4150E+05	5.0000E-01	2.3000E+03	2.3000E+03	1.0000E+00	0.0000E+00
1.6900E+05	5.0000E-01	6.9000E+02	6.9000E+02	1.0000E+00	0.0000E+00
1.8800E+05	5.0000E-01	3.1600E+03	3.1600E+03	1.0000E+00	0.0000E+00
2.2000E+05	5.0000E-01	1.3000E+03	1.3000E+03	1.0000E+00	0.0000E+00
2.4350E+05	5.0000E-01	3.0000E+02	3.0000E+02	1.0000E+00	0.0000E+00
2.7300E+05	5.0000E-01	3.5000E+03	3.5000E+03	1.0000E+00	0.0000E+00
3.1500E+05	5.0000E-01	5.5000E+03	5.5000E+03	1.0000E+00	0.0000E+00
3.6000E+05	5.0000E-01	9.3000E+03	9.3000E+03	1.0000E+00	0.0000E+00
3.8200E+05	5.0000E-01	1.0000E+04	1.0000E+04	1.0000E+00	0.0000E+00

MASS OF THE ISOTOPE IN UNITS OF NEUTRON MASS 5.5454E+01 SCATTERING LENGTH(A=) 0.0000E+00 ANGULAR MOMENTUM 1 NO OF RESONANCES 12

ERES	SPIN	GTOT	GN	GGAMMA	GF
1.1500E+03	5.0000E-01	6.1600E-01	5.2000E-02	5.6400E-01	0.0000E+00
2.3500E+03	5.0000E-01	1.0004E+00	4.0000E-04	1.0000E+00	0.0000E+00
1.1200E+04	1.5000E+00	1.0220E+00	2.2000E-02	1.0000E+00	0.0000E+00
2.2700E+04	1.5000E+00	1.0550E+00	1.0550E-01	1.0000E+00	0.0000E+00
3.4100E+04	1.5000E+00	2.3460E+00	3.4600E-01	2.0000E+00	0.0000E+00
3.6600E+04	5.0000E-01	1.4300E+00	4.3000E-01	1.0000E+00	0.0000E+00
3.8300E+04	1.5000E+00	1.2980E+00	2.9800E-01	1.0000E+00	0.0000E+00
4.5800E+04	5.0000E-01	2.3810E+00	3.8100E-01	2.0000E+00	0.0000E+00
5.1900E+04	5.0000E-01	2.6850E+00	6.8500E-01	2.0000E+00	0.0000E+00
5.3300E+04	1.5000E+00	1.8700E+00	3.7000E-01	1.0000E+00	0.0000E+00
5.5000E+04	5.0000E-01	1.1625E+00	1.6250E-01	1.0000E+00	0.0000E+00
5.9000E+04	5.0000E-01	2.7400E+00	7.4000E-01	2.0000E+00	0.0000E+00

DATA FOR ISOTOPE NUMBER 3

(Z,A) DESIGNATION OF THE ISOTOPE 2.6057E+04 FRACTIONAL ABUNDANCE 2.1700E-02 NO OF ENERGY RANGES 1  
 LOWER LIMIT OF THE ENERGY RANGE(KEV) 4.7500E+03 UPPER LIMIT(KEV) 1.0000E+05 LRU= 1 LRF= 2  
 NUCLEAR SPIN 0.0000E-01 SCATTERING LENGTH 6.0000E-01 NO OF L-VALUES 2  
 MASS OF THE ISOTOPE IN UNITS OF NEUTRON MASS 5.6446E+01 SCATTERING LENGTH(A=) 0.0000E+00 ANGULAR MOMENTUM 0 NO OF RESONANCES 5

ERES	SPIN	GTOT	GN	GGAMMA	GF
3.9000E+03	0.0000E+00	2.4150E+02	2.4000E+02	1.5000E+00	0.0000E+00

6.3000E+03	1.0000E+00	4.6373E+02	4.6000E+02	3.7300E+00	0.0000E+00
2.8000E+04	1.0000E+00	3.0050E+03	3.0000E+03	5.0000E+00	0.0000E+00
4.0500E+04	0.0000E+00	2.5168E+03	2.5160E+03	8.3000E-01	0.0000E+00
4.5500E+04	1.0000E+00	2.6983E+02	2.6900E+02	8.3000E-01	0.0000E+00

MASS OF THE ISOTOPE IN UNITS OF NEUTRON MASS 5.6446E+01 SCATTERING LENGTH(A\*) 0.0000E+00 ANGULAR MOMENTUM 1 NO OF RESONANCES 8

ERES	SPIN	CTOT	GN	GGAMMA	GF
1.6300E+03	0.0000E+00	1.0800E+00	2.5000E-01	8.3000E-01	0.0000E+00
4.7500E+03	0.0000E+00	1.0860E+00	2.5600E-01	8.3000E-01	0.0000E+00
7.2200E+03	1.0000E+00	1.7530E+00	9.2300E-01	8.3000E-01	0.0000E+00
7.9000E+03	1.0000E+00	1.1460E+00	3.1600E-01	8.3000E-01	0.0000E+00
1.2800E+04	2.0000E+00	1.3360E+00	5.0600E-01	8.3000E-01	0.0000E+00
1.3900E+04	2.0000E+00	2.4260E+00	7.7600E-01	1.6500E+00	0.0000E+00
1.8000E+04	1.0000E+00	2.7100E+00	1.0600E+00	1.6500E+00	0.0000E+00
2.1300E+04	1.0000E+00	6.9200E+00	1.9200E+00	5.0000E+00	0.0000E+00

DATA FOR ISOTOPE NUMBER 4

(Z,A) DESIGNATION OF THE ISOTOPE 2.6058E+04 FRACTIONAL ABUNDANCE 3.1000E-03 NO OF ENERGY RANGES 1  
 LOWER LIMIT OF THE ENERGY RANGE(EV) 4.7500E+03 UPPER LIMIT(EV) 1.0000E+05 LRU= 1 LRF= 2  
 NUCLEAR SPIN 0.0000E+00 SCATTERING LENGTH 6.0000E-01 NO OF L-VALUES 2  
 MASS OF THE ISOTOPE IN UNITS OF NEUTRON MASS 5.7436E+01 SCATTERING LENGTH(A\*) 0.0000E+00 ANGULAR MOMENTUM 0 NO OF RESONANCES 1

ERES	SPIN	CTOT	GN	GGAMMA	GF
-6.0000E+02	5.0000E-01	3.9700E+00	2.5700E+00	1.0000E+00	0.0000E+00

MASS OF THE ISOTOPE IN UNITS OF NEUTRON MASS 5.7436E+01 SCATTERING LENGTH(A\*) 0.0000E+00 ANGULAR MOMENTUM 1 NO OF RESONANCES 2

ERES	SPIN	CTOT	GN	GGAMMA	GF
2.3000E+02	5.0000E-01	1.0065E+00	6.9400E-03	1.0000E+00	0.0000E+00
3.5900E+02	5.0000E-01	1.0173E+00	1.7300E-02	1.0000E+00	0.0000E+00

CROSS-SECTIONS AT THERMAL ENERGY

NEUTRON ENERGY( EV)	SIGNN	SIGCAP	SIGF	SIGT	SIGNMULT	SIGTMULT
2.530000E-02	1.336535E+01	2.523121E+00	0.000000E+00	1.588847E+01	1.137350E+01	1.389662E+01



NEUTRON ENERGY ( EV )	SIGNN	SIGCAP	SIGF	SIGT	SIGNNMULT	SIGTMULT
4.750000E+03	6.786218E+00	5.598869E-01	0.000000E+00	7.344115E+00	5.693567E+00	6.253464E+00
4.981865E+03	6.502924E+00	5.413977E-03	0.000000E+00	6.508338E+00	5.432383E+00	5.437797E+00
5.137500E+03	6.466145E+00	5.974332E-03	0.000000E+00	6.472119E+00	5.410671E+00	5.416645E+00
5.121373E+03	6.461260E+00	6.344216E-03	0.000000E+00	6.467604E+00	5.413503E+00	5.419848E+00
5.152500E+03	6.581146E+00	8.971746E-03	0.000000E+00	6.590118E+00	5.570591E+00	5.579563E+00
5.836227E+03	7.276019E+00	1.642974E-02	0.000000E+00	7.292449E+00	6.323516E+00	6.339946E+00
5.912500E+03	7.694269E+00	2.030127E-02	0.000000E+00	7.714371E+00	6.780655E+00	6.780655E+00
6.068113E+03	9.350635E+00	3.430841E-02	0.000000E+00	9.384944E+00	8.444000E+00	8.478308E+00
6.300000E+03	1.367694E+01	6.214332E-02	0.000000E+00	1.373908E+01	1.252278E+01	1.258993E+01
6.330000E+03	1.153929E+01	3.518072E-02	0.000000E+00	1.157447E+01	1.011330E+01	1.0116827E+01
6.531865E+03	1.151864E+01	3.49715E-02	0.000000E+00	1.155362E+01	1.011224E+01	1.014719E+01
6.176000E+03	1.040249E+01	2.129222E-02	0.000000E+00	1.042178E+01	9.016798E+00	9.038091E+00
6.763730E+03	1.040148E+01	2.120134E-02	0.000000E+00	1.042268E+01	9.018405E+00	9.039606E+00
6.199000E+03	1.129585E+01	1.964598E-02	0.000000E+00	1.131549E+01	9.952143E+00	9.971789E+00
7.1218247E+03	1.416031E+01	3.259774E-01	0.000000E+00	1.448628E+01	1.288619E+01	1.321217E+01
7.219123E+03	1.467864E+01	7.805316E-01	0.000000E+00	1.545917E+01	1.340463E+01	1.418547E+01
7.220000E+03	1.533666E+01	1.538638E+00	0.000000E+00	1.707550E+01	1.426337E+01	1.502221E+01
7.221753E+03	1.421574E+01	3.260880E-01	0.000000E+00	1.454183E+01	1.294327E+01	1.326936E+01
7.229200E+03	1.400368E+01	3.794072E-02	0.000000E+00	1.404159E+01	1.343530E+01	1.421580E+01
7.327500E+03	1.657625E+01	3.764881E-02	0.000000E+00	1.660390E+01	1.540332E+01	1.277256E+01
7.525000E+03	1.98824E+01	3.282913E-02	0.000000E+00	2.002107E+01	1.899490E+01	1.902773E+01
7.677500E+03	2.331014E+01	3.711650E-02	0.000000E+00	2.334725E+01	2.258919E+01	2.342631E+01
7.830000E+03	2.513752E+01	3.810985E-02	0.000000E+00	2.517563E+01	2.473374E+01	2.47185E+01
7.847500E+03	2.59689E+01	3.798863E-02	0.000000E+00	2.523488E+01	2.482780E+01	2.486579E+01
7.865000E+03	2.522289E+01	3.791625E-02	0.000000E+00	2.526081E+01	2.488735E+01	2.492546E+01
7.882500E+03	2.521602E+01	3.851254E-02	0.000000E+00	2.525453E+01	2.491332E+01	2.495183E+01
7.898854E+03	2.52331E+01	2.988650E-01	0.000000E+00	2.522218E+01	2.499031E+01	2.524887E+01
7.999427E+03	2.58810E+01	5.915923E-01	0.000000E+00	2.597979E+01	2.511580E+01	2.570750E+01
7.900000E+03	2.59837E+01	1.146621E+00	0.000000E+00	2.674499E+01	2.532708E+01	2.647370E+01
7.900573E+03	2.59865E+01	5.916741E-01	0.000000E+00	2.597722E+01	2.511576E+01	2.577744E+01
7.901146E+03	2.525729E+01	2.58180E-01	0.000000E+00	2.551611E+01	2.498801E+01	2.524683E+01
8.295000E+03	1.921428E+01	2.252651E-02	0.000000E+00	1.923683E+01	1.925329E+01	1.927584E+01
8.690000E+03	1.336351E+01	1.200501E-02	0.000000E+00	1.337551E+01	1.331083E+01	1.332283E+01
9.085000E+03	1.020825E+01	7.084410E-03	0.000000E+00	1.021533E+01	1.000447E+01	1.005125E+01
9.477960E+03	9.328068E+00	8.359765E-01	0.000000E+00	1.031640E+01	9.088678E+00	9.924655E+00
9.478980E+03	1.062111E+01	2.083741E+00	0.000000E+00	1.270485E+01	1.038167E+01	1.246541E+01
9.480000E+03	1.278791E+01	4.164793E+00	0.000000E+00	1.695270E+01	1.254779E+01	1.671258E+01
9.481420E+03	1.062600E+01	2.083611E+00	0.000000E+00	1.270962E+01	1.038520E+01	1.246881E+01
9.482000E+03	9.323698E+00	8.360245E-01	0.000000E+00	1.015992E+01	9.083046E+00	9.919071E+00
9.910000E+03	7.315977E+00	3.245635E-03	0.000000E+00	7.319223E+00	7.024135E+00	7.027400E+00
1.034000E+04	6.567085E+00	2.421979E-03	0.000000E+00	6.569507E+00	6.244069E+00	6.246491E+00
1.077000E+04	6.033419E+00	1.928640E-03	0.000000E+00	6.0355346E+00	5.691669E+00	5.693896E+00
1.119898E+04	5.662268E+00	1.862818E+00	0.000000E+00	7.022000E+00	5.391626E+00	7.173443E+00
1.119949E+04	5.721642E+00	4.654700E+00	0.000000E+00	1.037634E+01	5.369999E+00	1.0022470E+01
1.120000E+04	5.831645E+00	9.307759E+00	0.000000E+00	1.313940E+01	5.479952E+00	1.478771E+01
1.120051E+04	5.736932E+00	4.654891E+00	0.000000E+00	1.039182E+01	5.385189E+00	1.004008E+01
1.120102E+04	5.67347E+00	1.862977E+00	0.000000E+00	7.536644E+00	5.321729E+00	7.184705E+00
1.160000E+04	5.321577E+00	1.382423E-03	0.000000E+00	5.322959E+00	4.965281E+00	4.966664E+00
1.200000E+04	5.063725E+00	1.214665E-03	0.000000E+00	5.064939E+00	4.706132E+00	4.707347E+00
1.240000E+04	4.839667E+00	1.098849E-03	0.000000E+00	4.840765E+00	4.483155E+00	4.484254E+00
1.279866E+04	4.803067E+00	2.698693E-01	0.000000E+00	5.072936E+00	4.449910E+00	4.471977E+00
1.279933E+04	5.048263E+00	6.733360E-01	0.000000E+00	5.721599E+00	4.695449E+00	5.368584E+00
1.280000E+04	5.460210E+00	1.345848E+00	0.000000E+00	6.5826049E+00	5.106525E+00	6.452362E+00





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101 CONTINUE
    NTOTAL=J1-1
    PHI=3.14159265359
    3 FORMAT(2E11,4,4I11)
    4 FORMAT(6E11,4)
    5 FORMAT(8E11,4,3I10)
    6 FORMAT(2X,2E11.4)
    7 FORMAT(76H NEUTRON ENERGY(EV)      SIGNN      SIGCAP      SIGRMP1122
    1F      SIGTOTAL)                      RMP1123
    8 FORMAT(2X,7E15.6)                    RMP1124
    9 FORMAT(10X,2E20.6)                  RMP1125
    10 FORMAT(20H ERROR IN INPUT DATA)    RMP1126
    11 FORMAT(10X,2I10)                   RMP1127
    12 FORMAT(10X,6I10)                    RMP1128
    16 FORMAT(15H NEUTRON ENERGYE15,6)   RMP1129
    14 FORMAT(53H CROSS-SECTIONS CALCULATED WITHOUT DOPPLER BROADENING) RMP1130
    15 FORMAT(50H CROSS-SECTIONS CALCULATED WITH DOPPLER BROADENING) RMP1131
    17 FORMAT(33H (Z,A) DESIGNATION OF THE ELEMENTE11,4,22H AT,WT/MASS OFRMP1132
    1 NEUTRONE11,4,15H NO OF ISOTOPES I5) RMP1133
    18 FORMAT(24H DATA FOR ISOTOPE NUMBER I5) RMP1134
    19 FORMAT(33H (Z,A) DESIGNATION OF THE ISOTOPEE11,4,21H FRACTIONAL ABRMP1135
    1UNDANCEE11,4,20H NO OF ENERGY RANGES I5) RMP1136
    20 FORMAT(36H LOWER LIMIT OF THE ENERGY RANGE(EV)E11,4,18H UPPER LIRMP1137
    1MIT(EV)E11,4,6H LRU=I5,6H LRF=I5) RMP1138
    21 FORMAT(13H NUCLEAR SPINE11,4,18H SCATTERING LENGTHE11,4,15H NO OF RMP1139
    1L-VALUES I5) RMP1140
    22 FORMAT(45H MASS OF THE ISOTOPE IN UNITS OF NEUTRON MASSE11,4,22H SRMP1141
    1CATTERING LENGTH(A-)E11,4,17H ANGULAR MOMENTUM I5,17H NO OF RESONANRMP1142
    2CES I5) RMP1143
    23 FORMAT(84H      ERES      SPIN      GN      GGAMMARMP1144
    1      GFA      GFB) RMP1145
    24 FORMAT(11H TITLE      7A4) RMP1146
    25 FORMAT(//) RMP1147
    26 FORMAT(6(2X,E11,4,2X)) RMP1148
    27 FORMAT(33H CROSS-SECTIONS AT THERMAL ENERGY) RMP1149
    28 FORMAT(2X,2E20.6,1I0) RMP1150
    29 FORMAT(2X,4E11,4) RMP1151
    30 FORMAT(22H EFFECTIVE TEMPERATUREF5,1,41H IN DEGREES KELVIN, NO RMP1152
    1OF PIVOT POINTS I5,18H CONVERGENCE ERROR E10,4,13H AND INCROSS=I5) RMP1153
    31 FORMAT(54H THE INTEGRAL FOR DOPPLER BROADENING DOES NOT CONVERGE) RMP1154
    33 FORMAT(126H1 PROGRAM RAMP1, PROGRAM TO CALCULATE CROSS-SECTIRMP1155
    1ONS ACCORDING TO THE REICH-MOORE FORMALISM, USES ENDF/B VERSION IIRMP1156
    2 DATA) RMP1157
C-----THIS IS WHERE RESONANCES OF EACH ISOTOPE ARE ARRANGED IN INCREASINRMP1158
C-----G ORDER IN L AND FOR EACH L IN INCREASING ORDER IN J, RMP1159
    DO 133 I=1,NIS RMP1160
    NRESI=NRES(I) RMP1161
    CALL ORDER(I,NRESI) RMP1162
133 CONTINUE RMP1163
    13 FORMAT(10I10) RMP1164
    NCOUNT=1 RMP1165
    DO 1330 I=1,NIS RMP1166
    XWR=AWRI(I) RMP1167
    YWR=XWR*1.008665 RMP1168
    YWR=YWR*(1.0/3.0) RMP1169
    APX=0.123*YWR+0.08 RMP1170
    NRESI=NRES(I) RMP1171
    NLMT=NCOUNT+NRESI-1 RMP1172
    DO 1331 J=NCOUNT,NLMT RMP1173
    CALL FACTS(ARRAY(1,J),IRAY(1,J),PENFAR(J),SHIFAR(J),PS,CONST,XWR, RMP1174
    1APX,1.0) RMP1175

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1331	CONTINUE	RMP1183
	NCOUNT=NCOUNT+NRESI	RMP1184
1330	CONTINUE	RMP1185
	DO 108 I=1,NTOTAL	RMP1186
	ERAN(1,I)=ARAY(1,I)	RMP1187
	ABGFA=ABS(ARAY(5,I))	RMP1188
	ABGFB=ABS(ARAY(6,I))	RMP1189
	ERAN(2,I)=ARAY(3,I)+ARAY(4,I)+ABGFA+ABGFB	RMP1190
108	CONTINUE	RMP1191
	CALL QIKS(1,NTOTAL,MOV,KOM)	RMP1192
C----	HERE RESONANCE IN AN ELEMENT ARE ARRANGED IN INCREASING ORDER IN	RMP1193
C----	ENERGY ALONG WITH THEIR TOTAL GAMMAS TO CALCULATE THE ENERGY MESH	RMP1194
C----	AT WHICH THE CROSS-SECTIONS ARE CALCULATED,	RMP1195
146	PRINT27	RMP1196
	PRINT25	RMP1197
	PRINT7	RMP1198
	E=ETHERM	RMP1199
	CALL RMSIGM(ETHERM,1)	RMP1200
	PRINT25	RMP1201
	ELO=EL(1,1)	RMP1202
	JFLAG(1)=1	RMP1203
	IRANGE=1	RMP1204
	PRINT8,ETHERM,(AREF(LL),LL=1,4)	RMP1205
148	PRINT25	RMP1206
	PRINT7	RMP1207
	PRINT25	RMP1208
	DO 124 JJ=1,NIS	RMP1209
	NERJJ=NER(JJ)	RMP1210
	DO 125 KK=1,NERJJ	RMP1211
	IRANGE=KK	RMP1212
	LRUJK=LRU(JJ,KK)	RMP1213
	IF(LRUJK=1)131,1321,125	RMP1214
131	PRINT10	RMP1215
	GO TO 130	RMP1216
1321	IF(JJ.EQ.1)GO TO 1320	RMP1217
	GO TO 132	RMP1218
1320	ELOREF=EL(JJ,KK)	RMP1219
	EHIREF=EH(JJ,KK)	RMP1220
	ELO=ELOREF	RMP1221
	EHI=EHIREF	RMP1222
	GO TO 1240	RMP1223
132	ELO=EL(JJ,KK)	RMP1224
	EHI=EH(JJ,KK)	RMP1225
	IF(ELO.EQ.ELOREF.AND.EHI.EQ.EHIREF)GO TO 124	RMP1226
	GO TO 1240	RMP1227
1240	MM=MAXPTS/(8*MAXRES)	RMP1228
	NN=MM	RMP1229
	IFLAG=1	RMP1230
	NLSKK=NLS(JJ,KK)	RMP1231
	J4=1	RMP1232
	ISTART=1	RMP1233
	IEND=1	RMP1234
117	IF(IEND.EQ.0)GO TO 125	RMP1235
	J5=J4+1	RMP1236
	E1=ERAN(1,J4)	RMP1237
	G1=ERAN(2,J4)	RMP1238
	E2=ERAN(1,J5)	RMP1239
	G2=ERAN(2,J5)	RMP1240
	IF(E1.LT.ELO.AND.E2.LT.ELO)GO TO 1120	RMP1241
1105	IF(E1.LE.ELO.AND.E2.GT.ELO)GO TO 1110	RMP1242
	GO TO 1111	RMP1243

1110	E1=ELO	RMP1244
	G1=G2	RMP1245
	ISTART=0	RMP1246
	GO TO 1114	RMP1247
1111	IF(E1.GT.ELO,AND,E2.LE,EHI)GO TO 1112	RMP1248
	GO TO 1113	RMP1249
1112	IF(J4.EQ.1,AND,ISTART,EQ,1)GO TO 1106	RMP1250
	GO TO 1114	RMP1251
1106	E2=E1	RMP1252
	G2=G1	RMP1253
	E1=ELO	RMP1254
	J4=J4-1	RMP1255
	ISTART=0	RMP1256
	GO TO 1114	RMP1257
1116	E2=EHI+G1/FLOAT (MM)	RMP1258
	G2=G1	RMP1259
	IFLAG=0	RMP1260
	GO TO 1114	RMP1261
1113	IF(E1.LT,EHI,AND,E2.GE,EHI)GO TO 1123	RMP1262
	GO TO 1124	RMP1263
1123	E2=EHI	RMP1264
	G2=G1	RMP1265
	IEND=0	RMP1266
	GO TO 1114	RMP1267
1124	IF(E1.GE,EHI,AND,E2.GT,EHI)GO TO 125	RMP1268
	GO TO 1125	RMP1269
1125	IF(IFLAG)1120,125,1120	RMP1270
1114	IF(E1.EQ,E2)GO TO 1120	RMP1271
	GO TO 1118	RMP1272
1118	CONTINUE	RMP1273
	CALL SIEVE(E1,G1,E2,G2,MM,NN,NX,TEFF,AWR)	RMP1274
	CALL QIKS(1,NX,MOVE,KOME)	RMP1275
	GO TO 116	RMP1276
1120	IF(IEND.EQ,0)GO TO 125	RMP1277
	J4=J4+1	RMP1278
	GO TO 117	RMP1279
116	DO 109 I=1,NX	RMP1280
	E=EX(I)	RMP1281
	JFLAGI=JFLAG(I)	RMP1282
	CALL RMSIGM(E,KK)	RMP1283
	PRINT8,E,(AREF(LL),LL=1,4)	RMP1284
	IF(IDPL.EQ,1)GO TO 141	RMP1285
	GO TO 109	RMP1286
141	IF(E.LT-ETHERM)GO TO 109	RMP1287
	GO TO 1410	RMP1288
C-----	IF THE NEUTRON ENERGY IS LESS THAN 0.0255 EV DOPPLER BROADENING IS	RMP1289
C-----	PASSED AS A DIFFERENT KERNEL SHOULD BE USED TO CALCULATE DOPPLER	RMP1290
C-----	BROADENED CROSS-SECTIONS.	RMP1291
1410	TEF=TEFF/293,0	RMP1292
	DELTA=0.3177*SQRT ((TEF*E)/AWR)	RMP1293
	GO TO (1121,1122),JFLAGI	RMP1294
1121	CALL GRID(E,DELTA,NTAB,XTAB)	RMP1295
32	FORMAT(2X,11E11,4)	RMP1296
	CALL GREAT2(DOPPLER,FINT,XTAB,NTAB,ERROR,IERR)	RMP1297
	PRINT28,E,FINT,JFLAG(I)	RMP1298
	IF(IERR.EQ,1)PRINT31	RMP1299
	GO TO 109	RMP1300
1122	CALL GAUSS(E,DELTA,DOPE)	RMP1301
	PRINT28,E,DOPE,JFLAG(I)	RMP1302
109	CONTINUE	RMP1303
	IF(IFLAG)1117,125,1117	RMP1304

1117	J4=J4+1	RMP1305
	IF (NTOTAL=J4) 125, 1250, 117	RMP1306
1250	E1=ERAN(1, J4)	RMP1307
	G1=ERAN(2, J4)	RMP1308
	GO TO 1116	RMP1309
125	CONTINUE	RMP1310
124	CONTINUE	RMP1311
120	CONTINUE	RMP1312
130	CALL EXIT	RMP1313
	END	RMP1314
	SUBROUTINE QIKS (MM, NN, MOVE, COMPAR)	QIKS0010
CQIKS	ALL-IN-MEMORY SORT PROGRAM	QIKS0020
C	MM = FIRST SUBSCRIPT	QIKS0030
C	NN = LAST SUBSCRIPT (ARRAY IS IN COMMON)	QIKS0040
C	MOVE AND COMPAR ARE USER SUPPLIED PROGRAMS	QIKS0050
	DIMENSION MSAVE(20), NSAVE(20)	QIKS0060
	KEYLOC(M, N) = (N+M)/2	QIKS0070
	I=0	QIKS0080
	J=0	QIKS0090
	LEVEL = 0	QIKS0100
	M=MM	QIKS0110
	N=NN	QIKS0120
35	CONTINUE	QIKS0130
C	TEST FOR ONE OR TWO ITEMS	QIKS0140
	IF (N=M-1) 31, 51, 32	QIKS0150
C	32 CONTINUE	QIKS0160
C	PARTITION AND SPREADER GO HERE, SEE BELOW. RETURN IS TO 8	QIKS0170
C	PUSH DOWN	QIKS0180
	8 LEVEL=LEVEL+1	QIKS0190
C	WORK ON SMALLEST PORTION	QIKS0200
	IF ((J=M) - (N-1)) 134, 134, 34	QIKS0210
134	MSAVE(LEVEL) = I	QIKS0220
	NSAVE(LEVEL)=N	QIKS0230
	N=J	QIKS0240
	GO TO 35	QIKS0250
34	MSAVE(LEVEL)=M	QIKS0260
	NSAVE(LEVEL)=J	QIKS0270
	M=I	QIKS0280
	GO TO 35	QIKS0290
51	IF (COMP(M, N)) 31, 31, 131	QIKS0300
C	SWAP IF ONLY TWO ITEMS ARE OUT OF ORDER	QIKS0310
131	CALL MOVE(M, 0)	QIKS0320
	CALL MOVE(N, M)	QIKS0330
	CALL MOVE(0, N)	QIKS0340
31	IF (LEVEL) 151, 150, 151	QIKS0350
150	RETURN	QIKS0360
C	POP UP	QIKS0370
151	M = MSAVE(LEVEL)	QIKS0380
	N=NSAVE(LEVEL)	QIKS0390
	LEVEL=LEVEL-1	QIKS0400
	GO TO 35	QIKS0410
C	END MAIN	QIKS0420
C	PARTITION	QIKS0430
32	I=M	QIKS0440
	J=N	QIKS0450
	KEY=KEYLOC(M, N)	QIKS0460
	CALL MOVE(KEY, 0)	QIKS0470
54	IF (N - KEY) 17, 1, 17	QIKS0480
17	CALL MOVE(N, KEY)	QIKS0490
1	CONTINUE	QIKS0500
C	HOLE AT BOTTOM	QIKS0510

	IF (COMPAR(0,I))3,2,2	QIKS0520
2	I=I+1	QIKS0530
	IF (I = J) 1, 4, 1	QIKS0540
3	CALL MOVE(I,J)	QIKS0550
	GO TO 5	QIKS0560
6	CONTINUE	QIKS0570
C	HOLE AT TOP	QIKS0580
	IF (COMPAR(0,J))5,5,7	QIKS0590
5	J=J-1	QIKS0600
	IF (I = J) 6, 4, 6	QIKS0610
7	CALL MOVE(J,I)	QIKS0620
	GO TO 2	QIKS0630
C	4 CONTINUE	QIKS0640
C	SPREADER GOES HERE	QIKS0650
C	END PARTITION	QIKS0660
C	SPREADER	QIKS0670
	4 CALL MOVE(0,I)	QIKS0680
12	IF (I = N) 110, 10, 110	QIKS0690
110	I = I + 1	QIKS0700
	IF (COMPAR(0,I))10,12,10	QIKS0710
10	IF (J = M) 108, 8, 108	QIKS0720
108	J = J - 1	QIKS0730
	IF (COMPAR(0,J))8,10,8	QIKS0740
C	8 CONTINUE	QIKS0750
C	RETURN TO MAIN PROGRAM	QIKS0760
	END	QIKS0770
	SUBROUTINE MOV(I,J)	MOV 001
	COMMON/D/ERAN(2,501)	MOV 002
	I1=I	MOV 003
	J1=J	MOV 004
	IF (I1.EQ,0) I1=501	MOV 005
	IF (J1.EQ,0) J1=501	MOV 006
	ERAN(1,J1)=ERAN(1,I1)	MOV 007
	ERAN(2,J1)=ERAN(2,I1)	MOV 008
	RETURN	MOV 009
	END	MOV 010
	SUBROUTINE MOVE(I,J)	MOVE001
	COMMON/C/EX(101),JFLAG(101)	MOVE002
	I1=I	MOVE003
	J1=J	MOVE004
	IF (I1.EQ,0) I1=101	MOVE005
	IF (J1.EQ,0) J1=101	MOVE006
	EX(J1)=EX(I1)	MOVE007
	JFLAG(J1)=JFLAG(I1)	MOVE008
	RETURN	MOVE009
	END	MOVE010
	FUNCTION KOM(I,J)	KOM 001
	COMMON/D/ERAN(2,501)	KOM 002
	I1=I	KOM 003
	J1=J	KOM 004
	IF (I1.EQ,0) I1=501	KOM 005
	IF (J1.EQ,0) J1=501	KOM 006
	EOM=ERAN(1,I1)-ERAN(1,J1)	KOM 007
	IF (EOM)100,101,102	KOM 008
100	KOM=-1	KOM 009
	GO TO 103	KOM 010
101	KOM=0	KOM 011
	GO TO 103	KOM 012
102	KOM=1	KOM 013
103	RETURN	KOM 014
	END	KOM 015



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FUNCTION KOME(I,J)                                KOME001
COMMON/C/EX(101),JFLAG(101)                     KOME002
I1=I                                              KOME003
J1=J                                              KOME004
IF(I1.EQ,0)I1=101                               KOME005
IF(J1.EQ,0)J1=101                               KOME006
EOX=EX(I1)-EX(J1)                               KOME007
IF(EOX)100,101,102                             KOME008
100 KOME=-1                                      KOME009
GO TO 103                                        KOME010
101 KOME=0                                       KOME011
GO TO 103                                        KOME012
102 KOME=1                                       KOME013
103 RETURN                                       KOME014
END                                              KOME015
SUBROUTINE GREAT2(F,FINT,XTAB,NTAB,ERROR,IERR)   GRT2001
C-----CARRY OUT CONVERGENCE INTEGRATION SCHEME USING UP TO 200 INTERVALS GRT2002
C-----WHICH ARE THEN FURTHER SUBDIVIDED UNTIL CONVERGENCE OCCURS OR THE GRT2003
C-----MAXIMUM ALLOWABLE NUMBER OF ITERATIONS IS EXCEEDED, THE SUBROUTINE GRT2004
C-----ARGUMENTS ARE DEFINED AS FOLLOWS..... GRT2005
C-----F      =FUNCTION TO BE INTEGRATED, GRT2006
C-----FINT   =THE RESULTING INTEGRAL GRT2007
C-----XTAB  =TABLE OF ORDINATES (INTEGRATION INTERVAL IS FROM XTAB(1) TO GRT2008
C-----      XTAB(NTAB)) GRT2009
C-----NTAB  =THE LENGTH OF THE XTAB TABLE (NUMBER OF ORDINATES), GRT2010
C-----ERROR =ALLOWABLE NORMAL ERROR, GRT2011
C-----IERR  =ERROR INDICATOR SET TO ZERO IF METHOD CONVERGES, SET TO GRT2012
C-----      ONE IF METHOD DOES NOT CONVERGE, GRT2013
C-----      ONE IF METHOD DOES NOT CONVERGE OR TABLE (XTAB) IS TOO LONG GRT2014
      DIMENSION XTAB(33),PARTS(33),GOOF(33),INTER(33) GRT2015
C-----DEFINE THE MAXIMUM ALLOWABLE NUMBER OF ITERATIONS AND THE MAXIMUM GRT2016
C-----TABLE LENGTH, GRT2017
      DATA JMAX,NTABMX/20,1000/ GRT2018
C-----DETERMINE IF TABLE IS TOO LONG GRT2019
      IF(NTAB.GT,NTABMX) GO TO 100 GRT2020
C-----CALL GENERAL INTEGRATION SUBROUTINE, GRT2021
      ZZZ=F(5.0) GRT2021.1
      CALL GREAT1(F,FINT,NTAB,JMAX,XTAB,PARTS,GOOF,INTER,ERROR,IERR) GRT2022
      RETURN GRT2023
C-----TABLE IS TOO LONG. GRT2024
100 IERR=1 GRT2025
      FINT=0.0 GRT2026
      RETURN GRT2027
      END GRT2028
SUBROUTINE GREAT1(F,FINT,NTAB,JMAX,XTAB,PARTS,GOOF,INTER,ERROR, GRT1001
1 IERR) GRT1002
C-----CARRY OUT CONVERGENCE INTEGRATION SCHEME USING TRAPAZOIDAL RULE GRT1003
C-----AND DOUBLING THE NUMBER OF REGIONS PER SUBINTERVAL FOR EACH GRT1004
C-----ITERATION, ONLY DOUBLE UP IN THOSE INTERVALS THAT HAVE NOT ALREADY GRT1005
C-----CONVERGED, GRT1006
C-----F      =SINGLE PRECISION FUNCTION TO BE INTEGRATED GRT1007
C-----FINT   =THE RESULTING INTEGRAL GRT1008
C-----NTAB  =NUMBER OF ORDINATES SUPPLIED (THERE ARE N-1 INTERVALS) GRT1009
C-----JMAX  =MAXIMUM ALLOWABLE NUMBER OF ITERATIONS GRT1010
C-----XTAB  =TABLE OF THE ORDINATE VALUES, RANGE OF INTEGRATION IS GRT1011
C-----      FROM XTAB(1) TO XTAB(NTAB) GRT1012
C-----PARTS =ARRAY OF DIMENSION NTAB, EQUAL TO THE PARTIAL INTEGRALS GRT1013
C-----      OVER EACH OF THE NTAB-1 INTERVALS GRT1014
C-----GOOF  =ARRAY OF DIMENSION NTAB, EQUAL TO THE NORMAL ERROR IN EACH GRT1015
C-----      OF THE NTAB-1 INTERVAL. GRT1016
C-----INTER =ARRAY OF DIMENSION NTAB, SEPECIFYING THE NUMBER OF GRT1017

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C-----	SUBINTERVALS IN EACH INTERVAL	GRT1018
C-----	ERROR =ACCEPTABLE NORMAL ERROR	GRT1019
C-----	IERR =ERROR INDICATOR, SET TO ZERO IF METHOD CONVERGES, SET TO	GRT1020
C-----	ONE IF METHOD DOES NOT CONVERGE	GRT1021
C-----	DIMENSION XTAB(NTAB),PARTS(NTAB),INTER(NTAB),GOOF(NTAB)	GRT1022
C-----	INITIALIZE VALUE OF THE INTEGRAL	GRT1023
	FINT=0.0	GRT1024
C-----	CALCULATE THE NUMBER OF INTERVALS	GRT1025
	NM1=NTAB+1	GRT1026
C-----	CALCULATE ALLOWABLE ERROR PER INTERVAL	GRT1027
	ERRN=ERROR/FLOAT(NM1)	GRT1028
C-----	INITIALIZE APPROXIMATION TO INTEGRAL	GRT1029
	TOTAL=0.0	GRT1030
C-----	CALCULATE INITIAL APPROXIMATION	GRT1031
	DO 10 I=1,NM1	GRT1032
	INTER(I)=1	GRT1033
	PARTS(I)=0.5*(XTAB(I+1)-XTAB(I))*(F(XTAB(I+1))+F(XTAB(I)))	GRT1034
	10 TOTAL=TOTAL+PARTS(I)	GRT1035
C-----	CALCULATE INITIAL ERRORS	GRT1036
	DO 15 I=1,NM1	GRT1037
	15 GOOF(I)=PARTS(I)	GRT1038
C-----	SET UP LOOP OVER ITERATIONS	GRT1039
	DO 100 J=1,JMAX	GRT1040
C-----	SAVE LAST APPROXIMATION	GRT1041
	TOTAL1=TOTAL	GRT1042
C-----	SET UP LOOP OVER INTERVALS	GRT1043
	DO 20 I=1,NM1	GRT1044
C-----	CHECK FOR CONVERGENCE IN THIS INTERVAL	GRT1045
	IF(ABS(GOOF(I)/TOTAL),LT,ERRN) GO TO 20	GRT1046
C-----	CALCULATE DOUBLE INTERVAL	GRT1047
	DX=(XTAB(I+1)-XTAB(I))/FLOAT(INTER(I))	GRT1048
C-----	DOUBLE NUMBER OF STEPS	GRT1049
	INTER(I)=2*INTER(I)	GRT1050
C-----	INITIALIZE CONTRIBUTION TO INTEGRAL	GRT1051
	REST=0.0	GRT1052
	II=INTER(I)	GRT1053
C-----	INITIALIZE ORDINATE	GRT1054
	XNOW=XTAB(I)+0.5*DX	GRT1055
C-----	SET UP LOOP OVER ORDINATES	GRT1056
	DO 30 K=1,II,2	GRT1057
	REST=REST+F(XNOW)	GRT1058
	30 XNOW=XNOW+DX	GRT1059
C-----	CALCULATE NEXT PARTIAL INTEGRAL	GRT1060
	REST=0.5*(PARTS(I)+DX*REST)	GRT1061
C-----	ADD NEW PARTIAL INTEGRAL AND SUBTRACT OLD PARTIAL INTEGRAL	GRT1062
	TOTAL=TOTAL+REST-PARTS(I)	GRT1063
C-----	CALCULATE NEW ERROR AND SET PARTIAL INTEGRAL TO NEW VALUE	GRT1064
	GOOF(I)=REST-PARTS(I)	GRT1065
	PARTS(I)=REST	GRT1066
	20 CONTINUE	GRT1067
C-----	CHECK FOR CONVERGENCE	GRT1068
	100 IF(ABS(1.-TOTAL1/TOTAL),LE,ERROR) GO TO 200	GRT1069
C-----	THE METHOD HAS NOT CONVERGED	GRT1070
	FINT=TOTAL	GRT1071
	IERR=1	GRT1072
	RETURN	GRT1073
C-----	THE METHOD HAS CONVERGED	GRT1074
	200 FINT=TOTAL	GRT1075
	IERR=0	GRT1076
	RETURN	GRT1077
	END	GRT1078

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SUBROUTINE GRID(Q,BELTA,NTAB,XTAB)
COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU,LRF,LANG,NLS,
1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,AWRI,AM,DREF,AREF,BREF,IRANGE,NIS,
3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR
DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),
1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),
2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),
3SHIFAR(500),SPI(10),AP(10),AWRI(10),AM(10),DREF(6),AREF(6),BREF(6,
410)
DIMENSION XTAB(33)
IGNORE=1
N2=NTAB/2
N21=N2+1
N22=N2+2
N3=NTAB-1
XTAB(N21)=0
DO 1410 I=N22,NTAB
XTAB(I)=XTAB(I-1)+BELTA
II=NTAB+1-I
XTAB(II)=XTAB(II+1)-BELTA
1410 CONTINUE
DO 1411 I=1,NTAB
XTAB(I)=XTAB(I)
IF(XTAB(I))1412,1412,1411
1412 IGNORE=0
1411 CONTINUE
IF(IGNORE,EQ,0)GO TO 1413
GO TO 1414
1413 XTAB(1)=1.0E=03
DO 1415 I=1,N3
I1=I+1
XTAB(I1)=XTAB(1)+FLOAT(I)*BELTA
1415 CONTINUE
1414 RETURN
END
SUBROUTINE GAUSS(Q,BELTA,DOPE)
COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU,LRF,LANG,NLS,
1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,AWRI,AM,DREF,AREF,BREF,IRANGE,NIS,
3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR
DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),
1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),
2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),
3SHIFAR(500),SPI(10),AP(10),AWRI(10),AM(10),DREF(6),AREF(6),BREF(6,
410)
DIMENSION ABC(9),WET(9)
DATA ABC/-3.19099320178153,-2.26658058453184,-1.46855328921667,-0,
172355101875284,0,0,0,72355101875284,1.46855328921667,2.26658058453
2184,3.19099320178153/
DATA WET/0.3960697726326E-04,0.4943624275537E-02,0.8847452739438E-
101,0.4326515570026E+00,0.7202352156061E+00,0.4326515570026E+00,0.8
2847452739438E-01,0.4943624275537E-02,0.3960697726326E-04/
DATA PHIRT/1.772454/
TEF=TEFF/293.0
TERM=0.0
DO 200 K=1,NIS
T1=0.0
XWR=AWRI(K)
BELTA=(0.3177E+00)*SQRT((Q*TEF)/XWR)
X=BELTA*ABC(9)
IF(E-X)100,100,101
101 DO 102 I=1,9

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      ABCI=ABC(I)
      WETI=WET(I)
      Z=E+ABCI*BELTA
      CALL RMSIGM(Z,IRANGE)
      T1=T1+BREF(INCROSS,K)*WETI
102  CONTINUE
      GO TO 110
100  T1=0.0
110  TERM=TERM+T1
200  CONTINUE
      DOPE=TERM/PHIRT
      RETURN
      END
      SUBROUTINE FACTS(Q,L,PF,SF,PS,CONSTE,BWR,BP,PLOD)
C
C   SUBROUTINE TO CALCULATE PENETRATION AND
C   SHIFT FACTORS
C   Q IS THE ENERGY L IS THE ANGULAR MOMENTUM PF PENETRATION FACTOR
C   SF THE SHIFT FACTOR AND PS THE PHASE SHIFT AP IS R CONSTE IS KM
C   FOR DETAILS OF FORMULAE SEE GREGSON ET AL AEEW-MS17(MLBW)1965
C
      DOUBLE PRECISION PS,CONSTE,ROE,ROE2,ROE4
      EAB=ABS(Q)
      CONHLD=2.196771E-03*BWR*SQRT(EAB)
      CONSTE=CONHLD/(BWR+1.0)
C-----SINCE AWR IS GIVEN WITH THE NEUTRON MASS AS UNITY WE ADD ONE ABOVE
C-----TO CONVERT TO THE CENTER-OF-MASS SYSTEM
      ROE=BP*CONSTE
      S=FLOAT(L)
      IF(L.LE.0)GO TO 100
      GO TO(110,120,130,140,150),L
100  PF=ROE
      SF=0.0
      IF(PLOD.LT.2,0) GO TO 160
      PS=ROE
      GO TO 170
110  ROE2=ROE*ROE
      DENOM=1.0+ROE2
      PF=ROE2*ROE/DENOM
      SF=-1.0/DENOM
      IF(PLOD.LT.2,0) GO TO 160
      PS=ROE-DATAN(ROE)
      IF(PS/ROE=0,000001)160,170,170
120  ROE2=ROE*ROE
      ROE4=ROE2*ROE2
      DENOM=3.0*ROE2+ROE4+9.0
      PF=ROE4*ROE/DENOM
      SF=-((18.0+3.0*ROE2)/DENOM)
      IF(PLOD.LT.2,0) GO TO 160
      PS=ROE-DATAN(3.0*ROE/(3.0-ROE2))
      IF(PS/ROE=0,000001)160,170,170
130  ROE2=ROE*ROE
      ROE4=ROE2*ROE2
      ROE6=ROE4*ROE2
      DENOM=225.0+45.0*ROE2+6.0*ROE4+ROE6
      PF=ROE6*ROE/DENOM
      SF=-((675.0+90.0*ROE2+6.0*ROE4)/DENOM)
      IF(PLOD.LT.2,0) GO TO 160
      PS=ROE-DATAN((15.0*ROE-ROE2*ROE)/(15.0-6.0*ROE2))
      IF(PS/ROE=0,000001)160,170,170
140  ROE2=ROE*ROE

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GAUS027
GAUS028
GAUS029
GAUS030
GAUS031
GAUS032
GAUS033
GAUS034
GAUS035
GAUS036
GAUS037
GAUS038
GAUS039
FACT001
FACT002
FACT003
FACT004
FACT005
FACT006
FACT007
FACT008
FACT009
FACT010
FACT011
FACT012
FACT013
FACT014
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FACT038
FACT039
FACT040
FACT041
FACT042
FACT043
FACT044
FACT045
FACT046
FACT047
FACT048

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	ROE4=ROE2*ROE2	FACT049
	ROE6=ROE4*ROE2	FACT050
	ROE8=ROE4*ROE4	FACT051
	DENOM=11025,0+1575,0*ROE2+135,0*ROE4+10,0*ROE6+ROE8	FACT052
	PF=ROE8*ROE/DENOM	FACT053
	IF(PL0D.LT,2,0) GO TO 160	FACT054
	SF=- (44100,0+4725,0*ROE2+270,0*ROE4+10,0*ROE6)/DENOM	FACT055
	PS=ROE-DATAN((105,0*ROE-10,0*ROE2*ROE)/(105,0-45,0	FACT056
	1*ROE2+ROE4))	FACT057
	IF(PS/ROE=0,000001)160,170,170	FACT058
150	ROE2=ROE*ROE	FACT059
	ROE4=ROE2*ROE2	FACT060
	ROE6=ROE4*ROE2	FACT061
	ROE8=ROE4*ROE4	FACT062
	ROE10=ROE6*ROE4	FACT063
	DENOM=893025,0+99225,0*ROE2+6300,0*ROE4+315,0*ROE6	FACT064
	1+15,0*ROE8+ROE10	FACT065
	PF=ROE10*ROE/DENOM	FACT066
	SF=4465125,0+396900,0*ROE2+18900,0*ROE4	FACT067
	1+630,0*ROE6+15,0*ROE8	FACT068
	SF=-SF/DENOM	FACT069
	IF(PL0D.LT,2,0) GO TO 160	FACT070
	PS=ROE-DATAN((945,0*ROE-ROE*(105,0*ROE2+ROE4))/(945,0-420,0*ROE2+	FACT071
	115,0*ROE4))	FACT072
	IF(PS/ROE.GE,0,000001) GO TO 170	FACT073
160	PS=0,0	FACT074
170	RETURN	FACT075
	END	FACT076
	SUBROUTINE ORDER(K,N1)	ORDR001
	COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU,LRF,LANG,NLS,	ORDR002
	1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,AWRI,AM,DREF,AREF,BREF,IRANGE,NIS,	ORDR003
	3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR	ORDR004
	DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),	ORDR005
	1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),	ORDR006
	2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),	ORDR007
	3SHIFAR(500),SPI(10),AP(10),AWRI(10),AM(10),DREF(6),AREF(6),BREF(6,	ORDR008
	410)	ORDR009
	IF(K-1)2,2,3	ORDR010
2	NTR=0	ORDR011
	NUML=0	ORDR012
	NUMJ=0	ORDR013
	NN=0	ORDR014
	MM=0	ORDR015
	JJ=0	ORDR016
	NC=0	ORDR017
	MC=0	ORDR018
3	NT=NTR+1	ORDR019
	NTR=NTR+N1	ORDR020
	OL=-0.9	ORDR021
8	OL=OL+1.0	ORDR022
	DO 101 N=NT,NTR	ORDR023
	TERM=FLOAT (IRAY(1,N))	ORDR024
	IF(OL-TERM)101,101,9	ORDR025
9	NN=NN+1	ORDR026
	DO 100 J=1,6	ORDR027
	A=ARAY(J,N)	ORDR028
	ARAY(J,N)=ARAY(J,NN)	ORDR029
	ARAY(J,NN)=A	ORDR030
100	CONTINUE	ORDR031
	DO 1001 J=1,3	ORDR032
	IA=IRAY(J,N)	ORDR033

	IRAY(J,N)=IRAY(J,NN)	ORDR034
	IRAY(J,NN)=IA	ORDR035
1001	CONTINUE	ORDR036
	DO 1002 J=1,2	ORDR037
	EA=ERAY(J,N)	ORDR038
	ERAY(J,N)=ERAY(J,NN)	ORDR039
	ERAY(J,NN)=EA	ORDR040
1002	CONTINUE	ORDR041
101	CONTINUE	ORDR042
	IF(NN-NC)8,8,11	ORDR043
11	NUML=NUML+1	ORDR044
	LN(NUML)=NN-NC	ORDR045
	NC=NN	ORDR046
	NU=NT+LN(NUML)-1	ORDR047
	OM=0,25	ORDR048
14	OM=OM+0.5	ORDR049
	DO 205 M=NT,NU	ORDR050
	TERMJ=ARAY(2,M)	ORDR051
	IF(OM-TERMJ)205,205,15	ORDR052
15	MM=MM+1	ORDR053
	DO 204 J=1,6	ORDR054
	A=ARAY(J,M)	ORDR055
	ARAY(J,M)=ARAY(J,MM)	ORDR056
	ARAY(J,MM)=A	ORDR057
204	CONTINUE	ORDR058
	DO 2041 J=1,3	ORDR059
	IA=IRAY(J,M)	ORDR060
	IRAY(J,M)=IRAY(J,MM)	ORDR061
	IRAY(J,MM)=IA	ORDR062
2041	CONTINUE	ORDR063
	DO 2042 J=1,2	ORDR064
	EA=ERAY(J,M)	ORDR065
	ERAY(J,M)=ERAY(J,MM)	ORDR066
	ERAY(J,MM)=EA	ORDR067
2042	CONTINUE	ORDR068
205	CONTINUE	ORDR069
	IF(MM-MC)14,14,16	ORDR070
16	NUMJ=NUMJ+1	ORDR071
	JN(NUMJ)=MM-MC	ORDR072
	MC=MM	ORDR073
	NT=NT+JN(NUMJ)	ORDR074
	IF(NN-MM)17,17,14	ORDR075
17	IF(NTR=NN)18,18,8	ORDR076
18	RETURN	ORDR077
	END	ORDR078
	FUNCTION DOPPLER(X)	DOPL001
	COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU,TRF,LANG,NLS,	DOPL002
	1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,AWRI,AM,DREF,AREF,BREF,IRANGE,NIS,	DOPL003
	3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR	DOPL004
	DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),	DOPL005
	1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),TRF(10,10),	DOPL006
	2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),	DOPL007
	3SHIFAR(500),SPI(10),AP(10),AWRI(10),AM(10),DREF(6),AREF(6),BREF(6,	DOPL008
	410)	DOPL009
	TEF=TEFF/293,0	DOPL010
	TERM=0,0	DOPL011
	CALL RMSIGM(X,IRANGE)	DOPL012
	DO 100 I=1,NIS	DOPL013
	XWR=AWRI(I)	DOPL014
	CELTA=(0,3177E+00)*SQRT((TEF*E)/XWR)	DOPL015
	Z=(E-X)/CELTA	DOPL016

Z2=Z*Z	DOPL017
T1=BREF(INCROSS,I)*EXP(-Z2)/(DELTA*1.772454)	DOPL018
TERM=TERM+T1	DOPL019
100 CONTINUE	DOPL020
DOPPLER=TERM	DOPL021
RETURN	DOPL022
END	DOPL023
SUBROUTINE ABCMAT(A,B,C)	ABCM001
DOUBLE PRECISION A,B,C	ABCM002
DIMENSION A(3,3),B(3,3),C(3,3)	ABCM003
DO 100 I=1,3	ABCM004
DO 101 J=1,3	ABCM005
C(I,J)=0,0	ABCM006
DO 102 K=1,3	ABCM007
C(I,J)=C(I,J)+A(I,K)*B(K,J)	ABCM008
102 CONTINUE	ABCM009
101 CONTINUE	ABCM010
100 CONTINUE	ABCM011
RETURN	ABCM012
END	ABCM013
SUBROUTINE FROBNS(A,B,C,D)	FROB001
DOUBLE PRECISION A,B,C,D,Q	FROB002
DIMENSION A(3,3),B(3,3),C(3,3),D(3,3),Q(3,3)	FROB003
C-----THIS SUBROUTINE INVERTS A COMPLEX MATRIX WITH REAL AND IMAGINARY	FROB004
C-----PARTS A AND B AND GIVES C AND D THE REAL AND IMAGINARY PARTS OF THE	FROB005
C-----E INVERSE. FROBENIUS-SCHUR METHOD OF INVERSION.	FROB006
DO 200 I=1,3	FROB007
DO 201 J=1,3	FROB008
C(I,J)=A(I,J)	FROB009
201 CONTINUE	FROB010
200 CONTINUE	FROB011
CALL THRINV(A,3,IND)	FROB012
IF(IND,EQ,1) GO TO 500	FROB013
CALL ABCMAT(A,B,Q)	FROB014
CALL ABCMAT(B,Q,D)	FROB015
DO 202 I=1,3	FROB016
DO 203 J=1,3	FROB017
C(I,J)=C(I,J)+D(I,J)	FROB018
203 CONTINUE	FROB019
202 CONTINUE	FROB020
CALL THRINV(C,3,IND)	FROB021
IF(IND,EQ,1) GO TO 500	FROB022
CALL ABCMAT(Q,C,D)	FROB023
DO 204 I=1,3	FROB024
DO 205 J=1,3	FROB025
D(I,J)=-D(I,J)	FROB026
205 CONTINUE	FROB027
204 CONTINUE	FROB028
GO TO 502	FROB029
500 PRINT501	FROB030
GO TO 502	FROB031
501 FORMAT(52H TROUBLE IN INVERTING THE COMPLEX MATRIX, JOB ABORT.)	FROB032
502 RETURN	FROB033
END	FROB034
SUBROUTINE THRINV(D,N,KIMERR)	THRI001
C INVERTS SYMMETRIC MATRIX (D(I,J),J=1,N,I=1,J)	THRI002
DOUBLE PRECISION D,S,FOOEY	THRI003
DIMENSION D(3,3),S(3)	THRI004
KIMERR=0	THRI005
55 CONTINUE	THRI006
26 DO1J=1,N	THRI007

29	D02I=1,J	THR1008
	D(I,J)=-D(I,J)	THR1009
2	D(J,I)=D(I,J)	THR1010
1	D(J,J)=1,+D(J,J)	THR1011
30	D07LR=1,N	THR1012
	FOOEY=1,-D(LR,LR)	THR1013
	IF(FOOEY, EQ, 0,0) GO TO 333	THR1014
	D(LR,LR) = 1./FOOEY	THR1015
31	CONTINUE	THR1016
	GO TO 27	THR1017
333	KIMERR=1	THR1018
	GOTO1001	THR1019
27	D041J=1,N	THR1020
	S(J)=D(LR,J)	THR1021
32	IF(J=LR)28,41,28	THR1022
28	D(J,LR)=D(J,LR)*D(LR,LR)	THR1023
	D(LR,J)=D(J,LR)	THR1024
41	CONTINUE	THR1025
33	DO 7J=1,N	THR1026
34	IF(J=LR) 6,7,6	THR1027
6	DO 503 I=1,J	THR1028
35	IF(I=LR) 8,503,8	THR1029
8	D(I,J)=D(I,J)+D(I,LR)*S(J)	THR1030
	D(J,I)=D(I,J)	THR1031
503	CONTINUE	THR1032
7	CONTINUE	THR1033
1001	RETURN	THR1034
	END	THR1035
	SUBROUTINE SIEVE(E1,G1,E2,G2,M,N,NX,BEFF,BWR)	SIEV001
	COMMON/C/EX(101),JFLAG(101)	SIEV002
	IF(E2.LT,E1)GO TO 101	SIEV003
	GO TO 300	SIEV0031
300	N2=2*N	SIEV004
	DO 1000I=1,100	SIEV005
	JFLAG(I)=2	SIEV006
1000	CONTINUE	SIEV007
	TEF=BEFF/293,0	SIEV008
	DP=(1,5885E+00)*SQRT (TEF/BWR)	SIEV009
C	WHEN MULTIPLIED BY SQRT(E) DP GIVES 5 TIMES CORRESPONDING DELTA	SIEV010
	DP1=DP*SQRT(E1)	SIEV011
	DP2=DP*SQRT (E2)	SIEV012
	DG1=G1/FLOAT (M)	SIEV013
	DG2=G2/FLOAT (M)	SIEV014
	EX(1)=E1	SIEV015
	IF(G1.LT,DP1)GO TO 1001	SIEV016
	GO TO 1002	SIEV0161
1001	JFLAG(1)=1	SIEV017
1002	ENDIF=ABS (E2-E1)	SIEV018
	NX=1	SIEV019
	DO 100 I=1,N	SIEV020
	XX=E1+DG1*FLOAT (I)	SIEV021
	IF(XX.LT,E2)GO TO 107	SIEV022
	GO TO 100	SIEV0221
107	NX=NX+1	SIEV023
	EX(NX)=XX	SIEV024
	IF(G1.LT,DP1)GO TO 1003	SIEV025
	GO TO 100	SIEV0251
1003	JFLAG(NX)=1	SIEV026
100	CONTINUE	SIEV027
	DO 200 I=1,N	SIEV028
	XX=E2+DG2*FLOAT (I)	SIEV029



IF (XX.GT,E1)GO TO 108	SIEV030
GO TO 200	SIEV0301
108 NX=NX+1	SIEV031
EX(NX)=XX	SIEV032
IF (G2.LT,DP2)GO TO 1005	SIEV033
GO TO 200	SIEV0331
1005 JFLAG(NX)=1	SIEV034
200 CONTINUE	SIEV035
110 DIFF=(E2-E1)/FLOAT (N2)	SIEV036
IF (DIFF)101,102,102	SIEV037
101 PRINT103	SIEV038
PRINT2000,E1,E2,DIFF	SIEV039
GO TO 104	SIEV040
103 FORMAT(32H CALLING SEQUENCE OF SIEVE WRONG)	SIEV041
2000 FORMAT(4H E1=E13,6,4H E2=E13,6,6H DIFF=E13,6)	SIEV042
102 N21=NX+1	SIEV043
NN=NX	SIEV044
N22=N21+N2-2	SIEV045
NX=N22	SIEV046
E21=(E1+E2)/2,0	SIEV047
DP12=DP*SQRT (E21)	SIEV048
E43=E2-E1-((G1+G2)/2,0)	SIEV049
IF (E43.LT,DP12)GO TO 1006	SIEV050
GO TO 1007	SIEV0501
1006 DO 111 I=N21,N22	SIEV051
I2=I+NN	SIEV052
EX(I)=E1+DIFF*FLOAT (I2)	SIEV053
JFLAG(I)=1	SIEV054
111 CONTINUE	SIEV055
GO TO 1040	SIEV056
1007 DO 112 I=N21,N22	SIEV057
I2=I+NN	SIEV058
EX(I)=E1+DIFF*FLOAT (I2)	SIEV059
DPTEST=DP*SQRT (EX(I))	SIEV060
IF (EX(I),LE,E21)GO TO 1008	SIEV061
GO TO 1009	SIEV0611
1008 IF (G1.LT,DPTEST)GO TO 1010	SIEV062
GO TO 112	SIEV0621
1010 JFLAG(I)=1	SIEV063
GO TO 112	SIEV064
1009 IF (G2.LT,DPTEST)GO TO 1011	SIEV065
GO TO 112	SIEV0651
1011 JFLAG(I)=1	SIEV066
112 CONTINUE	SIEV067
1040 DO 113 I=1,NX	SIEV068
DPF=DP*SQRT (EX(I))	SIEV069
IF (DPF,EQ,0,0)GO TO 113	SIEV0691
TERM=EX(I)/DPF	SIEV070
IF (TERM.LT,25.)GO TO 114	SIEV071
GO TO 113	SIEV0711
114 JFLAG(I)=1	SIEV072
113 CONTINUE	SIEV073
104 RETURN	SIEV074
END	SIEV075
SUBROUTINE RMSIGM(G,KK)	RMSG001
COMMON/E/XMIN(6),XMAX(6),XREF(6)	RMSG002
COMMON ARAY,IRAY,ERAY,NOT,ZAI,ABN,NER,LFW,EL,EH,LRU,LPF,LANG,NLS,	RMSG003
1NRES,LN,JN,PENFAR,SHIFAR,SPI,AP,AWRI,AM,DREF,AREF,BREF,IRANGE,NIS,	RMSG004
3INCROSS,IVSPIN,ELO,TEFF,DELTA,E,AWR	RMSG005
DIMENSION ARAY(6,500),IRAY(3,500),ERAY(2,500),NOT(20),ZAI(10),	RMSG006
1ABN(10),NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LPF(10,10),RMSG007	

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2LANG(10,5,5),NLS(10,10),NRES(10),LN(50),JN(150),PENFAR(500),      RMSG008
3SHIFAR(500),SPI(10),AP(10),AWRI(10),AM(10),DREF(6),AREF(6),BREF(6,RMSG009
410)      RMSG010
DOUBLEPRECISIONR,S,RI,S1,B,DEN,DIFF,P1,R2,RH01,RH02,GJ,T1,T2,T3,T4RMSG011
1,TERMT,TERMN,TERMF,TERMA,TERMG,SIGNNI,SINGNI,SIGNFI,SIGNAI,SIGNTI,RMSG012
2BETA,TRM,SIGP,CONSTE,CONSTA,PI,PS      RMSG013
DIMENSION R(3,3),S(3,3),RI(3,3),SI(3,3),B(3,3)      RMSG014
C-----THIS SUBROUTINE USES THE FROBENIUS-SCHUR METHOD FOR INVERTING THE      RMSG015
C-----COMPLEX MATRIX.      RMSG016
P1=3,141592653590+00      RMSG017
Q2=SQRT(Q)      RMSG018
DO 4 J=1,6      RMSG019
AREF(J)=0,0      RMSG020
DO 5 K=1,10      RMSG021
BREF(J,K)=0,0      RMSG022
5 CONTINUE      RMSG023
4 CONTINUE      RMSG024
L2=0      RMSG025
N2=0      RMSG026
LA=0      RMSG027
JA=0      RMSG028
NTR=0      RMSG029
DO 112 I=1,NIS      RMSG030
NRESI=NRES(I)      RMSG031
API=AP(I)      RMSG032
XWR=AWRI(I)      RMSG033
YWR=XWR*1,008665      RMSG034
YWR=YWR**(1,0/3,0)      RMSG035
APX=0,123*YWR+0,08      RMSG036
3 NTR=NTR+NRESI      RMSG037
IF(NRESI)110,110,100      RMSG038
100 LA=LA+1      RMSG039
102 L2=L2+LN(LA)      RMSG040
CALL FACTS(Q,IRAY(1,L2),PF,SF,PX,CONSTE,XWR,APX,3,0)      RMSG041
CALL FACTS(Q,IRAY(1,L2),PX,SX,PS,CONSTE,XWR,API,3,0)      RMSG042
SIGNNI=0,0      RMSG043
SINGNI=0,0      RMSG044
SIGNFI=0,0      RMSG045
SIGNAI=0,0      RMSG046
SIGNTI=0,0      RMSG047
103 JA=JA+1      RMSG048
104 N1=N2+1      RMSG049
N2=N2+JN(JA)      RMSG050
GJ=2,0*(2,0*SPI(I)+1,0)      RMSG051
GJ=(2,0*ARAY(2,N1)+1,0)/GJ      RMSG052
3001 DO 7 J=1,3      RMSG053
DO 8 K=1,3      RMSG054
S(J,K)=0,0      RMSG055
IF(J,EQ,K)GO TO 9      RMSG056
GO TO 10      RMSG057
9 R(J,K)=1,0      RMSG058
GO TO 8      RMSG059
10 R(J,K)=0,0      RMSG060
8 CONTINUE      RMSG061
7 CONTINUE      RMSG062
DO 108 K=N1,N2      RMSG063
DIFF=ARAY(1,K)-Q      RMSG064
A1=ARAY(3,K)      RMSG065
A1=(A1*PF)/PENFAR(K)      RMSG066
A1=SQRT(A1)      RMSG067
A2=ARAY(5,K)      RMSG068

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IF(A2)200,201,202
200 A2=-SQRT(-A2)
GO TO 300
201 A2=0,0
GO TO 300
202 A2=SQRT(A2)
300 A3=ARRAY(6,K)
IF(A3)301,302,303
301 A3=-SQRT(-A3)
GO TO 400
302 A3=0,0
GO TO 400
303 A3=SQRT(A3)
400 DEN=DIFF**2+0,25*ARRAY(4,K)*ARRAY(4,K)
R(1,1)=R(1,1)+((0,25*ARRAY(4,K)*A1*A1)/DEN)
S(1,1)=S(1,1)-((0,5*DIFF*A1*A1)/DEN)
R(1,2)=R(1,2)+((0,25*ARRAY(4,K)*A1*A2)/DEN)
S(1,2)=S(1,2)-((0,5*DIFF*A1*A2)/DEN)
R(1,3)=R(1,3)+((0,25*ARRAY(4,K)*A1*A3)/DEN)
S(1,3)=S(1,3)-((0,5*DIFF*A1*A3)/DEN)
R(2,2)=R(2,2)+((0,25*ARRAY(4,K)*A2*A2)/DEN)
S(2,2)=S(2,2)-((0,5*DIFF*A2*A2)/DEN)
R(3,3)=R(3,3)+((0,25*ARRAY(4,K)*A3*A3)/DEN)
S(3,3)=S(3,3)-((0,5*DIFF*A3*A3)/DEN)
R(2,3)=R(2,3)+((0,25*ARRAY(4,K)*A2*A3)/DEN)
S(2,3)=S(2,3)-((0,5*DIFF*A2*A3)/DEN)
108 CONTINUE
R(2,1)=R(1,2)
S(2,1)=S(1,2)
R(3,1)=R(1,3)
S(3,1)=S(1,3)
R(3,2)=R(2,3)
S(3,2)=S(2,3)
DO 11 JJJ=1,3
DO 12 KKK=1,3
B(JJJ,KKK)=R(JJJ,KKK)
12 CONTINUE
11 CONTINUE
CALL FROBNS(R,S,RI,SI)
RH01=RI(1,1)
RH02=SI(1,1)
P1=DCOS(2,0*PS)
P2=-DSIN(2,0*PS)
TERMT=(1,0-P1*(2,0*RH01=1,0)+2,0*P2*RH02)*2,0
TERMT=GJ*TERMT-4,0*GJ*DSIN(PS)*DSIN(PS)
T1=RI(1,2)
T2=SI(1,2)
T3=RI(1,3)
T4=SI(1,3)
TERMF=GJ*(T1**2+T2**2+T3**2+T4**2)*4,0
TERMG=(RH01**2+RH02**2)*(B(1,1)-1,0)+(T1**2+T2**2)*(B(2,2)-1,0)+
1(T3**2+T4**2)*(B(3,3)-1,0)
TERMG=TERMG+2,0*(RH01*T1+RH02*T2)*B(1,2)+2,0*(RH01*T3+RH02*T4)*
1B(1,3)+2,0*(T1*T3+T2*T4)*B(2,3)
TERMG=4,0*GJ*TERMG
TERMN=TERMT-TERMF=TERMG
SIGNNI=SIGNNI+TERMN
SIGNGI=SINGI+TERMG
SIGNFI=SIGNFI+TERMF
SIGNTI=SIGNTI+TERMT
IF(L2-N2)109,109,103
RMSG069
RMSG070
RMSG071
RMSG072
RMSG073
RMSG074
RMSG075
RMSG076
RMSG077
RMSG078
RMSG079
RMSG080
RMSG081
RMSG082
RMSG083
RMSG084
RMSG085
RMSG086
RMSG087
RMSG088
RMSG089
RMSG090
RMSG091
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RMSG100
RMSG101
RMSG102
RMSG103
RMSG104
RMSG105
RMSG106
RMSG107
RMSG108
RMSG109
RMSG110
RMSG111
RMSG112
RMSG113
RMSG114
RMSG115
RMSG116
RMSG117
RMSG118
RMSG119
RMSG120
RMSG121
RMSG122
RMSG123
RMSG124
RMSG125
RMSG126
RMSG127
RMSG128
RMSG129

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109	BETA=PI*ABN(I)/(CONSTE*CONSTE)	RMSG130
	AREF(1)=AREF(1)*SIGNNI*BETA	RMSG131
	AREF(2)=AREF(2)*SIGNGI*BETA	RMSG132
	AREF(3)=AREF(3)*SIGNFI*BETA	RMSG133
	AREF(4)=AREF(4)*SIGNTI*BETA	RMSG134
	BREF(1,I)=BREF(1,I)*SIGNNI*BETA	RMSG135
	BREF(2,I)=BREF(2,I)*SIGNGI*BETA	RMSG136
	BREF(3,I)=BREF(3,I)*SIGNFI*BETA	RMSG137
	BREF(4,I)=BREF(4,I)*SIGNTI*BETA	RMSG138
	IF(L2=NTR)100,110,110	RMSG139
110	SIGP=0,0	RMSG140
	LRUJK=LRU(I,KK)	RMSG141
	IF(LRUJK=1)1250,1250,125	RMSG142
1250	NLSKK=NLS(I,KK)	RMSG143
	DO 126 LL=1,NLSKK	RMSG144
	LURE=LANG(I,KK,LL)	RMSG145
	SS=FLOAT(LURE)	RMSG146
	CALL FACTS(Q,LURE,PZ,SZ,PS,CONSTA,XWR,API,3,0)	RMSG147
	TRM=(2,0*SS+1,0)*4,0*PI	RMSG148
	TRM=TRM*DSIN(PS)*DSIN(PS)/(CONSTA*CONSTA)	RMSG149
	SIGP=SIGP+TRM	RMSG150
126	CONTINUE	RMSG151
125	AREF(1)=AREF(1)+SIGP*ABN(I)	RMSG152
	AREF(4)=AREF(4)+SIGP*ABN(I)	RMSG153
	BREF(1,I)=BREF(1,I)+SIGP*ABN(I)	RMSG154
	BREF(4,I)=BREF(4,I)+SIGP*ABN(I)	RMSG155
112	CONTINUE	RMSG156
	RETURN	RMSG157
	END	RMSG158

MOCK PU-241	RAMP1 TEST DATA,	0550.0	11	4	1.0E-04	
940241.0	238,9859	0	0	1	1	0
940241.0	1.0	0	1	1	1	0
1.0	20.0	1	3	0	0	0
2.5	0,9772	0	0	1	1	0
238,9859	0.0	0	0	90	15	15
0.160	2.0	0,029E-03	4,0E-02	4,000E-02	2,000E-02	2,000E-02
0.260	3.0	0,051E-03	4,0E-02	5,000E-02	2,500E-02	2,500E-02
4.300	2.0	0,660E-03	4,0E-02	-1,600E-02	1,600E-02	1,600E-02
4.580	3.0	0,430E-03	4,0E-02	8,000E-02	8,000E-02	8,000E-02
5.920	2.0	2,430E-03	4,0E-02	10,000E-02	-35,000E-02	35,000E-02
6.930	3.0	0,710E-03	4,0E-02	3,500E-02	6,000E-02	6,000E-02
8.600	2.0	1,000E-03	4,0E-02	-2,000E-02	6,000E-02	6,000E-02
9.500	3.0	0,180E-03	4,0E-02	-4,000E-02	8,000E-02	8,000E-02
10.100	2.0	1,500E-03	4,0E-02	0,000E-02	90,000E-02	90,000E-02
12.780	3.0	0,790E-03	4,0E-02	20,000E-02	3,500E-02	3,500E-02
13.400	2.0	2,200E-03	4,0E-02	1,400E-02	2,500E-02	2,500E-02
14.750	3.0	6,200E-03	4,0E-02	1,400E-02	1,400E-02	1,400E-02
15.980	2.0	1,520E-03	4,0E-02	40,000E-02	6,500E-02	6,500E-02
16.690	3.0	1,230E-03	4,0E-02	10,000E-02	8,000E-02	8,000E-02
17.830	2.0	3,200E-03	4,0E-02	-0,300E-02	2,000E-02	2,000E-02

PROGRAM RAMP1, PROGRAM TO CALCULATE CROSS-SECTIONS ACCORDING TO THE REICH-MOORE FORMALISM, USES ENDF/B VERSION II

TITLE MOCK PU-241 RAMP1 TEST DATA,

(Z,A) DESIGNATION OF THE ELEMENT 9,4024E+05 AT.WT/MASS OF NEUTRON 2,3899E+02 NO OF ISOTOPES 1

DATA FOR ISOTOPE NUMBER 1

(Z,A) DESIGNATION OF THE ISOTOPE 9,4024E+05 FRACTIONAL ABUNDANCE 1,0000E+00 NO OF ENERGY RANGES 1  
LOWER LIMIT OF THE ENERGY RANGE(EV) 1,0000E+00 UPPER LIMIT(EV) 2,0000E+01 LRU= 1 LRF= 3  
NUCLEAR SPIN 2,5000E+00 SCATTERING LENGTH 9,7720E-01 NO OF L-VALUES 1  
MASS OF THE ISOTOPE IN UNITS OF NEUTRON MASS 2,3899E+02 SCATTERING LENGTH(A-) 0,0000E+00 ANGULAR MOMENTUM 0 NO OF RESO

ERES	SPIN	GN	GGAMMA	GFA	GFB
-1,6000E-01	2,0000E+00	2,9000E-05	4,0000E-02	4,0000E-02	2,0000E+02
2,6000E-01	3,0000E+00	5,1000E-05	4,0000E-02	5,0000E-02	2,5000E-02
4,3000E+00	2,0000E+00	6,6000E-04	4,0000E-02	-1,6000E-02	1,6000E-02
4,5800E+00	3,0000E+00	4,3000E-04	4,0000E-02	8,0000E-02	8,0000E-02
5,9200E+00	2,0000E+00	2,4300E-03	4,0000E-02	1,0000E+00	-3,5000E-01
6,9300E+00	3,0000E+00	7,1000E-04	4,0000E-02	3,5000E-02	6,0000E-02
8,6000E+00	2,0000E+00	1,0000E-03	4,0000E-02	-2,0000E-02	6,0000E-02
9,5000E+00	3,0000E+00	1,8000E-04	4,0000E-02	-4,0000E-02	8,0000E-02
1,0100E+01	2,0000E+00	1,5000E-03	4,0000E-02	0,0000E+00	9,0000E-01
1,2780E+01	3,0000E+00	7,9000E-04	4,0000E-02	2,0000E-01	3,5000E-02
1,3400E+01	2,0000E+00	2,2000E-03	4,0000E-02	1,4000E-02	2,5000E-02
1,4750E+01	3,0000E+00	6,2000E-03	4,0000E-02	1,4000E-02	1,4000E-02
1,5980E+01	2,0000E+00	1,5200E-03	4,0000E-02	4,0000E-01	6,5000E-02
1,6690E+01	3,0000E+00	1,2300E-03	4,0000E-02	1,0000E-01	8,0000E-02
1,7830E+01	2,0000E+00	3,2000E-03	4,0000E-02	-3,0000E-03	2,0000E-02

CROSS-SECTIONS AT THERMAL ENERGY

NEUTRON ENERGY(EV)	SIGNN	SIGCAP	SIGF	SIGTOTAL
2,530000E-02	9,968436E+00	3,062950E+02	5,856657E+02	9,019291E+02

NEUTRON ENERGY(EV)	SIGNN	SIGCAP	SIGF	SIGTOTAL
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1.000000E+00	1.058544E+01	4.900407E+00	6.772793E+00	2.225864E+01
1.036330E+00	1.055058E+01	4.522330E+00	6.920150E+00	2.202306E+01
1.072660E+00	1.051761E+01	4.253114E+00	7.085793E+00	2.185652E+01
1.825000E+00	1.001607E+01	2.271752E+00	1.118875E+01	2.347657E+01
2.650000E+00	9.478008E+00	2.614635E+00	1.666293E+01	2.875557E+01
3.475000E+00	8.536163E+00	5.725111E+00	2.680162E+01	4.106289E+01
4.227340E+00	5.104560E+00	2.650225E+02	1.355504E+02	4.056774E+02
4.263670E+00	8.831456E+00	6.450148E+02	3.402282E+02	9.940745E+02
4.300000E+00	3.043822E+01	1.584601E+03	1.069601E+03	2.684640E+03
4.336330E+00	3.186469E+01	9.107009E+02	9.132591E+02	1.855825E+03
4.370000E+00	2.108056E+01	3.779431E+02	5.675073E+02	9.665309E+02
4.372660E+00	2.052070E+01	3.567806E+02	5.526902E+02	9.299915E+02
4.379570E+00	1.921911E+01	3.099162E+02	5.199569E+02	8.490922E+02
4.440000E+00	1.322645E+01	1.463447E+02	4.368031E+02	5.963742E+02
4.479785E+00	1.177551E+01	1.314830E+02	4.885665E+02	6.318250E+02
4.510000E+00	1.150440E+01	1.400460E+02	5.650123E+02	7.165627E+02
4.580000E+00	1.384179E+01	1.699030E+02	7.029183E+02	8.866631E+02
4.680215E+00	1.510298E+01	8.895554E+01	3.722261E+02	4.762846E+02
4.780430E+00	1.332331E+01	4.045471E+01	2.030781E+02	2.568561E+02
4.372660E+00	1.183322E+01	2.079535E+01	1.519174E+02	1.845459E+02
5.223785E+00	1.036864E+01	1.163614E+01	1.708226E+02	1.928274E+02
5.250000E+00	1.030179E+01	1.147385E+01	1.754491E+02	1.972248E+02
5.585000E+00	9.990475E+00	1.203536E+01	2.565913E+02	2.786171E+02
5.920000E+00	1.065095E+01	1.366816E+01	3.219918E+02	3.463109E+02
6.172500E+00	1.115306E+01	1.348941E+01	3.000274E+02	3.246699E+02
6.425000E+00	1.091760E+01	1.446035E+01	2.438126E+02	2.691905E+02
6.616215E+00	1.004552E+01	2.218022E+01	2.202129E+02	2.524387E+02
6.677500E+00	9.570393E+00	2.959330E+01	2.264784E+02	2.656421E+02
6.794290E+00	8.371799E+00	7.467768E+01	3.153549E+02	3.984044E+02
6.862145E+00	8.879052E+00	1.775740E+02	5.515465E+02	7.379996E+02
6.930000E+00	1.809265E+01	3.452943E+02	9.409558E+02	1.304343E+03
6.997855E+00	2.107452E+01	1.728051E+02	5.203538E+02	7.142335E+02
7.065710E+00	1.792169E+01	7.144360E+01	2.726230E+02	3.619883E+02
7.347500E+00	1.344669E+01	1.236468E+01	1.138863E+02	1.396976E+02
7.765000E+00	1.166345E+01	6.508113E+00	9.027773E+01	1.084493E+02
8.182500E+00	1.025646E+01	1.088876E+01	1.142373E+02	1.353825E+02
8.479000E+00	9.194361E+00	7.555025E+01	3.162147E+02	4.009593E+02
8.539500E+00	1.204646E+01	1.851301E+02	5.432464E+02	7.404229E+02
8.600000E+00	2.572665E+01	3.831015E+02	7.050983E+02	1.113926E+03
8.660500E+00	2.454734E+01	1.891886E+02	1.836176E+02	3.973535E+02
8.721000E+00	1.864061E+01	7.491894E+01	2.864011E+01	1.221997E+02
8.825000E+00	1.468965E+01	2.658259E+01	3.616975E+00	4.488922E+01
9.050000E+00	1.213703E+01	1.003372E+01	2.632857E+01	4.849932E+01
9.275000E+00	1.090433E+01	1.096461E+01	6.047112E+01	8.234005E+01
9.339820E+00	1.054623E+01	1.473751E+01	7.964074E+01	1.049245E+02
9.419910E+00	1.016821E+01	2.829259E+01	1.305088E+02	1.689696E+02
9.500000E+00	1.119660E+01	5.097808E+01	2.142998E+02	2.764744E+02
9.580000E+00	1.216397E+01	2.855911E+01	1.639949E+02	2.047180E+02
9.629250E+00	1.198685E+01	1.877122E+01	1.430153E+02	1.737734E+02
9.650000E+00	1.190027E+01	1.639476E+01	1.395057E+02	1.678008E+02
9.660180E+00	1.186079E+01	1.547843E+01	1.385668E+02	1.659060E+02
9.800000E+00	1.160841E+01	1.061038E+01	1.504076E+02	1.726264E+02
9.950000E+00	1.186901E+01	1.025375E+01	1.728589E+02	1.949816E+02
1.010000E+01	1.242248E+01	1.001515E+01	1.730137E+02	1.954513E+02
1.057075E+01	1.253795E+01	5.386169E+00	6.741065E+01	8.533478E+01
1.077000E+01	1.208537E+01	4.153931E+00	4.115512E+01	5.739442E+01
1.104130E+01	1.147766E+01	3.316095E+00	2.293927E+01	3.773303E+01
1.144000E+01	1.065231E+01	3.060883E+00	1.302784E+01	2.674104E+01
1.211000E+01	9.053921E+00	5.067992E+00	1.926266E+01	3.338657E+01
1.250421E+01	7.469381E+00	1.438958E+01	7.350651E+01	9.536547E+01
1.264210E+01	7.049704E+00	3.017804E+01	1.655657E+02	2.027934E+02







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C      AAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAAADLR123
      DO 1000 J=J1,J3                                ADLR124
              READ4,(ARAY1(K,J),K=1,6)              ADLR125
              READ4,(ARAY2(K,J),K=1,6)              ADLR126
1000  CONTINUE                                       ADLR127
C-----THESE ARE THE ADLER-ADLER RESONANCE PARAMETERS. ADLR128
C-----ARAY1(1,J)=MUT,ARAY1(2,J)=NUT,ARAY1(3,J)=GT,ARAY1(4,J)=HT, ADLR129
C-----ARAY1(5,J)=MUF,ARAY1(6,J)=NUF,ARAY2(1,J)=GF,ARAY2(2,J)=HF, ADLR130
C-----ARAY2(3,J)=MUC,ARAY2(4,J)=NUC,ARAY2(5,J)=GC,ARAY2(6,J)=HC, ADLR131
      PRINT25                                         ADLR132
      PRINT 9                                         ADLR133
      PRINT 25                                        ADLR134
      PRINT30                                        ADLR135
      PRINT23,(ARAY1(1,J),ARAY1(2,J),ARAY1(3,J),ARAY1(4,J),J=J1,J3) ADLR136
      PRINT25                                         ADLR137
      PRINT31                                         ADLR138
      PRINT23,(ARAY1(5,J),ARAY1(6,J),ARAY2(1,J),ARAY2(2,J),J=J1,J3) ADLR139
      PRINT25                                         ADLR140
      PRINT32                                         ADLR141
      PRINT23,(ARAY2(3,J),ARAY2(4,J),ARAY2(5,J),ARAY2(6,J),J=J1,J3) ADLR142
      J1=J1+NLJ                                       ADLR143
      J4=J4+1                                         ADLR144
      IF(J4-NJSIJ)202,202,203                          ADLR145
203  JL=JL+1                                         ADLR146
      PRINT25                                         ADLR147
      IF(NMOM-NLS(I,J2))104,104,103                    ADLR148
103  NRANGE=NRANGE+1                                  ADLR149
      J2=J2+1                                         ADLR150
      IF(NRANGE-NERI)106,106,1010                      ADLR160
1010 NRES(I)=J1-JFIN                                  ADLR161
      JFID=J1                                         ADLR162
101  CONTINUE                                       ADLR163
      NTOTAL=J1+1                                       ADLR164
      PHI=3,14159265                                    ADLR165
      2  FORMAT(26H OPTION TO DOPPLER BROADENIS,26H EFFECTIVE TEMPERATURE(*ADLR166
      1K)F10,3)                                       ADLR167
      3  FORMAT(2E11,4,4I11)                            ADLR168
      4  FORMAT(6E11,4)                                  ADLR169
      8  FORMAT(2X,4(2X,E20,6,2X))                       ADLR170
      9  FORMAT(40H ADLER-ADLER PARAMETERS FOR THIS ISOTOPE) ADLR171
      10 FORMAT(20H ERROR IN INPUT DATA)                ADLR172
      11 FORMAT(44H ADLER-ADLER CROSS-SECTIONS FOR THIS ELEMENT) ADLR173
      12 FORMAT(37H CROSS-SECTIONS NOT DOPPLER BROADENED) ADLR174
      13 FORMAT(33H CROSS-SECTIONS DOPPLER BROADENED)   ADLR175
      14 FORMAT(98H      NEUTRON ENERGY(EV)      TOTAL X-SECTION ADLR176
      1FISSION X-SECTION      CAPTURE X-SECTION) ADLR177
      17 FORMAT(33H (Z,A) DESIGNATION OF THE ELEMENTE11,4,22H AT,WT/MASS OFADLR178
      1 NEUTRONE11,4,15H NO OF ISOTOPEI5) ADLR179
      18 FORMAT(24H DATA FOR ISOTOPE NUMBERI5) ADLR180
      19 FORMAT(33H (Z,A) DESIGNATION OF THE ISOTOPEE11,4,21H FRACTIONAL ABADLR181
      1UNDANCEE11,4,20H NO OF ENERGY RANGEI5) ADLR182
      20 FORMAT(36H LOWER LIMIT OF THE ENERGY RANGE(EV)E11,4,18H  UPPER LIADLR183
      1MIT(EV)E11,4,6H  LRU=15,6H  LRF=15) ADLR184
      21 FORMAT(13H NUCLEAR SPINE11,4,18H SCATTERING LENGTHE11,4,15H NO OF ADLR185
      1L-VALUESI5) ADLR186
      22 FORMAT(41H CONSTANT USED TO CALCULATE PENETRABILITYE11,4,22H SCATTADLR187
      1ERING LENGTH(A-)E11,4,17H ANGULAR MOMENTUMI5,17H NO OF RESONANCESIADLR188
      25) ADLR189
      23 FORMAT(2X,4(E20,6)) ADLR190
      24 FORMAT(11H TITLE      7A4) ADLR191
      25 FORMAT(//) ADLR192

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26	FORMAT(12(1X,F8,5,2X))			ADLR193	
27	FORMAT(33H CROSS-SECTIONS AT THERMAL ENERGY)			ADLR194	
28	FORMAT(4(E13,6,1X,I1))			ADLR195	
29	FORMAT(30H THE BACKGROUND PARAMETERS ARE)			ADLR196	
30	FORMAT(74H	MUT	NUT	GT	ADLR197
	1	HT)			ADLR198
31	FORMAT(74H	MUF	NUF	GF	ADLR199
	1	HF)			ADLR200
32	FORMAT(74H	MUC	NUC	GC	ADLR201
	1	HC)			ADLR202
33	FORMAT(50H BACKGROUND PARAMETERS FOR THE TOTAL CROSS-SECTION)			ADLR203	
34	FORMAT(52H BACKGROUND PARAMETERS FOR THE FISSION CROSS-SECTION)			ADLR204	
35	FORMAT(52H BACKGROUND PARAMETERS FOR THE CAPTURE CROSS-SECTION)			ADLR205	
36	FORMAT(4H A1=E18,6,4H A2=E18,6,4H A3=E18,6,4H A4=E18,6,4H B1=E18,6,4H B2=E18,6)			ADLR206	
37	FORMAT(48H MASS OF THIS ISOTOPE IN UNITS OF NEUTRON MASS E11,4)			ADLR207	
38	FORMAT(4H NX=15,102H IF NX=2 TOTAL AND CAPTURE BCKGRND PARAMETERS GIVEN, IF NX=3 TOTAL, CAPTURE AND FISSION PARAMETERS GIVEN)			ADLR209	
39	FORMAT(35H ANGULAR MOMENTUM OF THE RESONANCES I10,19H NUMBER OF J-SATES I10)			ADLR211	
40	FORMAT(29H J=VALUE FOR THESE RESONANCES F>.2,57H NUMBER OF RESONANCES FOR THE ABOVE L-VALUE AND THIS J ISI10)			ADLR213	
41	FORMAT(4H LI=15,109H IF LI=5 TOTAL AND CAPTURE, LI=6 FISSION AND CAPTURE, AND LI=7 TOTAL CAPTURE AND FISSION CROSS-SECTIONS GIVEN)			ADLR215	
42	FORMAT(106H1 PROGRAM ADLER, CALCULATES CROSS-SECTIONS FROM ADLER-ADLER PARAMETERS WITH OPTION FOR DOPPLER BROADENING,)			ADLR217	
43	FORMAT(24H ENDF/B VERSION II DATA,)			ADLR218	
	DO 108 I=1,NTOTAL			ADLR219	
	TERM1=ARAY1(1,I)			ADLR220	
	TERM2=ARAY1(2,I)			ADLR221	
	IF(TERM1,EQ,0,0,OR,TERM2,EQ,0,0)GO TO 1080			ADLR222	
	GO TO 1081			ADLR223	
1080	TERM1=ARAY1(5,I)			ADLR224	
	TERM2=ARAY1(6,I)			ADLR225	
	IF(TERM1,EQ,0,0,OR,TERM2,EQ,0,0)GO TO 1082			ADLR226	
	GO TO 1083			ADLR2261	
1081	ERAN(1,I)=TERM1			ADLR227	
	ERAN(2,I)=TERM2			ADLR228	
	GO TO 108			ADLR229	
1082	TERM1=ARAY2(3,I)			ADLR230	
	TERM2=ARAY2(4,I)			ADLR231	
	IF(TERM1,EQ,0,0,OR,TERM2,EQ,0,0)GO TO 1084			ADLR232	
	GO TO 1085			ADLR2321	
1083	ERAN(1,I)=TERM1			ADLR233	
	ERAN(2,I)=TERM2			ADLR234	
	GO TO 108			ADLR235	
1084	PRINT10			ADLR236	
	GO TO 130			ADLR237	
1085	ERAN(1,I)=TERM1			ADLR238	
	ERAN(2,I)=TERM2			ADLR239	
108	CONTINUE			ADLR240	
	CALL QIKS(1,NTOTAL,MOV,KOM)			ADLR241	
	PRINT11			ADLR242	
	PRINT25			ADLR243	
	PRINT27			ADLR244	
	PRINT25			ADLR245	
	PRINT14			ADLR246	
	PRINT25			ADLR247	
	E=ETHERM			ADLR248	
	CALL ADSIGMA(E,NIS,1,0)			ADLR249	
	PRINT8,E,(AREF(LL),LL=1,3)			ADLR250	

PRINT25	ADLR251
IF(IDPL.EQ.1)GOTO1500	ADLR252
PRINT12	ADLR253
PRINT25	ADLR254
GO TO 1501	ADLR255
1500 PRINT13	ADLR256
PRINT25	ADLR257
1501 PRINT14	ADLR258
PRINT25	ADLR259
120 CONTINUE	ADLR260
DO 124 JJ=1,NIS	ADLR261
NERJJ=NER(JJ)	ADLR262
DO 125 KK=1,NERJJ	ADLR263
IRANGE=KK	ADLR264
LRUJK=LRU(JJ,KK)	ADLR265
IF(LRUJK-1)131,1321,125	ADLR266
131 PRINT10	ADLR267
GO TO 130	ADLR268
1321 IF(JJ.EQ.1)GO TO 1320	ADLR269
GO TO 132	ADLR270
1320 ELOREF=EL(JJ,KK)	ADLR271
EHIREF=EH(JJ,KK)	ADLR272
ELO=ELOREF	ADLR273
EHI=EHIREF	ADLR274
GO TO 1240	ADLR275
132 ELO=EL(JJ,KK)	ADLR276
EHI=EH(JJ,KK)	ADLR277
IF(ELO.EQ.ELOREF.AND.EHI.EQ.EHIREF)GO TO 124	ADLR278
GO TO 1240	ADLR279
1240 MM=MAXPTS/(4*MAXRES)	ADLR280
NN=MM	ADLR281
IFLAG=1	ADLR282
NLSKK=NLS(JJ,KK)	ADLR283
J4=1	ADLR284
ISTART=1	ADLR285
IEND=1	ADLR286
117 IF(IEND.EQ.0)GO TO 125	ADLR287
J5=J4+1	ADLR288
E1=ERAN(1,J4)	ADLR289
G1=ERAN(2,J4)	ADLR290
E2=ERAN(1,J5)	ADLR291
G2=ERAN(2,J5)	ADLR292
IF(E1.LT.ELO.AND.E2.LT.ELO)GO TO 1120	ADLR293
GO TO 1105	ADLR294
1105 IF(E1.LE.ELO.AND.E2.GT.ELO)GO TO 1110	ADLR295
GO TO 1111	ADLR296
1110 E1=ELO	ADLR297
G1=G2	ADLR298
ISTART=0	ADLR299
GO TO 1114	ADLR300
1111 IF(E1.GT.ELO.AND.E2.LE.EHI)GO TO 1112	ADLR301
GO TO 1113	ADLR302
1112 IF(J4.EQ.1.AND.ISTART.EQ.1)GO TO 1106	ADLR303
GO TO 1114	ADLR304
1106 E2=E1	ADLR305
G2=G1	
E1=ELO	
J4=J4-1	
ISTART=0	
GO TO 1114	
1116 E2=EHI+G1/FLOAT (MM)	

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1113 IF(E1,LT,EHI,AND,E2,GE,EHI)GO TO 1123
GO TO 1124
1123 E2=EHI
G2=G1
IEND=0
GO TO 1114
1124 IF(E1,GE,EHI,AND,E2,GT,EHI)GO TO 125
GO TO 1125
1125 IF(IFLAG)1120,125,1120
1114 IF(E1,EQ,E2)GO TO 1120
GO TO 1118
1118 CONTINUE
CALL STEVE(E1,G1,E2,G2,MH,NN,NX,TEFF,AWR)
CALL QIKS(1,NX,MOVE,KOME)
GO TO 116
1120 IF(IEND.EQ,0)GO TO 125
J4=J4+1
GO TO 117
116 DO 109 I=1,NX
E=EX(I)
JFLAG1=JFLAG(I)
CALL ADSIGMA(E,NIS,KK,1DPL)
PRINT8,E,(AREF(LL),LL=1,3)
109 CONTINUE
IF(IFLAG)1117,125,1117
1117 J4=J4+1
IF(NTOTAL-J4)125,1250,117
1250 E1=ERAN(1,J4)
G1=ERAN(2,J4)
GO TO 1116
125 CONTINUE
124 CONTINUE
130 CALL EXIT
END
SUBROUTINE ADSIGMA(Q,NIT,KK,1DPL)
COMMON/D/ERAN(2,501)
COMMON/C/EX(101),JFLAG(101)
COMMON ARAY(6,500),ARAY2(6,500),NOT(20),ZAI(20),ABN(10),
1NER(10),LFW(10),EL(10,10),EH(10,10),LRU(10,10),LRF(10,10),
2LANG(10,5,5),NLS(10,10),NRES(10),SPI(10),AP(10),LIS(10),AM(10),
3AWRJ(10),LI(10),NXX(10),ABG(10,6,3),NJS(10,5,5),AJ(10,5,5),
4AREF(6),TEFF,DELTA,E
TEFF=TEFF/293.0
E12=SQRT(Q)
T1=1.0/E12
N2=0
NTR=0
DO 4 J=1,6
AREF(J)=0.0
4 CONTINUE
DO 112 I=1,NIT
LT=1
LC=1
LF=1
LI=LI(I)
IF(LI=5)500,501,502
500 PRINT1005
1005 FORMAT(23H ERROR INPUT DATA LI(1))
ADLR309
ADLR3091
ADLR310
ADLR310
ADLR311
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GO TO 112	ADSG025
501 LF=0	ADSG026
GO TO 600	ADSG027
502 IF(LII-6)500,503,504	ADSG028
503 LT=0	ADSG029
GO TO 600	ADSG030
504 IF(LII-7)500,505,500	ADSG031
505 CONTINUE	ADSG032
600 NRESI=NRES(I)	ADSG033
API=AP(I)	ADSG034
AWRJI=AWRJ(I)	ADSG035
WN=2.196771E-03*(AWRJI/(AWRJI+1.0))*API	ADSG036
WAVE=2.196771E-03*(AWRJI/(AWRJI+1.0))	ADSG037
CC=1.0/(WAVE**2)	ADSG038
CC=CC*3.1415927	ADSG039
BELTA=0.3177*SQRT((TEF*Q)/AWRJI)	ADSG040
IF(IDPL.EQ.0)GO TO 700	ADSG0401
BETA=(CC*1.7724538)/BELTA	ADSG041
700 XOMEGA=2.0*WN*F12	ADSG042
SIGT=0.0	ADSG043
SIGC=0.0	ADSG044
SIGF=0.0	ADSG045
NXXI=NXX(I)	ADSG046
IF(NXXI.EQ.2)GO TO 1000	ADSG047
GO TO 1001	ADSG0471
1000 TAILT=ABG(I,1,1)+(ABG(I,2,1)/Q)+(ABG(I,3,1)/(Q**2))+	ADSG048
1(ABG(I,4,1)/(Q**3))+ABG(I,5,1)*Q+ABG(I,6,1)*Q*Q	ADSG049
TAILT=TAILT*CC/E12	ADSG050
TAILC=ABG(I,1,2)+(ABG(I,2,2)/Q)+(ABG(I,3,2)/(Q**2))+	ADSG051
1(ABG(I,4,2)/(Q**3))+ABG(I,5,2)*Q+ABG(I,6,2)*Q*Q	ADSG052
TAILC=TAILC*CC/E12	ADSG053
TAILF=0.0	ADSG054
GO TO 1010	ADSG055
1001 IF(NXXI.EQ.3)GO TO 1002	ADSG056
GO TO 1003	ADSG0561
1002 TAILT=ABG(I,1,1)+(ABG(I,2,1)/Q)+(ABG(I,3,1)/(Q**2))+	ADSG057
1(ABG(I,4,1)/(Q**3))+ABG(I,5,1)*Q+ABG(I,6,1)*Q*Q	ADSG058
TAILT=TAILT*CC/E12	ADSG059
TAILF=ABG(I,1,2)+(ABG(I,2,2)/Q)+(ABG(I,3,2)/(Q**2))+	ADSG060
1(ABG(I,4,2)/(Q**3))+ABG(I,5,2)*Q+ABG(I,6,2)*Q*Q	ADSG061
TAILF=TAILF*CC/E12	ADSG062
TAILC=ABG(I,1,3)+(ABG(I,2,3)/Q)+(ABG(I,3,3)/(Q**2))+	ADSG063
1(ABG(I,4,3)/(Q**3))+ABG(I,5,3)*Q+ABG(I,6,3)*Q*Q	ADSG064
TAILC=TAILC*CC/E12	ADSG065
GO TO 1010	ADSG066
1003 PRINT1004	ADSG067
1004 FORMAT(24H ERROR INPUT DATA NXX(I))	ADSG068
1010 N1=N2+1	ADSG069
N2=N2+NRESI	ADSG070
DO 108 K=N1,N2	ADSG071
IF(LT.EQ.0)GO TO 300	ADSG072
XMUT=ARRAY1(1,K)	ADSG073
XNUT=ARRAY1(2,K)	ADSG074
XGT=ARRAY1(3,K)	ADSG075
XHT=ARRAY1(4,K)	ADSG076
S1=XGT*COS(XOMEGA)+XHT*SIN(XOMEGA)	ADSG077
S2=XHT*COS(XOMEGA)-XGT*SIN(XOMEGA)	ADSG078
IF(IDPL.EQ.0)GO TO 201	ADSG079
GO TO 202	ADSG0791
201 DEN=(XMUT=Q)**2+(XNUT**2)	ADSG080
TERM=(XNUT*S1+(XMUT=Q)*S2)/DEN	ADSG081

	SIGT=SIGT+(TERM*CC*T1)	ADSG082
	GO TO 300	ADSG083
202	SXI=(XMUT-Q)/BELTA	ADSG084
	ETA=XNUT/BELTA	ADSG085
	CALL PFCN(SXI,ETA,U,V)	ADSG086
	TERM=T1*(S1*U+S2*V)	ADSG087
	SIGT=SIGT+TERM*BETA	ADSG088
300	IF(LF,EQ,0)GO TO 400	ADSG089
	XMUF=ARAY1(5,K)	ADSG090
	XNUF=ARAY1(6,K)	ADSG091
	XGF=ARAY2(1,K)	ADSG092
	XHF=ARAY2(2,K)	ADSG093
	IF(IDPL-EQ,0)GO TO 301	ADSG094
	GO TO 302	ADSG0941
301	DEN=(XMUF-Q)**2+(XNUF**2)	ADSG095
	TERM=(XNUF*XGF+(XMUF-Q)*XHF)/DEN	ADSG096
	SIGF=SIGF+TERM*CC*T1	ADSG097
	GO TO 400	ADSG098
302	SXI=(XMUF-Q)/BELTA	ADSG099
	ETA=XNUF/BELTA	ADSG100
	CALL PFCN(SXI,ETA,U,V)	ADSG101
	TERM=T1*(U*XGF+V*XHF)	ADSG102
	SIGF=SIGF+TERM*BETA	ADSG103
400	IF(LC,EQ,0)GO TO 108	ADSG104
	XMUC=ARAY2(3,K)	ADSG105
	XMUC=ARAY2(3,K)	ADSG106
	XNUC=ARAY2(4,K)	ADSG107
	XGC=ARAY2(5,K)	ADSG108
	XHC=ARAY2(6,K)	ADSG109
	IF(IDPL-EQ,0)GO TO 401	ADSG110
	GO TO 402	ADSG1101
401	DEN=(XMUC-Q)**2+(XNUC**2)	ADSG111
	TERM=(XNUC*XGC+(XMUC-Q)*XHC)/DEN	ADSG112
	SIGC=SIGC+TERM*CC*T1	ADSG113
	GO TO 108	ADSG114
402	SXI=(XMUC-Q)/BELTA	ADSG115
	ETA=XNUC/BELTA	ADSG116
	CALL PFCN(SXI,ETA,U,V)	ADSG117
	TERM=T1*(U*XGC+V*XHC)	ADSG118
	SIGC=SIGC+TERM*BETA	ADSG119
108	CONTINUE	ADSG120
	SIGP=(2-Q/Q)*(1,0-COS(XOMEGA))*CC	ADSG121
	SIGT=SIGT+SIGP	ADSG122
	SIGT=SIGT+TAILT	ADSG123
	SIGF=SIGF+TAILF	ADSG124
	SIGC=SIGC+TAILC	ADSG125
	IF(LT,EQ,0)SIGT=0,0	ADSG126
	AREF(1)=AREF(1)+ABN(I)*SIGT	ADSG127
	AREF(2)=AREF(2)+ABN(I)*SIGF	ADSG128
	AREF(3)=AREF(3)+ABN(I)*SIGC	ADSG129
112	CONTINUE	ADSG130
	RETURN	ADSG131
	END	ADSG132
	SUBROUTINE SIEVE(E1,G1,E2,G2,M,N,NX,SEFF,BWR)	SIEV001
	COMMON/C/EX(101),JFLAG(101)	SIEV002
	IF(E2.LT,E1)GO TO 101	SIEV003
	GO TO 300	SIEV0031
300	N2=2*N	SIEV004
	DO 1000 I=1,100	SIEV005
	JFLAG(I)=2	SIEV006
1000	CONTINUE	SIEV007

	TEF=SEFF/293,0	SIEV008
	DP=(1.5885E+00)*SQRT (TEF/BWR)	SIEV009
C	WHEN MULTIPLIED BY SQRT(E) DP GIVES 5 TIMES CORRESPONDING DELTA	SIEV010
	DP1=DP*SQRT(E1)	SIEV011
	DP2=DP*SQRT (E2)	SIEV012
	DG1=G1/FLOAT (M)	SIEV013
	DG2=G2/FLOAT (M)	SIEV014
	EX(1)=E1	SIEV015
	IF(G1.LT,DP1)GO TO 1001	SIEV016
	GO TO 1002	SIEV0161
1001	JFLAG(1)=1	SIEV017
1002	ENDIF=ABS (E2-E1)	SIEV018
	NX=1	SIEV019
	DO 100 I=1,N	SIEV020
	XX=E1+DG1*FLOAT (I)	SIEV021
	IF(XX.LT,E2)GO TO 107	SIEV022
	GO TO 100	SIEV0221
107	NX=NX+1	SIEV023
	EX(NX)=XX	SIEV024
	IF(G1.LT,DP1)GO TO 1003	SIEV025
	GO TO 100	SIEV0251
1003	JFLAG(NX)=1	SIEV026
100	CONTINUE	SIEV027
	DO 200 I=1,N	SIEV028
	XX=E2-DG2*FLOAT (I)	SIEV029
	IF(XX.GT,E1)GO TO 108	SIEV030
	GO TO 200	SIEV0301
108	NX=NX+1	SIEV031
	EX(NX)=XX	SIEV032
	IF(G2.LT,DP2)GO TO 1005	SIEV033
	GO TO 200	SIEV0331
1005	JFLAG(NX)=1	SIEV034
200	CONTINUE	SIEV035
110	DIFF=(E2-E1)/FLOAT (N2)	SIEV036
	IF(DIFF)101,101,102	SIEV037
101	PRINT103	SIEV038
	GO TO 104	SIEV039
103	FORMAT(32H CALLING SEQUENCE OF SIEVE WRONG)	SIEV040
102	N21=NX+1	SIEV041
	NN=NX	SIEV042
	N22=N21+N2-2	SIEV043
	NX=N22	SIEV044
	E21=(E1+E2)/2,0	SIEV045
	DP12=DP*SQRT (E21)	SIEV046
	E43=E2-E1=((G1+G2)/2,0)	SIEV047
	IF(E43.LT,DP12)GO TO 1006	SIEV048
	GO TO 1007	SIEV0481
1006	DO 111 I=N21,N22	SIEV049
	I2=I-NN	SIEV050
	EX(I)=E1+DIFF*FLOAT (I2)	SIEV051
	JFLAG(I)=1	SIEV052
111	CONTINUE	SIEV053
	GO TO 1040	SIEV054
1007	DO 112 I=N21,N22	SIEV055
	I2=I-NN	SIEV056
	EX(I)=E1+DIFF*FLOAT (I2)	SIEV057
	DPTEST=DP*SQRT (EX(I))	SIEV058
	IF(EX(I),LE,E21)GO TO 1008	SIEV059
	GO TO 1009	SIEV0591
1008	IF(G1.LT,DPTEST)GO TO 1010	SIEV060
	GO TO 112	SIEV0601



1010	JFLAG(I)=1	SIEV061
	GO TO 112	SIEV062
1009	IF(G2.LT,DPTEST)GO TO 1011	SIEV063
	GO TO 112	SIEV0631
1011	JFLAG(I)=1	SIEV064
112	CONTINUE	SIEV065
1040	DO 113 I=1,NX	SIEV066
	DPF=DP*SQRT (EX(I))	SIEV067
	IF(DPF,EQ,0,0)GO TO 113	SIEV0671
	TERM=EX(I)/DPF	SIEV068
	IF(TERM LT,5,0)GO TO 114	SIEV069
	GO TO 113	SIEV0691
114	JFLAG(I)=1	SIEV070
113	CONTINUE	SIEV071
104	RETURN	SIEV072
	END	SIEV073
	SUBROUTINE PFCN(SXI,ETA,U,V)	PFCN0001
CPFC2	SUBROUTINE TO EVALUATE THE COMPLEX PROBABILITY INTEGRAL	PFCN0002
C	AS A CONTOUR INTEGRAL	PFCN0003
	UREF(Z)=(H/PHI)*(Y1*EXP (-(Z**2)))/((X1-Z)**2+Y1**2))	PFCN0005
	VIMF(Z)=(H/PHI)*((X1-Z)*EXP (-(Z**2)))/((X1-Z)**2+Y1**2))	PFCN0006
	TANF(Z)=SIN(Z)/COS(Z)	PFCN0007
	VALF(Z)=(0,56419139392619+Z*(29,33733781>464+Z*(563,226>17080	PFCN0008
	114+Z*(5026,5043121835+Z*(21563,202428660+Z*(41170,756829233+	PFCN0009
	2Z*(27662,791034654+Z*(2810,0614940005)))))/(1,0+Z*(52,5	PFCN0010
	3+Z*(1023,75+Z*(9384,375+Z*(42229,6875+Z*(88682,34375	PFCN0011
	4+Z*(73901,953125+Z*(15836,1328125))))))	PFCN0012
	TERROR=1,0E=07	PFCN0013
	PHI=3,1415926536	PFCN0014
	X1=ABS(SXI)	PFCN0015
	Y1=ABS(ETA)	PFCN0016
	IF (X1) 11,22,11	PFCN0017
11	IF (Y1) 77,99,77	PFCN0018
99	IF (X1-2,0) 991,991,992	PFCN0019
992	IF (X1-5,9) 9921,9922,9922	PFCN0020
9922	I=0	PFCN0021
	DWSN=0,0	PFCN0022
	DW=1,0	PFCN0023
993	I=I+1	PFCN0024
	GIG=1	PFCN0025
	DW=DW*((2,0*GIG-1,0)/(2,0*(X1**2)))	PFCN0026
	IF (DW=TERROR) 994,994,995	PFCN0027
995	DWSN=DWSN+DW	PFCN0028
	GO TO 993	PFCN0029
994	DWSN=DWSN+1,0	PFCN0030
	DWSN=(DWSN)/(2,0*X1)	PFCN0031
	IF (SXI) 9941,9941,9942	PFCN0032
9941	U=EXP (-(X1**2))	PFCN0033
	V=((2,0)/SQRT (PHI))*DWSN	PFCN0034
	V=-V	PFCN0035
	GO TO 88	PFCN0036
9942	U=EXP (-(X1**2))	PFCN0037
	V=((2,0)/SQRT (PHI))*DWSN	PFCN0038
	GO TO 88	PFCN0039
9921	I=0	PFCN0040
	DWSN=0,0	PFCN0041
	AXE=(0,1)/(X1**2)	PFCN0042
9923	I=I+1	PFCN0043
	GIG=1	PFCN0044
	GIG=2,0*GIG-1,0	PFCN0045
	GIG=GIG*GIG	PFCN0046

	TERM=(EXP (-(GIG*AXE*(X1**2)))/(GIG*AXE-1,0)	PFCN0047
	ABSTRM=ABS (TERM)	PFCN0048
	IF (ABSTRM-TERROR) 9925,9925,9924	PFCN0049
9924	DWSN=DWSN+TERM	PFCN0050
	GO TO 9923	PFCN0051
9925	DWSN=(2.0)*SQRT (AXE/PHI)*DWSN	PFCN0052
	DWSN1=(0.5)*SQRT (PHI)*EXP (-(X1**2))*TANF(PHI/(2.0*SQRT (AXE)))	PFCN0053
	DWSN=-DWSN	PFCN0054
	DWSN=DWSN+DWSN1	PFCN0055
	IF (SX1) 9926,9926,9927	PFCN0056
9926	U=EXP (-(X1**2))	PFCN0057
	V=((2.0)/SQRT (PHI))*DWSN	PFCN0058
	V=-V	PFCN0059
	GO TO 88	PFCN0060
9927	U=EXP (-(X1**2))	PFCN0061
	V=((2.0)/SQRT (PHI))*DWSN	PFCN0062
	GO TO 88	PFCN0063
991	I=0	PFCN0064
	DWSN=0,0	PFCN0065
	DW=(1,0)	PFCN0066
996	I=I+1	PFCN0067
	GIG=I	PFCN0068
	DW=DW*((2.0*(X1**2))/(2.0*GIG-1,0))	PFCN0069
	DW=-DW	PFCN0070
	ABSOW=ABS (DW)	PFCN0071
	IF (ABSOW-TERROR) 997,997,998	PFCN0072
998	DWSN=DWSN+DW	PFCN0073
	GO TO 996	PFCN0074
997	DWSN=DWSN/(2.0*X1)	PFCN0075
	IF (SX1) 9971,9971,9972	PFCN0076
9971	U=EXP (-(X1**2))	PFCN0077
	V=((2.0)/SQRT (PHI))*DWSN	PFCN0078
	V=-V	PFCN0079
	GO TO 88	PFCN0080
9972	U=EXP (-(X1**2))	PFCN0081
	V=((2.0)/SQRT (PHI))*DWSN	PFCN0082
	GO TO 88	PFCN0083
22	IF (ETA) 44,55,66	PFCN0084
44	IF (Y1-1.5)444,445,445	PFCN0085
444	U=EXP (Y1**2)*(1,0+ERRORF(Y1))	PFCN0086
	V=0,0	PFCN0087
	GO TO 88	PFCN0088
445	X2=1,0/(Y1*Y1)	PFCN0089
	U=2,0*EXP (Y1**2)*(VALF(X2)/Y1)	PFCN0090
	V=0,0	PFCN0091
	GO TO 88	PFCN0092
55	U=1,0	PFCN0093
	V=0,0	PFCN0094
	GO TO 88	PFCN0095
66	IF (Y1-1.5)664,665,665	PFCN0096
664	U=EXP (Y1**2)*(1,0+ERRORF(Y1))	PFCN0097
	V=0,0	PFCN0098
	GO TO 88	PFCN0099
665	X2=1,0/(Y1*Y1)	PFCN0100
	U=VALF(X2)/Y1	PFCN0101
	V=0,0	PFCN0102
	GO TO 88	PFCN0103
77	IF (X1-0.04)770,770,771	PFCN0104
770	IF (Y1-0.04)772,772,771	PFCN0105
772	H=0,5	PFCN0106
	GO TO 773	PFCN0107

771	RHO=SQRT (X1**2+Y1**2)	PFCN0108
	TERL=ALOG(TERROR)	PFCN0109
	RHO1=PHI*PHI=Y1*Y1	PFCN0110
	IF (RHO1=0,1)1011,1012,1012	PFCN0111
1011	RHO1=0,1	PFCN0112
1012	RHO1=ABS (RHO1)	PFCN0113
	RHO2=ALOG((1,13*RHO)/RHO1)	PFCN0114
	H1=PHI/SQRT (RHO2-TERL)	PFCN0115
	RHO3=(PHI/H1)**2=Y1*Y1	PFCN0116
	IF (RHO3=0,1)1021,1022,1022	PFCN0117
1021	RHO3=0,1	PFCN0118
1022	RHO3=ABS (RHO3)	PFCN0119
	RHO4=ALOG((1,13*RHO)/RHO3)	PFCN0120
	H=PHI/SQRT (RHO4-TERL)	PFCN0121
773	AL=-(2,0)*PHI*Y1/H	PFCN0122
	BM=(2,0)*X1*Y1	PFCN0123
	CN=(2,0)*PHI*X1/H	PFCN0124
	T=0,0	PFCN0125
	AU=UREF(0,0)	PFCN0126
	UPOS=0,0	PFCN0127
123	T=T+H	PFCN0128
	UT=UREF(T)	PFCN0129
	IF (UT=TERROR) 122,122,1231	PFCN0130
1231	UPOS=UPOS+UT	PFCN0131
	GO TO 123	PFCN0132
122	UNEG=0,0	PFCN0133
	S=0,0	PFCN0134
125	S=S-H	PFCN0135
	US=UREF(S)	PFCN0136
	IF (US=TERROR) 124,124,1241	PFCN0137
1241	UNEG=UNEG+US	PFCN0138
	GO TO 125	PFCN0139
124	AU=AU+UPOS+UNEG	PFCN0140
	GO TO 126	PFCN0141
126	VPOS=0,0	PFCN0142
	AV=VIMF(0,0)	PFCN0143
	T=0,0	PFCN0144
128	T=T+H	PFCN0145
	VT=VIMF(T)	PFCN0146
	ABSPT=ABS (VT)	PFCN0147
	IF (ABSPT=TERROR) 127,127,1271	PFCN0148
1271	VPOS=VPOS+VT	PFCN0149
	GO TO 128	PFCN0150
127	S=0,0	PFCN0151
	VNEG=0,0	PFCN0152
130	S=S-H	PFCN0153
	VS=VIMF(S)	PFCN0154
	ABSPS=ABS (VS)	PFCN0155
	IF (ABSPS=TERROR) 129,129,1291	PFCN0156
1291	VNEG=VNEG+VS	PFCN0157
	GO TO 130	PFCN0158
129	AV=AV+VPOS+VNEG	PFCN0159
	U1=AU	PFCN0160
	V1=AV	PFCN0161
	POLR=(2,0*EXP (Y1**2-X1**2)*(EXP (2,0*AL)*COS (BM)-EXP (AL)*	PFCN0162
	1COS (CN-BM)))/(1,0-2,0*EXP (AL)*COS (CN)+EXP (2,0*AL))	PFCN0163
	POLI=-((2,0*EXP (Y1**2-X1**2)*(EXP (2,0*AL)*SIN (BM)*EXP (AL)*	PFCN0164
	1SIN (CN-BM)))/(1,0-2,0*EXP (AL)*COS (CN)+EXP (2,0*AL))	PFCN0165
	PHIH=PHI/H	PFCN0166
	IF (Y1-PHIH) 300,400,500	PFCN0167
300	A=1,0	PFCN0168

B=1,0	PFCN0169
GO TO 600	PFCN0170
400 A=0,5	PFCN0171
B=0,5	PFCN0172
GO TO 600	PFCN0173
500 A=0,0	PFCN0174
B=0,0	PFCN0175
600 U1=U1+A*POLR	PFCN0176
V1=V1+B*POLI	PFCN0177
GO TO 33	PFCN0178
33 IF (SX1) 331,88,333	PFCN0179
331 IF (ETA) 441,88,443	PFCN0180
333 IF (ETA) 661,88,663	PFCN0181
441 U=2,0*EXP (Y1**2-X1**2)*COS (2,0*X1*Y1)=U1	PFCN0182
V=-2,0*EXP (Y1**2-X1**2)*SIN (2,0*X1*Y1)-V1	PFCN0183
GO TO 88	PFCN0184
443 U=U1	PFCN0185
V=-V1	PFCN0186
GO TO 88	PFCN0187
661 U=2,0*EXP (Y1**2-X1**2)*COS (2,0*X1*Y1)=U1	PFCN0188
V=2,0*EXP (Y1**2-X1**2)*SIN (2,0*X1*Y1)+V1	PFCN0189
GO TO 88	PFCN0190
663 U=U1	PFCN0191
V=V1	PFCN0192
88 RETURN	PFCN0193
END	PFCN0194
FUNCTION ERRORF(X)	ERRF001
DATA P,A1,A2,A3,A4,A5/0,3275911,0,254829>92,0,284496736,	ERRF002
1 1,421413741,-1,453152027,1,061405429/	ERRF003
T=1,0/(1,0+P*X)	ERRF004
ERRORF=1,0-(((A5*T+A4)*T+A3)*T+A2)*T+A1)*T*EXP(-X**2)	ERRF005
RETURN	ERRF006
END	ERRF007
SUBROUTINE MOV(I,J)	MOV001
COMMON/D/ERAN(2,501)	MOV002
I1=I	MOV003
J1=J	MOV004
IF(I1.EQ,0)I1=501	MOV005
IF(J1.EQ,0)J1=501	MOV006
ERAN(1,J1)=ERAN(1,I1)	MOV007
ERAN(2,J1)=ERAN(2,I1)	MOV008
RETURN	MOV009
END	MOV010
SUBROUTINE MOVE(I,J)	MOVE001
COMMON/C/EX(101),JFLAG(101)	MOVE002
I1=I	MOVE003
J1=J	MOVE004
IF(I1.EQ,0)I1=101	MOVE005
IF(J1.EQ,0)J1=101	MOVE006
EX(J1)=EX(I1)	MOVE007
JFLAG(J1)=JFLAG(I1)	MOVE008
RETURN	MOVE009
END	MOVE010
FUNCTION KOM(I,J)	KOM001
COMMON/D/ERAN(2,501)	KOM002
I1=I	KOM003
J1=J	KOM004
IF(I1.EQ,0)I1=501	KOM005
IF(J1.EQ,0)J1=501	KOM006
EOM=ERAN(1,I1)-ERAN(1,J1)	KOM007
IF(EOM)100,101,102	KOM008

100	KOM=1	KOM009
	GO TO 103	KOM010
101	KOM=0	KOM011
	GO TO 103	KOM012
102	KOM=1	KOM013
103	RETURN	KOM014
	END	KOM015
	FUNCTION KOME(I,J)	KOME001
	COMMON/C/EX(101),JFLAG(101)	KOME002
	I1=I	KOME003
	J1=J	KOME004
	IF(I1.EQ.0)I1=101	KOME005
	IF(J1.EQ.0)J1=101	KOME006
	EOX=EX(I1)-EX(J1)	KOME007
	IF(EOX)100,101,102	KOME008
100	KOME=1	KOME009
	GO TO 103	KOME010
101	KOME=0	KOME011
	GO TO 103	KOME012
102	KOME=1	KOME013
103	RETURN	KOME014
	END	KOME015
	SUBROUTINE QIKS (MM,NN,MOVE,COMPAR)	QIKS0010
CQIKS	ALL=IN-MEMORY SORT PROGRAM	QIKS0020
C	MM = FIRST SUBSCRIPT	QIKS0030
C	NN = LAST SUBSCRIPT (ARRAY IS IN COMMON)	QIKS0040
C	MOVE AND COMPARE ARE USER SUPPLIED PROGRAMS	QIKS0050
	DIMENSION MSAVE(20),NSAVE(20)	QIKS0060
	KEYLOC(M,N)=(N+M)/2	QIKS0070
	I=0	QIKS0080
	J=0	QIKS0090
	LEVEL = 0	QIKS0100
	M=MM	QIKS0110
	N=NN	QIKS0120
35	CONTINUE	QIKS0130
C	TEST FOR ONE OR TWO ITEMS	QIKS0140
	IF(N=M-1) 31,51,32	QIKS0150
C	32 CONTINUE	QIKS0160
C	PARTITION AND SPREADER GO HERE, SEE BELOW, RETURN IS TO 8	QIKS0170
C	PUSH DOWN	QIKS0180
8	LEVEL=LEVEL+1	QIKS0190
C	WORK ON SMALLEST PORTION	QIKS0200
	IF ((J-M) - (N-I)) 134, 134, 34	QIKS0210
134	MSAVE(LEVEL) = I	QIKS0220
	NSAVE(LEVEL)=N	QIKS0230
	N=J	QIKS0240
	GO TO 35	QIKS0250
34	MSAVE(LEVEL)=M	QIKS0260
	NSAVE(LEVEL)=J	QIKS0270
	M=I	QIKS0280
	GO TO 35	QIKS0290
51	IF(COMPARE(M,N))31,31,131	QIKS0300
C	SWAP IF ONLY TWO ITEMS ARE OUT OF ORDER	QIKS0310
131	CALL MOVE(M,0)	QIKS0320
	CALL MOVE(N,M)	QIKS0330
	CALL MOVE(0,N)	QIKS0340
31	IF (LEVEL) 151, 150, 151	QIKS0350
150	RETURN	QIKS0360
C	POP UP	QIKS0370
151	M = MSAVE(LEVEL)	QIKS0380
	N=NSAVE(LEVEL)	QIKS0390

	LEVEL=LEVEL-1	QIKS0400
	GO TO 35	QIKS0410
C	END MAIN	QIKS0420
C	PARTITION	QIKS0430
	32 I=M	QIKS0440
	J=N	QIKS0450
	KEY=KEYLOC(M,N)	QIKS0460
	CALL MOVE(KEY, 0)	QIKS0470
	54 IF (N - KEY) 17, 1, 17	QIKS0480
	17 CALL MOVE(N,KEY)	QIKS0490
	1 CONTINUE	QIKS0500
C	HOLE AT BOTTOM	QIKS0510
	IF(COMPARE(0,I))3,2,2	QIKS0520
	2 I=I+1	QIKS0530
	IF (I - J) 1, 4, 1	QIKS0540
	3 CALL MOVE(I,J)	QIKS0550
	GO TO 5	QIKS0560
	6 CONTINUE	QIKS0570
C	HOLE AT TOP	QIKS0580
	IF(COMPARE(0,J))5,5,7	QIKS0590
	5 J=J-1	QIKS0600
	IF (I - J) 6, 4, 6	QIKS0610
	7 CALL MOVE(J,I)	QIKS0620
	GO TO 2	QIKS0630
C	4 CONTINUE	QIKS0640
C	SPREADER GOES HERE	QIKS0650
C	END PARTITION	QIKS0660
C	SPREADER	QIKS0670
	4 CALL MOVE(0,I)	QIKS0680
	12 IF (I - N) 110, 10, 110	QIKS0690
	110 I = I + 1	QIKS0700
	IF(COMPARE(0,I))10,12,10	QIKS0710
	10 IF (J - M) 108, 8, 108	QIKS0720
	108 J = J - 1	QIKS0730
	IF(COMPARE(0,J))8,10,8	QIKS0740
C	8 CONTINUE	QIKS0750
C	RETURN TO MAIN PROGRAM	QIKS0760
	END	QIKS0770

ADLER TEST, U-233 DATA,

0293.0

92233,	231,0375	0	0	1	0
92233,	1.0	0	1	1	0
0.790	60.0	1	4	0	0
2.5	1,00925	0	0	1	0
231,0375	0.0	6	0	18	3
0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0	0	1	0
2.5	0.0	0	0	876	73
0.	0.	0.	0.	-2.7900E+00	3.7000E-01
-2.5726E-03	-8.2336E-04	-2.7900E+00	3.7000E-01	1.6119E-04	-6.8078E-06
0.	0.	0.	0.	1.8000E-01	7.0000E-02
-3.1983E-07	-1.2945E-06	1.8000E-01	7.0000E-02	4.2644E-07	-6.0920E-08
0.	0.	0.	0.	1.4200E+00	3.5000E-01
9.8401E-05	-5.1965E-05	1.4200E+00	3.5000E-01	3.5486E-06	-1.1103E-05
0.	0.	0.	0.	1.7800E+00	1.2000E-01
1.6998E-04	-4.4167E-07	1.7800E+00	1.2000E-01	3.9887E-05	8.8334E-06
0.	0.	0.	0.	2.2900E+00	5.0000E-02
6.5002E-05	2.6881E-05	2.2900E+00	5.0000E-02	5.6747E-05	2.8328E-06
0.	0.	0.	0.	3.3000E+00	5.0000E-01
5.6869E-05	-6.4606E-05	3.3000E+00	5.0000E-01	2.4520E-06	1.0661E-06
0.	0.	0.	0.	3.6300E+00	8.0000E-02
3.1404E-05	1.0707E-05	3.6300E+00	8.0000E-02	1.4057E-05	1.3250E-06
0.	0.	0.	0.	4.5200E+00	3.9000E-01
6.6570E-05	-8.2684E-05	4.5200E+00	3.9000E-01	5.7874E-06	-4.1730E-06
0.	0.	0.	0.	5.7300E+00	1.8000E-01
1.5626E-05	-3.8745E-05	5.7300E+00	1.8000E-01	5.1020E-06	-3.2744E-06
0.	0.	0.	0.	6.8000E+00	9.0000E-02
2.5643E-04	5.2802E-05	6.8000E+00	9.0000E-02	8.7314E-05	4.0359E-06
0.	0.	0.	0.	7.4900E+00	9.0000E-02
7.9501E-06	2.1170E-06	7.4900E+00	9.0000E-02	2.6805E-06	1.5078E-06
0.	0.	0.	0.	8.6300E+00	2.6000E-01
2.3332E-05	-1.1118E-06	8.6300E+00	2.6000E-01	3.5029E-06	-2.8328E-06
0.	0.	0.	0.	9.1500E+00	1.4000E-01
2.2373E-05	-2.3180E-05	9.1500E+00	1.4000E-01	4.8431E-06	-9.4426E-07
0.	0.	0.	0.	1.0350E+01	1.6000E-01
4.1572E-04	5.1934E-06	1.0350E+01	1.6000E-01	8.2866E-05	3.6099E-06
0.	0.	0.	0.	1.1280E+01	2.0000E-01
5.2970E-05	1.4057E-05	1.1280E+01	2.0000E-01	5.4523E-06	-5.0107E-06
0.	0.	0.	0.	1.1750E+01	1.6000E-01
9.7624E-06	-6.3204E-06	1.1750E+01	1.6000E-01	-1.0493E-05	-3.5029E-07
0.	0.	0.	0.	1.2760E+01	1.7000E-01
3.5308E-04	6.7225E-05	1.2760E+01	1.7000E-01	4.8873E-05	3.5334E-06
0.	0.	0.	0.	1.3470E+01	2.0000E-01
5.1934E-05	2.5495E-05	1.3470E+01	2.0000E-01	1.4910E-05	-5.3610E-06
0.	0.	0.	0.	1.3660E+01	1.4000E-01
7.4794E-05	-3.2013E-05	1.3660E+01	1.4000E-01	3.1678E-06	2.3759E-06
0.	0.	0.	0.	1.5280E+01	1.2000E-01
1.8151E-04	-5.5650E-05	1.5280E+01	1.2000E-01	7.0576E-05	-4.4167E-06
0.	0.	0.	0.	1.6130E+01	2.2000E-01
1.5429E-04	-7.5693E-06	1.6130E+01	2.2000E-01	8.2090E-06	-4.5842E-06
0.	0.	0.	0.	1.6520E+01	1.3000E-01
1.4357E-04	4.0527E-05	1.6520E+01	1.3000E-01	3.0475E-05	6.6250E-06
0.	0.	0.	0.	1.7930E+01	1.2000E-01
6.4438E-05	6.3357E-06	1.7930E+01	1.2000E-01	1.4651E-05	2.1627E-06
0.	0.	0.	0.	1.8420E+01	2.1000E-01
9.0755E-05	7.4627E-07	1.8420E+01	2.1000E-01	1.00006E-05	-1.9190E-06
0.	0.	0.	0.	1.8860E+01	1.5000E-01
3.2556E-04	-6.9144E-05	1.8860E+01	1.5000E-01	5.3670E-05	4.6908E-06

0.	0.	0.	0.	2.0530E+01	2.0000E-01
1.6876E-04	1.0158E-05	2.0530E+01	2.0000E-01	2.8617E-05	1.2184E-06
0.	0.	0.	0.	2.1850E+01	1.3000E-01
1.9918E-04	1.3316E-04	2.1850E+01	1.3000E-01	5.2391E-05	1.7316E-05
0.	0.	0.	0.	2.2230E+01	2.4000E-01
8.1222E-04	1.2172E-04	2.2230E+01	2.4000E-01	9.8431E-05	-1.2047E-05
0.	0.	0.	0.	2.2940E+01	3.8000E-01
1.4414E-04	2.2236E-06	2.2940E+01	3.8000E-01	-1.4179E-05	-1.1895E-05
0.	0.	0.	0.	2.3540E+01	3.3000E-01
9.8112E-05	1.4114E-04	2.3540E+01	3.3000E-01	6.1072E-06	4.6147E-06
0.	0.	0.	0.	2.5130E+01	1.9000E-01
1.2617E-04	6.4088E-05	2.5130E+01	1.9000E-01	2.1109E-05	-4.8736E-07
0.	0.	0.	0.	2.6190E+01	1.7000E-01
4.8584E-06	1.5946E-05	2.6190E+01	1.7000E-01	-8.6963E-06	-2.1322E-06
0.	0.	0.	0.	2.6570E+01	2.4000E-01
9.4563E-05	1.7773E-05	2.6570E+01	2.4000E-01	1.9631E-05	1.3783E-05
0.	0.	0.	0.	2.7390E+01	4.3000E-01
2.0302E-05	1.6707E-05	2.7390E+01	4.3000E-01	1.1636E-05	5.3457E-06
0.	0.	0.	0.	2.8330E+01	1.6000E-01
3.4603E-05	3.6933E-05	2.8330E+01	1.6000E-01	1.7758E-05	-6.3966E-07
0.	0.	0.	0.	2.8990E+01	3.0000E-01
3.1153E-04	8.7572E-06	2.8990E+01	3.0000E-01	2.6835E-05	-1.1666E-05
0.	0.	0.	0.	2.9660E+01	7.0000E-02
6.6860E-06	1.7469E-05	2.9660E+01	7.0000E-02	4.8584E-06	-1.0052E-06
0.	0.	0.	0.	3.0150E+01	1.0000E-01
4.0055E-06	-2.8785E-06	3.0150E+01	1.0000E-01	-9.5949E-07	-1.9494E-06
0.	0.	0.	0.	3.0760E+01	1.4000E-01
7.9394E-05	7.2205E-05	3.0760E+01	1.4000E-01	1.7910E-05	1.2945E-06
0.	0.	0.	0.	3.1200E+01	4.7000E-01
2.1057E-04	-1.1311E-04	3.1200E+01	4.7000E-01	1.8809E-05	-8.7420E-06
0.	0.	0.	0.	3.1980E+01	1.4000E-01
1.6314E-04	1.9007E-05	3.1980E+01	1.4000E-01	3.5227E-05	-1.0265E-05
0.	0.	0.	0.	3.2740E+01	4.3000E-01
6.1103E-05	-1.4001E-04	3.2740E+01	4.3000E-01	-1.3098E-06	-1.6464E-05
0.	0.	0.	0.	3.4030E+01	6.6000E-01
1.4634E-04	4.8660E-05	3.4030E+01	6.6000E-01	-3.4648E-05	-3.6994E-05
0.	0.	0.	0.	3.4530E+01	4.2000E-01
2.6161E-04	4.9741E-05	3.4530E+01	4.2000E-01	6.2748E-06	2.2201E-05
0.	0.	0.	0.	3.5190E+01	1.2000E-01
4.0420E-05	9.2446E-06	3.5190E+01	1.2000E-01	-5.5589E-06	1.8885E-06
0.	0.	0.	0.	3.5460E+01	1.7000E-01
1.7773E-05	3.5958E-05	3.5460E+01	1.7000E-01	1.7362E-06	9.4578E-06
0.	0.	0.	0.	3.6540E+01	9.0000E-02
8.5593E-05	2.8130E-05	3.6540E+01	9.0000E-02	2.9988E-05	8.3613E-06
0.	0.	0.	0.	3.7500E+01	2.4000E-01
1.1392E-04	4.5766E-05	3.7500E+01	2.4000E-01	7.9957E-06	4.7061E-06
0.	0.	0.	0.	3.9460E+01	2.8000E-01
1.7370E-04	1.7536E-04	3.9460E+01	2.8000E-01	-2.2083E-06	-1.8733E-05
0.	0.	0.	0.	3.9570E+01	1.6000E-01
2.9546E-06	-9.8538E-05	3.9570E+01	1.6000E-01	-6.4271E-06	1.3067E-05
0.	0.	0.	0.	4.0060E+01	4.9000E-01
1.4452E-04	1.4173E-04	4.0060E+01	4.9000E-01	1.3052E-05	1.6677E-05
0.	0.	0.	0.	4.1060E+01	9.0000E-02
3.1755E-05	2.0195E-05	4.1060E+01	9.0000E-02	1.6372E-05	4.9802E-06
0.	0.	0.	0.	4.2620E+01	1.2000E-01
9.3923E-05	2.5434E-05	4.2620E+01	1.2000E-01	2.6424E-05	5.4371E-06
0.	0.	0.	0.	4.3470E+01	1.4000E-01
5.0685E-05	8.5136E-06	4.3470E+01	1.4000E-01	1.0539E-05	-1.6753E-07
0.	0.	0.	0.	4.4640E+01	5.6000E-01
1.1797E-04	3.8715E-05	4.4640E+01	5.6000E-01	5.3305E-06	9.1228E-06
0.	0.	0.	0.	4.5310E+01	5.2000E-01



1.6966E-05-6	0691E-05	4.5310E+01	5.2000E-01	6.8383E-06-6	9.601E-06
0.	0	0.	0.	4.6010E+01	8.0000E-02
3.8760E-05-2	4612E-05	4.6010E+01	8.0000E-02	2.1977E-05-6	6.2291E-06
0.	0	0.	0.	4.7170E+01	2.3000E-01
1.1409E-04-9	8081E-06	4.7170E+01	2.3000E-01	5.5894E-06-5	5.6656E-06
0.	0	0.	0.	4.8640E+01	1.3000E-01
2.5373E-04-3	2836E-05	4.8640E+01	1.3000E-01	1.2224E-04	5.0107E-06
0.	0	0.	0.	4.9120E+01	9.0000E-02
1.3753E-05-9	7320E-06	4.9120E+01	9.0000E-02	3.3049E-06-7	7.0819E-06
0.	0	0.	0.	5.0210E+01	4.5000E-01
7.7673E-05-4	5705E-05	5.0210E+01	4.5000E-01	2.5891E-07-6	6.1529E-06
0.	0	0.	0.	5.0990E+01	3.8000E-01
2.7277E-05-6	8535E-07	5.0990E+01	3.8000E-01	2.2845E-06-1	1.2489E-05
0.	0	0.	0.	5.1950E+01	6.2000E-01
2.3652E-05-6	6174E-05	5.1950E+01	6.2000E-01	2.4886E-05	1.0813E-06
0.	0	0.	0.	5.2910E+01	2.2000E-01
7.2875E-05-9	7700E-05	5.2910E+01	2.2000E-01	1.2397E-05	3.6704E-06
0.	0	0.	0.	5.3970E+01	1.4000E-01
9.1837E-05-3	4435E-05	5.3970E+01	1.4000E-01	1.7179E-05	3.4724E-06
0.	0	0.	0.	5.4770E+01	9.0000E-02
9.1928E-05	1.1362E-05	5.4770E+01	9.0000E-02	3.0780E-05	3.9141E-06
0.	0	0.	0.	5.6090E+01	2.7000E-01
9.3314E-05	1.9525E-04	5.6090E+01	2.7000E-01	8.8334E-06	3.8075E-07
0.	0	0.	0.	5.6350E+01	3.0000E-01
3.3395E-04-8	1937E-05	5.6350E+01	3.0000E-01	3.4344E-05	8.0414E-06
0.	0	0.	0.	5.7480E+01	4.9000E-01
4.3587E-04	3.5943E-05	5.7480E+01	4.9000E-01	2.4002E-05	4.8888E-06
0.	0	0.	0.	5.8510E+01	2.3000E-01
1.4106E-04	3.9598E-05	5.8510E+01	2.3000E-01	1.5763E-05-3	3.0765E-06
0.	0	0.	0.	6.1300E+01	4.0000E-01
2.8253E-04	7.2312E-05	6.1300E+01	4.0000E-01	1.2717E-05-1	1.7971E-06
0.	0	0.	0.	6.2500E+01	2.0000E-01
1.6427E-04-2	2784E-05	6.2500E+01	2.0000E-01	8.5410E-05-3	9.903E-06
0.	0	0.	0.	6.4300E+01	4.0000E-01
3.4727E-04-3	3582E-05	6.4300E+01	4.0000E-01	5.4082E-05-2	4.642E-05

PROGRAM ADLER, CALCULATES CROSS-SECTIONS FROM ADLER-ADLER PARAMETERS WITH OPTION FOR DOPPLER BROADENING,

ENDF/B VERSION 11 DATA.

TITLE ADLER TEST, U-233 DATA.

OPTION TO DOPPLER BROADEN 0 EFFECTIVE TEMPERATURE(\*K) 295.000

(Z,A) DESIGNATION OF THE ELEMENT 9,2233E+04 AT.WT/MASS OF NEUTRON 2,3104E+02 NO OF ISOTOPES 1

DATA FOR ISOTOPE NUMBER 1

(Z,A) DESIGNATION OF THE ISOTOPE 9,2233E+04 FRACTIONAL ABUNDANCE 1,0000E+00 NO OF ENERGY RANGES 1  
LOWER LIMIT OF THE ENERGY RANGE(EV) 7,9000E-01 UPPER LIMIT(EV) 6,0000E+01 LRU# 1 LRF# 4  
NUCLEAR SPIN 2,5000E+00 SCATTERING LENGTH 1,0002E+00 NO OF L-VALUES 1  
MASS OF THIS ISOTOPE IN UNITS OF NEUTRON MASS 2,3104E+02  
LI# 6 IF LI=5 TOTAL AND CAPTURE, LI=6 FISSION AND CAPTURE, AND LI=7 TOTAL CAPTURE AND FISSION CROSS-SECTIONS GIVEN  
NX# 3 IF NX=2 TOTAL AND CAPTURE BKGRND PARAMETERS GIVEN, IF NX=3 TOTAL,CAPTURE AND FISSION PARAMETERS GIVEN

BACKGROUND PARAMETERS FOR THE TOTAL CROSS-SECTION  
A1# 0,000000E+00 A2# 0,000000E+00 A3# 0,000000E+00 A4# 0,000000E+00 B1# 0,000000E+00 B2# 0,000000E+00

BACKGROUND PARAMETERS FOR THE FISSION CROSS-SECTION  
A1# 0,000000E+00 A2# 0,000000E+00 A3# 0,000000E+00 A4# 0,000000E+00 B1# 0,000000E+00 B2# 0,000000E+00

BACKGROUND PARAMETERS FOR THE CAPTURE CROSS-SECTION  
A1# 0,000000E+00 A2# 0,000000E+00 A3# 0,000000E+00 A4# 0,000000E+00 B1# 0,000000E+00 B2# 0,000000E+00

ANGULAR MOMENTUM OF THE RESONANCES 0 NUMBER OF J-STATES 1

J-VALUE FOR THESE RESONANCES 2,50 NUMBER OF RESONANCES FOR THE ABOVE L-VALUE AND THIS J IS 73

ADLER-ADLER PARAMETERS FOR THIS ISOTOPE





3.403000E+01	6.600000E-01	1.463400E-04	4.866000E-05
3.453000E+01	4.200000E-01	2.616100E-04	4.974100E-05
3.519000E+01	1.200000E-01	4.042000E-05	-9.244600E-06
3.546000E+01	1.700000E-01	1.777300E-05	-3.595800E-05
3.654000E+01	9.000000E-02	8.559300E-05	2.813000E-05
3.750000E+01	2.400000E-01	1.139200E-04	4.576600E-05
3.946000E+01	2.800000E-01	1.737000E-04	1.753600E-04
3.957000E+01	1.600000E-01	2.954600E-06	-9.853800E-05
4.006000E+01	4.900000E-01	1.445200E-04	-1.417300E-04
4.106000E+01	9.000000E-02	3.175500E-05	2.019500E-05
4.262000E+01	1.200000E-01	9.392300E-05	2.543400E-05
4.347000E+01	1.400000E-01	5.068500E-05	8.513600E-06
4.464000E+01	5.600000E-01	1.179700E-04	3.871500E-05
4.531000E+01	5.200000E-01	1.696600E-05	-6.069100E-05
4.601000E+01	8.000000E-02	3.876000E-05	-2.461200E-05
4.717000E+01	2.300000E-01	1.140900E-04	-9.808100E-06
4.864000E+01	1.300000E-01	2.537300E-04	-3.283600E-05
4.912000E+01	9.000000E-02	1.375300E-05	-9.732000E-06
5.021000E+01	4.500000E-01	7.767300E-05	-4.570500E-05
5.099000E+01	3.800000E-01	2.727700E-05	-6.853500E-07
5.195000E+01	6.200000E-01	2.365200E-05	-6.617400E-05
5.291000E+01	2.200000E-01	7.287500E-05	-9.770000E-05
5.397000E+01	1.400000E-01	9.183700E-05	-3.443500E-05
5.477000E+01	9.000000E-02	9.192800E-05	1.136200E-05
5.609000E+01	2.700000E-01	9.331400E-05	1.952500E-04
5.635000E+01	3.000000E-01	3.339500E-04	-8.193700E-05
5.748000E+01	4.900000E-01	4.358700E-04	3.594300E-05
5.851000E+01	2.300000E-01	1.410600E-04	3.959800E-05
6.130000E+01	4.000000E-01	2.825300E-04	7.231200E-05
6.250000E+01	2.000000E-01	1.642700E-04	-2.278400E-05
6.430000E+01	4.000000E-01	3.472700E-04	-3.358200E-05

MUC	NUC	GC	HC
-2.790000E+00	3.700000E-01	1.611900E-04	-6.807800E-06
1.800000E-04	7.000000E-02	4.264400E-07	-6.092000E-08
1.420000E+00	3.500000E-01	3.548600E-06	-1.110300E-05
1.780000E+00	1.200000E-01	3.988700E-05	8.833400E-06
2.290000E+00	5.000000E-02	5.674700E-05	2.832800E-06
3.300000E+00	5.000000E-01	2.452000E-06	1.066100E-06
3.630000E+00	8.000000E-02	1.405700E-05	1.325000E-06
4.520000E+00	3.900000E-01	5.787400E-06	-4.173000E-06
5.730000E+00	1.800000E-01	5.102000E-06	-3.274400E-06
6.800000E+00	9.000000E-02	8.731400E-05	4.035900E-06
7.490000E+00	9.000000E-02	2.680500E-06	1.507800E-06
8.630000E+00	2.600000E-01	3.502900E-06	-2.832800E-06
9.150000E+00	1.400000E-01	4.843100E-06	-9.442600E-07
1.035000E+01	1.600000E-01	8.286600E-05	3.609500E-06
1.128000E+01	2.000000E-01	5.452300E-06	-5.010700E-06
1.175000E+01	1.600000E-01	-1.049300E-05	-3.502900E-07
1.276000E+01	1.700000E-01	4.887300E-05	3.533400E-06
1.347000E+01	2.000000E-01	1.491000E-05	-5.361000E-06
1.366000E+01	1.400000E-01	3.167800E-06	2.375900E-06
1.528000E+01	1.200000E-01	7.057600E-05	-4.416700E-06
1.613000E+01	2.200000E-01	8.209000E-06	-4.584200E-06
1.652000E+01	1.300000E-01	3.047500E-05	6.625000E-06
1.793000E+01	1.200000E-01	1.465100E-05	2.162700E-06
1.842000E+01	2.100000E-01	1.000600E-05	-1.919000E-06
1.886000E+01	1.500000E-01	5.367000E-05	4.690800E-06
2.053000E+01	2.000000E-01	2.861700E-05	1.218400E-06

2,185000E+01	1,300000E-01	5,239100E-05	1,731600E-05
2,223000E+01	2,400000E-01	9,843100E-05	-1,204700E-05
2,294000E+01	3,800000E-01	-1,417900E-05	-1,189500E-05
2,354000E+01	3,300000E-01	6,107200E-06	4,614700E-06
2,513000E+01	1,900000E-01	2,110900E-05	-4,873600E-07
2,619000E+01	1,700000E-01	-8,696300E-06	-2,132200E-06
2,657000E+01	2,400000E-01	1,963100E-05	1,378300E-05
2,739000E+01	4,300000E-01	1,163600E-05	5,345700E-06
2,833000E+01	1,600000E-01	1,775800E-05	-6,396600E-07
2,899000E+01	3,000000E-01	2,683500E-05	-1,166600E-05
2,966000E+01	7,000000E-02	4,858400E-06	-1,005200E-06
3,015000E+01	1,000000E-01	-9,594900E-07	-1,949400E-06
3,076000E+01	1,400000E-01	1,791000E-05	1,294500E-06
3,120000E+01	4,700000E-01	1,880900E-05	-8,742000E-06
3,198000E+01	1,400000E-01	3,522700E-05	-1,026500E-05
3,274000E+01	4,300000E-01	-1,309800E-06	-1,646400E-05
3,403000E+01	6,600000E-01	-3,464800E-05	-3,699400E-05
3,453000E+01	4,200000E-01	6,274800E-06	2,228100E-05
3,519000E+01	1,200000E-01	-5,558900E-06	1,888500E-06
3,546000E+01	1,700000E-01	1,736200E-06	9,457800E-06
3,654000E+01	9,000000E-02	2,998800E-05	8,361300E-06
3,750000E+01	2,400000E-01	7,995700E-06	4,706100E-06
3,946000E+01	2,800000E-01	-2,208300E-06	-1,873300E-05
3,957000E+01	1,600000E-01	-6,427100E-06	1,306700E-05
4,006000E+01	4,900000E-01	1,305200E-05	1,667700E-05
4,106000E+01	9,000000E-02	1,637200E-05	4,980200E-06
4,262000E+01	1,200000E-01	2,642400E-05	5,437100E-06
4,347000E+01	1,400000E-01	1,053900E-05	-1,675300E-07
4,464000E+01	5,600000E-01	5,330500E-06	9,122800E-06
4,531000E+01	5,200000E-01	6,838300E-06	-6,960100E-06
4,601000E+01	8,000000E-02	2,197700E-05	-6,229100E-06
4,717000E+01	2,300000E-01	5,589400E-06	-5,665600E-06
4,864000E+01	1,300000E-01	1,222400E-04	5,010700E-06
4,912000E+01	9,000000E-02	-3,304900E-06	-7,081900E-06
5,021000E+01	4,500000E-01	-2,589100E-07	-6,152900E-06
5,099000E+01	3,800000E-01	-2,284500E-06	-1,248900E-05
5,195000E+01	6,200000E-01	-2,488600E-05	1,081300E-06
5,291000E+01	2,200000E-01	1,239700E-05	3,670400E-06
5,397000E+01	1,400000E-01	1,717900E-05	3,472400E-06
5,477000E+01	9,000000E-02	3,078000E-05	3,914100E-06
5,609000E+01	2,700000E-01	8,833400E-06	3,807500E-07
5,635000E+01	3,000000E-01	3,434400E-05	8,041400E-06
5,748000E+01	4,900000E-01	2,400200E-05	4,888800E-06
5,851000E+01	2,300000E-01	1,576300E-05	-3,076500E-06
6,130000E+01	4,000000E-01	1,271700E-05	-1,797100E-06
6,250000E+01	2,000000E-01	8,541000E-05	-3,990300E-06
6,430000E+01	4,000000E-01	5,408200E-05	-2,464200E-05

ADLER-ADLER CROSS-SECTIONS FOR THIS ELEMENT

CROSS-SECTIONS AT THERMAL ENERGY

NEUTRON ENERGY(EV)

TOTAL X-SECTION

FISSION X-SECTION

CAPTURE X-SECTION

2,530000E+02

0,000000E+00

5,212307E+02

4,774971E+01

CROSS-SECTIONS NOT DOPPLER BROADENED

NEUTRON ENERGY(EV)	TOTAL X-SECTION	FISSION X-SECTION	CAPTURE X-SECTION
7,900000E-01	0,000000E+00	1,161008E+02	9,006434E+00
8,530000E-01	0,000000E+00	1,185189E+02	9,343464E+00
8,600000E-01	0,000000E+00	1,189266E+02	9,395523E+00
9,160000E-01	0,000000E+00	1,233242E+02	9,936258E+00
9,300000E-01	0,000000E+00	1,247669E+02	1,011010E+01
9,790000E-01	0,000000E+00	1,310541E+02	1,086522E+01
1,000000E+00	0,000000E+00	1,343985E+02	1,126910E+01
1,042000E+00	0,000000E+00	1,424159E+02	1,225153E+01
1,070000E+00	0,000000E+00	1,488460E+02	1,305792E+01
1,070000E+00	0,000000E+00	1,488460E+02	1,305792E+01
1,105000E+00	0,000000E+00	1,582335E+02	1,426979E+01
1,140000E+00	0,000000E+00	1,692363E+02	1,574855E+01
1,140000E+00	0,000000E+00	1,692363E+02	1,574855E+01
1,168000E+00	0,000000E+00	1,792582E+02	1,715593E+01
1,210000E+00	0,000000E+00	1,963328E+02	1,970238E+01
1,231000E+00	0,000000E+00	2,057450E+02	2,119558E+01
1,280000E+00	0,000000E+00	2,206199E+02	2,532049E+01
1,294000E+00	0,000000E+00	2,368252E+02	2,667538E+01
1,350000E+00	0,000000E+00	2,664782E+02	3,293553E+01
1,357000E+00	0,000000E+00	2,702130E+02	3,381631E+01
1,420000E+00	0,000000E+00	3,034496E+02	4,281927E+01
1,456000E+00	0,000000E+00	3,224419E+02	4,897963E+01
1,490000E+00	0,000000E+00	3,415267E+02	5,572214E+01
1,492000E+00	0,000000E+00	3,427206E+02	5,615359E+01
1,528000E+00	0,000000E+00	3,665928E+02	6,477248E+01
1,560000E+00	0,000000E+00	3,937754E+02	7,419964E+01
1,564000E+00	0,000000E+00	3,977481E+02	7,552899E+01
1,600000E+00	0,000000E+00	4,415726E+02	8,943715E+01
1,630000E+00	0,000000E+00	4,929178E+02	1,043572E+02
1,636000E+00	0,000000E+00	5,052494E+02	1,077749E+02
1,660000E+00	0,000000E+00	5,625275E+02	1,229980E+02
1,672000E+00	0,000000E+00	5,961533E+02	1,315074E+02
1,684000E+00	0,000000E+00	6,329760E+02	1,405066E+02
1,700000E+00	0,000000E+00	6,861321E+02	1,529312E+02
1,708000E+00	0,000000E+00	7,137733E+02	1,591180E+02
1,708000E+00	0,000000E+00	7,137733E+02	1,591180E+02
1,732000E+00	0,000000E+00	7,945725E+02	1,758568E+02
1,744000E+00	0,000000E+00	8,290315E+02	1,820382E+02
1,756000E+00	0,000000E+00	8,554532E+02	1,898469E+02
1,770000E+00	0,000000E+00	8,722724E+02	1,865439E+02
1,780000E+00	0,000000E+00	8,733790E+02	1,843268E+02
1,804000E+00	0,000000E+00	8,381879E+02	1,703944E+02
1,828000E+00	0,000000E+00	7,618652E+02	1,483086E+02
1,831000E+00	0,000000E+00	7,506169E+02	1,452918E+02
1,852000E+00	0,000000E+00	6,682678E+02	1,242388E+02
1,876000E+00	0,000000E+00	5,771687E+02	1,025709E+02
1,882000E+00	0,000000E+00	5,561347E+02	9,778110E+01
1,900000E+00	0,000000E+00	4,984142E+02	8,505967E+01









	RHO2=RHO**2	AVG3182
	RHOPN2=RHOPEN**2	AVG3183
	WAVE=2,196771E-03*E2*(AWRI/(AWRI+1,0))	AVG3184
	PSS=RHO	AVG3185
	PSP=RHO*ATAN (RHO)	AVG3186
	SIGPTS=(SIN (PSS)/WAVE)**2	AVG3187
	SIGPTS=SIGPTS*PHIFCR	AVG3188
	SIGPTP=(SIN (PSP)/WAVE)**2	AVG3189
	SIGPTP=SIGPTP*PHIFOR	AVG3190
	SIGPTP=3,0*SIGPTP	AVG3191
	DO 201 J=1,JA	AVG3192
	GJ=(2,0*XXJA(J)+1,0)/(2,0*SPIN+1,0)	AVG3193
	GJ=GJ/2,0	AVG3194
	XXJAJ=XXJA(J)	AVG3195
	GN=GNO(J)*E2*XXJAJ	AVG3196
	MU=INT (XXJAJ)	AVG3197
	GAMMA=GG(J)	AVG3198
	GALPHA=GN	AVG3199
	GBETA=0,0	AVG3200
	GF=0,0	AVG3201
	TERM=(CONST*GJ*GN*GG(J))/(E*DA(J))	AVG3202
	TERS=(CONST*GJ*GN*GN)/(E*DA(J))	AVG3203
	CALL GCAP(GALPHA,GBETA,GAMMA,GF,MU,GC)	AVG3204
	CALL GSCAT(GALPHA,GBETA,GAMMA,GF,MU,GS)	AVG3205
	GC=GC*TERM	AVG3206
	GS=GS*TERS	AVG3207
	CORR=(CONST*GJ*2,0*GN*SIN(PSS)*SIN(PSS))/(E*DA(J))	AVG32071
	GS=GS-CORR	AVG32072
	GIG=GIG+GC	AVG3208
	GIS=GIS+GS	AVG3209
201	CONTINUE	AVG3210
	GIGGS(I)=GIG	AVG3211
	GISS(I)=GIS+SIGPTS	AVG3212
	IF(NR=2)205,206,88	AVG3213
206	GIG=0,0	AVG3214
	GIS=0,0	AVG3215
	DO 207 J=1,JB	AVG3216
	GJ=(2,0*XXJB(J)+1,0)/(2,0*SPIN+1,0)	AVG3217
	GJ=GJ/2,0	AVG3218
	VL=RHOPN2/(RHO*PN2+1,0)	AVG3219
	XXJB=XXJB(J)	AVG3220
	MU=INT (XXJB)	AVG3221
	GN=GNOB(J)*E2*VL*XXJB	AVG3222
	GAMMA=GGB(J)	AVG3223
	GF=0,0	AVG3224
	GALPHA=GN	AVG3225
	GBETA=0,0	AVG3226
	TERM=(CONST*GJ*GN*GGB(J))/(E*DAB(J))	AVG3227
	TERS=(CONST*GJ*GN*GN)/(E*DAB(J))	AVG3228
	CALL GCAP(GALPHA,GBETA,GAMMA,GF,MU,GC)	AVG3229
	CALL GSCAT(GALPHA,GBETA,GAMMA,GF,MU,GS)	AVG3230
	GC=GC*TERM	AVG3231
	GS=GS*TERS	AVG3232
	CORR=(CONST*GJ*2,0*GN*SIN(PSP)*SIN(PSP))/(E*DAB(J))	AVG32321
	GS=GS-CORR	AVG32322
	GIG=GIG+GC	AVG3233
	GIS=GIS+GS	AVG3234
207	CONTINUE	AVG3235
	GIGGP(I)=GIG	AVG3236
	GISP(I)=GIS+SIGPTP	AVG3237
205	E=E+ESTEP	AVG3238

	IF(E,GT,EN)GO TO 202	AVG3239
	GO TO 203	AVG32391
203	I=I+1	AVG3240
	GO TO 204	AVG3241
202	NC=I	AVG3242
	GO TO 400	AVG3243
300	DO 210 I=1,NE	AVG3244
	E=ES(I)	AVG3245
	E2=SQRT(E)	AVG3246
	RHO=C*E2	AVG3247
	RHOPEN=CPEN*E2	AVG3248
	WAVE=2.196771E-03*E2*(AWRI/(AWRI+1,0))	AVG3249
	PSS=RHO	AVG3250
	PSP=RHO*ATAN (RHO)	AVG3251
	SIGPTS=(SIN(PSS)/WAVE)**2	AVG3252
	SIGPTS=SIGPTS*PHIFOR	AVG3253
	SIGPTP=(SIN(PSP)/WAVE)**2	AVG3254
	SIGPTP=SIGPTP*PHIFOR	AVG3255
	SIGPTP=3,0*SIGPTP	AVG3256
	RHO2=RHO**2	AVG3257
	RHOPN2=RHOPEN**2	AVG3258
	VL=RHOPN2/(RHOPN2+1,0)	AVG3259
	GIG=0,0	AVG3260
	GIF=0,0	AVG3261
	GIS=0,0	AVG3262
	DO 211 J=1,JA	AVG3263
	GJ=(2,0*XXJA(J)+1,0)/(2,0*SPIN+1,0)	AVG3264
	GJ=GJ/2,0	AVG3265
	XXJAJ=XXJA(J)	AVG3266
	MU=INT (XXJAJ)	AVG3267
	NU=MUFA(J)	AVG3268
	GN=GNO(J)*E2*XXJAJ	AVG3269
	GAMMA=GG(J)	AVG3270
	GALPHA=GN	AVG3271
	GBETA=GFE(I,J)	AVG3272
	TERM=(CONST*GJ*GN*GFE(I,J))/(E*DA(J))	AVG3273
	TERG=(CONST*GJ*GG(J)*GN)/(E*DA(J))	AVG3274
	TERS=(CONST*GJ*GN*GN)/(E*DA(J))	AVG3275
	CALL GFIS(GALPHA,GBETA,GAMMA,MU,NU,GS)	AVG3276
	CALL GSPE(GALPHA,GBETA,GAMMA,MU,NU,GC)	AVG3277
	CALL SCAF(GALPHA,GBETA,GAMMA,MU,NU,SF)	AVG3278
	GS=GS*TERM	AVG3279
	GC=GC*TERG	AVG3280
	SF=SF*TERS	AVG3281
	CORR=(CONST*GJ*2,0*GN*SIN(PSS)*SIN(PSS))/(E*DA(J))	AVG32812
	SF=SF-CORR	AVG3282
	GIG=GIG+GC	AVG3283
	GIF=GIF+GS	AVG3284
	GIS=GIS+SF	AVG3285
211	CONTINUE	AVG3286
	GIGGS(I)=GIG	AVG3287
	GIGFS(I)=GIF	AVG3288
	GISS(I)=GIS+SIGPTS	AVG3289
	IF(NR-2)210,212,88	AVG3290
212	GIG=0,0	AVG3291
	GIF=0,0	AVG3292
	GIS=0,0	AVG3293
	DO 213 J=1,JB	AVG3294
	GJ=(2,0*XXJB(J)+1,0)/(2,0*SPIN+1,0)	AVG3295
	GJ=GJ/2,0	AVG3296
	XXJBJ=XXJB(J)	

MU=INT (XXJBJ)	AVG3297
NU=MUFBJ	AVG3298
GN=GNOR(J)*E2*XXJBJ*VL	AVG3299
GAMMA=GGB(J)	AVG3300
GALPHA=GN	AVG3301
GBETA=GFEB(I,J)	AVG3302
TERM=(CONST*GJ*GFEB(I,J)*GN)/(E*DAB(J))	AVG3303
TERG=(CONST*GJ*GN*GGB(J))/(E*DAB(J))	AVG3304
TERS=(CONST*GJ*GN*GN)/(E*DAB(J))	AVG3305
CALL GFIS(GALPHA,GBETA,GAMMA,MU,NU,GS)	AVG3306
CALL GSPE(GALPHA,GBETA,GAMMA,MU,NU,GC)	AVG3307
CALL SCAF(GALPHA,GBETA,GAMMA,MU,NU,SF)	AVG3308
GS=GS*TERM	AVG3309
GC=GC*TERG	AVG3310
SF=SF*TERS	AVG3311
CORR=(CONST*GJ*2,0*GN*SIN(PSP)*SIN(PSP))/(E*DAB(J))	AVG33111
SF=SF+CORR	AVG33112
GIG=GIG+GC	AVG3312
GIF=GIF+GS	AVG3313
GIS=GIS+SF	AVG3314
213 CONTINUE	AVG3315
GIGGP(I)=GIG	AVG3316
GIGFP(I)=GIF	AVG3317
GISP(I)=GIS+SIGPTP	AVG3318
210 CONTINUE	AVG3319
GO TO 410	AVG3320
400 PRINT0	AVG3321
10 FORMAT(72H AVERAGE SCATTERING AND CAPTURE CROSS-SECTIONS FOR A NON	AVG3322
1-FISSILE NUCLEUS)	AVG3323
PRINT11,(RUN(J),J=1,7)	AVG3324
11 FORMAT(9H TITLE 7A4)	AVG3325
PRINT12,EO,EN	AVG3326
12 FORMAT(24H ENERGY LIMITS LOWER E10.4,10H UPPER E10.4)	AVG3327
GO TO (401,402),NR	AVG3328
401 PRINT21	AVG3329
PRINT36	AVG3330
PRINT14,(ES(I),GISS(I),I=1,NC)	AVG3331
PRINT35	AVG3332
PRINT13	AVG3333
13 FORMAT(53H NEUTRON ENERGY(EV) S-WAVE CAPTURE CROSS-SECTION)	AVG3334
36 FORMAT(53H NEUTRON ENERGY(EV) S-WAVE SCATRNG CROSS-SECTION)	AVG3335
14 FORMAT(2E20,6)	AVG3336
PRINT14,(ES(I),GIGGS(I),I=1,NC)	AVG3337
GO TO 800	AVG3338
402 PRINT21	AVG3339
PRINT37	AVG3340
DO 7001 I=1,NC	AVG3341
TOTAL=GISS(I)+GISP(I)	AVG3342
PRINT16,ES(I),GISS(I),GISP(I),TOTAL	AVG3343
7001 CONTINUE	AVG3344
PRINT35	AVG3345
PRINT15	AVG3346
15 FORMAT(110H NEUTRON ENERGY(EV) S-WAVE CAPTURE CROSS-SECTION	AVG3347
1 P-WAVE CAPTURE CROSS-SECTION TOTAL)	AVG3348
37 FORMAT(110H NEUTRON ENERGY(EV) S-WAVE SCATRNG CROSS-SECTION	AVG3349
1 P-WAVE SCATRNG CROSS-SECTION TOTAL)	AVG3350
16 FORMAT(4X,E13.6,17X,E13.6,21X,E13.6,21X,E13.6)	AVG3351
DO 7000 I=1,NC	AVG3352
TOTAL=GIGGS(I)+GIGGP(I)	AVG3353
PRINT16,ES(I),GIGGS(I),GIGGP(I),TOTAL	AVG3354
7000 CONTINUE	AVG3355

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      GO TO 880
410 PRINT17
17 FORMAT(76H AVERAGE SCATTERING CAPTURE AND FISSION CROSS-SECTIONS FOR A FISSION NUCLEUS)
PRINT11,(RUN(J),J=1,7)
GO TO (411,412),NR
411 PRINT21
PRINT36
PRINT14,(ES(I),GISS(I),I=1,NE)
PRINT35
PRINT13
PRINT14,(ES(I),GIGGS(I),I=1,NE)
PRINT18
18 FORMAT(53H NEUTRON ENERGY(EV) S-WAVE FISSION CROSS-SECTION)
PRINT14,(ES(I),GIGFS(I),I=1,NE)
GO TO 880
412 PRINT21
PRINT37
DO 7002 I=1,NE
TOTAL=GISS(I)+GISP(I)
PRINT16,ES(I),GISS(I),GISP(I),TOTAL
7002 CONTINUE
PRINT35
PRINT15
DO 7003 I=1,NE
TOTAL=GIGGS(I)+GIGGP(I)
PRINT16,ES(I),GIGGS(I),GIGGP(I),TOTAL
7003 CONTINUE
PRINT19
19 FORMAT(110H NEUTRON ENERGY(EV) S-WAVE FISSION CROSS-SECTION
1 P-WAVE NEUTRON CROSS-SECTION TOTAL)
DO 7004 I=1,NE
TOTAL=GIGFS(I)+GIGFP(I)
PRINT16,ES(I),GIGFS(I),GIGFP(I),TOTAL
7004 CONTINUE
GO TO 880
88 PRINT20
20 FORMAT(47H INPUT ERROR NUMBER OF L VALUES LARGER THAN TWO)
21 FORMAT(62H AVERAGE CROSS-SECTIONS CALCULATED USING GREEBLER APPROXIMATION)
22 FORMAT(31H DATA FOR A NON-FISSION NUCLEUS)
23 FORMAT(27H DATA FOR A FISSION NUCLEUS)
24 FORMAT(12H S-WAVE DATA)
C CONTINUE
25 FORMAT(12H P-WAVE DATA)
26 FORMAT(20H ENERGY LIMITS LOWERE20,6,7H UPPERE20,6,7H LRU=15,7H
1 LRF=15,7H LFI=15)
27 FORMAT(7H RUN NO15,9H TITLE 7A4,4H EOE13,6,4H ENE13,6,7H ESTEAVG3403
1PE13,6)
28 FORMAT(12H TARGET SPINE11,4,18H SCATTERING LENGTH11,4,54H NO OF EAVG3404
1ENERGY VALUES AT WHICH FISSION WIDTHS ARE GIVEN15)
29 FORMAT(51H FISSION WIDTHS ARE GIVEN AT THE FOLLOWING ENERGIES)
30 FORMAT(19H MEAN LEVEL SPACING11,4,11H LEVEL SPINE11,4,22H REDUCEDAVG3407
1 NEUTRON WIDTH11,4,12H GAMMA GAMMAE11,4)
31 FORMAT(56H NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTIONAVG3409
1I7)
32 FORMAT(56H NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTIONAVG3411
1I7)
33 FORMAT(23H THE FISSION WIDTHS ARE)
34 FORMAT(14H ISOTOPIC MASSE11,4,17H ANGULAR MOMENTUM15,18H NO OF SPIAVG3414
1N STATES15)

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35 FORMAT(//)
38 FORMAT(46H NUCLEAR RADIUS A=(1.23*MASS**1/3+0.8)*0.1 =E11.4)
39 FORMAT(80H1 PROGRAM AVRAGE3, CALCULATES CROSS-SECTIONS IN THE UNRESOLVED RESONANCE REGION,)
40 FORMAT(59H ENDP/B VERSION II DATA WITH ENERGY INDEPENDENT PARAMETERS)
880 GO TO 881
8800 RETURN
      END
      SUBROUTINE GCAP(GALPHA,GBETA,GAMMA,GGF,MU,SC)
      COMMON/XBAR/XX(4,10)
      SC=0.0
      DO 100 J=1,10
      XJ=XX(MU,J)
      VALUE=XJ/(GALPHA*XJ+GBETA*GGF+GAMMA)
      SC=SC+VALUE
100 CONTINUE
      SC=SC/10.0
      RETURN
      END
      SUBROUTINE GFIS(GALPHA,GBETA,GAMMA,MU,NU,S)
      COMMON/XBAR/XX(4,10)
      S=0.0
      DO 100 J=1,10
      YJ=XX(NU,J)
      CALL GCAP(GALPHA,GBETA,GAMMA,YJ,MU,SC)
      S=S+YJ*SC
100 CONTINUE
      S=S/10.0
      RETURN
      END
      SUBROUTINE GSPE(GALPHA,GBETA,GAMMA,MU,NU,S)
      COMMON/XBAR/XX(4,10)
      S=0.0
      DO 100 J=1,10
      YJ=XX(NU,J)
      CALL GCAP(GALPHA,GBETA,GAMMA,YJ,MU,SC)
      S=S+SC
100 CONTINUE
      S=S/10.0
      RETURN
      END
      SUBROUTINE GSCT(GALPHA,GBETA,GAMMA,GGF,MU,SC)
      COMMON/XBAR/XX(4,10)
      SC=0.0
      DO 100 J=1,10
      XJ=XX(MU,J)
      VALUE=(XJ*XJ)/(GALPHA*XJ+GBETA*GGF+GAMMA)
      SC=SC+VALUE
100 CONTINUE
      SC=SC/10.0
      RETURN
      END
      SUBROUTINE SCAF(GALPHA,GBETA,GAMMA,MU,NU,S)
      COMMON/XBAR/XX(4,10)
      S=0.0
      DO 100 J=1,10
      YJ=XX(NU,J)
      CALL GSCT(GALPHA,GBETA,GAMMA,YJ,MU,SC)
      S=S+SC
100 CONTINUE

```

```

AVG3416
AVG3417
AVG3418
AVG3419
AVG3420
AVG3421
AVG3422
AVG3423
AVG3424
GCAP001
GCAP002
GCAP003
GCAP004
GCAP005
GCAP006
GCAP007
GCAP008
GCAP009
GCAP010
GCAP011
GFIS001
GFIS002
GFIS003
GFIS004
GFIS005
GFIS006
GFIS007
GFIS008
GFIS009
GFIS010
GFIS011
GSPE001
GSPE002
GSPE003
GSPE004
GSPE005
GSPE006
GSPE007
GSPE008
GSPE009
GSPE010
GSPE011
GSCT001
GSCT002
GSCT003
GSCT004
GSCT005
GSCT006
GSCT007
GSCT008
GSCT009
GSCT010
GSCT011
SCAF001
SCAF002
SCAF003
SCAF004
SCAF005
SCAF006
SCAF007
SCAF008

```

S=S/10.0  
RETURN  
END

SCAF009  
SCAF010  
SCAF011



1 AVERAGE3 TEST, PU=239 DATA													
3.00000+	2	1.00000+	5	2	1	0	01051	2151	203				
5.00000-	1	9.05000-	1	0	0	16	21051	2151	204				
3.00000+	2	6.00000+	2	1.00000+	3	1.50000+	3	3.50000+	31051	2151	205		
5.00000+	3	8.00000+	3	1.30000+	4	2.00000+	4	3.00000+	4	4.00000+	41051	2151	206
5.00000+	4	6.00000+	4	8.00000+	4	1.00000+	5			1051	2151	207	
236,9985	0.	0.	0	0	0	0	2	01051	2151	208			
0.	0.	0.	0	0	0	0	22	01051	2151	209			
8.78000+	0	0.	0	1.00000+	0	9.40000-	4	3.87000-	2	0.	01051	2151	210
2.80000+	0	2.80000+	0	2.80000+	0	2.80000+	0	2.80000+	0	2.80000+	01051	2151	211
2.80000+	0	2.80000+	0	2.80000+	0	2.80000+	0	2.80000+	0	2.80000+	01051	2151	212
2.80000+	0	2.80000+	0	2.80000+	0	2.80000+	0						
0.	0.	0.	0	0	0	0	22	01051	2151	214			
3.12000+	0	1.00000+	0	1.00000+	0	3.34000-	4	3.87000-	2	0.	01051	2151	215
5.52000-	2	5.59000-	2	5.68000-	2	5.78000-	2	5.93200-	2	6.23000-	21051	2151	216
6.57000-	2	7.33000-	2	8.72000-	2	1.10200-	1	1.50200-	1	1.97500-	11051	2151	217
2.48000-	1	3.00000-	1	3.86000-	1	4.85000-	1			1051	2151	218	
236,9985	0.	0.00000+	0	0	1	0	3	01051	2151	219			
0.	0.	0.	0	1	2	22	01051	2151	220				
8.78000+	0	0.	0	1.00000+	0	2.19500-	03	3.87000-	02	0.	01051	2151	
.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000			
.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000			
.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000			
0.00000+	0	0.00000+	0	0	1	2	22	0					
3.12000+	0	1.00000+	0	2.00000+	0	7.80000-	04	3.87000-	02	0.00000+	0		
.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000			
.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000			
.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000			
0.00000+	0	0.00000+	0	0	1	2	22	0					
2.12000+	0	2.00000+	0	1.00000+	0	5.30000-	04	3.87000-	02	0.00000+	0		
.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000			
.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000			
.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000	.04000			
2 AVERAGE3 TEST, U=238 DATA													
3.9200E+03	5.0000E+04	2	1	0				01047	2151	226			
0.0	0.9184	1	0	0	2			11047	2151	227			
236,0058	0.0	0	0	6				0,01047	2151	228			
18,5	0,5	1.0	1.739-3	24.6-3				21047	2151	229			
236,0058	0.0	1	0	12				0,01047	2151	230			
18,5	0,5	1.0	2.923-3	24.6-3				0,01047	2151	23			
9.25	1.5	1.0	1.4615-3	24.6-3									
3 AVERAGE3 TEST, U=235 DATA													
6.4504E+01	5.0E+04	2	1	0				01044	2151	186			
3,5	8.3668E-01	0	0	25				21044	2151	187			
6.4504E+01	8.2E+01	1.25E+02	1.75E+02	2.25E+02	2.75E+02	3.1044	2151	188					
3.50E+02	4.50E+02	6.00E+02	8.50E+02	1.25E+03	1.75E+03	31044	2151	189					
2.50E+03	3.50E+03	4.50E+03	5.50E+03	7.00E+03	9.00E+03	31044	2151	190					
1.25E+04	1.75E+04	2.25E+04	2.75E+04	3.50E+04	4.50E+04	41044	2151	191					
5.00E+04								1044	2151	192			
233,0247	0.0	0	0	2				01044	2151	193			
0.0	0.0	0	0	2	31			01044	2151	194			
1.00	3.0	1.0	1.0E-04	0.035				0,01044	2151	195			
2.9474E-01	2.9264E-01	2.4623E-01	2.4258E-01	2.6413E-01	4.9705E-01	011044	2151	196					
2.7310E-01	4.5109E-01	4.4004E-01	2.3327E-01	3.0220E-01	3.5300E-01	011044	2151	197					
4.2449E-01	3.2358E-01	3.2196E-01	3.2284E-01	3.3009E-01	3.3291E-01	011044	2151	198					
4.3837E-01	4.3870E-01	4.5035E-01	4.7280E-01	5.2078E-01	5.9992E-01	011044	2151	199					
5.7033E-01								1044	2151	200			
0.0	0.0	0	1	31				01044	2151	201			
1.00	4.0	1.0	1.0E-04	0.035				0,01044	2151	202			
1.4737E-01	1.4632E-01	1.2311E-01	1.2129E-01	1.3207E-01	2.4852E-01	011044	2151	203					
1.3655E-01	2.2554E-01	2.2002E-01	1.1663E-01	1.5110E-01	1.7650E-01	011044	2151	204					

2.1225E-01	1.6179E-01	1.6098E-01	1.6142E-01	1.6505E-01	1.6646E-01	11044	2151	205
2.1918E-01	2.1935E-01	2.2517E-01	2.3640E-01	2.6039E-01	2.9996E-01	11044	2151	206
2.8517E-01						1044	2151	207
233,0247	0,0	1	0	4	01044	2151	208	
0,0	0,0	1	2	31	01044	2151	209	
1.16	2,0	1,0	2,32E-04	0,035	0,01044	2151	210	
3,32E-01	3,32E-01	3,32E-01	3,32E-01	3,32E-01	3,32E-01	11044	2151	211
3,32E-01	3,32E-01	3,32E-01	3,32E-01	3,32E-01	3,32E-01	11044	2151	212
3,32E-01	3,32E-01	3,32E-01	3,32E-01	3,32E-01	3,32E-01	11044	2151	213
3,32E-01	3,32E-01	3,32E-01	3,32E-01	3,32E-01	3,32E-01	11044	2151	214
3,32E-01					1044	2151	215	
0,0	0,0	1	1	31	01044	2151	216	
1,00	3,0	2,0	2,00E-04	0,035	0,01044	2151	217	
1,27E-01	1,27E-01	1,27E-01	1,27E-01	1,27E-01	1,27E-01	11044	2151	218
1,27E-01	1,27E-01	1,27E-01	1,27E-01	1,27E-01	1,27E-01	11044	2151	219
1,27E-01	1,27E-01	1,27E-01	1,27E-01	1,27E-01	1,27E-01	11044	2151	220
1,27E-01	1,27E-01	1,27E-01	1,27E-01	1,27E-01	1,27E-01	11044	2151	221
1,27E-01					1044	2151	222	
0,0	0,0	1	2	31	01044	2151	223	
1,00	4,0	2,0	2,00E-04	0,035	0,01044	2151	224	
2,86E-01	2,86E-01	2,86E-01	2,86E-01	2,86E-01	2,86E-01	11044	2151	225
2,86E-01	2,86E-01	2,86E-01	2,86E-01	2,86E-01	2,86E-01	11044	2151	226
2,86E-01	2,86E-01	2,86E-01	2,86E-01	2,86E-01	2,86E-01	11044	2151	227
2,86E-01	2,86E-01	2,86E-01	2,86E-01	2,86E-01	2,86E-01	11044	2151	228
2,86E-01					1044	2151	229	
0,0	0,0	1	1	31	01044	2151	230	
1.12	5,0	1,0	2.24E-04	0,035	0,01044	2151	231	
1,43E-01	1,43E-01	1,43E-01	1,43E-01	1,43E-01	1,43E-01	11044	2151	232
1,43E-01	1,43E-01	1,43E-01	1,43E-01	1,43E-01	1,43E-01	11044	2151	233
1,43E-01	1,43E-01	1,43E-01	1,43E-01	1,43E-01	1,43E-01	11044	2151	234
1,43E-01	1,43E-01	1,43E-01	1,43E-01	1,43E-01	1,43E-01	11044	2151	235
1,43E-01					1044	2151	236	

PROGRAM AVRA3, CALCULATES CROSS-SECTIONS IN THE UNRESOLVED RESONANCE REGION,

ENDF/B VERSION II DATA WITH ENERGY INDEPENDENT PARAMETERS.

RUN NO 1 TITLE AVERAGES TEST, PU-239 DATA EO 0.000000E+00 EN 0.000000E+00 ESTEP 0.000000E+00  
ENERGY LIMITS LOWER 3.000000E+02 UPPER 1.000000E+05 LRU= 2 LRF= 1 LFI= 0  
TARGET SPIN 5.0000E-01 SCATTERING LENGTH 9.0500E-01 NO OF ENERGY VALUES AT WHICH FISSION WIDTHS ARE GIVEN  
DATA FOR A FISSION NUCLEUS

S-WAVE DATA

FISSION WIDTHS ARE GIVEN AT THE FOLLOWING ENERGIES  
3.0000E+02 6.0000E+02 1.0000E+03 1.5000E+03 2.5000E+03 3.5000E+03  
5.0000E+03 8.0000E+03 1.3000E+04 2.0000E+04 3.0000E+04 4.0000E+04  
5.0000E+04 6.0000E+04 8.0000E+04 1.0000E+05  
ISOTOPIC MASS 2.3700E+02 ANGULAR MOMENTUM 0 NO OF SPIN STATES 2

MEAN LEVEL SPACING 8.7800E+00 LEVEL SPIN 0.0000E+00 REDUCED NEUTRON WIDTH 9.4000E-04 GAMMA GAMMA 3.8700E-01  
NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 1  
NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTION 2  
THE FISSION WIDTHS ARE  
2.8000E+00 2.8000E+00 2.8000E+00 2.8000E+00 2.8000E+00 2.8000E+00  
2.8000E+00 2.8000E+00 2.8000E+00 2.8000E+00 2.8000E+00 2.8000E+00  
2.8000E+00 2.8000E+00 2.8000E+00 2.8000E+00

MEAN LEVEL SPACING 3.1200E+00 LEVEL SPIN 1.0000E+00 REDUCED NEUTRON WIDTH 3.3400E-04 GAMMA GAMMA 3.8700E-01  
NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 1  
NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTION 1  
THE FISSION WIDTHS ARE  
5.5200E-02 5.5900E-02 5.6800E-02 5.7800E-02 5.9320E-02 6.2300E-02  
6.5700E-02 7.3300E-02 8.7200E-02 1.1020E-01 1.5020E-01 1.9750E-01  
2.4800E-01 3.0000E-01 3.8600E-01 4.8500E-01

P-WAVE DATA

ISOTOPIC MASS 2.3700E+02 ANGULAR MOMENTUM 1 NO OF SPIN STATES 3

MEAN LEVEL SPACING 8.7800E+00 LEVEL SPIN 0.0000E+00 REDUCED NEUTRON WIDTH 2.1950E-03 GAMMA GAMMA 3.8700E-01  
NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 1  
NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTION 2  
THE FISSION WIDTHS ARE  
4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02  
4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02

4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02

MEAN LEVEL SPACING 3.1200E+00 LEVEL SPIN 1.0000E+00 REDUCED NEUTRON WIDTH 7.8000E-04 GAMMA GAMMA 3.8700E-02  
NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 2  
NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTION 2  
THE FISSION WIDTHS ARE  
4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02  
4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02  
4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02

MEAN LEVEL SPACING 2.1200E+00 LEVEL SPIN 2.0000E+00 REDUCED NEUTRON WIDTH 5.3000E-04 GAMMA GAMMA 3.8700E-02  
NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 1  
NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTION 2  
THE FISSION WIDTHS ARE  
4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02  
4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02  
4.0000E-02 4.0000E-02 4.0000E-02 4.0000E-02

NUCLEAR RADIUS  $A=(1.23 \cdot \text{MASS}^{1/3} + 0.8) \cdot 0.1 = 8.4337E-01$   
AVERAGE SCATTERING CAPTURE AND FISSION CROSS-SECTIONS FOR A FISSION NUCLEUS  
TITLE AVERAGE3 TEST,PU=239 DATA

AVERAGE CROSS-SECTIONS CALCULATED USING GREENBLER APPROXIMATION

NEUTRON ENERGY (EV)	S-WAVE SCATRNG CROSS-SECTION	P-WAVE SCATRNG CROSS-SECTION	TOTAL
3.000000E+02	1.383416E+01	1.296935E-04	1.383429E+01
6.000000E+02	1.347005E+01	5.165503E-04	1.347056E+01
1.000000E+03	1.316930E+01	1.425274E-03	1.317073E+01
1.500000E+03	1.291372E+01	3.176370E-03	1.291690E+01
2.000000E+03	1.257470E+01	8.631692E-03	1.258333E+01
3.000000E+03	1.232965E+01	1.650611E-02	1.234616E+01
5.000000E+03	1.206458E+01	3.235447E-02	1.209694E+01
8.000000E+03	1.169198E+01	7.591461E-02	1.176790E+01
1.300000E+04	1.127335E+01	1.724855E-01	1.144583E+01
2.000000E+04	1.085939E+01	3.332512E-01	1.119264E+01
3.000000E+04	1.041848E+01	5.767438E-01	1.099523E+01
4.000000E+04	1.006689E+01	8.139086E-01	1.088080E+01
5.000000E+04	9.769172E+00	1.036500E+00	1.080567E+01
6.000000E+04	9.506816E+00	1.242964E+00	1.074978E+01
8.000000E+04	9.057618E+00	1.611006E+00	1.066862E+01
1.000000E+05	8.660133E+00	1.928741E+00	1.058887E+01

NEUTRON ENERGY (EV)	S-WAVE CAPTURE CROSS-SECTION	P-WAVE CAPTURE CROSS-SECTION	TOTAL
3.000000E+02	9.295319E+00	1.070727E-01	9.402392E+00
6.000000E+02	6.096594E+00	1.510540E-01	6.247648E+00
1.000000E+03	4.415238E+00	1.942551E-01	4.609493E+00
1.500000E+03	3.391673E+00	2.365860E-01	3.628259E+00
2.000000E+03	2.410175E+00	3.014797E-01	2.711655E+00
3.000000E+03	1.901494E+00	3.514680E-01	2.252962E+00
5.000000E+03	1.472163E+00	4.098882E-01	1.882051E+00
8.000000E+03	1.035008E+00	4.911123E-01	1.526120E+00
1.300000E+04	7.044900E-01	5.685306E-01	1.273021E+00
2.000000E+04	4.887895E-01	6.162974E-01	1.105078E+00
3.000000E+04	3.372530E-01	6.302902E-01	9.675432E-01
4.000000E+04	2.546110E-01	6.181940E-01	8.728050E-01
5.000000E+04	2.032893E-01	5.963265E-01	7.996159E-01
6.000000E+04	1.685859E-01	5.712251E-01	7.398140E-01
8.000000E+04	1.267224E-01	5.210052E-01	6.477276E-01

NEUTRON ENERGY (EV)	S-WAVE FISSION CROSS-SECTION	P-WAVE NEUTRON CROSS-SECTION	TOTAL
1.0000000E+05	1.003833E-01	4.757889E-01	5.761712E-01
3.0000000E+02	1.258888E+01	7.497054E-02	1.266305E+01
6.0000000E+02	8.656434E+00	1.058106E-01	8.762245E+00
1.0000000E+03	6.545967E+00	1.361744E-01	6.682141E+00
1.5000000E+03	5.232046E+00	1.660404E-01	5.398047E+00
2.5000000E+03	3.930985E+00	2.121837E-01	4.143168E+00
3.5000000E+03	3.272720E+00	2.481861E-01	3.520906E+00
5.0000000E+03	2.688795E+00	2.910436E-01	2.979833E+00
8.0000000E+03	2.087673E+00	3.529202E-01	2.440601E+00
1.3000000E+04	1.624818E+00	4.168780E-01	2.041696E+00
2.0000000E+04	1.322885E+00	4.635778E-01	1.786382E+00
3.0000000E+04	1.11848E+00	4.884854E-01	1.600334E+00
4.0000000E+04	9.94528E-01	4.905240E-01	1.485052E+00
5.0000000E+04	9.143779E-01	4.82187E-01	1.396566E+00
6.0000000E+04	8.537798E-01	4.690790E-01	1.322859E+00
8.0000000E+04	7.561141E-01	4.381376E-01	1.194252E+00
1.0000000E+05	6.926107E-01	4.071803E-01	1.0998807E+00

PROGRAM AVRA3, CALCULATES CROSS-SECTIONS IN THE UNRESOLVED RESONANCE REGION.

ENDF/B VERSION II DATA WITH ENERGY INDEPENDENT PARAMETERS.

RUN NO 2 TITLE AVERAGE3 TEST,U-238DATA EO 1.000000E+03 EN 1.000000E+05 ESTEP 1.000000E+03  
ENERGY LIMITS LOWER 3.920000E+03 UPPER 5.000000E+04 LRU= 2 LRF= 1 LFI= 0  
TARGET SPIN 0.0000E+00 SCATTERING LENGTH 9.1840E-01 NO OF ENERGY VALUES AT WHICH FISSION WIDTHS ARE GIVEN 2  
DATA FOR A NON-FISSILE NUCLEUS

S-WAVE DATA

ISOTOPIC MASS 2.3601E+02 ANGULAR MOMENTUM 0 NO OF SPIN STATES 1  
MEAN LEVEL SPACING 1.8500E+01 LEVEL SPIN 5.0000E-01 REDUCED NEUTRON WIDTH 1.7390E-03 GAMMA GAMMA 2.4600E-02  
NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 1

P-WAVE DATA

ISOTOPIC MASS 2.3601E+02 ANGULAR MOMENTUM 1 NO OF SPIN STATES 2  
MEAN LEVEL SPACING 1.8500E+01 LEVEL SPIN 5.0000E-01 REDUCED NEUTRON WIDTH 2.9230E-03 GAMMA GAMMA 2.4600E-02  
NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 1  
MEAN LEVEL SPACING 9.2500E+00 LEVEL SPIN 1.5000E+00 REDUCED NEUTRON WIDTH 1.4615E-03 GAMMA GAMMA 2.4600E-02  
NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 1  
NUCLEAR RADIUS  $A=(1.23*MASS**1/3+0.8)*0.1 = 8.4230E-01$

AVERAGE SCATTERING AND CAPTURE CROSS-SECTIONS FOR A NON-FISSILE NUCLEUS

TITLE AVERAGE3 TEST,U-238DATA

ENERGY LIMITS LOWER 1.0000E+03 UPPER 1.0000E+05

AVERAGE CROSS-SECTIONS CALCULATED USING GREENBLER APPROXIMATION

NEUTRON ENERGY(EV)	S-WAVE SCATRNG CROSS-SECTION	P-WAVE SCATRNG CROSS-SECTION	TOTAL
1.000000E+03	2.014256E+01	4.648083E-03	2.014721E+01
2.000000E+03	1.764954E+01	1.744892E-02	1.766709E+01
3.000000E+03	1.644058E+01	3.647962E-02	1.647706E+01
4.000000E+03	1.567848E+01	5.999283E-02	1.573847E+01
5.000000E+03	1.513575E+01	8.659303E-02	1.522235E+01
6.000000E+03	1.472052E+01	1.152270E-01	1.483574E+01
7.000000E+03	1.438738E+01	1.451215E-01	1.453250E+01
8.000000E+03	1.411092E+01	1.757174E-01	1.428663E+01
9.000000E+03	1.387560E+01	2.066137E-01	1.408222E+01
1.000000E+04	1.367133E+01	2.375251E-01	1.390886E+01
1.100000E+04	1.349119E+01	2.682505E-01	1.375944E+01
1.200000E+04	1.333027E+01	2.986493E-01	1.362892E+01
1.300000E+04	1.318497E+01	3.286254E-01	1.351359E+01
1.400000E+04	1.305258E+01	3.581147E-01	1.341069E+01
1.500000E+04	1.293100E+01	3.870764E-01	1.331808E+01
1.600000E+04	1.281862E+01	4.154869E-01	1.323411E+01
1.700000E+04	1.271411E+01	4.433347E-01	1.315745E+01
1.800000E+04	1.261643E+01	4.706171E-01	1.308705E+01
1.900000E+04	1.252471E+01	4.973383E-01	1.302205E+01
2.000000E+04	1.243823E+01	5.235065E-01	1.296174E+01
2.100000E+04	1.235641E+01	5.491333E-01	1.290554E+01
2.200000E+04	1.227872E+01	5.742326E-01	1.285295E+01
2.300000E+04	1.220474E+01	5.988195E-01	1.280356E+01
2.400000E+04	1.213411E+01	6.229101E-01	1.275702E+01
2.500000E+04	1.206650E+01	6.465207E-01	1.271302E+01
2.600000E+04	1.200164E+01	6.696681E-01	1.267131E+01
2.700000E+04	1.193929E+01	6.923688E-01	1.263166E+01

2.8000000E+04	1.187924E+01	7.146391E+01	1.259388E+01
3.9000000E+04	1.182129E+01	7.364949E+01	1.255779E+01
3.0000000E+04	1.176529E+01	7.579516E+01	1.252324E+01
3.1000000E+04	1.171108E+01	7.790243E+01	1.249010E+01
3.2000000E+04	1.165854E+01	7.997275E+01	1.245826E+01
3.3000000E+04	1.160754E+01	8.200751E+01	1.242761E+01
3.4000000E+04	1.155790E+01	8.400803E+01	1.239806E+01
3.5000000E+04	1.150977E+01	8.597562E+01	1.236952E+01
3.6000000E+04	1.146281E+01	8.791149E+01	1.234193E+01
3.7000000E+04	1.141703E+01	8.981682E+01	1.231520E+01
3.8000000E+04	1.137236E+01	9.169274E+01	1.228929E+01
3.9000000E+04	1.132873E+01	9.354032E+01	1.226413E+01
4.0000000E+04	1.128608E+01	9.536058E+01	1.223968E+01
4.1000000E+04	1.124435E+01	9.715452E+01	1.221590E+01
4.2000000E+04	1.120356E+01	9.892306E+01	1.219273E+01
4.3000000E+04	1.116348E+01	1.006671E+00	1.217015E+01
4.4000000E+04	1.112424E+01	1.023875E+00	1.214812E+01
4.5000000E+04	1.108575E+01	1.040850E+00	1.212660E+01
4.6000000E+04	1.104797E+01	1.057606E+00	1.210557E+01
4.7000000E+04	1.101086E+01	1.074148E+00	1.208501E+01
4.8000000E+04	1.097439E+01	1.09048E+00	1.206488E+01
4.9000000E+04	1.093854E+01	1.106620E+00	1.204516E+01
5.0000000E+04	1.090328E+01	1.122565E+00	1.202584E+01
5.1000000E+04	1.086857E+01	1.138322E+00	1.200689E+01
5.2000000E+04	1.083439E+01	1.153900E+00	1.198829E+01
5.3000000E+04	1.080074E+01	1.169302E+00	1.197004E+01
5.4000000E+04	1.076757E+01	1.184535E+00	1.195210E+01
5.5000000E+04	1.073487E+01	1.199604E+00	1.193448E+01
5.6000000E+04	1.070263E+01	1.214514E+00	1.191714E+01
5.7000000E+04	1.067082E+01	1.229270E+00	1.190009E+01
5.8000000E+04	1.063943E+01	1.243876E+00	1.188331E+01
5.9000000E+04	1.060844E+01	1.258336E+00	1.186678E+01
6.0000000E+04	1.057785E+01	1.272655E+00	1.185050E+01
6.1000000E+04	1.054762E+01	1.286837E+00	1.183446E+01
6.2000000E+04	1.051776E+01	1.300886E+00	1.181865E+01
6.3000000E+04	1.048825E+01	1.314806E+00	1.180305E+01
6.4000000E+04	1.045907E+01	1.328599E+00	1.178767E+01
6.5000000E+04	1.043022E+01	1.342270E+00	1.177249E+01
6.6000000E+04	1.040169E+01	1.355822E+00	1.175751E+01
6.7000000E+04	1.037346E+01	1.369258E+00	1.174272E+01
6.8000000E+04	1.034529E+01	1.382581E+00	1.172810E+01
6.9000000E+04	1.031737E+01	1.395794E+00	1.171367E+01
7.0000000E+04	1.029058E+01	1.408900E+00	1.169940E+01
7.1000000E+04	1.026380E+01	1.421901E+00	1.168530E+01
7.2000000E+04	1.023656E+01	1.434801E+00	1.167136E+01
7.3000000E+04	1.020997E+01	1.447601E+00	1.165757E+01
7.4000000E+04	1.018333E+01	1.460305E+00	1.164393E+01
7.5000000E+04	1.015753E+01	1.472913E+00	1.163044E+01
7.6000000E+04	1.013166E+01	1.485430E+00	1.161709E+01
7.7000000E+04	1.010611E+01	1.497856E+00	1.160387E+01
7.8000000E+04	1.008099E+01	1.510195E+00	1.159079E+01
7.9000000E+04	1.005553E+01	1.522447E+00	1.157783E+01
8.0000000E+04	1.003039E+01	1.534646E+00	1.156500E+01
8.1000000E+04	1.000559E+01	1.546702E+00	1.155229E+01
8.2000000E+04	9.980994E+00	1.558708E+00	1.153970E+01
8.3000000E+04	9.956592E+00	1.570636E+00	1.152723E+01
8.4000000E+04	9.932377E+00	1.582486E+00	1.151486E+01
8.5000000E+04	9.908347E+00	1.594262E+00	1.150261E+01
8.6000000E+04	9.884498E+00	1.605963E+00	1.149046E+01
8.7000000E+04	9.860824E+00	1.617593E+00	1.147842E+01
8.8000000E+04	9.837322E+00	1.629152E+00	1.146647E+01

8.900000E+04	9.813988E+00	1.640642E+00	1.145463E+01
9.000000E+04	9.790817E+00	1.652064E+00	1.144288E+01
9.100000E+04	9.767808E+00	1.663419E+00	1.143123E+01
9.200000E+04	9.744955E+00	1.674709E+00	1.141966E+01
9.300000E+04	9.722257E+00	1.685936E+00	1.140819E+01
9.400000E+04	9.699708E+00	1.697100E+00	1.139681E+01
9.500000E+04	9.677307E+00	1.708202E+00	1.138551E+01
9.600000E+04	9.655050E+00	1.719244E+00	1.137429E+01
9.700000E+04	9.632934E+00	1.730226E+00	1.136316E+01
9.800000E+04	9.610957E+00	1.741150E+00	1.135211E+01
9.900000E+04	9.589115E+00	1.752017E+00	1.134113E+01
1.000000E+05	9.567467E+00	1.762828E+00	1.133023E+01

NEUTRON ENERGY (EV)	S-WAVE CAPTURE CROSS-SECTION	P-WAVE CAPTURE CROSS-SECTION	TOTAL
1.000000E+03	2.602705E+00	2.045669E+01	2.807272E+00
2.000000E+03	1.450008E+00	2.775752E-01	1.727583E+00
3.000000E+03	1.022994E+00	3.238675E-01	1.346861E+00
4.000000E+03	7.964915E-01	3.550220E-01	1.151513E+00
5.000000E+03	6.549666E-01	3.762565E-01	1.031223E+00
6.000000E+03	5.576891E-01	3.905912E-01	9.482803E-01
7.000000E+03	4.864937E-01	3.999717E-01	8.864654E-01
8.000000E+03	4.320128E-01	4.057238E-01	8.377366E-01
9.000000E+03	3.889101E-01	4.087823E-01	7.976924E-01
1.000000E+04	3.539154E-01	4.098224E-01	7.637378E-01
1.100000E+04	3.249098E-01	4.093407E-01	7.342505E-01
1.200000E+04	3.004580E-01	4.077075E-01	7.081655E-01
1.300000E+04	2.795524E-01	4.052024E-01	6.847548E-01
1.400000E+04	2.614641E-01	4.0220384E-01	6.635024E-01
1.500000E+04	2.456523E-01	3.983793E-01	6.440316E-01
1.600000E+04	2.317074E-01	3.943520E-01	6.260594E-01
1.700000E+04	2.193130E-01	3.900552E-01	6.093682E-01
1.800000E+04	2.082209E-01	3.855662E-01	5.937872E-01
1.900000E+04	1.982336E-01	3.809460E-01	5.791795E-01
2.000000E+04	1.891916E-01	3.762422E-01	5.654338E-01
2.100000E+04	1.809653E-01	3.714927E-01	5.524579E-01
2.200000E+04	1.734476E-01	3.667273E-01	5.401749E-01
2.300000E+04	1.665495E-01	3.619697E-01	5.285192E-01
2.400000E+04	1.601967E-01	3.572384E-01	5.174351E-01
2.500000E+04	1.543261E-01	3.525480E-01	5.068741E-01
2.600000E+04	1.488841E-01	3.479098E-01	4.967939E-01
2.700000E+04	1.438249E-01	3.433327E-01	4.871576E-01
2.800000E+04	1.391089E-01	3.388234E-01	4.779323E-01
2.900000E+04	1.347020E-01	3.343868E-01	4.690888E-01
3.000000E+04	1.305743E-01	3.300268E-01	4.606011E-01
3.100000E+04	1.266999E-01	3.257457E-01	4.524457E-01
3.200000E+04	1.230558E-01	3.215455E-01	4.446013E-01
3.300000E+04	1.196219E-01	3.174269E-01	4.370488E-01
3.400000E+04	1.163802E-01	3.133903E-01	4.297705E-01
3.500000E+04	1.133149E-01	3.094358E-01	4.227507E-01
3.600000E+04	1.104117E-01	3.055628E-01	4.159745E-01
3.700000E+04	1.076500E-01	3.017705E-01	4.094285E-01
3.800000E+04	1.050424E-01	2.980579E-01	4.031004E-01
3.900000E+04	1.025547E-01	2.944239E-01	3.969786E-01
4.000000E+04	1.001855E-01	2.908670E-01	3.910526E-01
4.100000E+04	9.792659E-02	2.873859E-01	3.853125E-01
4.200000E+04	9.577024E-02	2.839790E-01	3.797492E-01
4.300000E+04	9.370056E-02	2.806446E-01	3.743542E-01
4.400000E+04	9.173027E-02	2.773812E-01	3.691195E-01
4.500000E+04	8.985000E-02	2.741871E-01	3.640377E-01



4.600000E+04  
4.700000E+04  
4.800000E+04  
4.900000E+04  
5.000000E+04  
5.100000E+04  
5.200000E+04  
5.300000E+04  
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6.300000E+04  
6.400000E+04  
6.500000E+04  
6.600000E+04  
6.700000E+04  
6.800000E+04  
6.900000E+04  
7.000000E+04  
7.100000E+04  
7.200000E+04  
7.300000E+04  
7.400000E+04  
7.500000E+04  
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8.500000E+04  
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9.200000E+04  
9.300000E+04  
9.400000E+04  
9.500000E+04  
9.600000E+04  
9.700000E+04  
9.800000E+04  
9.900000E+04  
1.000000E+05

8.804128E-02  
8.630548E-02  
8.463876E-02  
8.303701E-02  
8.149648E-02  
8.001369E-02  
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7.720864E-02  
7.588064E-02  
7.459881E-02  
7.336078E-02  
7.216430E-02  
7.100729E-02  
6.988782E-02  
6.880407E-02  
6.775433E-02  
6.673701E-02  
6.575061E-02  
6.479374E-02  
6.386507E-02  
6.296335E-02  
6.208743E-02  
6.123619E-02  
6.040800E-02  
5.960367E-02  
5.882049E-02  
5.805815E-02  
5.731585E-02  
5.659278E-02  
5.588821E-02  
5.520143E-02  
5.453176E-02  
5.387856E-02  
5.324123E-02  
5.261919E-02  
5.201190E-02  
5.141802E-02  
5.083946E-02  
5.027335E-02  
4.972002E-02  
4.917906E-02  
4.865003E-02  
4.813256E-02  
4.762626E-02  
4.713076E-02  
4.664573E-02  
4.617083E-02  
4.570575E-02  
4.525018E-02  
4.480382E-02  
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4.393766E-02  
4.351732E-02  
4.310516E-02  
4.270091E-02

2.710607E-01  
2.580001E-01  
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2.536293E-01  
2.509303E-01  
2.482861E-01  
2.456952E-01  
2.431563E-01  
2.406678E-01  
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2.358370E-01  
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2.311924E-01  
2.289369E-01  
2.267242E-01  
2.245533E-01  
2.224231E-01  
2.203325E-01  
2.182805E-01  
2.162660E-01  
2.142880E-01  
2.123457E-01  
2.104381E-01  
2.085644E-01  
2.067236E-01  
2.049149E-01  
2.031376E-01  
2.013908E-01  
1.996738E-01  
1.979858E-01  
1.963262E-01  
1.946942E-01  
1.930892E-01  
1.915106E-01  
1.899576E-01  
1.884297E-01  
1.869264E-01  
1.854469E-01  
1.839908E-01  
1.825576E-01  
1.811466E-01  
1.797574E-01  
1.783896E-01  
1.770425E-01  
1.757158E-01  
1.744090E-01  
1.731217E-01  
1.718534E-01  
1.706037E-01  
1.693722E-01  
1.681585E-01  
1.669623E-01

3.591020E-01  
3.543056E-01  
3.496427E-01  
3.451073E-01  
3.406942E-01  
3.363983E-01  
3.322147E-01  
3.281389E-01  
3.241667E-01  
3.202940E-01  
3.165170E-01  
3.128321E-01  
3.092358E-01  
3.057248E-01  
3.022961E-01  
2.989467E-01  
2.956739E-01  
2.924748E-01  
2.893471E-01  
2.862882E-01  
2.832959E-01  
2.803679E-01  
2.775021E-01  
2.746966E-01  
2.719494E-01  
2.692586E-01  
2.666225E-01  
2.640394E-01  
2.615077E-01  
2.590258E-01  
2.565922E-01  
2.542055E-01  
2.518644E-01  
2.495674E-01  
2.473134E-01  
2.451011E-01  
2.429294E-01  
2.407971E-01  
2.387031E-01  
2.366464E-01  
2.346260E-01  
2.326409E-01  
2.306901E-01  
2.287729E-01  
2.268882E-01  
2.250353E-01  
2.232134E-01  
2.214216E-01  
2.196592E-01  
2.179255E-01  
2.162198E-01  
2.145413E-01  
2.128895E-01  
2.112637E-01  
2.096633E-01

PROGRAM AVRA3, CALCULATES CROSS-SECTIONS IN THE UNRESOLVED RESONANCE REGION,

ENDF/B VERSION II DATA WITH ENERGY INDEPENDENT PARAMETERS,

RUN NO 3 TITLE AVERAGE3 TEST, U-235 DATA E0 0.000000E+00 EN 0.000000E+20 ESTEP 0.000000E+00  
ENERGY LIMITS LOWER 6.450400E+01 UPPER 5.000000E+04 LRU= 2 LRF= 1 LFI= 0  
TARGET SPIN 3.5000E+00 SCATTERING LENGTH 8.3668E-01 NO OF ENERGY VALUES AT WHICH FISSION WIDTHS ARE GIVEN 25  
DATA FOR A FISSION NUCLEUS

S-WAVE DATA

FISSION WIDTHS ARE GIVEN AT THE FOLLOWING ENERGIES  
6.4504E+01 8.2000E+01 1.2500E+02 1.7500E+02 2.2500E+02 2.7500E+02  
3.5000E+02 4.5000E+02 6.0000E+02 8.5000E+02 1.2500E+03 1.7500E+03  
2.5000E+03 3.5000E+03 4.5000E+03 5.5000E+03 7.0000E+03 9.0000E+03  
1.2500E+04 1.7500E+04 2.2500E+04 2.7500E+04 3.5000E+04 4.5000E+04  
5.0000E+04  
ISOTOPIC MASS 2.3302E+02 ANGULAR MOMENTUM 0 NO OF SPIN STATES 2

MEAN LEVEL SPACING 1.0000E+00 LEVEL SPIN 3.0000E+00 REDUCED NEUTRON WIDTH 1.0000E-04 GAMMA GAMMA 3.5000E-02  
NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 1  
NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTION 2  
THE FISSION WIDTHS ARE  
2.9474E-01 2.9264E-01 2.4623E-01 2.4258E-01 2.6413E-01 4.9705E-01  
2.7310E-01 4.5109E-01 4.4004E-01 2.3327E-01 3.0220E-01 3.5300E-01  
4.2449E-01 3.2358E-01 3.2196E-01 3.2284E-01 3.3009E-01 3.3291E-01  
4.3837E-01 4.3870E-01 4.5035E-01 4.7280E-01 5.2078E-01 5.9992E-01  
5.7033E-01

MEAN LEVEL SPACING 1.0000E+00 LEVEL SPIN 4.0000E+00 REDUCED NEUTRON WIDTH 1.0000E-04 GAMMA GAMMA 3.5000E-02  
NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 1  
NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTION 1  
THE FISSION WIDTHS ARE  
1.4737E-01 1.4632E-01 1.2311E-01 1.2129E-01 1.3207E-01 2.4852E-01  
1.3655E-01 2.2554E-01 2.2002E-01 1.1663E-01 1.5110E-01 1.7650E-01  
2.1225E-01 1.6179E-01 1.6098E-01 1.6142E-01 1.6505E-01 1.6646E-01  
2.1918E-01 2.1935E-01 2.2517E-01 2.3640E-01 2.6039E-01 2.9996E-01  
2.8517E-01

P-WAVE DATA

ISOTOPIC MASS 2.3302E+02 ANGULAR MOMENTUM 1 NO OF SPIN STATES 4

MEAN LEVEL SPACING 1.1600E+00 LEVEL SPIN 2.0000E+00 REDUCED NEUTRON WIDTH 2.3200E-04 GAMMA GAMMA 3.5000E-02  
 NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 1  
 NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTION 2  
 THE FISSION WIDTHS ARE  
 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01  
 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01  
 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01  
 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01 3.3200E-01  
 3.3200E-01

MEAN LEVEL SPACING 1.0000E+00 LEVEL SPIN 3.0000E+00 REDUCED NEUTRON WIDTH 2.0000E-04 GAMMA GAMMA 3.5000E-02  
 NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 2  
 NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTION 1  
 THE FISSION WIDTHS ARE  
 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01  
 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01  
 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01  
 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01 1.2700E-01  
 1.2700E-01

MEAN LEVEL SPACING 1.0000E+00 LEVEL SPIN 4.0000E+00 REDUCED NEUTRON WIDTH 2.0000E-04 GAMMA GAMMA 3.5000E-02  
 NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 2  
 NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTION 2  
 THE FISSION WIDTHS ARE  
 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01  
 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01  
 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01  
 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01 2.8600E-01  
 2.8600E-01

MEAN LEVEL SPACING 1.1200E+00 LEVEL SPIN 5.0000E+00 REDUCED NEUTRON WIDTH 2.2400E-04 GAMMA GAMMA 3.5000E-02  
 NO OF DEGREES OF FREEDOM FOR NEUTRON WIDTH DISTRIBUTION 1  
 NO OF DEGREES OF FREEDOM FOR FISSION WIDTH DISTRIBUTION 1  
 THE FISSION WIDTHS ARE  
 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01  
 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01  
 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01  
 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01 1.4300E-01  
 1.4300E-01

NUCLEAR RADIUS A=(1.23\*MASS\*\*1/3+0.8)\*0.1 = 6.3908E-01  
 AVERAGE SCATTERING CAPTURE AND FISSION CROSS-SECTIONS FOR A FISSION NUCLEUS  
 TITLE AVERAGES TEST, U-235 DATA  
 AVERAGE CROSS-SECTIONS CALCULATED USING GREENBLER APPROXIMATION  
 NEUTRON ENERGY(EV) S-WAVE SCATRNG CROSS-SECTION P-WAVE SCATRNG CROSS-SECTION TOTAL  
 6.450400E+01 9.786764E+00 9.226386E-07 9.788764E+00  
 8.200000E+01 9.783050E+00 1.490894E-06 9.783051E+00  
 1.250000E+02 9.837830E+00 3.463222E-06 9.837833E+00  
 1.750000E+02 9.826114E+00 6.785592E-06 9.826121E+00  
 2.250000E+02 9.775332E+00 1.121284E-05 9.775334E+00  
 2.750000E+02 9.523842E+00 1.674392E-05 9.523858E+00  
 3.250000E+02 9.731142E+00 2.710691E-05 9.731169E+00  
 4.500000E+02 9.525672E+00 4.477490E-05 9.525717E+00  
 6.000000E+02 9.511716E+00 7.950534E-05 9.511795E+00  
 8.500000E+02 9.708309E+00 1.592399E-04 9.708468E+00  
 1.250000E+03 9.1565566E+00 3.432135E-04 9.1565909E+00

1.750000E+03	9.467040E+00	6.697206E-04	9.467710E+00
2.500000E+03	9.354840E+00	1.357264E+03	9.356197E+00
3.500000E+03	9.376833E+00	2.634245E+03	9.379467E+00
4.500000E+03	9.325037E+00	4.310002E+03	9.329347E+00
5.500000E+03	9.276947E+00	6.370052E+03	9.283317E+00
7.000000E+03	9.207707E+00	1.014860E+02	9.217856E+00
9.000000E+03	9.131486E+00	1.639498E+02	9.147881E+00
1.250000E+04	8.953983E+00	3.032915E+02	8.984312E+00
1.750000E+04	8.821273E+00	5.588043E+02	8.877153E+00
2.250000E+04	8.698854E+00	8.676379E+02	8.785617E+00
2.750000E+04	8.582843E+00	1.217690E+01	8.704612E+00
3.500000E+04	8.419337E+00	1.799386E+01	8.599276E+00
4.500000E+04	8.219320E+00	2.644437E+01	8.483764E+00
5.000000E+04	8.144976E+00	3.085493E+01	8.453526E+00

NEUTRON ENERGY (EV)	S-WAVE CAPTURE CROSS-SECTION	P-WAVE CAPTURE CROSS-SECTION	TOTAL
6.450400E+01	1.670961E+01	2.245335E+02	1.673206E+01
8.200000E+01	1.480249E+01	2.531427E+02	1.482780E+01
1.250000E+02	1.275553E+01	3.124925E+02	1.278678E+01
1.750000E+02	1.075604E+01	3.696708E+02	1.079301E+01
2.250000E+02	9.102277E+00	4.190795E+02	9.144683E+00
2.750000E+02	6.249314E+00	4.632106E+02	6.295635E+00
3.500000E+02	7.099218E+00	5.224000E+02	7.151458E+00
4.500000E+02	5.017959E+00	5.920781E+02	5.077167E+00
6.000000E+02	4.344129E+00	6.831923E+02	4.412448E+00
8.500000E+02	4.670069E+00	8.121629E+02	4.751285E+00
1.250000E+03	3.401904E+00	9.828374E+02	3.500267E+00
1.750000E+03	2.642962E+00	1.159675E+01	2.758929E+00
2.500000E+03	1.997828E+00	1.379888E+01	2.135816E+00
3.500000E+03	1.841602E+00	1.622263E+01	2.003828E+00
4.500000E+03	1.592930E+00	1.826941E+01	1.775625E+00
5.500000E+03	1.413095E+00	2.005299E+01	1.613625E+00
7.000000E+03	1.212624E+00	2.236819E+01	1.436306E+00
9.000000E+03	1.038101E+00	2.496294E+01	1.287730E+00
1.250000E+04	7.600101E-01	2.856517E+01	1.045662E+00
1.750000E+04	6.166210E-01	3.233384E+01	9.399593E-01
2.250000E+04	5.208346E-01	3.502874E+01	8.711220E-01
2.750000E+04	4.494779E-01	3.698578E+01	8.193356E-01
3.500000E+04	3.701678E-01	3.896464E+01	7.598143E-01
4.500000E+04	2.967705E-01	4.042575E+01	7.010280E-01
5.000000E+04	2.828500E-01	4.081669E+01	6.910168E-01
NEUTRON ENERGY (EV)	S-WAVE FISSION CROSS-SECTION	P-WAVE NEUTRON CROSS-SECTION	TOTAL
6.450400E+01	3.363107E+01	4.449157E+02	3.367556E+01
8.200000E+01	2.973384E+01	5.016079E+02	2.978400E+01
1.250000E+02	2.306274E+01	6.192206E+02	2.312466E+01
1.750000E+02	1.935532E+01	7.325386E+02	1.942857E+01
2.250000E+02	1.737230E+01	8.304681E+02	1.745534E+01
2.750000E+02	1.784734E+01	9.179468E+02	1.793913E+01
3.500000E+02	1.395819E+01	1.035292E+01	1.406172E+01
4.500000E+02	1.363367E+01	1.173465E+01	1.375102E+01
6.000000E+02	1.170601E+01	1.354217E+01	1.184143E+01
8.500000E+02	8.476841E+00	1.610252E+01	8.637866E+00
1.250000E+03	7.385552E+00	1.949551E+01	7.580507E+00
1.750000E+03	6.413942E+00	2.301918E+01	6.644134E+00
2.500000E+03	5.531043E+00	2.742395E+01	5.805282E+00
3.500000E+03	4.353070E+00	3.230284E+01	4.676098E+00
4.500000E+03	3.798900E+00	3.645792E+01	4.163479E+00
5.500000E+03	3.410830E+00	4.011337E+01	3.811963E+00
7.000000E+03	3.008405E+00	4.492115E+01	3.457617E+00

9.000000E+03  
1.250000E+04  
1.750000E+04  
2.250000E+04  
2.750000E+04  
3.500000E+04  
4.500000E+04  
5.000000E+04

2.627382E+00  
2.345241E+00  
1.947829E+00  
1.703901E+00  
1.540581E+00  
1.376495E+00  
1.234570E+00  
1.149153E+00

5.042107E-01  
5.633680E-01  
6.716611E-01  
7.405824E-01  
7.958978E-01  
8.604654E-01  
9.222714E-01  
9.455514E-01

3.131593E+00  
2.928609E+00  
2.619490E+00  
2.444483E+00  
2.336479E+00  
2.236960E+00  
2.156841E+00  
2.094705E+00





	P-WAVE SIGMAFISS	D-WAVE SIGMAFISS	TOTAL SIGMAAVG
1			AVG4122
2	FISS)		AVG4123
37	FORMAT(33H AVERAGE SCATTERING CROSS-SECTION)		AVG4124
38	FORMAT(30H AVERAGE CAPTURE CROSS-SECTION)		AVG4125
39	FORMAT(30H AVERAGE FISSION CROSS-SECTION)		AVG4126
40	FORMAT(2X,7E15,6)		AVG4127
41	FORMAT(45H INPUT PARAMETERS WITH CALCULATED TOTAL WIDTH)		AVG4128
42	FORMAT(10H L-VALUE=15,10H J-STATE=F5,2)		AVG4129
43	FORMAT(79H1 PROGRAM AVRAGE4, CALCULATES CROSS-SECTIONS IN THE UNRESOLVED RESONANCE REGION)		AVG4130
44	FORMAT(56H ENDF/B VERSION II DATA WITH ENERGY DEPENDENT PARAMETERS)		AVG4131
1)			AVG4132
300	T=2.196771E-03*(AWRI/(AWRI+1.0))		AVG4133
	CONST=19.7392088/(T*T)		AVG4134
	PHIFOUR=12.566371		AVG4135
	CPEN=2.196771E-03*(AWRI/(AWRI+1.0))*APEN		AVG4136
	C=2.196771E-03*(AWRI/(AWRI+1.0))*A		AVG4137
	DO 403 I=1,3		AVG4138
	DO 405 K=1, 75		AVG4139
	DO 404 J=1,6		AVG4140
	SIGC(I,J,K)=0.0		AVG4141
	SIGS(I,J,K)=0.0		AVG4142
	SIGF(I,J,K)=0.0		AVG4143
	GTC(I,J,K)=0.0		AVG4144
404	CONTINUE		AVG4145
	SIGCT(I,K)=0.0		AVG4146
	SIGST(I,K)=0.0		AVG4147
	SIGFT(I,K)=0.0		AVG4148
	SIGPT(I,K)=0.0		AVG4149
405	CONTINUE		AVG4150
403	CONTINUE		AVG4151
	DO 400 I=1,NLS		AVG4152
	NJSI=NJS(I)		AVG4153
	LI=L(I)		AVG4154
	FIL=FLOAT (LI)		AVG4155
	LI=LI+1		AVG4156
	DO 401 J=1,NJSI		AVG4157
	AJIJ=AJ(I,J)		AVG4158
	NEIJ=NE(I,J)		AVG4159
	GJ=(2.0*AJIJ+1.0)/(4.0*SPIN+2.0)		AVG4160
	AMUNIJ=AMUN(I,J)		AVG4161
	AMUFIJ=AMUF(I,J)		AVG4162
	AMUXIJ=AMUX(I,J)		AVG4163
	MU=INT(AMUNIJ)		AVG4164
	NU=INT(AMUFIJ)		AVG4165
	LAMBDA=INT(AMUXIJ)		AVG4166
	DO 402 K=1,NEIJ		AVG4167
	EIJK=E(I,J,K)		AVG4168
	E2=SQRT(EIJK)		AVG4169
	WAVE=2.196771E-03*(AWRI/(AWRI+1.0))*E2		AVG4170
	RHO=C*E2		AVG4171
	RHOPEN=CPEN*E2		AVG4172
	GO TO(500,501,502),LII		AVG4173
500	VL=E2*AMUN(I,J)		AVG4174
	PS=RHO		AVG4175
	GO TO 503		AVG4176
501	VL=E2*(RHOPEN**2/(1.0+RHOPEN**2))*AMUN(I,J)		AVG4177
	PS=RHO-ATAN(RHO)		AVG4178
	GO TO 503		AVG4179
502	VL=E2*(RHOPEN**4/(RHOPEN**4+3.0*RHOPEN*RHOPEN+9.0))*AMUN(I,J)		AVG4180
	PS=RHO-ATAN(3.0*RHO/(3.0+RHOPEN**2))		AVG4181



503	SIGPOT=(SIN(PS)/WAVE)**2	AVG4182
	SIGPOT=SIGPOT*PHIFOUR*(2,0*FIL+1,0)	AVG4183
	GN=GNO(I,J,K)*VL	AVG4184
	GAMMA=GG(I,J,K)	AVG4185
	GALPHA=GN	AVG4186
	GBETA=GF(I,J,K)	AVG4187
	DIFF=GX(I,J,K)	AVG4188
	GTC(I,J,K)=GN+GAMMA+GBETA+DIFF	AVG4189
752	TERG=(CONST*GJ*GN*GAMMA)/(EIJK*D(I,J,K))	AVG4190
	TERS=(CONST*GJ*GN*GN)/(EIJK*D(I,J,K))	AVG4191
	TERF=(CONST*GJ*GN*GBETA)/(EIJK*D(I,J,K))	AVG4192
	CALL GNRL(GALPHA,GBETA,GAMMA,MU,NU,LAMBDA,GS,DIFF,1)	AVG4193
	CALL GNRL(GALPHA,GBETA,GAMMA,MU,NU,LAMBDA,GC,DIFF,2)	AVG4194
	CALL GNRL(GALPHA,GBETA,GAMMA,MU,NU,LAMBDA,GFF,DIFF,3)	AVG4195
	GS=GS*TERS	AVG4196
	GC=GC*TERG	AVG4197
	GFF=GFF*TERF	AVG4198
	CORR=(CONST*GJ*2,0*GN*SIN(PS)*SIN(PS))/(EIJK*D(I,J,K))	AVG41981
	GS=GS-CORR	AVG41982
	SIGC(I,J,K)=GC	AVG4199
	SIGS(I,J,K)=GS	AVG4200
	SIGF(I,J,K)=GFF	AVG4201
	SIGPT(I,K)=SIGPCT	AVG4202
402	CONTINUE	AVG4203
401	CONTINUE	AVG4204
400	CONTINUE	AVG4205
	PRINT25	AVG4206
	PRINT41	AVG4207
	PRINT25	AVG4208
	DO 8000 I=1,NLS	AVG4209
	LII=L(I)	AVG4210
	NJSI=NJS(I)	AVG4211
	DO 8001 J=1,NJSI	AVG4212
	AJIJ=AJ(I,J)	AVG4213
	NEIJ=NE(I,J)	AVG4214
	PRINT42,LII,AJIJ	AVG4215
	PRINT25	AVG4216
	PRINT22	AVG4217
	PRINT40,(E(I,J,KK),D(I,J,KK),GX(I,J,KK),GTC(I,J,KK),GNO(I,J,KK),	AVG4218
	1GG(I,J,KK),GF(I,J,KK),KK=1,NEIJ)	AVG4219
8001	CONTINUE	AVG4220
8000	CONTINUE	AVG4221
	DO 800 K=1,75	AVG4222
	DO 801 I=1,3	AVG4223
	DO 802 J=1,6	AVG4224
	SIGCT(I,K)=SIGCT(I,K)+SIGC(I,J,K)	AVG4225
	SIGST(I,K)=SIGST(I,K)+SIGS(I,J,K)	AVG4226
	SIGFT(I,K)=SIGFT(I,K)+SIGF(I,J,K)	AVG4227
802	CONTINUE	AVG4228
	SIGST(I,K)=SIGST(I,K)+SIGPT(I,K)	AVG4229
801	CONTINUE	AVG4230
800	CONTINUE	AVG4231
	NN=NE(1,1)	AVG4232
	PRINT25	AVG4233
	PRINT37	AVG4234
	PRINT25	AVG4235
	PRINT34	AVG4236
	DO 900 K=1,NN	AVG4237
	TERM=0,0	AVG4238
	DO 901 I=1,3	AVG4239
	TERM=TERM+SIGST(I,K)	AVG4240

901	CONTINUE	AVG4241
	PRINT 24,E(1,1,K),SIGST(1,K),SIGST(2,K),SIGST(3,K),TERM	AVG4242
900	CONTINUE	AVG4243
	PRINT25	AVG4244
	PRINT38	AVG4245
	PRINT25	AVG4246
	PRINT35	AVG4247
	DO 902 K=1,NN	AVG4248
	TERM=0.0	AVG4249
	DO 903 I=1,3	AVG4250
	TERM=TERM+SIGCT(I,K)	AVG4251
903	CONTINUE	AVG4252
	PRINT 24,E(1,1,K),SIGCT(1,K),SIGCT(2,K),SIGCT(3,K),TERM	AVG4253
902	CONTINUE	AVG4254
	PRINT25	AVG4255
	PRINT39	AVG4256
	PRINT25	AVG4257
	PRINT36	AVG4258
	DO 904 K=1,NN	AVG4259
	TERM=0.0	AVG4260
	DO 905 I=1,3	AVG4261
	TERM=TERM+SIGFT(I,K)	AVG4262
905	CONTINUE	AVG4263
	PRINT 24,E(1,1,K),SIGFT(1,K),SIGFT(2,K),SIGFT(3,K),TERM	AVG4264
904	CONTINUE	AVG4265
	GO TO 901	AVG4266
8800	CALL EXIT	AVG4267
	END	AVG4268
	SUBROUTINE GNRL(GALPHA,GBETA,GAMMA,MU,NU,LAMBDA,S,DF,IO)	GNRL001
	COMMON/XBAR/XX(4,10)	GNRL002
	S=0.0	GNRL003
	IF(GALPHA)1000,1000,1001	GNRL004
1001	IF(GAMMA)1000,1000,1002	GNRL005
1002	IF(GBETA)1000,1003,1004	GNRL006
1003	IF(DF)1000,1005,1006	GNRL007
1005	DO 100 J=1,10	GNRL008
	XJ=XX(MU,J)	GNRL009
	GO TO(200,201,202),IO	GNRL010
200	S=S+((XJ*XJ)/(GALPHA*XJ+GAMMA))	GNRL011
	GO TO 100	GNRL012
201	S=S+(XJ/(GALPHA*XJ+GAMMA))	GNRL013
202	CONTINUE	GNRL014
100	CONTINUE	GNRL015
	S=S/10.0	GNRL016
	GO TO 1000	GNRL017
1006	DO 101 J=1,10	GNRL018
	XJ=XX(MU,J)	GNRL019
	DO 102 K=1,10	GNRL020
	XK=XX(LAMBDA,K)	GNRL021
	GO TO(300,301,302),IO	GNRL022
300	S=S+((XJ*XJ)/(GALPHA*XJ+GAMMA+DF*XK))	GNRL023
	GO TO 100	GNRL024
301	S=S+(XJ/(GALPHA*XJ+GAMMA+DF*XK))	GNRL025
302	CONTINUE	GNRL026
102	CONTINUE	GNRL027
101	CONTINUE	GNRL028
	S=S/100.0	GNRL029
	GO TO 1000	GNRL030
1004	IF(DF)1000,1007,1008	GNRL031
1007	DO 103 J=1,10	GNRL032
	XJ=XX(MU,J)	GNRL033

DO 104 K=1,10	GNRL034
XK=XX(NU,K)	GNRL035
GO TO(400,401,402),ID	GNRL036
400 S=S+((XJ*XJ)/(GALPHA*XJ+GBETA*XK+GAMMA))	GNRL037
GO TO 104	GNRL038
401 S=S+(XJ/(GALPHA*XJ+GBETA*XK+GAMMA))	GNRL039
GO TO 104	GNRL040
402 S=S+((XJ*XK)/(GALPHA*XJ+GBETA*XK+GAMMA))	GNRL041
104 CONTINUE	GNRL042
103 CONTINUE	GNRL043
S=S/100.0	GNRL044
GO TO 1000	GNRL045
1008 DO 105 J=1,10	GNRL046
XJ=XX(MU,J)	GNRL047
DO 106 K=1,10	GNRL048
XK=XX(NU,K)	GNRL049
DO 107 L=1,10	GNRL050
XL=XX(LAMBDA,L)	GNRL051
GO TO(500,501,502),ID	GNRL052
500 S=S+((XJ*XJ)/(GALPHA*XJ+GBETA*XK+GAMMA+DF*XL))	GNRL053
GO TO 107	GNRL054
501 S=S+(XJ/(GALPHA*XJ+GBETA*XK+GAMMA+DF*XL))	GNRL055
GO TO 107	GNRL056
502 S=S+((XJ*XK)/(GALPHA*XJ+GBETA*XK+GAMMA+DF*XL))	GNRL057
107 CONTINUE	GNRL058
106 CONTINUE	GNRL059
105 CONTINUE	GNRL060
S=S/1000.0	GNRL061
1000 RETURN	GNRL062
END	GNRL063

100 AVERAGE4 TEST, U-235 DATA

64.504	24788.0	2	2	0	01102	2151
3.5	0.926	0	0	2	01102	2151
233.025	0.0	0	0	2	01102	2151
3.0000E+00	0.0	5	0	156	251102	2151
0.	0.	0.	1.0000E+00	0.	2.0000E+00	01102 2151
6.4504E+01	1.0000E+00	0.	7.1807E-05	3.5000E-02	2.9347E-01	
8.2902E+01	1.0000E+00	0.	8.1753E-05	3.5000E-02	2.9133E-01	
1.1569E+02	1.0000E+00	0.	9.0472E-05	3.5000E-02	2.4665E-01	
1.4855E+02	1.0000E+00	0.	1.0486E-04	3.5000E-02	2.1766E-01	
1.9074E+02	1.0000E+00	0.	1.0389E-04	3.5000E-02	2.6593E-01	
2.4491E+02	1.0000E+00	0.	1.3175E-04	3.5000E-02	3.8029E-01	
3.1447E+02	1.0000E+00	0.	9.6060E-05	3.5000E-02	3.5141E-01	
4.0379E+02	1.0000E+00	0.	8.8629E-05	3.5000E-02	3.7344E-01	
5.1848E+02	1.0000E+00	0.	1.1455E-04	3.5000E-02	5.1390E-01	
6.6574E+02	1.0000E+00	0.	1.1126E-04	3.5000E-02	3.4713E-01	
8.5482E+02	1.0000E+00	0.	1.0479E-04	3.5000E-02	2.5096E-01	
1.0976E+03	1.0000E+00	0.	1.1267E-04	3.5000E-02	2.5373E-01	
1.4093E+03	1.0000E+00	0.	9.9890E-05	3.5000E-02	3.4813E-01	
1.8096E+03	1.0000E+00	0.	1.0160E-04	3.5000E-02	3.7083E-01	
2.3236E+03	1.0000E+00	0.	9.8627E-05	3.5000E-02	4.3610E-01	
2.9836E+03	1.0000E+00	0.	9.9029E-05	3.5000E-02	4.3348E-01	
3.8310E+03	1.0000E+00	0.	1.0729E-04	3.5000E-02	4.2475E-01	
4.9191E+03	1.0000E+00	0.	9.9664E-05	3.5000E-02	4.3055E-01	
6.3163E+03	1.0000E+00	0.	9.6419E-05	3.5000E-02	4.3506E-01	
8.1103E+03	1.0000E+00	0.	9.4417E-05	3.5000E-02	4.4334E-01	
1.0414E+04	1.0000E+00	0.	9.7638E-05	3.5000E-02	4.4325E-01	
1.3372E+04	1.0000E+00	0.	9.9719E-05	3.5000E-02	4.4530E-01	
1.7169E+04	1.0000E+00	0.	9.8693E-05	3.5000E-02	4.5646E-01	
2.2046E+04	1.0000E+00	0.	9.5268E-05	3.5000E-02	4.7366E-01	
2.4788E+04	1.0000E+00	0.	1.0075E-04	3.5000E-02	4.6219E-01	
4.0000E+00	0.	5	0	156	251102	2151
0.	0.	0.	1.0000E+00	0.	1.0000E+00	01102 2151
6.4504E+01	1.0000E+00	0.	7.1807E-05	3.5000E-02	1.4673E-01	
8.2902E+01	1.0000E+00	0.	8.1753E-05	3.5000E-02	1.4567E-01	
1.1569E+02	1.0000E+00	0.	9.0472E-05	3.5000E-02	1.2333E-01	
1.4855E+02	1.0000E+00	0.	1.0486E-04	3.5000E-02	1.0883E-01	
1.9074E+02	1.0000E+00	0.	1.0389E-04	3.5000E-02	1.3297E-01	
2.4491E+02	1.0000E+00	0.	1.3175E-04	3.5000E-02	1.9015E-01	
3.1447E+02	1.0000E+00	0.	9.6060E-05	3.5000E-02	1.7571E-01	
4.0379E+02	1.0000E+00	0.	8.8629E-05	3.5000E-02	1.8672E-01	
5.1848E+02	1.0000E+00	0.	1.1455E-04	3.5000E-02	2.5695E-01	
6.6574E+02	1.0000E+00	0.	1.1126E-04	3.5000E-02	1.7357E-01	
8.5482E+02	1.0000E+00	0.	1.0479E-04	3.5000E-02	1.2548E-01	
1.0976E+03	1.0000E+00	0.	1.1267E-04	3.5000E-02	1.2687E-01	
1.4093E+03	1.0000E+00	0.	9.9890E-05	3.5000E-02	1.7406E-01	
1.8096E+03	1.0000E+00	0.	1.0160E-04	3.5000E-02	1.8542E-01	
2.3236E+03	1.0000E+00	0.	9.8627E-05	3.5000E-02	2.1805E-01	
2.9836E+03	1.0000E+00	0.	9.9029E-05	3.5000E-02	2.1674E-01	
3.8310E+03	1.0000E+00	0.	1.0729E-04	3.5000E-02	2.1238E-01	
4.9191E+03	1.0000E+00	0.	9.9664E-05	3.5000E-02	2.1520E-01	
6.3163E+03	1.0000E+00	0.	9.6419E-05	3.5000E-02	2.1753E-01	
8.1103E+03	1.0000E+00	0.	9.4417E-05	3.5000E-02	2.2167E-01	
1.0414E+04	1.0000E+00	0.	9.7638E-05	3.5000E-02	2.2163E-01	
1.3372E+04	1.0000E+00	0.	9.9719E-05	3.5000E-02	2.2265E-01	
1.7169E+04	1.0000E+00	0.	9.8693E-05	3.5000E-02	2.2823E-01	
2.2046E+04	1.0000E+00	0.	9.5268E-05	3.5000E-02	2.3683E-01	
2.4788E+04	1.0000E+00	0.	1.0075E-04	3.5000E-02	2.3110E-01	
2.3302E+02	0.	1	0	4	1102	2151
2.0000E+00	0.	5	0	156	251102	2151
0.	0.	0.	1.0000E+00	0.	2.0000E+00	1102 2151



4.0379E+02	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
5.1848E+02	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
6.6574E+02	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
8.5482E+02	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
1.0976E+03	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
1.4093E+03	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
1.8096E+03	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
2.3236E+03	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
2.9836E+03	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
3.8310E+03	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
4.9191E+03	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
6.3163E+03	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
8.1103E+03	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
1.0414E+04	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
1.3372E+04	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
1.7169E+04	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
2.2046E+04	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
2.4788E+04	1.0000E+00	0.	2.0000E-04	3.5000E-02	2.8600E-01
5.0000E+00	0.	0.	5	0	156
0.	0.	0.	1.0000E+00	0.	1.0000E+00
6.4504E+01	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
8.2902E+01	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
1.1569E+02	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
1.4855E+02	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
1.9074E+02	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
2.4491E+02	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
3.1447E+02	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
4.0379E+02	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
5.1848E+02	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
6.6574E+02	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
8.5482E+02	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
1.0976E+03	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
1.4093E+03	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
1.8096E+03	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
2.3236E+03	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
2.9836E+03	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
3.8310E+03	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
4.9191E+03	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
6.3163E+03	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
8.1103E+03	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
1.0414E+04	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
1.3372E+04	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
1.7169E+04	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
2.2046E+04	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01
2.4788E+04	1.1200E+00	0.	2.2400E-04	3.5000E-02	1.4300E-01

PROGRAM AVRA4, CALCULATES CROSS-SECTIONS IN THE UNRESOLVED RESONANCE REGION

ENDF/B VERSION II DATA WITH ENERGY DEPENDENT PARAMETERS

RUN NO 100 TITLE AVERAGE4 TEST, U=235 DATA

ENERGY LIMITS LOWER 6.450400E+01 UPPER 2.478800E+04 LRU= 2 LRF= 2

TARGET SPIN 3.5000E+00 SCATTERING LENGTH 9.2600E-01 NUMBER OF L-STATES 2

NUCLEAR RADIUS 'A' AS CALCULATED FROM  $A=(1.23*(\text{MASS}^{1/3})+0.8)*0.1$  = 8.3908E-01

NUCLEAR MASS/NEUTRON MASS 2.3302E+02 ANGULAR MOMENTUM 0 NUMBER OF J-STATES FOR THIS L-VALUE 2

SPIN 3.0000E+00 INTERPOLATION CODE 5 NUMBER OF ENERGY POINTS 25  
DEGREES OF FREEDOM, NU INELASTIC 0.0000E+00  
ENERGY(KEV) GAMMA INELAS NU NEUTRON 1.0000E+00 GAMMA N NOT NU GAMMA 0.0000E+00 GAMMA GAMMA  
6.450402E+01 1.000000E+00 0.000000E+00 0.000000E+00 7.180700E-05 3.500000E-02 GAMMAFISS  
8.7290200E+01 1.000000E+00 0.000000E+00 0.000000E+00 8.175300E-05 3.500000E-02 2.934700E-01  
1.156900E+02 1.000000E+00 0.000000E+00 0.000000E+00 9.047200E-05 3.500000E-02 2.913300E-01  
1.485500E+02 1.000000E+00 0.000000E+00 0.000000E+00 1.048600E-04 3.500000E-02 2.466500E-01  
1.907400E+02 1.000000E+00 0.000000E+00 0.000000E+00 1.038900E-04 3.500000E-02 2.176600E-01  
2.449100E+02 1.000000E+00 0.000000E+00 0.000000E+00 1.317500E-04 3.500000E-02 3.659300E-01  
3.144700E+02 1.000000E+00 0.000000E+00 0.000000E+00 9.606000E-05 3.500000E-02 3.802900E-01  
4.037900E+02 1.000000E+00 0.000000E+00 0.000000E+00 8.862300E-05 3.500000E-02 3.514100E-01  
5.184800E+02 1.000000E+00 0.000000E+00 0.000000E+00 1.145200E-04 3.500000E-02 3.734400E-01  
6.657400E+02 1.000000E+00 0.000000E+00 0.000000E+00 1.112000E-04 3.500000E-02 5.139000E-01  
8.548200E+02 1.000000E+00 0.000000E+00 0.000000E+00 1.047900E-04 3.500000E-02 3.471300E-01  
1.097600E+03 1.000000E+00 0.000000E+00 0.000000E+00 1.126700E-04 3.500000E-02 2.509600E-01  
1.409300E+03 1.000000E+00 0.000000E+00 0.000000E+00 9.989000E-05 3.500000E-02 2.537300E-01  
1.809600E+03 1.000000E+00 0.000000E+00 0.000000E+00 1.016000E-04 3.500000E-02 3.481300E-01  
2.323600E+03 1.000000E+00 0.000000E+00 0.000000E+00 9.862700E-05 3.500000E-02 3.708300E-01  
2.983600E+03 1.000000E+00 0.000000E+00 0.000000E+00 9.902300E-05 3.500000E-02 4.361000E-01  
3.831000E+03 1.000000E+00 0.000000E+00 0.000000E+00 1.072900E-04 3.500000E-02 4.334000E-01  
4.919100E+03 1.000000E+00 0.000000E+00 0.000000E+00 9.966400E-05 3.500000E-02 4.247500E-01  
6.316300E+03 1.000000E+00 0.000000E+00 0.000000E+00 9.641900E-05 3.500000E-02 4.305500E-01  
8.110300E+03 1.000000E+00 0.000000E+00 0.000000E+00 9.441700E-05 3.500000E-02 4.433400E-01  
1.041400E+04 1.000000E+00 0.000000E+00 0.000000E+00 9.763800E-05 3.500000E-02 4.350000E-01  
1.337200E+04 1.000000E+00 0.000000E+00 0.000000E+00 9.971900E-05 3.500000E-02 4.432500E-01  
1.716900E+04 1.000000E+00 0.000000E+00 0.000000E+00 9.869300E-05 3.500000E-02 4.453000E-01  
4.564600E-01





8.540200E+02	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
1.097600E+03	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
1.409300E+03	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
1.809600E+03	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
2.323600E+03	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
2.983600E+03	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
3.833000E+03	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
4.919100E+03	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
6.310300E+03	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
8.110300E+03	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
1.044400E+04	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
1.337200E+04	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
1.715900E+04	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
2.204600E+04	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01
2.478800E+04	1.160000E+00	0.000000E+00	2.320000E-04	3.500000E-02	3.300000E-01

SPIN 4.0000E+00 INTERPOLATION CODE 5 NUMBER OF ENERGY POINTS 25  
 DEGREES OF FREEDOM, NU INELASTIC 0.0000E+00

6.450400E+01	1.000000E+00	0.000000E+00	0.000000E+00	0.0000E+00	NU FISSION 1.0000E+00
8.292000E+01	1.000000E+00	0.000000E+00	0.000000E-04	GAMMA GAMMA	GAMMAFISS
1.150900E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
1.485500E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
1.907400E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
2.449100E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
3.144700E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
4.037900E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
5.184800E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
6.657400E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
8.548200E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
1.097600E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
1.409300E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
1.809600E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
2.323600E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
2.983600E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
3.833000E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
4.919100E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
6.310300E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
8.110300E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
1.044400E+04	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
1.337200E+04	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
1.715900E+04	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
2.204600E+04	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01
2.478800E+04	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	1.270000E-01

SPIN 4.0000E+00 INTERPOLATION CODE 5 NUMBER OF ENERGY POINTS 25  
 DEGREES OF FREEDOM, NU INELASTIC 0.0000E+00

6.450400E+01	1.000000E+00	0.000000E+00	0.000000E+00	0.0000E+00	NU FISSION 2.0000E+00
8.292000E+01	1.000000E+00	0.000000E+00	0.000000E-04	GAMMA GAMMA	GAMMAFISS
1.156900E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
1.485500E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
1.907400E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
2.449100E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
3.144700E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
4.037900E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01

4.037900E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
5.184800E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
6.657400E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
8.548200E+02	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
1.097600E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
1.409300E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
1.809600E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
2.323600E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
2.983600E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
3.831000E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
4.919100E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
6.316300E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
8.110300E+03	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
1.041400E+04	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
1.337200E+04	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
1.716900E+04	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
2.204600E+04	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01
2.478800E+04	1.000000E+00	0.000000E+00	2.000000E-04	3.500000E-02	2.860000E-01

SPIN 5.0000E+00 INTERPOLATION CODE 5 NUMBER OF ENERGY POINTS 25  
DEGREES OF FREEDOM, NU INELASTIC 0.0000E+00 NU NEUTRON 1.0000E+00 NU GAMMA 0.0000E+00 NU FISSION 1.0

ENERGY(EV)	SPACING	GAMMA INELAS	GAMMA N NOT	GAMMA GAMMA	GAMMAFISS
6.450400E+01	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
8.290200E+01	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
1.156900E+02	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
1.485500E+02	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
1.907400E+02	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
2.449100E+02	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
3.144700E+02	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
4.037900E+02	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
5.184800E+02	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
6.657400E+02	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
8.548200E+02	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
1.097600E+03	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
1.409300E+03	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
1.809600E+03	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
2.323600E+03	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
2.983600E+03	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
3.831000E+03	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
4.919100E+03	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
6.316300E+03	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
8.110300E+03	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
1.041400E+04	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
1.337200E+04	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
1.716900E+04	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
2.204600E+04	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01
2.478800E+04	1.120000E+00	0.000000E+00	2.240000E-04	3.500000E-02	1.430000E-01

INPUT PARAMETERS WITH CALCULATED TOTAL WIDTH

L-VALUE= 0 J-STATE= 3.00

ENERGY(EV)	SPACING	GAMMA INELAS	GAMMA TOTAL	GAMMA N NOT	GAMMA GAMMA	GAMMA FISS
6.450400E+01	1.000000E+00	0.000000E+00	3.290467E+01	7.180700E+05	3.500000E-02	2.934700E-01
8.290200E+01	1.000000E+00	0.000000E+00	3.270744E-01	8.175300E-05	3.500000E-02	2.913300E-01
1.156900E+02	1.000000E+00	0.000000E+00	2.826231E+01	9.047200E-05	3.500000E-02	2.466500E-01
1.485500E+02	1.000000E+00	0.000000E+00	2.539380E-01	1.048600E-04	3.500000E-02	2.176600E-01
1.907400E+02	1.000000E+00	0.000000E+00	3.023648E-01	1.038900E-04	3.500000E-02	2.659300E-01
2.449100E+02	1.000000E+00	0.000000E+00	4.173518E-01	1.317500E-04	3.500000E-02	3.802900E-01
3.144700E+02	1.000000E+00	0.000000E+00	3.881135E+01	9.606000E-05	3.500000E-02	3.514100E-01
4.037900E+02	1.000000E+00	0.000000E+00	4.102210E-01	8.862900E-05	3.500000E-02	3.734400E-01
5.184800E+02	1.000000E+00	0.000000E+00	5.515083E-01	1.145500E-04	3.500000E-02	5.139000E-01
6.657400E+02	1.000000E+00	0.000000E+00	3.850007E+01	1.112600E-04	3.500000E-02	3.471300E-01
8.548200E+02	1.000000E+00	0.000000E+00	2.890238E-01	1.047900E-04	3.500000E-02	2.509600E-01
1.097600E+03	1.000000E+00	0.000000E+00	2.924628E-01	1.126700E-04	3.500000E-02	2.537300E-01
1.409300E+03	1.000000E+00	0.000000E+00	3.868799E-01	9.989000E-05	3.500000E-02	3.481300E-01
1.809600E+03	1.000000E+00	0.000000E+00	4.101520E-01	1.016000E-04	3.500000E-02	3.708300E-01
2.323600E+03	1.000000E+00	0.000000E+00	4.758542E-01	9.862700E-05	3.500000E-02	4.361000E-01
2.983600E+03	1.000000E+00	0.000000E+00	4.738892E-01	9.902900E-05	3.500000E-02	4.334800E-01
3.831000E+03	1.000000E+00	0.000000E+00	4.663907E-01	1.072900E-04	3.500000E-02	4.247500E-01
4.919100E+03	1.000000E+00	0.000000E+00	4.725401E+01	9.966400E-05	3.500000E-02	4.305500E-01
6.316300E+03	1.000000E+00	0.000000E+00	4.777229E-01	9.641900E-05	3.500000E-02	4.350600E-01
8.110300E+03	1.000000E+00	0.000000E+00	4.868429E-01	9.441700E-05	3.500000E-02	4.433400E-01
1.041400E+04	1.000000E+00	0.000000E+00	4.882139E-01	9.763800E-05	3.500000E-02	4.432500E-01
1.337200E+04	1.000000E+00	0.000000E+00	4.918312E-01	9.971900E-05	3.500000E-02	4.453000E-01
1.716900E+04	1.000000E+00	0.000000E+00	5.043918E-01	9.869300E-05	3.500000E-02	4.564600E-01
2.204600E+04	1.000000E+00	0.000000E+00	5.228053E-01	9.526800E-05	3.500000E-02	4.736600E-01
2.478800E+04	1.000000E+00	0.000000E+00	5.130523E-01	1.007500E-04	3.500000E-02	4.621900E-01

L-VALUE= 0 J-STATE= 4,00

ENERGY(EV)	SPACING	GAMMA INELAS	GAMMA TOTAL	GAMMA N NOT	GAMMA GAMMA	GAMMA FISS
6.450400E+01	1.000000E+00	0.000000E+00	1.823067E+01	7.180700E-05	3.500000E-02	1.467300E-01
8.290200E+01	1.000000E+00	0.000000E+00	1.814144E-01	8.175300E-05	3.500000E-02	1.456700E-01
1.156900E+02	1.000000E+00	0.000000E+00	1.593031E-01	9.047200E-05	3.500000E-02	1.233300E-01
1.485500E+02	1.000000E+00	0.000000E+00	1.451080E-01	1.048600E-04	3.500000E-02	1.088300E-01
1.907400E+02	1.000000E+00	0.000000E+00	1.694048E-01	1.038900E-04	3.500000E-02	1.329700E-01
2.449100E+02	1.000000E+00	0.000000E+00	2.272118E-01	1.317500E-04	3.500000E-02	1.901500E-01
3.144700E+02	1.000000E+00	0.000000E+00	2.124435E-01	9.606000E-05	3.500000E-02	1.757100E-01
4.037900E+02	1.000000E+00	0.000000E+00	2.235010E-01	8.862900E-05	3.500000E-02	1.867200E-01
5.184800E+02	1.000000E+00	0.000000E+00	2.945583E+01	1.145500E-04	3.500000E-02	2.569500E-01
6.657400E+02	1.000000E+00	0.000000E+00	2.114407E-01	1.112600E-04	3.500000E-02	1.735700E-01
8.548200E+02	1.000000E+00	0.000000E+00	1.635438E-01	1.047900E-04	3.500000E-02	1.254800E-01
1.097600E+03	1.000000E+00	0.000000E+00	1.656028E-01	1.126700E-04	3.500000E-02	1.268700E-01
1.409300E+03	1.000000E+00	0.000000E+00	2.128099E-01	9.989000E-05	3.500000E-02	1.740600E-01
1.809600E+03	1.000000E+00	0.000000E+00	2.247420E-01	1.016000E-04	3.500000E-02	1.854200E-01
2.323600E+03	1.000000E+00	0.000000E+00	2.578042E-01	9.862700E-05	3.500000E-02	2.180500E-01
2.983600E+03	1.000000E+00	0.000000E+00	2.571492E-01	9.902900E-05	3.500000E-02	2.167400E-01
3.831000E+03	1.000000E+00	0.000000E+00	2.540207E-01	1.072900E-04	3.500000E-02	2.123800E-01
4.919100E+03	1.000000E+00	0.000000E+00	2.572701E-01	9.966400E-05	3.500000E-02	2.152800E-01
6.316300E+03	1.000000E+00	0.000000E+00	2.601929E-01	9.641900E-05	3.500000E-02	2.175300E-01
8.110300E+03	1.000000E+00	0.000000E+00	2.651729E-01	9.441700E-05	3.500000E-02	2.216700E-01
1.041400E+04	1.000000E+00	0.000000E+00	2.665939E-01	9.763800E-05	3.500000E-02	2.216300E-01
1.337200E+04	1.000000E+00	0.000000E+00	2.691812E-01	9.971900E-05	3.500000E-02	2.226500E-01
1.716900E+04	1.000000E+00	0.000000E+00	2.761518E-01	9.869300E-05	3.500000E-02	2.282300E-01
2.204600E+04	1.000000E+00	0.000000E+00	2.859753E-01	9.526800E-05	3.500000E-02	2.368300E-01
2.478800E+04	1.000000E+00	0.000000E+00	2.819623E-01	1.007500E-04	3.500000E-02	2.311000E-01

L-VALUE= 1 J-STATE= 2,00

ENERGY (EV)	SPACING	GAMMA INELAS	GAMMA TOTAL	GAMMA N NOT	GAMMA GAMMA	GAMMA FISSION
6.450400E+01	1.160000E+00	0.000000E+00	3.670004E-01	2.320000E-04	3.500000E-02	3.320000E-01
8.290200E+01	1.160000E+00	0.000000E+00	3.670006E-01	2.520000E-04	3.500000E-02	3.320000E-01
1.156900E+02	1.160000E+00	0.000000E+00	3.670010E-01	2.520000E-04	3.500000E-02	3.320000E-01
1.485500E+02	1.160000E+00	0.000000E+00	3.670014E-01	2.520000E-04	3.500000E-02	3.320000E-01
1.907400E+02	1.160000E+00	0.000000E+00	3.670021E-01	2.520000E-04	3.500000E-02	3.320000E-01
2.449100E+02	1.160000E+00	0.000000E+00	3.670033E-01	2.520000E-04	3.500000E-02	3.320000E-01
3.144700E+02	1.160000E+00	0.000000E+00	3.670044E-01	2.320000E-04	3.500000E-02	3.320000E-01
4.037900E+02	1.160000E+00	0.000000E+00	3.670063E-01	2.320000E-04	3.500000E-02	3.320000E-01
5.184800E+02	1.160000E+00	0.000000E+00	3.670099E-01	2.320000E-04	3.500000E-02	3.320000E-01
6.657400E+02	1.160000E+00	0.000000E+00	3.670134E-01	2.320000E-04	3.500000E-02	3.320000E-01
8.548200E+02	1.160000E+00	0.000000E+00	3.670195E-01	2.320000E-04	3.500000E-02	3.320000E-01
1.097600E+03	1.160000E+00	0.000000E+00	3.670283E-01	2.320000E-04	3.500000E-02	3.320000E-01
1.409300E+03	1.160000E+00	0.000000E+00	3.670412E-01	2.320000E-04	3.500000E-02	3.320000E-01
1.809600E+03	1.160000E+00	0.000000E+00	3.670598E-01	2.320000E-04	3.500000E-02	3.320000E-01
2.323600E+03	1.160000E+00	0.000000E+00	3.670866E-01	2.320000E-04	3.500000E-02	3.320000E-01
2.983600E+03	1.160000E+00	0.000000E+00	3.671261E-01	2.320000E-04	3.500000E-02	3.320000E-01
3.831000E+03	1.160000E+00	0.000000E+00	3.671833E-01	2.320000E-04	3.500000E-02	3.320000E-01
4.919100E+03	1.160000E+00	0.000000E+00	3.672655E-01	2.320000E-04	3.500000E-02	3.320000E-01
6.316300E+03	1.160000E+00	0.000000E+00	3.673841E-01	2.320000E-04	3.500000E-02	3.320000E-01
8.1110300E+03	1.160000E+00	0.000000E+00	3.675555E-01	2.320000E-04	3.500000E-02	3.320000E-01
1.041400E+04	1.160000E+00	0.000000E+00	3.678224E-01	2.320000E-04	3.500000E-02	3.320000E-01
1.337200E+04	1.160000E+00	0.000000E+00	3.681564E-01	2.320000E-04	3.500000E-02	3.320000E-01
1.716900E+04	1.160000E+00	0.000000E+00	3.686622E-01	2.320000E-04	3.500000E-02	3.320000E-01
2.204600E+04	1.160000E+00	0.000000E+00	3.693814E-01	2.320000E-04	3.500000E-02	3.320000E-01
2.478800E+04	1.160000E+00	0.000000E+00	3.698152E-01	2.320000E-04	3.500000E-02	3.320000E-01

L-VALUE= 1 J-STATE= 3.00

ENERGY (EV)	SPACING	GAMMA INELAS	GAMMA TOTAL	GAMMA N NOT	GAMMA GAMMA	GAMMA FISSION
6.450400E+01	1.000000E+00	0.000000E+00	1.620007E-01	2.000000E-04	3.500000E-02	1.270000E-01
8.290200E+01	1.000000E+00	0.000000E+00	1.620010E-01	2.000000E-04	3.500000E-02	1.270000E-01
1.156900E+02	1.000000E+00	0.000000E+00	1.620017E-01	2.000000E-04	3.500000E-02	1.270000E-01
1.485500E+02	1.000000E+00	0.000000E+00	1.620024E-01	2.000000E-04	3.500000E-02	1.270000E-01
1.907400E+02	1.000000E+00	0.000000E+00	1.620035E-01	2.000000E-04	3.500000E-02	1.270000E-01
2.449100E+02	1.000000E+00	0.000000E+00	1.620052E-01	2.000000E-04	3.500000E-02	1.270000E-01
3.144700E+02	1.000000E+00	0.000000E+00	1.620075E-01	2.000000E-04	3.500000E-02	1.270000E-01
4.037900E+02	1.000000E+00	0.000000E+00	1.620109E-01	2.000000E-04	3.500000E-02	1.270000E-01
5.184800E+02	1.000000E+00	0.000000E+00	1.620159E-01	2.000000E-04	3.500000E-02	1.270000E-01
6.657400E+02	1.000000E+00	0.000000E+00	1.620231E-01	2.000000E-04	3.500000E-02	1.270000E-01
8.548200E+02	1.000000E+00	0.000000E+00	1.620336E-01	2.000000E-04	3.500000E-02	1.270000E-01
1.097600E+03	1.000000E+00	0.000000E+00	1.620488E-01	2.000000E-04	3.500000E-02	1.270000E-01
1.409300E+03	1.000000E+00	0.000000E+00	1.620710E-01	2.000000E-04	3.500000E-02	1.270000E-01
1.809600E+03	1.000000E+00	0.000000E+00	1.621031E-01	2.000000E-04	3.500000E-02	1.270000E-01
2.323600E+03	1.000000E+00	0.000000E+00	1.621498E-01	2.000000E-04	3.500000E-02	1.270000E-01
2.983600E+03	1.000000E+00	0.000000E+00	1.622174E-01	2.000000E-04	3.500000E-02	1.270000E-01
3.831000E+03	1.000000E+00	0.000000E+00	1.623154E-01	2.000000E-04	3.500000E-02	1.270000E-01
4.919100E+03	1.000000E+00	0.000000E+00	1.624573E-01	2.000000E-04	3.500000E-02	1.270000E-01
6.316300E+03	1.000000E+00	0.000000E+00	1.626623E-01	2.000000E-04	3.500000E-02	1.270000E-01
8.1110300E+03	1.000000E+00	0.000000E+00	1.629580E-01	2.000000E-04	3.500000E-02	1.270000E-01
1.041400E+04	1.000000E+00	0.000000E+00	1.633835E-01	2.000000E-04	3.500000E-02	1.270000E-01
1.337200E+04	1.000000E+00	0.000000E+00	1.639938E-01	2.000000E-04	3.500000E-02	1.270000E-01
1.716900E+04	1.000000E+00	0.000000E+00	1.648656E-01	2.000000E-04	3.500000E-02	1.270000E-01
2.204600E+04	1.000000E+00	0.000000E+00	1.661058E-01	2.000000E-04	3.500000E-02	1.270000E-01
2.478800E+04	1.000000E+00	0.000000E+00	1.668534E-01	2.000000E-04	3.500000E-02	1.270000E-01

ENERGY (eV)	SPACING	GAMMA INELAS	GAMMA TOTAL	GAMMA N NOT	GAMMA GAMMA	GAMMA FISS
6.450400E+01	1.000000E+00	0.000000E+00	3.210007E+01	2.000000E-04	3.500000E-02	2.860000E-01
8.290200E+01	1.000000E+00	0.000000E+00	3.210010E+01	2.000000E-04	3.500000E-02	2.860000E-01
1.156900E+02	1.000000E+00	0.000000E+00	3.210017E+01	2.000000E-04	3.500000E-02	2.860000E-01
1.485500E+02	1.000000E+00	0.000000E+00	3.210022E+01	2.000000E-04	3.500000E-02	2.860000E-01
1.907400E+02	1.000000E+00	0.000000E+00	3.210035E+01	2.000000E-04	3.500000E-02	2.860000E-01
2.449100E+02	1.000000E+00	0.000000E+00	3.210052E+01	2.000000E-04	3.500000E-02	2.860000E-01
3.144700E+02	1.000000E+00	0.000000E+00	3.210075E+01	2.000000E-04	3.500000E-02	2.860000E-01
4.037900E+02	1.000000E+00	0.000000E+00	3.210109E+01	2.000000E-04	3.500000E-02	2.860000E-01
5.184800E+02	1.000000E+00	0.000000E+00	3.210159E+01	2.000000E-04	3.500000E-02	2.860000E-01
6.657400E+02	1.000000E+00	0.000000E+00	3.210231E+01	2.000000E-04	3.500000E-02	2.860000E-01
8.548200E+02	1.000000E+00	0.000000E+00	3.210333E+01	2.000000E-04	3.500000E-02	2.860000E-01
1.097600E+03	1.000000E+00	0.000000E+00	3.210488E+01	2.000000E-04	3.500000E-02	2.860000E-01
1.409300E+03	1.000000E+00	0.000000E+00	3.210710E+01	2.000000E-04	3.500000E-02	2.860000E-01
1.809600E+03	1.000000E+00	0.000000E+00	3.211103E+01	2.000000E-04	3.500000E-02	2.860000E-01
2.323600E+03	1.000000E+00	0.000000E+00	3.211498E+01	2.000000E-04	3.500000E-02	2.860000E-01
2.983600E+03	1.000000E+00	0.000000E+00	3.212174E+01	2.000000E-04	3.500000E-02	2.860000E-01
3.831000E+03	1.000000E+00	0.000000E+00	3.213154E+01	2.000000E-04	3.500000E-02	2.860000E-01
4.919100E+03	1.000000E+00	0.000000E+00	3.214573E+01	2.000000E-04	3.500000E-02	2.860000E-01
6.316300E+03	1.000000E+00	0.000000E+00	3.216223E+01	2.000000E-04	3.500000E-02	2.860000E-01
8.110300E+03	1.000000E+00	0.000000E+00	3.219580E+01	2.000000E-04	3.500000E-02	2.860000E-01
1.041400E+04	1.000000E+00	0.000000E+00	3.223835E+01	2.000000E-04	3.500000E-02	2.860000E-01
1.337200E+04	1.000000E+00	0.000000E+00	3.229933E+01	2.000000E-04	3.500000E-02	2.860000E-01
1.716900E+04	1.000000E+00	0.000000E+00	3.238656E+01	2.000000E-04	3.500000E-02	2.860000E-01
2.204600E+04	1.000000E+00	0.000000E+00	3.251105E+01	2.000000E-04	3.500000E-02	2.860000E-01
2.478800E+04	1.000000E+00	0.000000E+00	3.258534E+01	2.000000E-04	3.500000E-02	2.860000E-01

L=VALUE= 1 J=STATE= 5.00

ENERGY (eV)	SPACING	GAMMA INELAS	GAMMA TOTAL	GAMMA N NOT	GAMMA GAMMA	GAMMA FISS
6.450400E+01	1.120000E+00	0.000000E+00	1.780004E-01	2.240000E-04	3.500000E-02	1.430000E-01
8.290200E+01	1.120000E+00	0.000000E+00	1.780006E-01	2.240000E-04	3.500000E-02	1.430000E-01
1.156900E+02	1.120000E+00	0.000000E+00	1.780009E-01	2.240000E-04	3.500000E-02	1.430000E-01
1.485500E+02	1.120000E+00	0.000000E+00	1.780011E-01	2.240000E-04	3.500000E-02	1.430000E-01
1.907400E+02	1.120000E+00	0.000000E+00	1.780022E-01	2.240000E-04	3.500000E-02	1.430000E-01
2.449100E+02	1.120000E+00	0.000000E+00	1.780042E-01	2.240000E-04	3.500000E-02	1.430000E-01
3.144700E+02	1.120000E+00	0.000000E+00	1.780061E-01	2.240000E-04	3.500000E-02	1.430000E-01
4.037900E+02	1.120000E+00	0.000000E+00	1.780089E-01	2.240000E-04	3.500000E-02	1.430000E-01
5.184800E+02	1.120000E+00	0.000000E+00	1.780125E-01	2.240000E-04	3.500000E-02	1.430000E-01
6.657400E+02	1.120000E+00	0.000000E+00	1.780181E-01	2.240000E-04	3.500000E-02	1.430000E-01
8.548200E+02	1.120000E+00	0.000000E+00	1.780273E-01	2.240000E-04	3.500000E-02	1.430000E-01
1.097600E+03	1.120000E+00	0.000000E+00	1.780391E-01	2.240000E-04	3.500000E-02	1.430000E-01
1.409300E+03	1.120000E+00	0.000000E+00	1.780577E-01	2.240000E-04	3.500000E-02	1.430000E-01
1.809600E+03	1.120000E+00	0.000000E+00	1.780833E-01	2.240000E-04	3.500000E-02	1.430000E-01
2.323600E+03	1.120000E+00	0.000000E+00	1.781216E-01	2.240000E-04	3.500000E-02	1.430000E-01
2.983600E+03	1.120000E+00	0.000000E+00	1.781766E-01	2.240000E-04	3.500000E-02	1.430000E-01
3.831000E+03	1.120000E+00	0.000000E+00	1.782561E-01	2.240000E-04	3.500000E-02	1.430000E-01
4.919100E+03	1.120000E+00	0.000000E+00	1.783099E-01	2.240000E-04	3.500000E-02	1.430000E-01
6.316300E+03	1.120000E+00	0.000000E+00	1.785365E-01	2.240000E-04	3.500000E-02	1.430000E-01
8.110300E+03	1.120000E+00	0.000000E+00	1.787747E-01	2.240000E-04	3.500000E-02	1.430000E-01
1.041400E+04	1.120000E+00	0.000000E+00	1.791165E-01	2.240000E-04	3.500000E-02	1.430000E-01
1.337200E+04	1.120000E+00	0.000000E+00	1.796047E-01	2.240000E-04	3.500000E-02	1.430000E-01
1.716900E+04	1.120000E+00	0.000000E+00	1.802999E-01	2.240000E-04	3.500000E-02	1.430000E-01

2.47880E+04 1.120000E+00 0.00000E+00 1.807179E+01 2.240000E-04 3.50000E-02 1.430000E-01

AVERAGE SCATTERING CROSS-SECTION

NEUTRON ENERGY (EV)  
 6.450400E+01  
 8.292200E+01  
 1.156900E+02  
 1.485500E+02  
 1.907400E+02  
 2.449100E+02  
 3.144700E+02  
 4.037900E+02  
 5.184800E+02  
 6.657400E+02  
 8.548200E+02  
 1.097600E+03  
 1.409300E+03  
 1.809600E+03  
 2.323600E+03  
 2.983600E+03  
 3.831000E+03  
 4.919100E+03  
 6.316300E+03  
 8.110300E+03  
 1.041400E+04  
 1.337200E+04  
 1.716900E+04  
 2.204600E+04  
 2.478800E+04

S-WAVE SIGMANN  
 1.128573E+01  
 1.143264E+01  
 1.162549E+01  
 1.195781E+01  
 1.182793E+01  
 1.218542E+01  
 1.154289E+01  
 1.139498E+01  
 1.163930E+01  
 1.172720E+01  
 1.171975E+01  
 1.181768E+01  
 1.144858E+01  
 1.141105E+01  
 1.128134E+01  
 1.123870E+01  
 1.127680E+01  
 1.113067E+01  
 1.102949E+01  
 1.093151E+01  
 1.086338E+01  
 1.076806E+01  
 1.063184E+01  
 1.046647E+01  
 1.041326E+01

P-WAVE SIGMANN  
 1.037337E-06  
 1.713097E-06  
 3.333888E-06  
 5.497965E-06  
 9.061713E-06  
 1.493374E-05  
 2.460894E-05  
 4.054633E-05  
 6.679261E-05  
 1.099958E-04  
 1.817774E-04  
 2.979523E-04  
 4.692263E-04  
 8.049817E-04  
 1.321153E-03  
 2.165018E-03  
 3.542597E-03  
 5.774555E-03  
 9.384230E-03  
 1.517711E-02  
 2.439221E-02  
 3.88194E-02  
 6.132624E-02  
 9.540830E-02  
 1.169041E-01

D-WAVE SIGMANN  
 0.000000E+00  
 0.000000E+00  
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TOTAL SIGMANN  
 1.128573E+01  
 1.143264E+01  
 1.162549E+01  
 1.195781E+01  
 1.182793E+01  
 1.218542E+01  
 1.154289E+01  
 1.139498E+01  
 1.163930E+01  
 1.172720E+01  
 1.171975E+01  
 1.181768E+01  
 1.144858E+01  
 1.141105E+01  
 1.128134E+01  
 1.123870E+01  
 1.124086E+01  
 1.128034E+01  
 1.113644E+01  
 1.103887E+01  
 1.094668E+01  
 1.088793E+01  
 1.080694E+01  
 1.069316E+01  
 1.056196E+01  
 1.053301E+01

AVERAGE CAPTURE CROSS-SECTION

NEUTRON ENERGY (EV)  
 6.450400E+01  
 8.292200E+01  
 1.156900E+02  
 1.485500E+02  
 1.907400E+02  
 2.449100E+02  
 3.144700E+02  
 4.037900E+02  
 5.184800E+02  
 6.657400E+02  
 8.548200E+02  
 1.097600E+03  
 1.409300E+03  
 1.809600E+03  
 2.323600E+03  
 2.983600E+03  
 3.831000E+03  
 4.919100E+03  
 6.316300E+03  
 8.110300E+03  
 1.041400E+04  
 1.337200E+04  
 1.716900E+04  
 2.204600E+04  
 2.478800E+04

S-WAVE SIGMANGAMMA  
 1.213343E+01  
 1.213746E+01  
 1.205822E+01  
 1.280140E+01  
 1.026890E+01  
 9.670739E+00  
 6.519591E+00  
 5.157919E+00  
 4.973499E+00  
 5.006695E+00  
 4.717705E+00  
 4.358181E+00  
 2.998975E+00  
 2.576139E+00  
 2.034650E+00

P-WAVE SIGMANGAMMA  
 2.245308E-02  
 2.545272E-02  
 3.006377E-02  
 3.406232E-02  
 3.859076E-02  
 4.371861E-02  
 4.952469E-02  
 5.609663E-02  
 6.353244E-02  
 7.194106E-02  
 8.144327E-02  
 9.217137E-02  
 1.042668E-01  
 1.176838E-01  
 1.331738E-01

D-WAVE SIGMANGAMMA  
 0.000000E+00  
 0.000000E+00  
 0.000000E+00  
 0.000000E+00  
 0.000000E+00  
 0.000000E+00  
 0.000000E+00  
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 0.000000E+00  
 0.000000E+00  
 0.000000E+00

TOTAL SIGMANGAMMA  
 1.215589E+01  
 1.216291E+01  
 1.208829E+01  
 1.283346E+01  
 1.030749E+01  
 9.714457E+00  
 6.569116E+00  
 5.214016E+00  
 5.036032E+00  
 5.078636E+00  
 4.799149E+00  
 4.450352E+00  
 3.103242E+00  
 2.694023E+00  
 2.167824E+00

2.983600E+03	1.774552E+00	1.502853E-01	0.000000E+00	1.924
3.831000E+03	1.656170E+00	1.693456E-01	0.000000E+00	1.825
4.919100E+03	1.338019E+00	1.904431E-01	0.000000E+00	1.528
6.316300E+03	1.118608E+00	2.135899E-01	0.000000E+00	1.332
8.110300E+03	9.401374E-01	2.386737E-01	0.000000E+00	1.178
1.041400E+04	8.303611E-01	2.654006E-01	0.000000E+00	1.095
1.337200E+04	7.228342E-01	2.932136E-01	0.000000E+00	1.016
1.716900E+04	6.079728E-01	3.212203E-01	0.000000E+00	9.291
2.204600E+04	4.986953E-01	3.481795E-01	0.000000E+00	8.468
2.478800E+04	4.873076E-01	3.600111E-01	0.000000E+00	8.473

AVERAGE FISSION CROSS-SECTION

NEUTRON ENERGY (EV)	S-WAVE SIGMAFISS	P-WAVE SIGMAFISS	D-WAVE SIGMAFISS	TOTAL SIGMA
6.450400E+01	2.421250E+01	4.449103E-02	0.000000E+00	2.425
8.290200E+01	2.421285E+01	5.043514E-02	0.000000E+00	2.426
1.156900E+02	2.175032E+01	5.957274E-02	0.000000E+00	2.180
1.485500E+02	2.145637E+01	6.749699E-02	0.000000E+00	2.152
1.907400E+02	1.965362E+01	7.647193E-02	0.000000E+00	1.973
2.449100E+02	2.356960E+01	8.663586E-02	0.000000E+00	2.365
3.144700E+02	1.499316E+01	9.814573E-02	0.000000E+00	1.509
4.037900E+02	1.234818E+01	1.111765E-01	0.000000E+00	1.245
5.184800E+02	1.481730E+01	1.259246E-01	0.000000E+00	1.494
6.657400E+02	1.171999E+01	1.426094E-01	0.000000E+00	1.186
8.548200E+02	9.004881E+00	1.614760E-01	0.000000E+00	9.166
1.097600E+03	8.484518E+00	1.827964E-01	0.000000E+00	8.667
1.409300E+03	7.155726E+00	2.068663E-01	0.000000E+00	7.362
1.809600E+03	6.467422E+00	2.340166E-01	0.000000E+00	6.701
2.323600E+03	5.705139E+00	2.645890E-01	0.000000E+00	5.969
2.983600E+03	5.013612E+00	2.989440E-01	0.000000E+00	5.312
3.831000E+03	4.712044E+00	3.374391E-01	0.000000E+00	5.049
4.919100E+03	3.860386E+00	3.804160E-01	0.000000E+00	4.240
6.316300E+03	3.281264E+00	4.284555E-01	0.000000E+00	3.709
8.110300E+03	2.824327E+00	4.808212E-01	0.000000E+00	3.305
1.041400E+04	2.542653E+00	5.383927E-01	0.000000E+00	3.081
1.337200E+04	2.262384E+00	6.005414E-01	0.000000E+00	2.862
1.716900E+04	1.963987E+00	6.664918E-01	0.000000E+00	2.630
2.204600E+04	1.671071E+00	7.349421E-01	0.000000E+00	2.406
2.478800E+04	1.634810E+00	7.673340E-01	0.000000E+00	2.402





