

DASA-2379

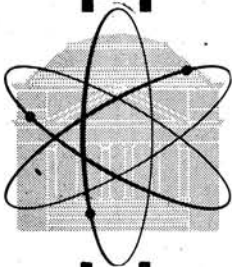
TRANSLATION TO ENDF/B AND "PHYSICS"
CHECKING OF CROSS SECTIONS FOR SHIELDING

Final Report

Contract No. DASA01-69-C-0029
Defense Atomic Support Agency
Washington, D.C. 20305

ENDF-130

Submitted by:
Donald J. Dudziak



Research Laboratories for the Engineering Sciences

University of Virginia

Charlottesville

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ENDF-130
Report No. NE-3383-104-69U

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Division of Nuclear Engineering
RESEARCH LABORATORIES FOR THE ENGINEERING SCIENCES
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ABSTRACT

Evaluations of neutron interaction and photon production cross sections for sodium, magnesium, chlorine, potassium, and calcium have been translated from a modified-UK format into ENDF/B format. The data have been reviewed and revised to a minor extent, and can be used by the LAPH code to generate multigroup photon production cross section matrices. All data sets have been transmitted to the University of California, Los Alamos Scientific Laboratory, to the National Neutron Cross Section Center at BNL, and to the Radiation Shielding Information Center at ORNL. Several "physics" checks have been proposed for the photon data, and a FORTRAN IV code, PHOX, has been written to incorporate some of these checks.

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1. Introduction And Summary

As part of the ENDF/B⁽¹⁾ effort, a format⁽²⁾ was devised for storing photon production and photon interaction data. In order to de-bug the photon production format, sodium data from a recent evaluation by Drake et al.⁽³⁾ were translated from a modified UK Data File format into the ENDF/B Data File format (cf. Ref. 2 for a listing of this translation). The translation was performed by a special-purpose FORTRAN IV code called LUTE. Because the entire sodium evaluation was of interest to the Shielding Subcommittee of the Cross Section Evaluation Working Group (CSEWG), the University of California, Los Alamos Scientific Laboratory undertook the translation of the neutron interaction data also. This latter translation⁽⁴⁾ was performed with the LATEX code, an extended version of the LATE code which had been previously used for translations of ⁶Li and ⁷Li.⁽⁵⁾ Later, the Los Alamos Scientific Laboratory undertook the translation⁽⁴⁾ of the calcium evaluation by Drake et al.,⁽³⁾ as well as a preliminary analysis of the translation procedures for chlorine, potassium and calcium.

This report describes in §2 the procedures and data revisions for the translations of Na, Mg, Cl, K, and Ca. Details of the revisions are given in Appendices A and B. Proposals for "physics" and internal consistency checks which might, in part, be incorporated in a checking code are given in §3. Particular emphasis is placed on checks which are applicable to the photon data. A code called PHOX was written to perform checks on the photon data. It is described in detail in §4, and a listing is given in Appendix C. The translation codes, LUTE and LATEX, are described in a separate report.⁽⁶⁾ For purposes of the present report the modified and extended UK Data File format used by Drake et al. will be referred to as simply the "UK format", and the entirety of their data as the "UK Data File".

2. Translations Of Na, Mg, Cl, K, and Ca To ENDF/B Format

The materials which were translated are identified on each UK-format card image by a nuclide identification number (NIN), and on each ENDF/B-format card image by a material number (MAT). Listed below in Table I are the materials and their corresponding NIN and MAT numbers.

TABLE I
Material Identifying Numbers

<u>Material</u>	<u>NIN(UK)</u>	<u>MAT(ENDF/B)</u>
Na	205	5001
Mg	206	5002
Cl	221	5004
K	227	5005
Ca	231	5006

2.1 Procedures

The translation procedure used was to start with the materials on data tapes in UK format, and attempt a run thru the LUTE and LATEX codes. Several iterations were required for each material before the UK-format tape had been corrected sufficiently to allow a successful translation. After correcting as many errors as the translation codes could detect (generally clerical errors, mispunches, cards out of sequence or missing, etc.), the data in both listed and plotted form were scanned visually for any obvious inconsistencies or other errors. Appendix A documents in minute detail the corrections and alterations to the UK Data File which have been made since July 1968. Appendix B documents similar information for the ENDF/B Data File.

Construction of a corresponding ENDF/B Data File for each material required several changes and additions (as opposed to corrections), which are described in detail in reference 6. In summary, these primarily consisted of the three changes described below.

2.1.1. Additions to Files 1 and 3

A complete File 1 was created for each material, including a table of contents and an index. A tabular section for the average cosine of the angle of elastic scattering in the laboratory system was automatically created by LATEX for File 3. This latter table of $\bar{\mu}_{\text{LAB}}$ values was calculated using the angular distributions of secondary neutrons from elastic scattering, as given in File 4 (MF = 4, MT = 2). The values of $\bar{\mu}_{\text{LAB}}$ were extended down to the lowest energy for which an elastic scattering cross section is given in File 3 (MF = 3, MT = 2), using a value $\bar{\mu}_{\text{LAB}} = \frac{2}{3(\text{AWR})}$ at this lowest energy. This value was also used at $0.75 E_3$, where E_3 is the lowest incident neutron energy for which an angular distribution is given in File 4.

2.1.2. Transition Probability Arrays

Because of an inherent difference between the allowable UK and ENDF/B formats for photon production cross sections, the photon production from inelastic scattering to discrete levels was not translated completely by the code LUTE. The ENDF/B format⁽²⁾ allows not only photon production cross sections (slightly disguised) or yields, as in the UK format, but also allows the alternate use of transition probability arrays when the level energies are well established. Thus, these arrays were entered for all levels up to the highest level for which the level energy and decay scheme are well established. However, photon production data were often given in the UK Data File for incident neutron energies above the energy of this highest level (denoted E_d), so other provisions had to be made for storing these data in ENDF/B format. The method chosen was to use photon production cross sections for incident neutron energies above E_d , exactly as they are given in the UK format. In order to accomplish this conveniently, a new reaction type number was defined for ENDF/B, as discussed in the next section.

2.1.3. Residual Photon Production (MT = 110)

A new reaction type number, MT = 110, was defined and used for residual photon production by incident neutrons with energies greater than E_d . Any inelastic scattering reaction (MT = 5 thru 14 and 51 thru 80) section with incident neutron energies greater than E_d automatically has the photon production cross sections above this energy translated by LUTE to a subsection of photon production cross sections within MT = 110. Also, the first time this case is encountered by LUTE, an MT = 110 section for File 3, with unit cross section, is generated. Thus, the photon production cross sections appear in File 15 under the guise of yields, but processing codes such as LAPH⁽⁷⁾ will properly construct photon production cross sections from the combined data of Files 3 and 15.

2.2. Major Modifications of the Data

Only the three major changes requiring discussion are given in this section. These changes were made in converting to ENDF/B format, but the UK Data File was not altered. Detailed minor corrections or alterations to the UK Data File are given in Appendix A. Minor changes to the ENDF/B Data File are given in Appendix B, and minor alterations for consistency and format purposes are discussed in §2.3.

2.2.1. Photon Production from Inelastic Scattering by ^{37}Cl

Level excitation cross sections for reaction types 5 through 14 and 51 through 53 are for the 1.22 MeV through 6.10 MeV levels, respectively, of ^{35}Cl . However, photon production cross sections in the UK Data File are given for the corresponding levels only for reaction types up to 51. Reaction types 52 through 54 are used to present photon production cross sections for three levels of ^{37}Cl (viz., 1.728, 3.087 and 3.71 MeV). Since the transition probability arrays in the ENDF/B Data File for chlorine do not contain the ^{37}Cl levels, the photon production cross sections for these levels were included in their entirety in the residual photon production section (MT = 110). That is, the parameter E_d was zero for MT = 52, 53 and 54. Photon production

for incident neutron energies below 5.22 MeV (E_d for ^{35}Cl) would thus be given only for ^{35}Cl by the transition probability arrays and corresponding excitation cross sections. Excitation cross sections for the levels of ^{37}Cl are not explicitly given in the UK Data File, but are included in the section for total inelastic scattering, reaction type number (RTN) 1004. They presumably are not included in the section for inelastic scattering to the continuum, RTN = 1015.

2.2.2. Photon Production by the (n,p) and (n, α) Reactions in Potassium

Photon production data for the (n,p) reaction in potassium are identified in the UK Data File by reaction type numbers 13121 and 13122. These RTN's are for the (n,p₁) and (n,p₂) reactions in ^{39}K ; i.e., leaving the residual ^{39}Ar nucleus in the first or second excited states, respectively. Because neutron interaction cross section were given only for the total (n,p) reaction, data for RTN = 13121 and 13122 were combined into one section with MT = 103. This is the ENDF/B reaction type number for the total (n,p) reaction. Angular distributions for these photons were likewise assigned to MT = 103 in File 14.

A similar case occurred for the (n, α) reaction in ^{39}K ; i.e., to the first excited state of ^{36}Cl . Photon production data for this reaction were given in the UK Data File by RTN = 13141, and the angular distribution by RTN = 11141. The data were placed in the ENDF/B Data File under MT = 107.

2.2.3. Photon Production by the (n,p) Reaction in Calcium

Photon production data for the (n,p) reaction in calcium are identified in the UK Data File by reaction type numbers 13060, 13061, and 13062. These RTN's are for the (n,p₁), (n,p₂), and (n,p₃) reactions in ^{40}Ca ; i.e., leaving the residual ^{40}K nucleus in one of its first three excited states. Also, photon production data for inelastic scattering to the continuum are given in RTN = 13015 for incident neutron energies from 6.0 to 20.0 MeV, whereas the corresponding excitation cross sections (RTN = 1015) are given for incident neutron energies from 9.0 to 20.0 MeV. Thus, after

consulting with Drake,⁽⁸⁾ the photon production from 6.0 to 9.0 MeV was assigned to the (n,p) reaction in ENDF/B (MT = 103). Also, as with potassium, the neutron interaction cross sections were given in the UK Data File only for the total (n,p) reaction, so the data in RTN = 13060, 13061, and 13062 were included in the ENDF/B reaction type number for the (n,p) reaction, MT = 103. In a similar manner, angular distributions of photons from the (n,p₁), (n,p₂), and (n,p₃) reactions were assigned to MT = 103.

2.3. Alterations to the Data During Translation to ENDF/B Format

All alterations which were made to the data in UK format were also carried through during translation to ENDF/B format. Since the changes in the UK Data File are documented in detail in Appendix A, they will not be repeated here. There is, however, a class of changes which appears only in the ENDF/B Data File, and those are the ones discussed here. Such changes are typically ones of normalization, consistency between level energies (Q values) and photon energies, etc. The details of the changes appear in Appendix B.

In translating neutron and photon angular distributions to ENDF/B format it was assumed that a zero appearing in the second field of a one-card section with a general classification number (GCN) of 2 or 11 implies an isotropic distribution. The isotropy is explicitly stated for most such cases listed in Tables 4 thru 8 of Reference 3. It was assumed and verified⁽⁸⁾ that the UK-format is consistent in this regard.

2.3.1. Normalizations

Data in the UK Data File were never altered to force normalization of neutron and photon angular distributions, or of neutron secondary energy distributions and photon energy distributions. However, all of these data are required in the ENDF/B Data File to be normalized to probability density functions. Thus, all of these normalizations were automatically performed in the translation procedure. Appendix A lists an example of the integrals of the photon angular distributions as they were determined for the

UK Data File. These re-normalization constants are given for information only; they were not used to alter the UK Data File. Assuming a linear interpolation between μ (i.e., $\cos \theta$) values, the original distributions were usually normalized to unity, within 1%. Re-normalization constants are not listed for the secondary neutron angular distributions, but they were usually within about 1% of unity. Some, however, differed from unity by up to about 15% (e.g., in RTN = 2002 for chlorine).

Figures 1 and 2 show typical plots of data for neutron angular distributions, where the value at $\mu = 0.45$ for an incident neutron energy of $4.8 \text{ E} - 1 \text{ MeV}$ apparently was in error. Correcting this error then introduced a slight error in the normalization, which was in turn corrected.

2.3.2. Miscellaneous

Certain alterations listed in Appendix B were tailored for the LAPH code.⁽⁷⁾ They involve no substantive changes in the data, but are necessary to satisfy the ENDF/B format requirements or to structure the data in an optional form which is simpler or more convenient. Examples of this type change are:

(1) Level energies or Q values in Files 3 and 15 (Option 2), principally in sodium and magnesium, were made consistent with photon energies in File 14. This is required to allow processing codes to correlate level transitions with the angular distributions of the corresponding photons. Any changes of Q value in File 3 were for purely esthetic reasons. A standardization on a particular value was not based upon any new physical data or revelation concerning the correct value among conflicting data. In no case was the difference between conflicting data significant for either data file (i.e., for normal nuclear engineering purposes). In many cases the PHQX code found threshold values lower than theoretically allowed by the Q values, but the values were consistent to within three significant figures so no changes were made in the UK Data File.

(2) In the magnesium data, section (MT) numbers 11, 12, and 13 correspond to the 2.565, 2.736 and 2.803 MeV levels of ^{25}Mg , for which the decay

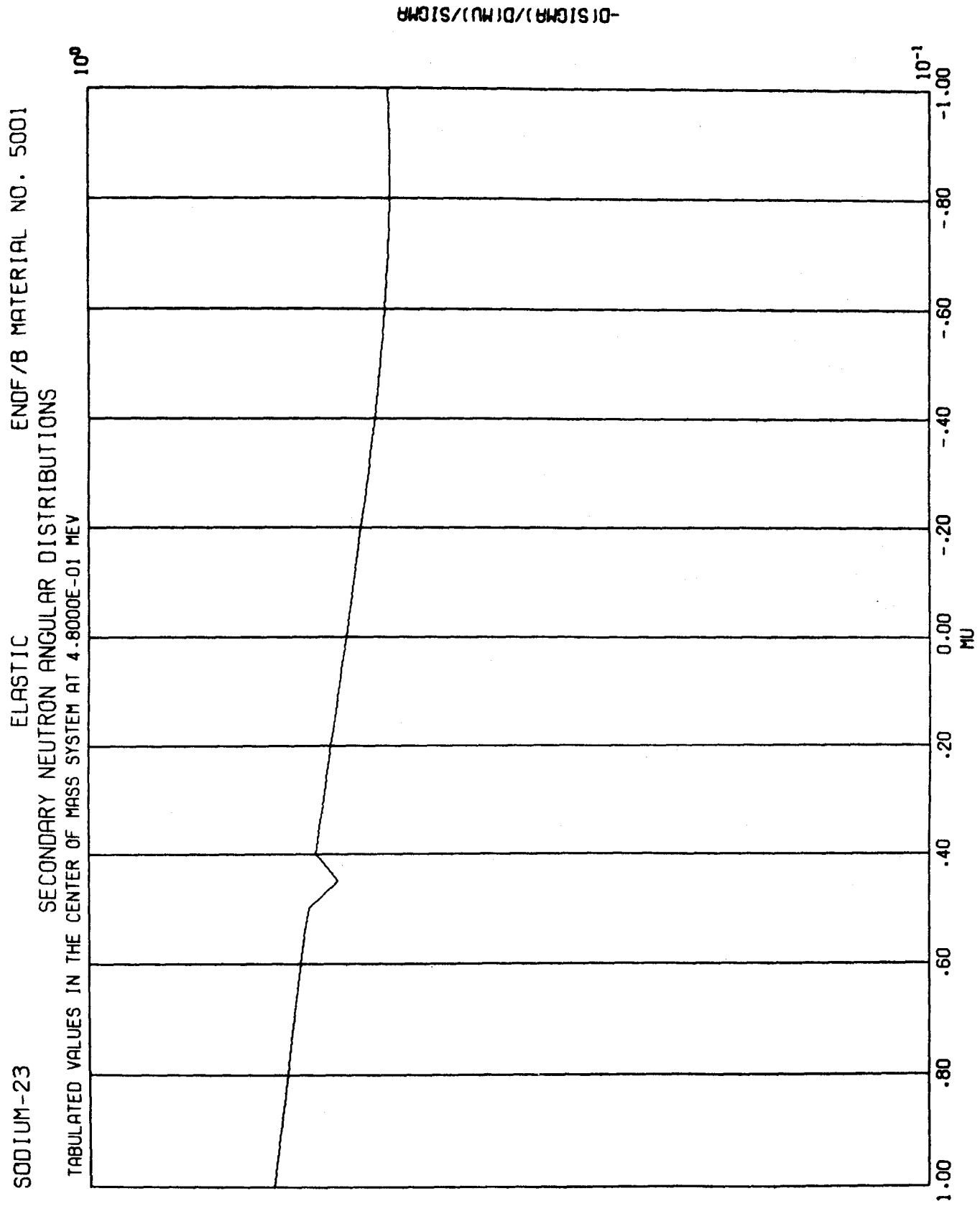


FIGURE 1

SODIUM-23
 ELASTIC
 SECONDARY NEUTRON ANGULAR DISTRIBUTIONS
 ENDF/B MATERIAL NO. 5001
 TABULATED VALUES IN THE CENTER OF MASS SYSTEM AT 4.9000E-01 MEV

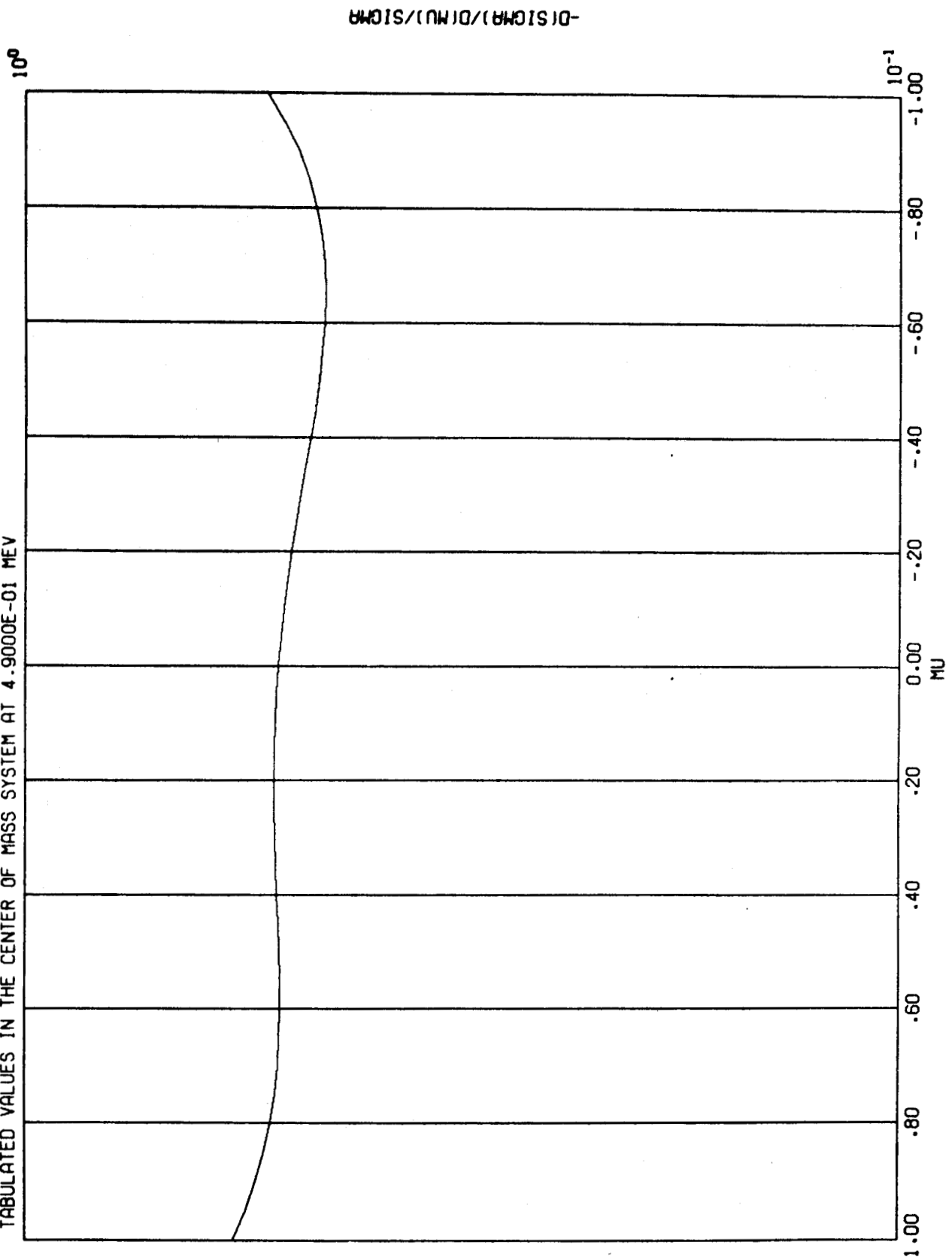


FIGURE 2

schemes are not known. However, MT = 14 corresponds to the 2.94 MeV level of ^{26}Mg , and MT = 51 thru 55 correspond to the 4.12 thru 6.44 MeV levels of ^{24}Mg , all of which have known decay schemes. In order not to preclude the use of transition probability arrays for these latter levels (MT = 14 and 51 thru 55), the levels of ^{25}Mg with unknown decay schemes were assigned zero transition probabilities. Such unorthodox transition probability arrays will be flagged by the photon "physics" checking code, PHQX, but will be acceptable to LAPH. They allow a simple, accurate and concise representation of all photon production from well-known level decay schemes.

(3) In the calcium transition probability arrays, MT = 6 corresponds to the first level of ^{40}Ca (3.35 MeV), which decays by electron-positron emission. In order to correctly compute the resulting annihilation photon source, the energy of this level is listed in File 15 as 0.51 MeV, and the transition probability is assigned the value 2.0. These will be flagged by PHQX as suspicious data.

2.4. Unresolved Inconsistencies

During review of the data several inconsistencies were noted between the UK Data File and the documentation of the data in the Appendices of GA-7829. Also, what seem to be clerical errors appear in these appendices. No changes were made on either the UK or ENDF/B Data File where a question concerning the correct data could not be resolved from the source documentation. However, the questionable data are noted below for possible future revision when time permits.

2.4.1. Sodium

Angular distribution data for secondary neutrons from inelastic scattering to the second (2.08 MeV) level differ considerably between the UK Data File and the documentation (GA-7829, Vol. 11, p. A-53). This discrepancy occurs at 8.5 and 9.0 MeV incident neutron energies, where the documentation lists angular distributions identical to that at 8.0 MeV. The UK Data File (RTN = 2006), on the other hand, lists substantially

different distributions, peaking strongly and irregularly about $\mu = 0$. Plots of the data indicate they are also irregular at 7.5 and 8.0 MeV.

Similarly, for the first excited state (0.4392 MeV level) the document and the UK Data File disagree at various incident energies between 6.0 and 9.0 MeV. Also, even where the data agree it appears from the plots that a discrepancy may occur at $\mu = -1.0$. Though the data were not altered it appears as if a simple extrapolation of the smooth curves to $\mu = -1.0$ would be satisfactory.

2.4.2. Magnesium

Plots of the angular distributions of secondary neutrons from elastic scattering showed irregularities which were not obvious errors, or which were apparently errors but did not seem to be rectifiable by a simple linear interpolation between neighboring points. These occurred at incident neutron energies of 0.19 and 0.68 MeV. A similar case existed at 0.21 MeV, but the data were smoothed for $0.1 \leq \mu \leq 0.4$. A comparison with the original documentation in GA-7829, Vol. III, will show the alterations performed.

2.4.3. Chlorine

A plot of the angular distribution of secondary neutrons from elastic scattering shows an irregularity at $\mu = 1.0$ for an incident neutron energy of 15 MeV. At this point the probability density drops abruptly, whereas at adjacent incident energies the probability rather smoothly approaches a maximum at $\mu = 1.0$.

2.4.4. Potassium

Angular distributions for secondary neutrons from inelastic scattering to the 10th through 17th levels (MT = 51 through 57) are not given at all in the UK Data File. However, Vol. I of GA-7829 states in Table 7, under "Remarks," that these are isotropic. Thus, isotropic angular distributions were not created by LATEX because of no entry being present in the UK Data File. It may be desirable to add these distributions to both

data files in the future. There seems to be no distinction between isotropic distributions which appear in the UK Data File in the form of a single-card section and those which do not appear at all. Secondary neutron angular distributions at 9.5, 10, 10.5, and 11.5 MeV show radical fluctuations at around $\mu = 0.3$. It was not obvious whether these are real or due to clerical errors, and the fluctuations occur for 2 to 3 consecutive data points. Thus, the data were not altered.

2.4.5. Calcium

Data for inelastic level excitation cross sections for the first four levels seem to be displaced in energy between the tabulations in the document and in the UK Data File. This displacement generally occurs for energies above about 3.6 MeV

2.5. Distribution of the Data

Copies of the corrected UK Data File were sent to the Radiation Shielding Information Center (RSIC) at Oak Ridge National Laboratory (ORNL), where a general UK \leftrightarrow ENDF/B translation code is under consideration. These data were also sent to the Los Alamos Scientific Laboratory (LASL) for the Cross Section Data Library (Dr. R. B. Lazarus). Copies of the ENDF/B Data Files were sent to the National Neutron Cross Section Center at Brookhaven National Laboratory (BNL), in addition to RSIC and the Reactor (K) Division at LASL. At LASL the data will be used by the LAPH code⁽⁷⁾ to generate multigroup photon production cross section matrices.

2.6. Translation Codes: LUTE and LATEX

The two codes, LUTE and LATEX, for translation from UK to ENDF/B format, are described in detail elsewhere.⁽⁶⁾ Briefly, LUTE translates the photon production data insofar as possible, and punches a data-card deck. File 1 data for ENDF/B, as well as the transition probability arrays, must be punched separately and used as input to LATEX. The LATEX code then reads these input cards along with the LUTE output deck, translates the neutron interaction data, creates a File 3 section for $\bar{\mu}_{LAB}$, and then outputs a

complete ENDF/B tape for the material.

A listing of the translation codes is given in the documentation,⁽⁶⁾ and copies of the codes were sent to the Radiation Shielding Information Center at ORNL, to the National Neutron Cross Section Center at BNL, and to the Reactor (K) Division at LASL.

3. Proposed "Physics" And Internal Consistency Checks

3.1. introduction

Due to the difficulty of creating an error-free ENDF/B data set, with its inherent complexity and size, some systematic checking procedures must be devised. Any checking procedure should begin with tests which can be performed by a simple computerized analysis of the data. Only tests which require no interactive capability between the computer and the evaluator are considered here. These tests can be divided into two types. Type I is consistency or format syntax tests similar to those in CHECKER.⁽⁹⁾ Some examples of Type I are tests to see that data lie within certain ranges, to see that the proper number of data points are present, and to determine that the data are in proper format. Type II is "physics" checks which will hopefully determine the physical realism and consistency of the data based upon known laws of physics. This type may print out processed data or plots for the program user to check against references or examine visually to detect questionable points. Any inconsistency or suspected error would be flagged by a comment on the output listing. Those checks which were incorporated into the PHOX Code are summarized in §4.

The symbols used in the following section refer to the ENDF/B format for neutron interaction, photon production, and photon interaction data.

3.2. File 3 Checks

Some of the "physics" and consistency checks proposed for File 3 are the following:

1. $E_i \geq E_{th}$, the incident neutron energy for a reaction should be greater than or equal to the threshold energy of that reaction. If $E_i < E_{th}$, flag the suspected energy and continue processing. E_{th} is calculated by the formula $E_{th} = \left(\frac{AWR + 1}{AWR}\right)(-Q)$, for $Q \leq 0$. For $Q > 0$, $E_{th} = 0$.

2. $Q < 0.0$ for MT = 5 thru 14 and 51 thru 80. If $Q \geq 0.0$, flag the suspected Q value and attempt to continue processing.

3. $10^4 \text{ eV} \leq |Q| \leq 2 \times 10^7$ for MT = 5 thru 14 and 51 thru 80. If not in this range, flag the suspected value and continue processing.

4. $Q = 0.0$ for MT = 15 or 110. If not, flag the suspected Q value, set $Q = 0.0$ and continue processing.

5. $Q \geq 0.0$ for MT = 102. If $Q < 0.0$, flag the suspected Q value, set $Q = 0.0$ and continue processing.

6. $1.7 \times 10^6 \text{ eV} \leq Q \leq 1.2 \times 10^7 \text{ eV}$ for MT = 102 if $Q \neq 0.0$. If Q is not in this range and $\neq 0.0$, flag the suspected value, set $Q = 0.0$, and continue processing.

7. For MT = 102, interpolate to find the 2200 m/sec cross section and print it for the user to check against references.

8. There is some question as to the proper Q values for the elements. Consider, for example, the materials translated and reviewed for this report. Except for sodium, which is monoisotopic, the other elements have different Q values for their differing isotopes. The proper weighting of the isotopic Q values (e.g. by abundance or product of abundance and 2200 m/sec cross section) is indeterminable. Thus, Q is simply set equal to zero.

9. $\sigma = 1.0$ for MT = 110. By definition of this reaction type, the cross section must be unity.

3.3. File 14 Checks

Some "physics" and consistency checks that are proposed for File 14 are the following:

1. LTT should be either 1 or 2. If not, assume LTT = 2 and attempt to continue processing under the assumption that angular distributions are given as tabulations vice Legendre coefficients.

2. LI should be either 0 or 1. If not, assume LI = 0 (i.e., a non-isotropic distribution, and attempt to continue processing).

3. NC should be either 0 or 1. If not, assume NC = 0 (i.e., no continuous photon energy spectra are given) and attempt to continue processing.

4. If $LI = 1$, test to see that the next card is a SEND card. If not, then set $LI = 0$ and attempt to continue processing.
5. If $LTT = 1$, then use LEGCK⁽⁹⁾ to test the Legendre coefficients. LEGCK is a computer code that checks Legendre coefficients for possibility and positivity. Any unreasonable or negative coefficients are flagged.
6. $NE > NR$, the number of neutron energy points given must be greater than the number of interpolates. If not, flag the suspected values, set $NR = i$, and attempt to continue processing.
7. $NR > 0$. If not, flag the suspected value, set $NR = 1$ and attempt to continue processing.
8. $INT(m) \neq INT(m-1)$. No two consecutive regions should have the same interpolation scheme. If two regions have the same scheme, flag the suspected region and attempt to continue processing.
9. $ES \geq 0$. If $ES < 0$, flag the suspected value, set $ES = 0$ and continue processing.
10. $EG_i \leq ES$ when $ES > 0$. The i th discrete photon energy is less than or equal to the energy of the state excited to produce the photon (when $ES > 0$). If not, flag the suspected value, set $EG_i = ES$ and continue processing.
11. $EG_i > 0$. If not, test that $ES = EG_i = 0$ and $NC = i$. If this is not the case, flag the suspected value and continue processing.
12. ES does not change within any MT number for inelastic scattering to a discrete level. If ES does change, assume ES to have the first value given, flag the inconsistency, and continue processing.
13. If $ND > 1$, the EG_i must change and must be in decreasing order. If not, flag the suspected values and continue processing.
14. $ES = |Q|$ for $MT = 5$ thru 14 and 51 thru 80. If not, flag the suspected value, set $ES = |Q|$ and continue processing.
15. $10^4 \text{ eV} \leq ES \leq 2 \times 10^7 \text{ eV}$ for $MT = 5$ thru 14 and 51 thru 80. If not, flag the suspected value and continue processing.

3.4. File 15 Checks

Some "physics" and consistency checks that are proposed for File 15 are the following:

1. The ES values must be the same as in File 14 for a given MT number. If not, flag the suspected value and continue processing.

2. All the tests for ES listed in File 14, Section 3.3 also apply in File 15.

3. The EG_i must have the same values as in File 14 for a given MT number. Under option 2 of File 15 all possible EG_i must be determined from the cascade and matched to an EG_i in File 14. The existence of a particular value of EG_i in File 14 requires a corresponding value in File 15, but not vice versa. If values differ or a File 14 subsection has no correspondent whatsoever in File 15, flag the suspected values and continue processing.

4. All the tests for EG_i listed in File 14, Section 3.3 also apply in File 15.

5. $L0$ should be either 1 or 2. If not, flag the suspected value, set $L0 = 1$ and attempt to continue processing with the assumption that data are given as photon production multiplicities.

6. LF should be either 1 or 2. If not, flag the suspected value, set $LF = 2$ and attempt to continue processing with the assumption that data are given by discrete photon energies instead of by tabulated distributions.

7. $NT \leq NS$, the number of transitions must be less than or equal to the number of levels below the present level (includes ground state). If not, flag the suspected values, set $NT = NS$ and attempt to continue processing.

8. Under option 2, $NS = MT - 4$ for $MT = 5$ thru 14 and $NS = MT - 40$ for $MT = 51$ thru 80. If not, flag the suspected value, set $NS = MT - 4$ or $MT - 40$, as appropriate, and continue processing.

9. $NR < NP$ is the same test as listed in File 14, Section 3.3.

10. The sum of the probabilities in a cascade should add to unity. If the sum differs from unity by more than 10^{-4} , flag the suspected cascade and continue processing.

11. $E_+ \leq E_C + Q$ for reactions in which the neutron disappears. For neutron disappearance reactions, in which a compound nucleus is formed, the total energy of the emitted photons, denoted E_+ , is less than or equal to the Q value plus the kinetic energy of the neutron, in the center of mass system, denoted E_C . It is assumed that the tabulated neutron energy in the laboratory system is a sufficiently accurate approximation of E_C . If $E_+ > (E_C + Q)$, flag the suspected value and continue processing. This can be calculated by the following:

$$[\bar{E}_\gamma(E_i) \cdot y_k(E_i) + \sum_k (EG_i)_k \cdot y_k(E_i)] \leq Q + E_i$$

where $\bar{E}_\gamma = \int dE_\gamma g(E_\gamma \leftarrow E_i) E_\gamma$, the $y_k(E_i)$ are the photon multiplicities, and the $g(E_\gamma \leftarrow E_i)$ are the probability density functions.

12. $E_+ \leq |Q|$ for reactions in which the neutron does not disappear. The total energy of the emitted photons, E_+ , should be less than or equal to magnitude of the Q value. If $E_+ > |Q|$, flag the suspected value and continue processing. This is calculated in the same manner as above.

13. If $L_0 = 1$, $Y(E) = \sum_{k=1}^{N_k} y_k(E)$, the total photon yield should equal the sum of the integrals over the secondary energies. These values should agree to within the fourth significant figure. If not, flag the suspected value and continue processing.

14. For $L_0 = 1$ and $LF = 1$, the normalization should be tested. If $I_1 = \int g(E_\gamma \leftarrow E_i) dE_\gamma$, where $g(E_\gamma \leftarrow E_i)$ is the normalized photon energy distribution (i.e., probability density function), then the normalization is tested by insuring $|I_1 - 1| \leq 10^{-4}$. If not, flag the suspected normalization value and continue processing.

3.5. File 23 Checks

The proposed "physics" and consistency checks for File 23 are the following:

1. $\sigma_{\gamma} = \sigma_{pe} + \sigma + \sigma_c + \sigma_{pp}$, total photon cross section equals the sum of the individual cross sections for photoelectric effect, Rayleigh or coherent scattering, Compton scattering, and pair production. For practical purposes the effects of the following are neglected: Delbruck or potential scattering, Thomson scattering by the nucleus, photonuclear reactions, and crystal scattering. The sum should agree with σ_{γ} to within the fourth significant figure. If not, flag the suspected value and continue processing.

2. The Compton scattering cross section is checked by the Klein-Nishina formula

$$\sigma = \frac{2\pi e^4}{m_0^2 c^4} \left\{ \frac{1+\alpha}{\alpha^2} \left[2 \frac{(1+\alpha)}{1+2\alpha} - \frac{1}{\alpha} \ln(1+2\alpha) \right] + \frac{1}{2\alpha} \ln(1+2\alpha) - \frac{1+3\alpha}{(1+2\alpha)^2} \right\}$$

where $\alpha = hv/m_0c^2$ and $e =$ an electron charge. The values should agree to within the second significant figure over most of the energies of practical interest. If not, flag the suspected value and continue processing.

3. For pair production $E_{\gamma} > 1.02$ MeV. If not, flag the suspected value, ignore the corresponding cross section and continue processing.

4. For pair production, the total cross section should monotonically increase with photon energy. If not, flag the suspected values and continue processing.

5. The energy at which pair production contributes exactly one-half the total cross section is computed, printed and checked by the user against references.

6. The energy at which the photoelectric effect contributes exactly one-half the total cross section is computed, printed and checked by user against references.

7. The photoelectric effect for each shell has a threshold energy below which the reaction can not take place. Therefore, the lowest energy present in the file is found and printed for checking by the user against references (electron binding energies).

8. For the photoelectric effect, the K-edge and all other discontinuities are computed and printed for checking by the user against references.

9. For the photoelectric effect, the cross section decreases monotonically with photon energy at the edges. Any discrepancy would be picked up and flagged as an "edge."

3.6. File 24 Checks

The proposed "physics" and consistency checks for File 24 are the following:

1. LTT follows same checks as listed in File 14, Section 3.3.
2. LCT should be either 1 or 2. If not, flag the suspected value, set LCT = 1 and attempt to continue processing with the assumption that data are given in the LAB system. Where the secondary particle is a photon, the convention adopted⁽²⁾ is that LCT = 1.
3. Normalization is tested by the following: $\int_{-1}^1 d\mu p(\mu, E_i) = 1$. If the values do not agree to within the fourth significant figure, flag the suspected values and continue processing.

3.7. File 27 Checks

The proposed "physics" and consistency checks for File 27 are the following:

1. Incoherent form factors (sometimes called incoherent scattering functions) should monotonically increase and approach unity as photon energy increases. They should be within 3% of unity at 1 MeV.
2. Coherent form factors should decrease and approach zero as photon energy increases.

4. PHOX, A "Physics" Checking Code For Photon Data In The ENDF/B Data File

4.1. Introduction and Summary

Much work has been and is being done to place data in the ENDF/B Data File format. In the process of this work there are naturally many errors which occur and which might pass undetected in a visual review of these data. Therefore, a code called CHECKER⁽⁹⁾ was written by BNL to check the mechanics (i.e., format syntax) of the data. However, no code existed which checked the physical aspects of the data, or otherwise determined whether the data were reasonable or even possible. Therefore, it is the purpose of this section to explain how several "physics" checks were incorporated into a computer code which does this to some degree for the photon data. The exact division between format syntax and "physics" types of checks is not well defined, so the pragmatic definition of "physics" checks is those checks not done by CHECKER.

There are several types of physical checks which are made by PHOX. They include checks such as testing that the values are within given ranges, that all energy points are above the theoretical threshold as determined from the Q value, that the total energy released by photons does not exceed the energy available as determined by the Q value and neutron energy, etc.

The PHOX code is designed in a manner similar to CHECKER in that it calls various subroutines which do the actual reading, checking and writing. It is written in FORTRAN IV and has been successfully run on the B5500 computer at the University of Virginia.

While the program is designed to attempt to process any section, even if an error in one of the control parameters is discovered, the code may terminate due to trying to read data in an alien format. When control parameters are out of the acceptable range, the code assumes a value within the acceptable range and attempts to proceed. Whenever an error is determined, a message is printed to that effect giving the necessary values, if needed.

4.2. PHOX Code and Subroutines

PHOX is a FORTRAN IV code designed to read an ENDF/B data tape and run certain checks on the data, flagging those it believes to be in error. It is designed primarily to read a BCD card image tape (mode 3) and, while not tested, it is also believed to be able to process a binary tape in standard arrangement for ENDF/B (i.e., mode 1). An INDEX'ed listing of PHOX, giving the statement numbers and variable names, is given in Appendix C.

The main program, PHOX, is essentially a calling routine which searches for the files to be checked and assigns the reading, checking, and writing tasks to the appropriate subroutines in the proper order. If the files of interest are not found on the data tape, messages to that effect are written, and the run is terminated. Several of the BNL retrieval subroutines⁽⁹⁾ were used in PHOX. These include RREC, TERPI, ERROR, and WREC with its supplemental subroutines. A modification of the CHECKER subroutine TEST2B(MT)⁽⁹⁾ was made and incorporated in PHOX. The purpose of this subroutine, called TEST2C(MT), is to check for the proper MT numbers in File 14.

4.2.1. CKHD(FILE)

CKHD is designed to check the HEAD records of Files 14 and 15. It checks the different fields (not including ZA and AWR) for range, and if discovered to be outside of the range, a "guess" is made and processing continues. When it is necessary to make a guess, a message to that effect is printed which informs the user as to the guessed value.

4.2.2. FIL3(AWR)

FIL3 is designed to calculate a theoretical threshold value for File 3, based on AWR and Q, and to test it against the first energy point given. If this energy point is found to be below the threshold value, a message to that effect is written, along with the theoretical value. FIL3 then stores Q (after checking it for reasonableness of sign and magnitude according to the reaction type) and the larger of either the theoretical threshold or the first energy point, for use in Files 14 and 15.

4.2.3. FIL14(N)

FIL14 is designed to test ES and EG for consistency and reasonableness of magnitude and sign. It also tests for a continuous spectrum and makes sure there is only one continuous spectrum. Using subroutine ESEGPR, FIL14 stores ES and EG for later use.

Each TABI record is tested for increasing order of incident neutron energy and for magnitude as compared with the threshold value stored in FIL3.

4.2.4. FIL15(N)

FIL15 is designed to check either option 1 or 2. In option 1 the subsection yields are totaled and checked against the total yields at the total yield energies. The total MeV released per interaction is calculated and compared against the sum of the Q value and kinetic energy, where appropriate. The incident neutron energies and the first energy in each array are checked against the threshold value stored in FIL3. The ES and EG pairs are also used in subroutine ESEGPR.

In option 2 the values of ES_i are checked for decreasing order, the TP_i for magnitude and total sum, and the GP_i for magnitude. The ES's are also checked against the magnitude of Q, as stored in FIL3, and that they correspond to previous state levels. Also the difference between each state level and the previous state levels are checked as ES and EG pairs by ESEGPR.

4.2.5. ESEGPR(N)

ESEGPR is designed to check that each ES-EG pair given in File 14 is used in File 15. In the case of option 1 in File 15 the comparison is direct, but for option 2 it is necessary to calculate the EG's by subtracting the lower state levels from the present state level. After completion of File 15, ESEGPR is called and a final check of all the values, (ES-EG pairs), is made to insure that each has been accounted for. Any that are found to remain unaccounted for are listed on the output.

4.2.6. STATE(LG)

STATE is designed to check that each value of ES_j corresponds to a previous value of ES as read from previous inelastic scattering sections, MT = 5-14 and 51-80.

4.3. Input and Output Specifications

4.3.1. PHOX input

The input consists of one ENDF/B data tape, designated unit NT, and two cards. The cards consist of

1) NT,MODE,MATW

entered in (3I11) format, where NT is the input tape I/O unit number, MODE is the mode of the input tape, and MATW is the material number of the material to be checked.

2) LIST entered in (13A6,A2) format. This card is reproduced identically as the first line of output on the listing. This enables the user to place any information he desires on the output.

The card reader is designated as I/O unit number 5 while the line printer is designated as I/O unit number 6. The choice of the NT number is left to the user.

4.3.2. PHOX Output

The output consists of a listing of Files 3, 14 and 15 with any comments which PHOX might print. It should be pointed out that all comments are written after the ENDF/B record in which a possible error is detected and not necessarily immediately after the card on which it occurs.

4.4. Burroughs B5500 Computer Fortran IV Compiler Features

Only two minor characteristics of the B5500 Fortran IV dialect are known which might affect the running of PHOX on other computers. These are:

1) Upon entry into a subroutine, the B5500 automatically initializes to zero all variables not held in COMMON. It also initializes all storage points to zero upon entry into the main program.

2) The method used on the B5500 to determine the statement to proceed to upon reaching an End-of-File is:

READ (U,F,END=S) LIST

where U is the unit number,

F is the format number,

S is the number of the statement to go to if an End-of-File is reached

and

LIST is the list of variables to be read.

APPENDIX A: Corrections and Alterations to the Data in UK Format

The following tabulation lists the card numbers, data changes and comments for all changes made to the data files in UK format since about July 1968. All changes made prior to that date were incorporated into the Cross Section Data Library at LASL, and were mostly to correct cards out of sequence, cards missing and other clerical errors. One alteration which was made after consultation with Drake was to change the RTN for the (n,n'p) reaction from 32 to 28, in agreement with the corresponding ENDF/B reaction type number, MT = 28.

Also found in this appendix, under the heading of A.1.2. are normalization values from File 14 and 15 of SODIUM for the photon secondary distributions as calculated by CHECKER. All materials were affected but only SODIUM is given here as an example. These are integrals found via the trapezoidal rule, as required by the interpolation scheme. They are only noted here; no renormalization was attempted in the UK Data File but corresponding data in ENDF/B were renormalized (cf. MF = 14).

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- A.1. UK Material Number (MIN) 205* SODIUM
 - A.1.1. Data File Changes
 - A.1.2. Normalization Value from CHECKER

- A.2. UK Material Number (NIN) 206 * MAGNESIUM
 - A.2.1. Data File Changes

- A.3. UK Material Number (NIN) 221 * CHLORINE
 - A.3.1. Data File Changes

- A.4. UK Material Number (NIN) 227 * POTASSIUM
 - A.4.1. Data File Changes

- A.5. UK Material Number (NIN) 231 * CALCIUM
 - A.5.1. Data File Changes

A.1. UK Material Number (NIN) 205 * SODIUM

A.1.1. Data File Changes

CARD(S) NUMBER: 000i0
CHANGE: Field 3: From 113 to 105
COMMENTS: Correct card count.

CARD(S) NUMBER: 00012, 00013
CHANGE: Field 3: From 97 to 89
COMMENTS: Correct card count.

CARD(S) NUMBER: 000i4
CHANGE: Field 3: From 89 to 81
COMMENTS: Correct card count.

CARD(S) NUMBER: 00019
CHANGE: Field 3: From 81 to 73
COMMENTS: Correct card count.

CARD(S) NUMBER: 00020
CHANGE: Field 3: From 57 to 49
COMMENTS: Correct card count.

CARD(S) NUMBER: 00022
CHANGE: Field 3: From 33 to 25
COMMENTS: Correct card count.

CARD(S) NUMBER: 03462
CHANGE: Field 6 From 5.94301E-1 to 5.75982E-1
COMMENTS: Error apparent from plot of data.

CARD(S) NUMBER: 03464
CHANGE: Field 2: From 5.66787E-1 to 6.18222E-1
COMMENTS: Error....

CARD(S) NUMBER: 03479
CHANGE: Field 2: From 5.68798E-1 to 6.07534E-1
COMMENTS: Error....

CARD(S) NUMBER: 03492
CHANGE: Field 6: From 4.85219E-1 to 5.22592E-1
COMMENTS: Error....

CARD(S) NUMBER: 03494
CHANGE: Field 2: From 5.44224E-1 to 5.31727E-1
COMMENTS: Error....

CARD(S) NUMBER: 03507
CHANGE: Field 6: From 5.04533E-1 to 5.42012E-1
COMMENTS: Error....

CARD(S) NUMBER: 03784
CHANGE: Field 6: From 2.95058E-1 to 2.68496E-1
COMMENTS: Error....

CARD(S) NUMBER: 03799
CHANGE: Field 6: From 3.05212E-1 to 2.68238E-1
COMMENTS: Error....

CARD(S) NUMBER: 03814
CHANGE: Field 6: From 2.96422E-1 to 2.59656E-1
COMMENTS: Error....

CARD(S) NUMBER: 03938
CHANGE: Field 6: From 1.70142E-1 to 3.61688E-1
COMMENTS: Error.....

CARD(S) NUMBER: 03953
CHANGE: Field 6: From 1.7185E-1 to 3.62734E-1
COMMENTS: Error.....

CARD(S) NUMBER: 03983
CHANGE: Field 6: From 4.54161E-1 to 3.39764E-1
COMMENTS: Error.....

CARD(S) NUMBER: 03998
CHANGE: Field 6: From 4.81876E-1 to 3.29298E-1
COMMENTS: Error.....

CARD(S) NUMBER: 03118
CHANGE: Field 6: From 3.44406E-1 to 2.95546E-1
COMMENTS: Error.....

CARD(S) NUMBER: 03270 (second)
CHANGE: Field 2: From 3.91512E-1 to 3.21048E-1
COMMENTS: Error.....

CARD(S) NUMBER: 08002
CHANGE: Field 5: From 69 to 68
COMMENTS: Clerical error in data pair count.

CARD(S) NUMBER: 10002
CHANGE: Field 5: From 63 to 61
COMMENTS: Clerical.....

CARD(S) NUMBER: 12002
CHANGE: Field 5: From 57 to _____
COMMENTS: Clerical.....

CARD(S) NUMBER: 14002
CHANGE: Field 5: From 57 to 55
COMMENTS: Clerical.....

CARD(S) NUMBER: 17001
CHANGE: Field 2: From 14 to
COMMENTS: Correct card count.

17010 to 17017
21010 to 21017
23010 to 23017
25010 to 25017
35010 to 35017
37010 to 37017

CARD(S) NUMBER: 41010 to 41017
CHANGE: Delete these cards.
COMMENTS: Neutron angular distributions below the thresholds (or essentially at threshold for PCN = 51) for inelastic scattering to discrete levels. Data not meaningful.

CARD(S) NUMBER: 21001
CHANGE: Field 2: From 12 to 11
COMMENTS: Correct card count.

CARD(S) NUMBER: 23001
CHANGE: Field 2: From 12 to 11
COMMENTS: Correct card count.

CARD(S) NUMBER: 25001
CHANGE: Field 2: From 11 to 10
COMMENTS: Correct card count.

CARD(S) NUMBER: 35001
CHANGE: Field 2: From 10 to 9
COMMENTS: Correct card count.

CARD(S) NUMBER: 37001
CHANGE: Field 2: From 7 to 6
COMMENTS: Correct card count.

CARD(S) NUMBER: 41001
CHANGE: Field 2: From 4 to 3
COMMENTS: Correct card count.

CARD(S) NUMBER: 65003
CHANGE: Field 2: From 9.0 to 9.05
COMMENTS: Clerical error.

A.1.2. Normalization Value from CHECKER (for Files14 and 15)

MF = 14 * MT = 5

<u>Energy (MeV)</u>	<u>Normalization Factor</u>	<u>Energy (MeV)</u>	<u>Normalization Factor</u>
0.4580	0.99986	5.0000	0.99984
0.5000	1.0003	5.5000	0.99985
1.0000	0.99981	6.0000	0.99986
1.5000	0.99987	6.5000	0.99987
2.0000	0.99986	7.0000	0.99987
2.5000	0.99986	7.5000	0.99987
3.0000	0.99985	8.0000	0.99987
3.5000	0.99984	8.5000	0.99987
4.0000	0.99983	9.0000	0.99986
4.5000	0.99983		

MT = 6

2.1700	0.99920	2.1700	0.99920
2.5000	0.99946	2.5000	0.99946
3.0000	0.99969	3.0000	0.99969
3.5000	0.99987	3.5000	0.99987
4.5000	1.00010	4.5000	1.00010
5.0000	1.00020	5.0000	1.00020
5.5000	0.99960	5.5000	0.99960
6.0000	0.99960	6.0000	0.99960
6.5000	0.99961	6.5000	0.99961
7.0000	0.99962	7.0000	0.99962
7.5000	0.99963	7.5000	0.99963
8.0000	0.99966	8.0000	0.99966
8.5000	0.99968	8.5000	0.99968
9.0000	0.99972	9.0000	0.99972

MT = 9

<u>Energy (MeV)</u>	<u>Normalization Factor</u>	<u>Energy (MeV)</u>	<u>Normalization Factor</u>
2.8230	1.00050	2.8230	1.00210
3.0000	1.00130	3.0000	1.00130
3.5000	1.00060	3.5000	1.00060
4.0000	1.00010	4.0000	1.00010
4.5000	0.99982	4.5000	0.99982
5.0000	0.99970	5.0000	0.99970
5.5000	1.00030	5.5000	1.00030
6.0000	1.00030	6.0000	1.00030
6.5000	1.00030	6.5000	1.00030
7.0000	1.00030	7.0000	1.00030
7.5000	1.00030	7.5000	1.00030
8.0000	1.00040	8.0000	1.00040
8.5000	1.00040	8.5000	1.00040
9.0000	1.00050	9.0000	1.00050

MT = 10

8.5000	0.99987	8.5000	0.99987
9.0000	0.99982	9.0000	0.99982

MT = 12

4.0170	0.99966	4.0170	0.99966
4.5000	0.99962	4.5000	0.99962
5.0000	0.99973	5.0000	0.99973
5.5000	0.99981	5.5000	0.99981
6.0000	0.99955	6.0000	0.99955
6.5000	0.99915	6.5000	0.99915
7.0000	0.99896	7.0000	0.99896
7.5000	0.99892	7.5000	0.99892
8.0000	0.99904	8.0000	0.99904
8.5000	0.99931	8.5000	0.99931
9.0000	0.99974	9.0000	0.99974

MT = 13

<u>Energy (MeV)</u>	<u>Normalization Factor</u>	<u>Energy (MeV)</u>	<u>Normalization Factor</u>
4.0850	0.99972	4.0850	0.99972
4.5000	0.99981	4.5000	0.99981
5.0000	0.99987	5.0000	0.99987
5.5000	0.99975	5.5000	0.99975
6.0000	0.99974	6.0000	0.99974
6.5000	0.99975	6.5000	0.99975
7.0000	0.99963	7.0000	0.99963
7.5000	0.99960	7.5000	0.99960
8.0000	0.99960	8.0000	0.99960
8.5000	0.99965	8.5000	0.99965
9.0000	0.99974	9.0000	0.99974

MT = 51

4.9860	0.99961	7.5000	0.99965
5.5000	0.99968	8.0000	0.99986
6.0000	0.99971	8.5000	1.00030
6.5000	0.99972	9.0000	1.00090
7.0000	0.99972	4.9860	0.99961
7.5000	0.99965	5.5000	0.99968
8.0000	0.99986	6.0000	0.99971
8.5000	1.00030	6.5000	0.99972
9.0000	1.00090	7.0000	0.99972
4.9860	0.99961	7.5000	0.99965
5.5000	0.99968	8.0000	0.99986
6.0000	0.99971	8.5000	1.00030
6.5000	0.99972	9.0000	1.00090
7.0000	0.99972	4.9860	0.99961
7.5000	0.99965	5.5000	0.99968
8.0000	0.99986	6.0000	0.99971
8.5000	1.00030	6.5000	0.99972
9.0000	1.00090	7.0000	0.99972
4.9860	0.99961	7.5000	0.99965
5.5000	0.99968	8.0000	0.99986
6.0000	0.99971	8.5000	1.00030
6.5000	0.99972	9.0000	1.00090
7.0000	0.99972		

MT = 53

<u>Energy (MeV)</u>	<u>Normalization Factor</u>	<u>Energy (MeV)</u>	<u>Normalization Factor</u>
8.5000	0.99978	8.5000	0.99978
9.0000	0.99964	9.0000	0.99964
8.5000	0.99978	8.5000	0.99978
9.0000	0.99964	9.0000	0.99964

MF = 15 * MT = 15

9.0500	1.01220
12.0000	1.00040
16.0000	-----

A.2. UK Material Number (NIN) 206 * MAGNESIUM

A.2.1. Data File Changes

CARD(S) NUMBER: 0000i
CHANGE: Field 2: From 71650 to 7165
COMMENTS: Card count changed - clerical error.

CARD(S) NUMBER: 03i00
CHANGE: Field 4: From 2.99689E-1 to 2.45057E-1
COMMENTS: Error apparent from plot of data.

CARD(S) NUMBER: 03i48
CHANGE: Field 3: From -0.1 to -0.55
Field 4: From 0.0 to 0.50028
COMMENTS: Appears to be an error. Values were interpolated between adjacent pairs in table to get an estimate of the correct value. Zero value in field 4 also occurs in the appendix of NDL-TR-89, Vol. 11.

CARD(S) NUMBER: 03i59 (second time)
CHANGE: Field 2: From 4.7732iE-1 to 4.32770E-1
COMMENTS: Error....

CARD(S) NUMBER: 03200
CHANGE: Field 4: From 1.38293 to 1.25720
COMMENTS: Error....

CARD(S) NUMBER: 0328i (second time)
CHANGE: Field 2: From 3.09070E-1 to 2.45343E-1
COMMENTS: Error....

CARD(S) NUMBER: 03429
CHANGE: Field 1: From -0.0 to -0.1
COMMENTS: Clerical error.

CARD(S) NUMBER: 03455 (second time)
CHANGE: Field 4: From 1.67767 to 1.460i8
COMMENTS: Error....

CARD(S) NUMBER: 15004
CHANGE: Field 2: From 4.32157E-1 to 5.08099E-1
COMMENTS: Error....

CARD(S) NUMBER: 27098
CHANGE: Field 2: From 4.75 to 4.25
COMMENTS: Clerical error.

CARD(S) NUMBER: 27125
CHANGE: Field 2: From 5.5 to 5.0
COMMENTS: Clerical error.

CARD(S) NUMBER: 29003 29011 29019 29027 29035 29043 29052
29061 29070 29079 29088 29097 29107 29117
29127 29137 29147 29157 29168 29179 29190
29201 29212 29223 29235 29247
31003 31013 31023 31033 31044 31055 31066
31077 31088 31099 31111 31123
33003 33013 33023 33033 33043 33053 33063
33074 33085 33096 33107 33118 33129 33141
33153

CHANGE: Field 2: From 1.00000-02 to 1.00010-02
COMMENTS: Change to avoid double values at 1.00000-02.

CARD(S) NUMBER: 48001
CHANGE: "P" removed from margin.
COMMENTS: Clerical or machine error.

CARD(S) NUMBER: 57018
CHANGE: Field 4: From 5.84000-01 to 1.96200+00
COMMENTS: Clerical error in photon energy.

A.3. UK Material Number (NIN) 22i * CHLORINE

A.3.1. Data File Changes

CARD(S) NUMBER: 00002
CHANGE: Field 5: From 2002 to 1002
COMMENTS: Clerical error in RTN number in the "index".

CARD(S) NUMBER: 09077
CHANGE: Field 4: From 3.1189i-0i to 4.85646-0i
COMMENTS: Consistency between Q values in File 3, photon energies in File 14, and level energies in File 15.

CARD(S) NUMBER: 09079
CHANGE: Field 4: From 3.1189i-0i to 4.85646-0i
COMMENTS: Consistency.....

CARD(S) NUMBER: 09085
CHANGE: Field 4: From 9.88596-0i to 3.86887-0i
COMMENTS: Consistency.....

CARD(S) NUMBER: 09087
CHANGE: Field 4: From 9.88596-0i to 3.86887-0i
COMMENTS: Consistency.....

CARD(S) NUMBER: 09093
CHANGE: Field 4: From 2.16940+00 to 2.17700-0i
COMMENTS: Consistency.....

CARD(S) NUMBER: 09095
CHANGE: Field 4: From 2.16940+00 to 2.17700-0i
COMMENTS: Consistency.....

CARD(S) NUMBER: 19002
CHANGE: Field 1: From 74.175 to 4.175
COMMENTS: Energy level in error. A clerical error.

CARD(S) NUMBER: 2800i
CHANGE: Field 3: From -1.6630+0i to -1.2650+0i
COMMENTS: Clerical error in Q value.

CARD(S) NUMBER: 35020
CHANGE: Field 2: From 5.06532-01 to 5.06896-01
COMMENTS: Consistency....

CARD(S) NUMBER: 35024
CHANGE: Field 6: From 5.06532-01 to 5.06896-01
COMMENTS: Consistency....

CARD(S) NUMBER: 35028
CHANGE: Field 2: From 5.10364-01 to 5.10953-01
COMMENTS: Consistency....

CARD(S) NUMBER: 35032
CHANGE: Field 6: From 5.10364-01 to 5.10953-01
COMMENTS: Consistency....

A.4. UK Material Number (N|N) 227 * POTASSIUM

A.4.1. Data File Changes

CARD(S) NUMBER: 03354
CHANGE: Field 6: From 9.703i2-02 to 9.4876i-02
COMMENTS: Error apparent from plot of data.

CARD(S) NUMBER: 03744
CHANGE: Field 6: From 1.01442-0i to 1.003238-0i
COMMENTS: Error....

CARD(S) NUMBER: 03774
CHANGE: Field 4: From 3.24552+00 to 8.58534-02
COMMENTS: Error....

CARD(S) NUMBER: 03789
CHANGE: Field 4: From 8.45403+00 to 2.71933-02
COMMENTS: Error....

CARD(S) NUMBER: 03804
CHANGE: Field 4: From 6.38497+00 to 6.53297-02
COMMENTS: Error....

CARD(S) NUMBER: 03808
CHANGE: Field 6: From 5.10289-02 to 1.16280-01
COMMENTS: Error....

CARD(S) NUMBER: 03823
CHANGE: Field 6: From 1.15560-0i to 2.91788-0i
COMMENTS: Error....

CARD(S) NUMBER: 03838
CHANGE: Field 6: From 1.96689-0i to 3.15894-0i
COMMENTS: Error....

CARDS: 17010
CHANGE: Field 6: From Blank to 21
COMMENTS: Clerical error - the number of data pairs in the subsection.

CARD(S) NUMBER: 27001

CHANGE: Field 2: From 60 to 6

COMMENTS: Clerical error.

CARD(S) NUMBER: 33001

CHANGE: Field 2: From blank to 1

COMMENTS: Clerical error.

A.5. UK Material Number (NIN) 231 * CALCIUM

A.5.1. Data File Changes

CARD(S) NUMBER: 0000i

CHANGE: (a) Field 2: From 5683 to 5695
(b) Field 3: From 38 to 39
(c) Field 6: From 74 to 75

COMMENTS: (a) Change of total number of cards to represent this nuclide including the cards in Section 0.
(b) Number of card in this index, including this card.
(c) The number of RTN sections in this material.

CARD(S) NUMBER: 00035

CHANGE: Field 3: From 95 to 71

COMMENTS: Number of cards in Section 13015.

CARD(S) NUMBER: 00036

CHANGE: Field 5: From 13066 to 13060

COMMENTS: Clerical Error.

CARD(S) NUMBER: 00039

CHANGE: ADD card for new section
Field 1 = 75
Field 2 = 13103 RTN
Field 3 = 34 number of cards
Field 4)
Field 5) - blank
Field 6)
Field 7 = 23100039 Material number and sequence number.

CARD(S) NUMBER: 21010

CHANGE: Field 1 Energy: From 6.0 to 6.2

COMMENTS: Second neutron energy tabulated is less than the first one in this section. A clerical error.

CARD(S) NUMBER: 26003
CHANGE: Field 3: From 9.001 (MeV) to 9.00010 (MeV)
Field 4: From 1.0 -20 to .2387
COMMENTS: To eliminate repetition of a zero (i.e., 10^{-20})
cross section.

CARD(S) NUMBER: 39010
CHANGE: Field 1: Energy: From 8.0 to 8.2
COMMENTS: Second energy less than first.

CARD(S) NUMBER: 43010
CHANGE: Field 1: Energy: From 8.5 to 8.7
COMMENTS: Second neutron energy less than the first. A
clerical error.

CARD(S) NUMBER: 66001
CHANGE: Field 6: Energy: Changed to 6.56
COMMENTS: Energy level corrected.

CARD(S) NUMBER: 67002
CHANGE: (a) Field 1: From 6.0 to 9.00010 (MeV)
(b) Field 3: From 94 to 70
COMMENTS: (a) Lower limit of incident neutron energy range
(MeV) changed to correspond with RTN 1015,
where lowest energy is 9.0 MeV.
(b) Number of cards used to represent this incident
neutron energy range, including this card.

CARD(S) NUMBER: 67003 thru 67026
CHANGE: Deleted section of data.
COMMENTS: These were tabulated energy and cross section
data for reactions occurring below threshold.
(ref. change on control card numbered 67002)
Data can now be found under Reaction Type
number 13103. Lower energy limit 9.00010 MeV
to avoid duplicate photon specification at
9.0 MeV.

CARD(S) NUMBER: 67027

CHANGE: (a) Field 2: From i0 to 7

(b) Field 3: From 9.0 to 9.000i0 (MeV)

COMMENTS: (a) Number of sub-sections in the section for this PCN.

(b) First energy at which photon production cross sections are specified.

CARD(S) NUMBER: 67036, 67045, 67055, 67065, 67075, 67085

CHANGE: Field 2: From i0 to 7

COMMENTS: Number of sub-sections in the section for this PCN.

CARD(S) NUMBER: 75001 thru 75035

CHANGE: New section for RTN 13i03: (n,p) reaction.

COMMENTS: Data were derived from the original cards 67003 thru 67026 with a change only in the sub-section count parameter.

APPENDIX B: Alterations to the Data in Transforming to
ENDF/B

As discussed in Section 2.3., several revisions were made to the data for compatibility with the ENDF/B system. These are documented in detail in this Appendix.

CONTENTS OF APPENDIX B

- B.1. ENDF/B Material Number (MAT) 5001 * SODIUM
 - B.1.1. Data File Changes
- B.2. ENDF/B Material Number (MAT) 5002 * MAGNESIUM
 - B.2.1. Data File Changes
- B.3. ENDF/B Material Number (MAT) 5004 * CHLORINE
 - B.3.1. Data File Changes
- B.4. ENDF/B Material Number (MAT) 5005 * POTASSIUM
 - B.4.1. Data File Changes
- B.5. ENDF/B Material Number (MAT) 5006 * CALCIUM
 - B.5.1. Data File Changes

B.1. ENDF/B Material Number (MAT) 5001 * SODIUM

B.1.1. Data File Changes

CARD(S) NUMBER: 695
CHANGE: Field 1: From 2.1710E+06 to 2.1713E+06
COMMENTS: Threshold altered to make consistent with Q value.

CARD(S) NUMBER: 814
CHANGE: Field 1: From 3.8390E+06 to 3.8395E+06
COMMENTS: Threshold....

CARD(S) NUMBER: 869
CHANGE: Field 1: From 4.6250E+06 to 4.6255E+06
COMMENTS: Threshold...

CARD(S) NUMBER: 913
CHANGE: Field 1: From 1.0950E+07 to 1.0959E+07
COMMENTS: Threshold...

CARD(S) NUMBER: 955
CHANGE: Field 2: From -0.620E+7 to -0.627E+7
COMMENTS: Consistency between Q values in File 3, photon energies in File 14, and level energies in File 15.

CARD(S) NUMBER: 966
CHANGE: Field 1: From 7.4220E+06 to 7.4221E+06
COMMENTS: Threshold...

CARD(S) NUMBER: 977
CHANGE: Field 2: From 0.0 to +6.959E+6
COMMENTS: Enter Q value for (n, γ) reaction in MF = 3, MT = 102. (Na is monoisotropic-- ^{23}Na).

CARD(S) NUMBER: 5370
CHANGE: Field 2: From 2.1700E+06 to 2.1713E+06
COMMENTS: Threshold...

CARD(S) NUMBER:	<u>5505</u>
CHANGE:	<u>Field 2: From $1.6400E+6$ to $1.6408E+6$</u>
COMMENTS:	<u>Consistency between Q values in File 3, photon energies in File i4, and level energies in File i5.</u>
CARD(S) NUMBER:	<u>5507</u>
CHANGE:	<u>Field 2: From $2.1700E+06$ to $2.1713E+06$</u>
COMMENTS:	<u>Threshold....</u>
CARD(S) NUMBER:	<u>5650, 5778</u>
CHANGE:	<u>Field 2: From $2.8230E+06$ to $2.8240E+06$</u>
COMMENTS:	<u>Threshold...</u>
CARD(S) NUMBER:	<u>5908, 6027</u>
CHANGE:	<u>Field 2: From $3.1140E+06$ to $3.1150E+06$</u>
COMMENTS:	<u>Threshold...</u>
CARD(S) NUMBER:	<u>6148, 6258, 6368, 6478</u>
CHANGE:	<u>Field 2: From $3.8380E+06$ to $3.8395E+06$</u>
COMMENTS:	<u>Threshold...</u>
CARD(S) NUMBER:	<u>6590, 6691</u>
CHANGE:	<u>Field 2: From $4.0170E+06$ to $4.0190E+06$</u>
COMMENTS:	<u>Threshold...</u>
CARD(S) NUMBER:	<u>6794, 6895, 7249, 7332</u>
CHANGE:	<u>Field 2: From $4.0850E+06$ to $4.0870E+06$</u>
COMMENTS:	<u>Threshold...</u>
CARD(S) NUMBER:	<u>7000, 7083, 7166</u>
CHANGE:	<u>Field 2: From $4.9860E+06$ to $4.9880E+06$</u>
COMMENTS:	<u>Threshold...</u>
CARD(S) NUMBER:	<u>7419, 7457, 7495, 7533</u>
CHANGE:	<u>Field 2: From $7.4220E+06$ to $7.4221E+06$</u>
COMMENTS:	<u>Threshold...</u>

CARD(S) NUMBER:	<u>7579</u>
CHANGE:	<u>Field 2: From 0.23 to 0.33</u>
COMMENTS:	<u>To correct error in Fig. 1 of Volume 2, (NDL-TR-89, Part II, GA-7829); transition probability array, 3rd level, as referenced in Fig. 1.</u>
CARD(S) NUMBER:	<u>7625</u>
CHANGE:	<u>Field 1: From 9.00E+6 to 9.05E+6</u>
COMMENTS:	<u>To agree with MF = 3, MT = 15 where cross section is essentially zero until 9.05 MeV.</u>
CARD(S) NUMBER:	<u>7839</u>
CHANGE:	<u>Field 2: From 1.6400E+6 to 1.6408E+6</u>
COMMENTS:	<u>Consistency....</u>
CARD(S) NUMBER:	<u>7851</u>
CHANGE:	<u>Field 2: From 1.9520E+6 to 1.9518E+6</u>
COMMENTS:	<u>Consistency....</u>
CARD(S) NUMBER:	<u>7863</u>
CHANGE:	<u>Field 2: From 2.2660E+6 to 2.2658E+6</u>
COMMENTS:	<u>Consistency....</u>
CARD(S) NUMBER:	<u>7881</u>
CHANGE:	<u>Field 2: From 2.5450E+6 to 2.5448E+6</u>
COMMENTS:	<u>Consistency....</u>
CARD(S) NUMBER:	<u>7893</u>
CHANGE:	<u>Field 2: From 3.2390E+6 to 3.2388E+6</u>
COMMENTS:	<u>Consistency....</u>
CARD(S) NUMBER:	<u>7929</u>
CHANGE:	<u>Field 2: From 3.4760E+6 to 3.4758E+6</u>
COMMENTS:	<u>Consistency....</u>
CARD(S) NUMBER:	<u>7947</u>
CHANGE:	<u>Field 2: From 4.3390E+6 to 4.3388E+6</u>
COMMENTS:	<u>Consistency....</u>

CARD(S) NUMBER: 797i
CHANGE: Field 2: From 3.8800E+6 to 3.8790E+6
COMMENTS: Consistency....

B.2. ENDF/B Material Number (MAT) 5002 * MAGNESIUM

B.2.1. Data File Changes

CARD(S) NUMBER:	<u>888, 1046</u>
CHANGE:	<u>Field 1: From $6.0760E+05$ to $6.0823E+05$</u>
COMMENTS:	<u>Threshold altered to make consistent with Q value.</u>
CARD(S) NUMBER:	<u>1099</u>
CHANGE:	<u>Field 1: From $1.0150E+06$ to $1.0165E+06$</u>
COMMENTS:	<u>Consistency between level energies (or Q values) in Files 3, 14, and 15.</u>
CARD(S) NUMBER:	<u>1144</u>
CHANGE:	<u>Field 2: From $-1.3678E+06$ to $-1.3680E+06$</u>
COMMENTS:	<u>Threshold....</u>
CARD(S) NUMBER:	<u>1229</u>
CHANGE:	<u>Field 1: From $1.6760E+6$ to $1.6779E+6$</u>
COMMENTS:	<u>Threshold....</u>
CARD(S) NUMBER:	<u>1265</u>
CHANGE:	<u>Field 1: From $1.8800E+6$ to $1.8851E+6$</u>
COMMENTS:	<u>Threshold....</u>
CARD(S) NUMBER:	<u>1297</u>
CHANGE:	<u>Field 1: From $2.0400E+6$ to $2.0434E+6$</u>
COMMENTS:	<u>Threshold....</u>
CARD(S) NUMBER:	<u>1326</u>
CHANGE:	<u>Field 1: From $2.6690E+6$ to $2.6715E+6$</u>
COMMENTS:	<u>Threshold....</u>
CARD(S) NUMBER:	<u>1345</u>
CHANGE:	<u>Field 1: From $2.8470E+6$ to $2.8496E+6$</u>
COMMENTS:	<u>Threshold....</u>
CARD(S) NUMBER:	<u>1361</u>
CHANGE:	<u>Field 1: From $2.9160E+6$ to $2.9193E+6$</u>
COMMENTS:	<u>Threshold....</u>

CARD(S) NUMBER: 1376
CHANGE: Field 1: From 3.0530E+6 to 3.0620E+6
COMMENTS: Threshold.....

CARD(S) NUMBER: 1450
CHANGE: Field 1: From 7.6200E+6 to 7.6279E+6
COMMENTS: Threshold.....

CARD(S) NUMBER: 1518
CHANGE: Field 2: From -4.23E+06 to -4.232E+06
COMMENTS: Consistency.....

CARD(S) NUMBER: 1564
CHANGE: Field 2: From -5.22E+06 to -5.224E+06
COMMENTS: Consistency.....

CARD(S) NUMBER: 1566
CHANGE: Field 1: From 5.4400E+6 to 5.4408E+6
COMMENTS: Threshold.....

CARD(S) NUMBER: 6686
CHANGE: Field 2: From 1.0150E+6 to 1.0165E+6
COMMENTS: Threshold.....

CARD(S) NUMBER: 6991
CHANGE: Field 2: From 1.6760E+6 to 1.6779E+6
COMMENTS: Threshold.....

CARD(S) NUMBER: 7058
CHANGE: Field 2: From 1.8800E+6 to 1.8851E+6
COMMENTS: Threshold.....

CARD(S) NUMBER: 7116
CHANGE: Field 2: From 2.0400E+6 to 2.0434E+6
COMMENTS: Threshold.....

CARD(S) NUMBER: 7165
CHANGE: Field 2: From 3.0530E+6 to 3.0620E+6
COMMENTS: Threshold.....

CARD(S) NUMBER:	7194
CHANGE:	Field 2: From <u>3.0530E+6</u> to <u>3.0620E+6</u>
COMMENTS:	Threshold....
CARD(S) NUMBER:	7223
CHANGE:	Field 2: From <u>2.735E+06</u> to <u>2.752E+06</u>
COMMENTS:	Consistency....
CARD(S) NUMBER:	7292
CHANGE:	Field 2: From <u>4.4080E+6</u> to <u>4.410E+6</u>
COMMENTS:	Threshold....
CARD(S) NUMBER:	7357
CHANGE:	Field 2: From <u>4.4080E+6</u> to <u>4.410E+6</u>
COMMENTS:	Threshold....
CARD(S) NUMBER:	7424
CHANGE:	Field 2: From <u>5.44000E+6</u> to <u>5.4408E+6</u>
COMMENTS:	Threshold....
CARD(S) NUMBER:	7471
CHANGE:	Field 2: From <u>4.6370E+06</u> to <u>4.6320E+06</u>
COMMENTS:	Consistency....
CARD(S) NUMBER:	7513
CHANGE:	Field 1: From <u>1.3676E+07</u> to <u>1.3680E+06</u>
COMMENTS:	Consistency....
CARD(S) NUMBER:	7530, 7534, 7538
CHANGE:	Field 2: From <u>1.0</u> to <u>0.0</u>
COMMENTS:	cf. Section 2.3.2. of text.
CARD(S) NUMBER:	7617
CHANGE:	Field 1: From <u>4.1203E+06</u> to <u>4.1260E+6</u>
COMMENTS:	Consistency....
CARD(S) NUMBER:	7618
CHANGE:	Field 1: From <u>1.3676E+06</u> to <u>1.3680E+6</u>
COMMENTS:	Consistency....

CARD(S) NUMBER: 7621
CHANGE: Field 1: From 4.2300E+06 to 4.2320E+06
COMMENTS: Consistency....

CARD(S) NUMBER: 7622
CHANGE: Field 1: From 1.3676E+06 to 1.3680E+06
COMMENTS: Consistency....

CARD(S) NUMBER: 7625
CHANGE: Field 1: From 5.2200E+06 to 5.2240E+06
COMMENTS: Consistency....

CARD(S) NUMBER: 7626
CHANGE: Field 1: From 1.3676E+06 to 1.3680E+06
COMMENTS: Consistency....

CARD(S) NUMBER: 7630
CHANGE: Field 1: From 4.2306E+06 to 4.2320E+6
Field 3: From 4.1203E+06 to 4.1200E+6
Field 5: From 1.3676E+06 to 1.3680E+6
COMMENTS: Consistency....

CARD(S) NUMBER: 7634
CHANGE: Field 1: From 4.2300E+06 to 4.2320E+06
Field 2: From 1.3676E+06 to 1.3680E+06
COMMENTS: Consistency....

CARD(S) NUMBER: 7778
CHANGE: Field 2: From 2.7350E+06 to 2.7520E+06
COMMENTS: Consistency....

CARD(S) NUMBER: 7806
CHANGE: Field 2: From 4.6370E+06 to 4.6320E+06
COMMENTS: Consistency....

CARD(S) NUMBER: 7813
CHANGE: Field 2: From 2.2100E+06 to 2.2080E+06
COMMENTS: Consistency....

CARD(S) NUMBER: 7818
CHANGE: Field 2: From 5.0700E+06 to 5.0720E+06
COMMENTS: Consistency....

B.3. ENDF/B Material Number (MAT) 5004 * CHLORINE

B.3.i. Data File Changes

CARD(S) NUMBER: 1278

CHANGE: Field 2: From -1.6630E+07 to -0.1265E+08

COMMENTS: Threshold altered to make consistent with Q Value.

CARD(S) NUMBER: 1302

CHANGE: Field 1: From 6.5500E+06 to 6.5512E+06

COMMENTS: Threshold...

CARD(S) NUMBER: 1329

CHANGE: Field 1: From 6.2720E+06 to -6.2736E+06

COMMENTS: Threshold...

CARD(S) NUMBER: 6451, 6452, 6453, 6454, 6455

CHANGE: Deleted.

COMMENTS: MF = 14, MT = 52, 53, 54 Combined and changed to MF = 14, MT = 110.

CARD(S) NUMBER: 6488

CHANGE: Field 1: From 0.0 to 1.22E+06

COMMENTS: Clerical Error.

CARD(S) NUMBER: Sections created using UK Data from RTN numbers 13052, 13053, 13054

COMMENTS: Excitation of first 3 levels of ³⁷Cl were entered in MT = 110 as photon production cross sections starting at E = 0.0. Other levels (MT = 5-14, 51) are for ³⁵Cl. (Cf. Sec. 2.2.1).

B.4. ENDF/B Material Number (MAT) 5005 * POTASSIUM

B.4.1. Data File Changes

CARD(S) NUMBER: 956

CHANGE: Field 1: From $2.5910E+06$ to $2.5912E+06$

COMMENTS: Threshold altered to be consistent with Q value

CARD(S) NUMBER: 1201

CHANGE: Field 1: From $6.3700E+06$ to $6.3702E+06$

COMMENTS: Threshold....

CARD(S) NUMBER: 5570

CHANGE: Field 2: From $3.0990E+06$ to $3.1000E+06$

COMMENTS: Threshold....

B.5. ENDF/B Material Number (MAT) 5006 * CALCIUM

B.5.1. Data File Changes

CARD(S) NUMBER: 1054
CHANGE: Field 1: From 1.18700E+06 to 1.1872E+06
COMMENTS: Threshold altered to make consistent with Q value.

CARD(S) NUMBER: 1134
CHANGE: Field 1: From 1.1870E+06 to 1.1872E+06
COMMENTS: Threshold....

CARD(S) NUMBER: 1162
CHANGE: Field 1: From 3.4300E+06 to 3.4344E+06
COMMENTS: Threshold....

CARD(S) NUMBER: 1236
CHANGE: Field 1: From 4.5900E+06 to 4.5928E+06
COMMENTS: Threshold....

CARD(S) NUMBER: 1250
CHANGE: Field 1: From 5.4000E+06 to 5.4027E+06
COMMENTS: Threshold...

CARD(S) NUMBER: 1262
CHANGE: Field 1: From 5.7600E+06 to 5.7615E+06
COMMENTS: Threshold...

CARD(S) NUMBER: 1292
CHANGE: Field 1: From 6.7200E+06 to 6.7251E+06
COMMENTS: Threshold...

CARD(S) NUMBER: 1313
CHANGE: Field 1: From 1.028E+07 to 1.0283E+07
COMMENTS: Threshold...

CARD(S) NUMBER: 1374
CHANGE: Field 1: From 8.2900E+06 to 8.2936E+06
COMMENTS: Threshold...

CARD(S) NUMBER: 1382
CHANGE: Field 1: From 8.5800E+06 to 8.5807E+06
COMMENTS: Threshold....

CARD(S) NUMBER: 5120
CHANGE: Field 2: From 3.8240E+06 to 3.8300E+06
COMMENTS: Threshold...

CARD(S) NUMBER: 5521
CHANGE: Field 2: From 5.4000E+06 to 5.4027E+06
COMMENTS: Threshold...

CARD(S) NUMBER: 5604
CHANGE: Field 2: From 5.4000E+06 to 5.4027E+06
COMMENTS: Threshold...

CARD(S) NUMBER: 5689
CHANGE: Field 2: From 5.7600E+06 to 5.7615E+06
COMMENTS: Threshold...

CARD(S) NUMBER: 5763
CHANGE: Field 6: From 8 to 7
COMMENTS: Clerical error

CARD(S) NUMBER: 5764
CHANGE: Field 1: From 8 to 7
COMMENTS: Clerical error.

CARD(S) NUMBER: 5973
CHANGE: Field 2: From 6.7200E+06 to 6.7251E+06
COMMENTS: Threshold

CARD(S) NUMBER: 6029
CHANGE: Field 2: From 6.7200E+06 to 6.7251E+06
COMMENTS: Threshold...

CARD(S) NUMBER: MF = 14 MT = 15
CHANGE: Added section
COMMENTS: Add isotropic distribution for photons, both discrete and continuum, from (n,p) reactions. Continuum photons from RTN 13015 (cf. section 2.2.3).

APPENDIX C: INDEX'ed Listing of PHOX

The following INDEX'ed listing of PHOX contains only the portions of the code which were written at the University of Virginia and does not include the standard ENDF/B retrieval subroutines distributed by the NNCSC. The INDEX'ed listing includes both the statement numbers and variable names.

C*****		PHX	1
C*		*PHX	2
C*	PHOX-A FORTRAN CODE TO CHECK PHOTON DATA IN ENDF/B DATA FILE	*PHX	3
C*	FORMAT	*PHX	4
C*		*PHX	5
C*	WRITTEN BY	*PHX	6
C*		*PHX	7
C*	JASON M. COOK	*PHX	8
C*	DEPARTMENT OF NUCLEAR ENGINEERING	*PHX	9
C*	UNIVERSITY OF VIRGINIA	*PHX	10
C*	THORNTON HALL	*PHX	11
C*	CHARLOTTESVILLE, VA. 22901	*PHX	12
C*	TELEPHONE 703-924-7136	*PHX	13
C*		*PHX	14
C*****		PHX	15
C		PHX	16
C		PHX	17
C	-----THE DATA, IN EITHER STANDARD BINARY ARRANGEMENT(MODE 1) OR BCD	PHX	18
C	CARD IMAGE FORM(MODE 3), IS ON INPUT TAPE NT(I/O UNIT NUMBER).	PHX	19
C		PHX	20
C	-----INPUT DATA, 2 CARDS	PHX	21
C		PHX	22
C	CARD 1--NT,MODE,MATW ENTERED IN (3I11) FORMAT	PHX	23
C	NT-I/O UNIT NUMBER	PHX	24
C	MODE-MODE ARRANGEMENT OF TAPE(EITHER 1 OR 3)	PHX	25
C	MATW-ENDF/B MATERIAL NUMBER OF MATERIAL BEING USED	PHX	26
C		PHX	27
C	CARD--2(ALL ALPHA FIELD) ENTERED IN (13A6,A2) FORMAT	PHX	28
C	THIS ALLOWS THE USER TO PLACE ANY HEADING HE DESIRES	PHX	29
C	ON THE OUTRUT LISTING.	PHX	30
C		PHX	31
C	-----ALL ERROR MESSAGES ARE PRINTED AFTER THE RECORD IN WHICH THE	PHX	32
C	ERROR IS DETECTED.	PHX	33
C		PHX	34
C	-----IN ORDER TO FACILITATE THE EASE OF READING THE RETRIVAL SUBROU-	PHX	35
C	TINES AND TO HELP UNDERSTAND THE LOGIC BEHIND THE PROGRAM, THE	PHX	36
C	FOLLOWING VARIABLES, ENDF/B RECORDS, HAVE BEEN DECLARED TO BE	PHX	37
1	INTEGER BCD,CONT,FEND,HEAD,HOL,SEND,TAB1,TAB2,TEND,TPID	PHX	38
C	LIST,MEND	PHX	39
C	AND HAVE BEEN ASSIGNED THE VALUES OF	PHX	40
2	BCD = 3	PHX	41
3	CONT = 1	PHX	42
4	FEND = 1	PHX	43
5	HEAD = 1	PHX	44
6	HOL = 5	PHX	45
7	LIST = 2	PHX	46
8	MEND = 1	PHX	47
9	SEND = 1	PHX	48
10	TAB1 = 3	PHX	49
11	TAB2 = 4	PHX	50

```

*****
12          TEND = 1                                PHX 51
13          TPID = 6                                PHX 52
          C                                         PHX 53
          C                                         PHX 54
14          DIMENSION A(14)                          PHX 55
15          COMMON/COUN/LG,NC,ND,NE,NI,NK,NP,NTAB,NS1  PHX 56
16          COMMON/RECS/MAT,MF,MT,C1,C2,L1,L2,N1,N2,NBT(100),JNT(100),X(2000),PHX 57
          1          Y(2000),B(2000),N1X,N2X,NS      PHX 58
17          N1X = 100                                PHX 59
18          N2X = 2000                                PHX 60
          C                                         PHX 61
          C-----READ INPUT.                       PHX 62
          C                                         PHX 63
19          READ (5,601,END=18) NT,MODE,MATW        PHX 64
20          READ (5,602,END=18) (A(I),I=1,14)       PHX 65
21          WRITE (6,603) (A(I),I=1,14)            PHX 66
          C                                         PHX 67
          C-----SEARCH FOR FILE 3.                PHX 68
          C                                         PHX 69
22          CALL SEARCH(NT,MODE,MATW,3,0,LNT)       PHX 70
23          BACKSPACE NT                             PHX 71
24          READ (NT,604) NS                          PHX 72
25          IF (LNT .EQ. 0) GO TO 2                  PHX 73
26          GO TO 19                                  PHX 74
          C                                         PHX 75
          C-----PROCESS FILE 3.                   PHX 76
          C                                         PHX 77
27          1 CALL RREC(HEAD,NT,MODE,-1.0)          PHX 78
28          2 CALL WREC(HEAD,6,BCD)                  PHX 79
29          IF (MF .EQ. 0) GO TO 3                   PHX 80
30          AWR = C2                                  PHX 81
31          CALL RREC(TAB1,NT,MODE,-1.0)            PHX 82
32          CALL WREC(TAB1,6,BCD)                    PHX 83
33          CALL FIL3(AWR)                            PHX 84
34          CALL RREC(SEND,NT,MODE,-1.0)            PHX 85
35          CALL WREC(SEND,6,BCD)                    PHX 86
36          GO TO 1                                   PHX 87
          C                                         PHX 88
          C-----SEARCH FOR FILE 14.               PHX 89
          C                                         PHX 90
37          3 CALL SEARCH(NT,MODE,MATW,14,0,LNT)    PHX 91
38          BACKSPACE NT                             PHX 92
39          READ (NT,604) NS                          PHX 93
40          IF (LNT .EQ. 0) GO TO 5                  PHX 94
41          GO TO 20                                  PHX 95
          C                                         PHX 96
          C-----PROCESS FILE 14.                   PHX 97
          C                                         PHX 98
42          4 CALL RREC(HEAD,NI,MODE,-1.0)          PHX 99
43          5 CALL WREC(HEAD,6,BCD)                  PHX 100

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44	IF (MF .EQ. 0) GO TO 12	PHX 101
45	CALL CKHD(MF)	PHX 102
46	CALL TEST2C(MT)	PHX 103
47	IF (L1 .EQ. 1) GO TO 8	PHX 104
48	IF (L2 .EQ. 1) GO TO 9	PHX 105
	C	PHX 106
	C TABULATED FORM	PHX 107
	C	PHX 108
49	NTA = ND + NC	PHX 109
50	DU 7 J = 1, NTA	PHX 110
51	CALL RREC(TAB2,NT,MODE,-1.0)	PHX 111
52	CALL WREC(TAB2,6,BCD)	PHX 112
53	CALL FIL14(1)	PHX 113
54	DU 6 I = 1, NE	PHX 114
55	CALL RREC(TAB1,NT,MODE,-1.0)	PHX 115
56	CALL WREC(TAB1,6,BCD)	PHX 116
57	6 CALL FIL14(2)	PHX 117
58	7 CALL FIL14(3)	PHX 118
59	8 CALL RREC(SEND,NT,MODE,-1.0)	PHX 119
60	CALL WREC(SEND,6,BCD)	PHX 120
61	GO TO 4	PHX 121
	C	PHX 122
	C LEGENDRE POLYNOMIAL FORM	PHX 123
	C	PHX 124
62	9 NTA = ND + NC	PHX 125
63	DU 11 J = 1, NTA	PHX 126
64	CALL RREC(TAB2,NT,MODE,-1.0)	PHX 127
65	CALL WREC(TAB2,6,BCD)	PHX 128
66	CALL FIL14(4)	PHX 129
67	DU 10 I = 1, NE	PHX 130
68	CALL RREC(LIST,NT,MODE,-1.0)	PHX 131
69	CALL WREC(LIST,6,BCD)	PHX 132
70	10 CALL FIL14(5)	PHX 133
71	11 CALL FIL14(6)	PHX 134
72	CALL RREC(SEND,NT,MODE,-1.0)	PHX 135
73	CALL WREC(SEND,6,BCD)	PHX 136
74	GO TO 4	PHX 137
	C	PHX 138
	C-----PROCESS FILE 15.	PHX 139
	C	PHX 140
75	12 CALL RREC(HEAD,NT,MODE,-1.0)	PHX 141
76	CALL WREC(HEAD,6,BCD)	PHX 142
77	IF (MF .EQ. 0) GO TO 17	PHX 143
78	CALL CKHD(MF)	PHX 144
79	IF (L1 .EQ. 2) GO TO 16	PHX 145
	C	PHX 146
	C OPTION 1	PHX 147
	C	PHX 148
80	CALL RREC(TAB1,NT,MODE,-1.0)	PHX 149
81	CALL WREC(TAB1,6,BCD)	PHX 150

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*****
82      CALL FIL15(1)                                PHX 151
83      DO 15 J = 1, NK                              PHX 152
84      CALL RREC(TAB1,NT,MODE,-1.0)                 PHX 153
85      CALL WREC(TAB1,6,BCD)                        PHX 154
86      IF (L2 .EQ. 2) GO TO 14                      PHX 155
      C                                             PHX 156
      C      ARBITRARY TABULATED FUNCTION            PHX 157
      C                                             PHX 158
87      CALL FIL15(2)                                PHX 159
88      CALL RREC(TAB2,NT,MODE,-1.0)                 PHX 160
89      CALL WREC(TAB2,6,BCD)                        PHX 161
90      CALL FIL15(3)                                PHX 162
91      DO 13 I = 1, NE                              PHX 163
92      CALL RREC(TAB1,NT,MODE,-1.0)                 PHX 164
93      CALL WREC(TAB1,6,BCD)                        PHX 165
94      13 CALL FIL15(4)                             PHX 166
95      CALL FIL15(5)                                PHX 167
96      GO TO 15                                     PHX 168
      C                                             PHX 169
      C      DISCRETE FINAL ENERGY                 PHX 170
      C                                             PHX 171
97      14 CALL FIL15(6)                             PHX 172
98      15 CONTINUE                                  PHX 173
99      CALL FIL15(7)                                PHX 174
100     CALL RREC(SEND,NT,MODE,-1.0)                 PHX 175
101     CALL WREC(SEND,6,BCD)                        PHX 176
102     GO TO 12                                     PHX 177
      C                                             PHX 178
      C      OPTION 2                               PHX 179
      C                                             PHX 180
103     16 CALL RREC(LIST,NT,MODE,-1.0)              PHX 181
104     CALL WREC(LIST,6,BCD)                        PHX 182
105     CALL FIL15(8)                                PHX 183
106     CALL RREC(SEND,NT,MODE,-1.0)                 PHX 184
107     CALL WREC(SEND,6,BCD)                        PHX 185
108     GO TO 12                                     PHX 186
109     17 CALL ESEGPR(5)                            PHX 187
110     STOP                                         PHX 188
111     18 WRITE (6,605)                             PHX 189
112     STOP                                         PHX 190
113     19 WRITE (6,606) NT,MODE,MATW                PHX 191
114     STOP                                         PHX 192
115     20 WRITE (6,607)                             PHX 193
116     STOP                                         PHX 194
117     601 FORMAT (3I11)                            PHX 195
118     602 FORMAT (13A6,A2)                          PHX 196
119     603 FORMAT (1X,13A6,A2//)                    PHX 197
120     604 FORMAT (75X,15)                          PHX 198
121     605 FORMAT (15(1H*),16H NO CARD INPUT. ,79(1H*)) PHX 199
122     606 FORMAT (15(1H*),19H FILE 3 NOT FOUND. ,6H NT = ,12,8H MODE = ,11,7PHX 200

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I N D E X

PAGE 5

123
124

1H MAT = ,14,51(1H*)
607 FQRMAT (1H1,14(1H*),20H FILE 14 NOT FOUND. ,75(1H*))
END

PHX 201
PHX 202
PHX 203-

SYMBOL	=	=	=	=	=	=	=	=	=	REFERENCES	=	=	=	=	=	=	=	=	=
1	-	27*	36																
2	-	25	28*																
3	-	29	37*																
4	-	42*	61	74															
5	-	40	43*																
6	-	54	57*																
7	-	50	58*																
8	-	47	59*																
9	-	48	62*																
10	-	07	70*																
11	-	03	71*																
12	-	44	75*	102	108														
13	-	91	94*																
14	-	06	97*																
15	-	03	96	98*															
16	-	79	103*																
17	-	77	109*																
18	-	111*																	
19	-	26	113*																
20	-	41	115*																
601	-	19RD	117*																
602	-	20RD	118*																
603	-	21WR	119*																
604	-	24RD	39RD	120*															
605	-	111WR	121*																
606	-	113WR	122*																
607	-	115WR	123*																
A	-	14DI	20RD	21WR															
AWR	-	30=	33AG																
B	-	16CD																	
BCD	-	11N	2=	28AG	32AG	35AG	43AG	52AG	56AG	60AG	65AG								
		09AG	73AG	76AG	81AG	85AG	89AG	93AG	101AG	104AG	107AG								
C1	-	16CD																	
C2	-	16CD	30																
CKHD	-	45	78																
CONT	-	11N	3=																
COUN	-	15CD																	
END	-	19RD	20RD																
ESEGPR	-	109																	
FEND	-	11N	4=																
FIL14	-	53	57	58	66	70	71												
FIL15	-	02	87	90	94	95	97	99	105										
FIL3	-	33																	
HEAD	-	11N	5=	27AG	28AG	42AG	43AG	75AG	76AG										
HOL	-	11N	6=																
I	-	20RD	21WR	54	67	91													
J	-	50	63	83															
JNT	-	16CD																	


```

*****
1      SUBROUTINE CKHD(FILE)                                CHD  1
2      COMMON/COUN/LG,NC,ND,NE,NI,NK,NP,NTAB,NS1           CHD  2
3      COMMON/RECS/MAT,MF,MT,C1,C2,L1,L2,N1,N2,NBT(100),JNT(100),X(2000),CHD  3
4      1      Y(2000),B(2000),N1X,N2X,NS                   CHD  4
5      IF (FILE .NE. 14) GO TO 4                           CHD  5
6      C-----CHECK FILE 14 HEAD CARD.                   CHD  6
7      C      CHECK L1.                                     CHD  7
8      C-----CHECK FILE 15 HEAD CARD.                   CHD  8
9      C      CHECK L1.                                     CHD  9
10     C      IF (L1.EQ.0 .OR. L1.EQ.1) GO TO 1             CHD 10
11     C      WRITE (6,601)                                  CHD 11
12     C      L1 = 0                                         CHD 12
13     C      CHECK LTT.                                     CHD 13
14     C      IF (L2.EQ.1 .OR. L2.EQ.2) GO TO 2             CHD 14
15     C      WRITE (6,602)                                  CHD 15
16     C      L2 = 2                                         CHD 16
17     C      CHECK ND.                                     CHD 17
18     C      CHECK ND.                                     CHD 18
19     C      2 IF (N1 .GT. (MT-4)) WRITE (6,603)           CHD 19
20     C      CHECK NC.                                     CHD 20
21     C      CHECK NC.                                     CHD 21
22     C      IF (N2.EQ.0 .OR. N2.EQ.1) GO TO 3             CHD 22
23     C      WRITE (6,604)                                  CHD 23
24     C      N2 = 1                                         CHD 24
25     C      3 ND = N1                                     CHD 25
26     C      NC = N2                                       CHD 26
27     C      RETURN                                         CHD 27
28     C      4 IF (FILE .NE. 15) GO TO 10                 CHD 28
29     C      CHECK LD.                                     CHD 29
30     C      CHECK LD.                                     CHD 30
31     C      IF (L1 .EQ. 2) GO TO 7                         CHD 31
32     C      IF (L1 .EQ. 1) GO TO 5                       CHD 32
33     C      WRITE (6,605)                                  CHD 33
34     C      L1 = 1                                         CHD 34
35     C      5 IF (L2 .NE. 0) WRITE (6,606)                CHD 35
36     C      CHECK ND.                                     CHD 36
37     C      CHECK ND.                                     CHD 37
38     C      IF (N1 .GT. (MT-4)) WRITE (6,603)             CHD 38
39     C      CHECK NK.                                     CHD 39
40     C      CHECK NK.                                     CHD 40
41     C      IF (N2 .GE. N1) GO TO 6                       CHD 41
42     C      WRITE (6,607)                                  CHD 42
43     C      WRITE (6,607)                                  CHD 43
44     C      WRITE (6,607)                                  CHD 44
45     C      WRITE (6,607)                                  CHD 45
46     C      WRITE (6,607)                                  CHD 46
47     C      WRITE (6,607)                                  CHD 47
48     C      WRITE (6,607)                                  CHD 48
49     C      WRITE (6,607)                                  CHD 49
50     C      WRITE (6,607)                                  CHD 50

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27	N2 = N1	CHD 51
28	6 ND = N1	CHD 52
29	NK = N2	CHD 53
30	RETURN	CHD 54
	C	CHD 55
	C CHECK LG.	CHD 56
	C	CHD 57
31	7 IF (L2.EQ.1 .OR. L2.EQ.2) GO TO 8	CHD 58
32	WRITE (6,608)	CHD 59
33	L2 = 3	CHD 60
	C	CHD 61
	C CHECK NS.	CHD 62
	C	CHD 63
34	8 IF (N1 .LE. (MT-4)) GO TO 9	CHD 64
35	WRITE (6,609)	CHD 65
36	NS1 = MT -4	CHD 66
37	9 IF (N2 .NE. 0) WRITE (6,610)	CHD 67
38	LG = L2	CHD 68
39	RETURN	CHD 69
40	10 WRITE (6,611)	CHD 70
41	RETURN	CHD 71
42	601 FORMAT (15(1H*), 46H LI NOT IN DEFINED RANGE. LI SET EQUAL TO 0. , 49(1H*))	CHD 72
43	602 FORMAT (15(1H*), 48H LTT NOT IN DEFINED RANGE. LTT SET EQUAL TO 2 , 47(1H*))	CHD 73
44	603 FORMAT (15(1H*), 84H ND LARGER THAN STATE LEVEL WILL ALLOW. WILL CONTINUE PROCESSING WITH ND AS GIVEN. , 11(1H*))	CHD 74
45	604 FORMAT (15(1H*), 46H NC NOT IN DEFINED RANGE. NC SET EQUAL TO 1. , 49(1H*))	CHD 75
46	605 FORMAT (15(1H*), 46H LD NOT IN DEFINED RANGE. LD SET EQUAL TO 1. , 49(1H*))	CHD 76
47	606 FORMAT (15(1H*), 27H FOURTH FIELD SHOULD BE 0. , 68(1H*))	CHD 77
48	607 FORMAT (15(1H*), 42H ND GREATER THAN NK. NK SET EQUAL TO ND. , 64(1H*))	CHD 78
49	608 FORMAT (15(1H*), 73H LG NOT IN DEFINED RANGE. PROCESSING OF THIS SECTION WILL BE ATTEMPTED. , 22(1H*))	CHD 79
50	609 FORMAT (15(1H*), 70H NS LARGER THAN STATE LEVEL WILL ALLOW. NS SET EQUAL TO STATE LEVEL. , 25(1H*))	CHD 80
51	610 FORMAT (15(1H*), 26H SIXTH FIELD SHOULD BE 0. , 69(1H*))	CHD 81
52	611 FORMAT (15(1H*), 36H HEAD CARD NOT PROCESSED DUE TO MF. , 59(1H*))	CHD 82
53	END	CHD 83
		CHD 84
		CHD 85
		CHD 86
		CHD 87
		CHD 88
		CHD 89
		CHD 90
		CHD 91-

SUBROUTINE CKHD(FILE)

SYMBOL	REFERENCES
1	5 8*
2	8 11*
3	12 15*
4	4 18*
5	20 23*
6	25 28*
7	19 31*
8	31 34*
9	34 37*
10	18 40*
601	6WR 42*
602	9WR 43*
603	11WR 24WR 44*
604	13WR 45*
605	21WR 46*
606	23WR 47*
607	26WR 48*
608	32WR 49*
609	35WR 50*
610	37WR 51*
611	40WR 52*
B	3CO
C1	3CO
C2	3CO
CKHD	1
COUN	2CO
FILE	1AG 4 18
JNT	3CO
L1	3CO 5 7= 19 20 22=
L2	3CO 8 10= 23 31 33= 38
LG	2CO 38=
MAT	3CO
MF	3CO
MT	3CO 11 24 34 36
N1	3CO 11 15 24 25 27 28 34
N1X	3CO
N2	3CO 12 14= 16 25 27= 29 37
N2X	3CO
NBT	3CO
NC	2CO 16=
ND	2CO 15= 28=
NE	2CO
NI	2CO
NK	2CO 29=
NP	2CO
NS	3CO
NS1	2CO 36=
NTAB	2CO

SUBROUTINE CKHD(FILE)

RECS - 300
RETURN - 17 30 39 41
X - 300
Y - 300

SUBROUTINE FIL3(AWR)

1	SUBROUTINE FIL3(AWR)	F 3	1
2	COMMON/RECS/MAT,MF,MT,C1,C2,L1,L2,N1,N2,NBT(100),JNT(100),X(2000),	F 3	2
	1 Y(2000),B(2000),N1X,N2X,NS	F 3	3
3	COMMON/SAVE/ETH(300),E(300),ETAB(2000),YTAB(2000),YKTAB(2000),	F 3	4
	1 YCAL(2000),YFIL(2000),EK(2000),YK(2000),ES(40)	F 3	5
	C	F 3	6
	C-----TEST Q.	F 3	7
	C	F 3	8
4	IF (MT.LE.4 .OR. (MT.GE.15 .AND. MT.LE.50) .OR. MT.GE.81) GO TO 1	F 3	9
5	IF (C2 .GE. 0.0) WRITE (6,601)	F 3	10
6	IF (ABS(C2).LT.1.0*10**4 .OR. ABS(C2).GT.2.0*10**7) WRITE (6,602)	F 3	11
7	1 IF (MT.NE.15 .AND. MT.NE.110) GO TO 2	F 3	12
8	IF (C2 .EQ. 0.0) GO TO 2	F 3	13
9	WRITE (6,603)	F 3	14
10	C2 = 0.0	F 3	15
11	2 IF (MT .NE. 102) GO TO 3	F 3	16
12	IF (C2 .LT. 0.0) WRITE (6,604)	F 3	17
13	IF (C2.NE.0 .AND. (C2.LT.1.7*10**6 .OR. C2.GT.1.2*10**7)) WRITE (6,	F 3	18
	1,605)	F 3	19
	C	F 3	20
	C-----CALCULATE AND TEST THRESHOLD.	F 3	21
	C	F 3	22
14	3 ETHEO = (AWR+1)*ABS(C2)/AWR	F 3	23
15	IF (C2 .GT. 0.0) ETHEO = 0.0	F 3	24
16	IF (ETHEO.GT.X(1) .AND. C2.LT.0.0) WRITE (6,606) ETHEO	F 3	25
	C	F 3	26
	C-----STORE Q AND THRESHOLD.	F 3	27
	C	F 3	28
17	Q(MT)=C2	F 3	29
18	ETH(MT) = X(1)	F 3	30
19	IF (ETHEO .GT. X(1)) ETH(MT) = ETHEO	F 3	31
	C	F 3	32
	C-----CALCULATE 2200 M/SEC CROSS SECTION, MT = 102.	F 3	33
	C	F 3	34
20	IF (MT .NE. 102) GO TO 8	F 3	35
21	K = 0	F 3	36
22	IF (X(1) .GT. 0.0253) GO TO 9	F 3	37
23	DO 4 I = 1, N2	F 3	38
24	K = K + 1	F 3	39
25	IF (X(I) .EQ. 0.0253) GO TO 5	F 3	40
26	4 IF (X(I).LT.0.0253 .AND. X(I+1).GT.0.0253) GO TO 6	F 3	41
27	5 WRITE (6,607) Y(K)	F 3	42
28	GO TO 8	F 3	43
29	6 DO 7 I = 1, N1	F 3	44
30	7 IF (K .LE. NBT(I)) INT = JNT(I)	F 3	45
31	ENG = 0.0253	F 3	46
32	CALL TERP1(X(K),Y(K),X(K+1),Y(K+1),ENG,SIGMA,INT)	F 3	47
33	WRITE (6,607) SIGMA	F 3	48
34	8 RETURN	F 3	49
35	9 WRITE (6,608)	F 3	50

SUBROUTINE FIL3(AWR)

36	RETURN	F 3	51
37	601 FORMAT (15(1H*),28H Q SHOULD BE LESS THAN 0.0. ,67(1H*))	F 3	52
38	602 FORMAT(15(1H*),46H Q SHOULD BE IN THE RANGE 1.0E+04 TO 2.0E+07. ,4F 3 19(1H*))	53	54
39	603 FORMAT (15(1H*),76H Q SHOULD BE EQUAL TO 0.0. Q SET EQUAL TO 0.0 F 3 1FOR REMAINDER OF PROCESSING. ,19(1H*))	55	56
40	604 FORMAT (15(1H*),43H Q SHOULD BE GREATER THAN OR EQUAL TO 0.0. ,52(F 3 11H*))	57	58
41	605 FORMAT (15(1H*),74H WHEN Q IS NOT EQUAL TO 0.0, Q SHOULD BE IN THE F 3 1 RANGE 1.7E+06 TO 1.2E+07. ,21(1H*))	59	60
42	606 FORMAT (15(1H*),65H EFFECTIVE THRESHOLD VALUE BELOW THEORETICAL ALF 3 1LOWED BY Q VALUE. ,30(1H*)/15(1H*),15H THEORETICAL = ,1PE12.5,38X,F 3 230(1H*))	61	62
43	607 FORMAT (81(1H*),15H SIGMA(2200) = ,1PE12.5,2H B)	F 3	64
44	608 FORMAT (81(1H*),29H SIGMA(2200) = DATA NOT GIVEN)	F 3	65
45	END	F 3	66-

SYMBOL	REFERENCES
1	4 7*
2	7 8 11*
3	11 14*
4	23 26*
5	25 27*
6	26 29*
7	29 30*
8	20 28 34*
9	22 35*
601	5WR 37*
602	6WR 38*
603	9WR 39*
604	12WR 40*
605	13WR 41*
606	16WR 42*
607	27WR 33WR 43*
608	35WR 44*
ABS	6 14
AWR	1AG 14
B	2CD
C1	2CD
C2	2CD 5 6 8 10= 12 13 14 15 16
EK	17 3CD
ENG	31= 32AG
ES	3CD
ETAB	3CD
ETH	3CD 18= 19=
ETHEO	14= 15= 16 19
FIL3	1
I	23 25 26 29 30
INT	30= 32AG
JNT	2CD 30
K	21= 24= 27WR 30 32AG
L1	2CD
L2	2CD
MAT	2CD
MF	2CD
MT	2CD 4 7 11 17 18 19 20
N1	2CD 29
N1X	2CD
N2	2CD 23
N2X	2CD
NBT	2CD 30
NS	2CD
Q	3CD 17=
RECS	2CD
RETURN	34 36

SAVE	-	3C0							
SIGMA	-	32AG	33WR						
TERP1	-	32							
X	-	2C0	16	18	19	22	25	26	32AG
Y	-	2C0	27WR	32AG					
YCAL	-	3C0							
YK	-	3C0							
YKTAB	-	3C0							
YTAB	-	3C0							
YFIL	-	3C0							

1	SUBROUTINE FIL14(N)	F14	1
2	COMMON/COUN/LG,NC,ND,NE,N1,NK,NP,NTAB,NS1	F14	2
3	COMMON/RECS/MAT,MF,MT,C1,C2,L1,L2,N1,N2,NBT(100),JNT(100),X(2000),	F14	3
	1 Y(2000),B(2000),N1X,N2X,NS	F14	4
4	COMMON/SAVE/ETH(300),B(300),ETAB(2000),YTAB(2000),YKTAB(2000),	F14	5
	1 YCAL(2000),YTIL(2000),EK(2000),YK(2000),ES(40)	F14	6
5	COMMON/SAV14/EG,EN,ESI,IL,IN	F14	7
6	GO TO (1,6,9,1,10,9), N	F14	8
	C	F14	9
	C-----TEST TAR2 RECORD.	F14	10
	C	F14	11
7	1 NE = N2	F14	12
8	CALL ESEGPR(1)	F14	13
9	IF ((MT.GE.5 .AND. MT.LE.14) .OR. (MT.GE.51 .AND. MT.LE.80)) GO TO	F14	14
	1 2	F14	15
	C	F14	16
	C- MT IN RANGE 1-4, 15-50, 81-UP	F14	17
	C TEST ES AND EGI.	F14	18
	C	F14	19
10	IF (C2 .LT. 0.0) WRITE (6,601)	F14	20
11	IF (C1 .LT. 0.0) WRITE (6,602)	F14	21
12	IF (C1.NE.0.0 .AND. C2.GT.C1) WRITE (6,603)	F14	22
	C	F14	23
	C TEST FOR CONTINUOUS SPECTRUM.	F14	24
	C	F14	25
13	EG = 1.0	F14	26
14	IF (MT .EQ. 110) GO TO 5	F14	27
15	IF (C1.NE.0.0 .OR. C2.NE.0.0) GO TO 5	F14	28
16	IL = JL + 1	F14	29
17	IF (IL.EQ.1 .AND. NC.NE.1) WRITE (6,604)	F14	30
18	IF (JL .GT. 1) WRITE (6,605)	F14	31
19	GO TO 5	F14	32
	C	F14	33
	C MT IN RANGE 5-14, 51-80	F14	34
	C TEST ES AND EGI.	F14	35
	C	F14	36
20	2 IF (C2 .GE. 0.0) GO TO 3	F14	37
21	WRITE (6,601)	F14	38
22	IF (C1 .LT. 0.0) WRITE (6,602)	F14	39
23	3 IF (C1 .LT. C2) WRITE (6,603)	F14	40
24	IF (C1 .NE. ABS(Q(MT))) WRITE (6,606)	F14	41
	C	F14	42
	C TEST ORDER OF ES AND EGI.	F14	43
	C	F14	44
25	IN = IN + 1	F14	45
26	IF (IN .GT. 1) GO TO 4	F14	46
27	ESI = C1	F14	47
28	EG = C2	F14	48
29	GO TO 5	F14	49
30	4 IF (C1 .NE. ESI) WRITE (6,607)	F14	50

	IF (C2 .GE. EG) WRITE (6,608)	F14	51
	EG = C2	F14	52
C		F14	53
C	CHECK INTERPOLATION SCHEME	F14	54
C		F14	55
	5 IF (N2 .LE. N1) WRITE (6,609)	F14	56
	IF (N1.NE.1 .OR. JNT(1).NE.2) WRITE (6,610)	F14	57
	RETURN	F14	58
C		F14	59
C	-----TEST TAB1 RECORD.	F14	60
C	TABULATED FORM	F14	61
C		F14	62
	6 IF (N1.NE.1 .OR. JNT(1).NE.2) WRITE (6,611)	F14	63
	IF (ETH(MT) .GT. C2) WRITE (6,612) ETH(MT)	F14	64
	IF (C2 .LE. EN) WRITE (6,613)	F14	65
	EN = C2	F14	66
	DO 7 I = 1, N2	F14	67
	7 IF (Y(I).LT.0.499 .OR. Y(I).GT.0.501) GO TO 8	F14	68
	IF (N2 .NE. 2) WRITE (6,614)	F14	69
	8 RETURN	F14	70
C		F14	71
C	-----RE-INITIALIZE.	F14	72
C		F14	73
	9 IF (NC.EQ.1 .AND. IL.EQ.0) WRITE (6,615)	F14	74
	IF (EG.EQ.0.0 .AND. IL.EQ.0) WRITE (6,616)	F14	75
	IF ((MT.GE.5 .AND. MT.LE.14) .OR. (MT.GE.51 .AND. MT.LE.80)) .AND	F14	76
	1. NC.EQ.1) WRITE (6,617)	F14	77
	EG = 0.0	F14	78
	EN = 0.0	F14	79
	ESI = 0.0	F14	80
	IL = 0	F14	81
	IN = 0	F14	82
	RETURN	F14	83
C		F14	84
C	-----TEST TAB1 RECORD.	F14	85
C	LEGENDRE POLYNOMIAL FORM	F14	86
C		F14	87
	10 IF (ETH(MT) .GT. C2) WRITE (6,612) ETH(MT)	F14	88
	IF (C2 .LE. EN) WRITE (6,613)	F14	89
	EN = C2	F14	90
	RETURN	F14	91
	601 FORMAT (15(1H*),45H EGI SHOULD BE GREATER THAN OR EQUAL TO 0.0. ,5F14	F14	92
	10(1H*))	F14	93
	602 FORMAT (15(1H*),44H ES SHOULD BE GREATER THAN OR EQUAL TO 0.0. ,51F14	F14	94
	1(1H*))	F14	95
	603 FORMAT (15(1H*),44H ES SHOULD BE GREATER THAN OR EQUAL TO EGI. ,51F14	F14	96
	1(1H*))	F14	97
	604 FORMAT (15(1H*),45H FOR A CONTINUOUS SPECTRUM, NC MUST EQUAL 1. ,5F14	F14	98
	10(1H*))	F14	99
	605 FORMAT (15(1H*),49H ONLY 1 CONTINUOUS SPECTRUM PER SECTION ALLOWEDF14	F14	100

	1. ,46(1H*))	F14 101
62	606 FORMAT (15(1H*),48H ES SHOULD BE EQUAL TO THE ABSOLUTE VALUE OF Q. ,47(1H*))	F14 102
	1 ,47(1H*))	F14 103
63	607 FORMAT (15(1H*),25H ALL ES SHOULD BE EQUAL. ,73(1H*))	F14 104
64	608 FORMAT (15(1H*),33H EGI MUST BE IN DECENDING ORDER. ,62(1H*))	F14 105
65	609 FORMAT (15(1H*),29H NP MUST BE GREATER THAN NR. ,65(1H*))	F14 106
66	610 FORMAT (15(1H*),72H INTERPOLATION SCHEME IS REQUIRED TO BE LINEAR THROUGHOUT ENTIRE RANGE. ,23(1H*))	F14 107
	1 THROUGHOUT ENTIRE RANGE. ,23(1H*))	F14 108
67	611 FORMAT (15(1H*),64H INTERPOLATION SCHEME SHOULD BE LINEAR THROUGHOUT ENTIRE RANGE. ,31(1H*))	F14 109
	1 ENTIRE RANGE. ,31(1H*))	F14 110
68	612 FORMAT (15(1H*),68H INCIDENT NEUTRON ENERGY LESS THAN EFFECTIVE THRESHOLD IN FILE 3(= ,1PE12.5,3H). ,12(1H*))	F14 111
	1 THRESHOLD IN FILE 3(= ,1PE12.5,3H). ,12(1H*))	F14 112
69	613 FORMAT (15(1H*),55H INCIDENT NEUTRON ENERGIES MUST BE IN ASCENDING ORDER. ,40(1H*))	F14 113
	1 ORDER. ,40(1H*))	F14 114
70	614 FORMAT (15(1H*),47H DISTRIBUTION SHOULD BE ENTERED ISOTROPICALLY. ,48(1H*))	F14 115
	1 ,48(1H*))	F14 116
71	615 FORMAT (15(1H*),54H FOR NC EQUAL 1, THERE MUST BE A CONTINUOUS SPECTRUM. ,41(1H*))	F14 117
	1 CTUM. ,41(1H*))	F14 118
72	616 FORMAT (15(1H*),37H FOR EGI EQUAL TO 0.0, NC MUST BE 1. ,58(1H*))	F14 119
73	617 FORMAT (15(1H*),54H THERE CAN BE NO CONTINUOUS SPECTRUM IN THIS SECTION. ,41(1H*))	F14 120
	1 CTION. ,41(1H*))	F14 121
74	END	F14 122-

SYMBOL	REFERENCES
1	6 7*
2	9 20*
3	20 23*
4	26 30*
5	14 15 19 89 33*
6	6 36*
7	40 41*
8	41 43*
9	6 44*
10	6 53*
601	10WR 21WR 57*
602	11WR 22WR 58*
603	12WR 23WR 59*
604	17WR 60*
605	18WR 61*
606	24WR 62*
607	30WR 63*
608	31WR 64*
609	33WR 65*
610	34WR 66*
611	36WR 67*
612	37WR 53WR 68*
613	38WR 54WR 69*
614	42WR 70*
615	44WR 71*
616	45WR 72*
617	46WR 73*
ABS	24
B	3C0
C1	3C0 11 12 15 22 23 24 27 30
C2	3C0 10 12 15 20 23 28 31 32 37
	38 39 53 54 55
CDUN	2C0
EG	5C0 13= 28= 31 32= 45 47=
EK	4C0
EN	5C0 38 39= 48= 54 55=
ES	4C0
ESEGPR	8
ESI	5C0 27= 30 49=
ETAB	4C0
ETH	4C0 37 53
FIL14	1
I	40 41
IL	5C0 16= 17 18 44 45 50=
IN	5C0 25= 26 51=
JNT	3C0 34 36
L1	3C0
L2	3C0

SUBROUTINE FIL14(N)

LG	-	2C0					
MAT	-	3C0					
MF	-	3C0					
MT	-	3C0	9	14	24	37	46 53
N	-	1AG	6				
N1	-	3C0	33	34	36		
N1X	-	3C0					
N2	-	3C0	7	33	40	42	
N2X	-	3C0					
NBT	-	3C0					
NC	-	2C0	17	44	46		
ND	-	2C0					
NE	-	2C0	7=				
NI	-	2C0					
NK	-	2C0					
NP	-	2C0					
NS	-	3C0					
NS1	-	2C0					
NTAB	-	2C0					
Q	-	4C0	24				
RECS	-	3C0					
RETURN	-	35	43	52	56		
SAV14	-	5C0					
SAVE	-	4C0					
X	-	3C0					
Y	-	3C0	41				
YCAL	-	4C0					
YK	-	4C0					
YKTAB	-	4C0					
YTAB	-	4C0					
YFIL	-	4C0					

1	SUBROUTINE FIL15(N)	F15	1
2	COMMON/COUN/LG,NC,ND,NE,NI,NK,NP,NTAB,NS1	F15	2
3	COMMON/RECS/MAT,MF,MT,C1,C2,L1,L2,N1,N2,NBT(100),JNT(100),X(2000),	F15	3
	1 Y(2000),B(2000),N1X,N2X,NS	F15	4
4	COMMON/SAVE/ETH(300),Q(300),ETAB(2000),YTAB(2000),YKTAB(2000),	F15	5
	1 YCAL(2000),YFIL(2000),EK(2000),YK(2000),ES(40)	F15	6
5	COMMON/SAV15/A(2000)	F15	7
6	GO TO (1,3,10,11,13,19,26,29), N	F15	8
	C	F15	9
	C-----STORE TABULATED ENERGIES AND YIELDS.	F15	10
	C	F15	11
7	1 DO 2 I = 1, N2	F15	12
8	ETAB(I) = X(I)	F15	13
9	2 YTAB(I) = Y(I)	F15	14
10	NTAB = N2	F15	15
11	IF (ETAB(1) .LT. ETH(MT)) WRITE (6,601) ETH(MT)	F15	16
12	RETURN	F15	17
	C	F15	18
	C-----LF = 1	F15	19
	C STORE SECTION ENERGIES AND YIELD.	F15	20
	C	F15	21
13	3 DO 4 I = 1, N2	F15	22
14	EK(I) = X(I)	F15	23
15	4 YK(I) = Y(I)	F15	24
16	NP = N2	F15	25
	C	F15	26
	C TEST ENERGIES.	F15	27
	C	F15	28
17	IF (EK(1) .LT. ETH(MT)) WRITE (6,601) ETH(MT)	F15	29
18	IF (EK(1).LT.ETAB(1) .OR. EK(NP).GT.ETAB(NTAB)) WRITE (6,602)	F15	30
19	CALL ESEGPR(2)	F15	31
	C	F15	32
	C CALCULATE SECTION YIELDS FOR TABULATED ENERGIES.	F15	33
	C	F15	34
20	DO 9 I = 1, NTAB	F15	35
21	L = N2 - 1	F15	36
22	K = 0	F15	37
23	DO 5 J = 1, L	F15	38
24	K = K + 1	F15	39
25	IF (EK(J) .EQ. ETAB(I)) GO TO 6	F15	40
26	5 IF (EK(J).LT.ETAB(I) .AND. EK(J+1).GT.ETAB(I)) GO TO 7	F15	41
27	K = K + 1	F15	42
28	IF (EK(N2) .EQ. ETAB(I)) GO TO 6	F15	43
29	GO TO 9	F15	44
30	6 YNTAB(I) = YK(K)	F15	45
31	GO TO 9	F15	46
32	7 DO 8 J = 1, N1	F15	47
33	8 IF (K .LE. NBT(J)) INT = JNT(J)	F15	48
34	CALL TERP1(EK(K),YK(K),EK(K+1),YK(K+1),ETAB(I),YKTAB(I),INT)	F15	49
35	9 YCAL(I) = YCAL(I) + YKTAB(I)	F15	50

36	RETURN	F15 51
	C	F15 52
	C-----TEST TAB2 RECURD.	F15 53
	C	F15 54
37	10 NE = N2	F15 55
38	IF (NE .NE. NP) WRITE (6,603)	F15 56
39	IF (N1.NE.1 .OR. JNT(1).NE.2) WRITE (6,604)	F15 57
40	RETURN	F15 58
	C	F15 59
	C CALCULATE TOTAL YIELD.	F15 60
	C	F15 61
41	11 NI = NI + 1	F15 62
	C	F15 63
	C TEST ENERGIES.	F15 64
	C	F15 65
42	IF (C2 .LT. ETH(MT)) WRITE (6,605) ETH(MT)	F15 66
43	IF (C2 .LT. EK(NI)) WRITE (6,606)	F15 67
44	L = N2 - 1	F15 68
	C	F15 69
	C INTEGRATE PHOTON YIELD PROBABILITIES.	F15 70
	C	F15 71
45	DO 12 I = 1, L	F15 72
46	A1 = A1 + (X(I+1)-X(I))*(Y(I+1)+Y(I))/2.0	F15 73
47	12 A2 = A2 + (X(I+1)-X(I))*(X(I+1)*Y(I+1)+X(I)*Y(I))/2.0	F15 74
48	IF (ABS(A1-1.0000) .GT. 0.0001) WRITE (6,607) A1	F15 75
49	A(NI) = A2/A1	F15 76
50	A2 = 0.0	F15 77
51	A1 = 0.0	F15 78
52	RETURN	F15 79
53	13 DO 18 I = 1, NTAB	F15 80
54	L = N2 - 1	F15 81
55	K = 0	F15 82
56	DO 14 J = 1, L	F15 83
57	K = K + 1	F15 84
58	IF (EK(J) .EQ. ETAB(I)) GO TO 15	F15 85
59	14 IF (EK(J).LT.ETAB(I) .AND. EK(J+1).GT.ETAB(I)) GO TO 16	F15 86
60	K = K + 1	F15 87
61	IF (EK(N2) .EQ. ETAB(I)) GO TO 15	F15 88
62	GO TO 17	F15 89
63	15 A3 = A(K)	F15 90
64	GO TO 17	F15 91
65	16 CALL TERP1(EK(K),A(K),EK(K+1),A(K+1),ETAB(I),A3,2)	F15 92
66	17 YTIL(J) = YTIL(I) + YKTAB(I)*A3	F15 93
67	18 A3 = 0.0	F15 94
68	RETURN	F15 95
	C	F15 96
	C-----LF = 2	F15 97
	C TEST ENERGIES.	F15 98
	C	F15 99
69	19 IF (X(1) .LT. ETH(MT)) WRITE (6,601) ETH(MT)	F15 100

70	IF (X(1).LT.ETAB(1) .OR. X(N2).GT.ETAB(NTAB)) WRITE (6,602)	F15 101
71	CALL ESEGPR(2)	F15 102
	C	F15 103
	C CALCULATE SECTION YIELDS FOR TABULATED ENERGIES.	F15 104
	C	F15 105
72	DO 25 I = 1, NTAB	F15 106
73	L = N2 - 1	F15 107
74	K = 0	F15 108
75	DO 20 J = 1, L	F15 109
76	K = K + 1	F15 110
77	IF (X(J) .EQ. ETAB(I)) GO TO 21	F15 111
78	20 IF (X(J).LT.ETAB(I) .AND. X(J+1).GT.ETAB(I)) GO TO 22	F15 112
79	K = K + 1	F15 113
80	IF (X(N2) .EQ. ETAB(I)) GO TO 21	F15 114
81	GO TO 24	F15 115
82	21 YNTAB(I) = Y(K)	F15 116
83	GO TO 24	F15 117
84	22 DO 23 J = 1, N1	F15 118
85	23 IF (K .LE. NB1(J)) INT = JNT(J)	F15 119
86	CALL TERP1(X(K),Y(K),X(K+1),Y(K+1),ETAB(I),YKTAB(I),INT)	F15 120
	C	F15 121
	C CALCULATE TOTAL YIELD.	F15 122
	C	F15 123
87	24 YCAL(I) = YCAL(I) + YKTAB(I)	F15 124
88	25 YTIL(I) = YTIL(I) + YNTAB(I)*C2	F15 125
89	RETURN	F15 126
	C	F15 127
	C-----TEST TOTAL YIELD.	F15 128
	C	F15 129
90	26 DO 27 I = 1, NTAB	F15 130
91	YDIFF = (YTAB(I) - YCAL(I))/YCAL(I)	F15 131
92	IF (ABS(YDIFF) .GT. 0.0001) WRITE (6,608) YTAB(I),YCAL(I),ETAB(I)	F15 132
93	IF ((MT.GE.5 .AND. MT.LE.14) .OR. (MT.GE.51 .AND. MT.LE.80)) .AND.F15 133	
	1. YTIL(I).GT.ABS(Q(MT))) WRITE (6,609) YTIL(I),Q(MT),ETAB(I)	F15 134
94	27 IF ((MT.LE.4 .OR.(MT.GE.15 .AND. MT.LE.50) .OR. MT.GE.81) .AND. YTF15 135	
	1IL(I).GT.(Q(MT)+ETAB(I))) WRITE (6,610) YTIL(I),ETAB(I)	F15 136
	C	F15 137
	C-----RE-INITIALIZE.	F15 138
	C	F15 139
95	DO 28 I = 1, 2000	F15 140
96	A(I) = 0.0	F15 141
97	ETAB(I) = 0.0	F15 142
98	EK(I) = 0.0	F15 143
99	YTAB(I) = 0.0	F15 144
100	YCAL(I) = 0.0	F15 145
101	YNTAB(I) = 0.0	F15 146
102	YN(I) = 0.0	F15 147
103	28 YTIL(I) = 0.0	F15 148
104	NI = 0	F15 149
105	RETURN	F15 150

	C		F15 151
	C	-----TEST LG.	F15 152
	C		F15 153
106		29 GO TO (30,34,39), LG	F15 154
	C		F15 155
	C	-----OPTION 1	F15 156
	C	CHECK 2NT = 2 * NT	F15 157
	C		F15 158
107		30 IF (N1 .EQ. (2*N2)) GO TO 31	F15 159
108		WRITE (6,611)	F15 160
109		N1 = 2 * N2	F15 161
	C		F15 162
	C	TEST ENERGIES.	F15 163
	C		F15 164
110		31 IF (B(1) .GE. C1) WRITE (6,612)	F15 165
111		IF (C1 .LT. ABS(Q(MT))) WRITE (6,613)	F15 166
112		DU 32 I = 3, N1, 2	F15 167
113		32 IF (B(I) .GE. B(I-2) .AND. N1.NE.2) WRITE (6,614) B(I)	F15 168
114		CALL STATE(LG)	F15 169
115		CALL ESEGPR(3)	F15 170
	C		F15 171
	C	TEST TP ARRAYS.	F15 172
	C		F15 173
116		DU 33 I = 2, N1, 2	F15 174
117		IF (B(I) .LE. 0.0) WRITE (6,615) B(I-1)	F15 175
118		IF (B(I) .GT. 1.0) WRITE (6,616) B(I-1)	F15 176
119		33 TP = TP + B(I)	F15 177
120		IF (TP .LE. 0.9999) WRITE (6,617) TP	F15 178
121		IF (TP .GT. 1.0001) WRITE (6,618) TP	F15 179
122		TP = 0.0	F15 180
123		RETURN	F15 181
	C		F15 182
	C	-----OPTION 2	F15 183
	C	CHECK 3NT = 3 * NT	F15 184
	C		F15 185
124		34 IF (N1 .EQ. (3*N2)) GO TO 35	F15 186
125		WRITE (6,611)	F15 187
126		N1 = 3 * N2	F15 188
	C		F15 189
	C	TEST ENERGIES.	F15 190
	C		F15 191
127		35 IF (B(1) .GE. C1) WRITE (6,612)	F15 192
128		IF (C1 .LT. ABS(Q(MT))) WRITE (6,613)	F15 193
129		DU 36 I = 4, N1, 3	F15 194
130		36 IF (B(I) .GE. B(I-3) .AND. N1.NE.3) WRITE (6,614) B(I)	F15 195
131		CALL STATE(LG)	F15 196
132		CALL ESEGPR(4)	F15 197
	C		F15 198
	C	TEST TP ARRAYS.	F15 199
	C		F15 200

SUBROUTINE FIL15(N)

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133      DO 37 I = 2, N1, 3                                F15 201
134      IF (B(I) .LE. 0.0) WRITE (6,615) B(I-1)          F15 202
135      IF (B(I) .GT. 1.0) WRITE (6,616) B(I-1)          F15 203
136      37 TH = TP + B(I)                                  F15 204
137      IF (TP .LE. 0.9999) WRITE (6,617) TP            F15 205
138      IF (TP .GT. 1.0001) WRITE (6,618) TP            F15 206
139      TP = 0.0                                           F15 207
C                                               F15 208
C      TEST GP ARRAYS.                                     F15 209
C                                               F15 210
140      DO 38 I = 3, N1, 3                                F15 211
141      IF (B(I) .LE. 0.0) WRITE (6,619) B(I-2)          F15 212
142      38 IF (B(I) .GT. 1.0) WRITE (6,620) B(I-2)      F15 213
143      RETURN                                             F15 214
C                                               F15 215
C-----TRY TO DETERMINE LG, IF NOT 1 OR 2.             F15 216
C                                               F15 217
144      39 RATIO = FLOAT(N1)/FLOAT(N2)                   F15 218
145      IF (RATIO .GE. 2.5000) GO TO 34                   F15 219
146      GO TO 30                                           F15 220
147      601 FORMAT (15(1H*),57H FIRST ENERGY LESS THAN EFFECTIVE THRESHOLD INF15 221
148      1 FILE 3( = ,1PE12.5,3H). ,23(1H*))              F15 222
149      602 FORMAT (15(1H*),87H SUB-SECTION YIELD ENERGY RANGE EXCEEDS (BELOW F15 223
150      1AND/OR ABOVE.) TOTAL YIELD ENERGY RANGE. ,8(1H*)) F15 224
151      603 FORMAT (15(1H*),48H NE NOT EQUAL TO NP. NE ASSUMED TO BE CORRECT.F15 225
152      1,47(1H*))                                         F15 226
153      604 FORMAT (15(1H*),64H INTERPOLATION SCHEME SHOULD BE LINEAR THROUGHOF15 227
154      1UT ENTIRE RANGE. ,31(1H*))                       F15 228
155      605 FORMAT (15(1H*),69H INCIDENT NEUTRON ENERGY LESS THAN EFFECTIVE THF15 229
156      1RESHOLD IN FILE 3( = ,1PE12.5,3H). 11(1H*))     F15 230
157      606 FURMAT (15(1H*),72H INCIDENT NEUTRON ENERGY NOT EQUAL TO CORRESPONF15 231
158      1DING TOTAL YIELD ENERGY. ,18(1H*)/15(1H*),20H TOTAL YIELD ENERGY ,F15 232
159      217HASSUMED CORRECT. , 40X,18(1H*))              F15 233
160      607 FURMAT (15(1H*),49H THE INTEGRAL OF THE PHOTON YIELD PROBABILITY (F15 234
161      1= ,F11,7,18H) NOT NORMALIZED. ,17(1H*))         F15 235
162      608 FURMAT (15(1H*),69H TABULATED TOTAL YIELD NOT EQUAL TO TOTAL OF THF15 236
163      1E SUR-SECTION YIELDS. ,26(1H*)/15(1H*),25H TABULATED TOTAL YIELD =F15 237
164      2 ,1PE11.4,33X,26(1H*)/15(1H*),26H CALCULATED TOTAL YIELD = ,1PE11.F15 238
165      34,32X,26(1H*)/15(1H*),10H ENERGY = ,1PE11.4,48X,26(1H*)) F15 239
166      609 FURMAT (15(1H*),50H TOTAL MEV/INTERACTION EXCEEDS THAT ALLOWED BY F15 240
167      1Q. ,45(1H*)/15(1H*), 19H MEV/INTERACTION = ,1PE11.4,20X,45(1H*)/15F15 241
168      2(1H*),5H R = ,1PE11.4,34X,45(1H*)/15(1H*),10H ENERGY = ,1PE11.4,29F15 242
169      3X,45(1H*))                                       F15 243
170      610 FURMAT (15(1H*),80H TOTAL MEV/INTERACTION EXCEEDS THAT ALLOWED BY F15 244
171      1Q + E (INCIDENT NEUTRON ENERGY). ,15(1H*)/15(1H*),19H MEV/INTERACTF15 245
172      2IDN = ,1PE11.4,50X,15(1H*)/15(1H*),10H ENERGY = ,1PE11.4,59X,15(1HF15 246
173      3*))                                              F15 247
174      611 FURMAT (15(1H*),52H FIFTH AND SIXTH FIELDS OF FIRST CARD DO NOT AGF15 248
175      1REE. ,43(1H*))                                    F15 249
176      612 FURMAT (15(1H*),26H ES(1) NOT EQUAL TO ESNS. ,69(1H*)) F15 250

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SUBROUTINE FIL15(N)

159	613	FORMAT (15(1H*),26H ES SHOULD BE EQUAL TO 0. ,69(1H*))	F15 251
160	614	FORMAT (15(1H*),27H ESI OUT OF ORDER AT ESI = ,1PE11.4,3H . ,54(1H* 1*))	F15 252 F15 253
161	615	FORMAT (15(1H*),40H TRI LESS THAN OR EQUAL TO 0.0 AT ESI = ,1PE11.4,3H . ,41(1H*))	F15 254 F15 255
162	616	FORMAT (15(1H*),31H TPI GREATER THAN 1.0 AT ESI = ,1PE11.4,3H . ,5F15 10(1H*))	F15 256 F15 257
163	617	FORMAT (15(1H*),28H TOTAL TP LESS THAN 0.9999. ,67(1H*)/15(1H*),6HF15 1 TP = ,E12.5,10X,67(1H*))	F15 258 F15 259
164	618	FORMAT (15(1H*),31H TOTAL TP GREATER THAN 1.0001. ,64(1H*)/15(1H*) 1,6H TP = ,1PE12.5,13X,64(1H*))	F15 260 F15 261
165	619	FORMAT (15(1H*),40H GPI LESS THAN OR EQUAL TO 0.0 AT ESI = ,1PE11.4,3H . ,41(1H*))	F15 262 F15 263
166	620	FORMAT (15(1H*),31H GPI GREATER THAN 1.0 AT ESI = ,1PE11.4,3H . ,5F15 10(1H*))	F15 264 F15 265
167		END	F15 266-

SYMBOL	=====	REFERENCES	=====
1	- 6	7*	
2	- 7	9*	
3	- 6	13*	
4	- 13	15*	
5	- 23	26*	
6	- 25	28	30*
7	- 26	32*	
8	- 32	33*	
9	- 20	29	31 35*
10	- 6	37*	
11	- 6	41*	
12	- 45	47*	
13	- 6	53*	
14	- 56	59*	
15	- 58	61	63*
16	- 59	65*	
17	- 62	64	66*
18	- 53	67*	
19	- 6	69*	
20	- 75	78*	
21	- 77	80	82*
22	- 78	84*	
23	- 84	85*	
24	- 81	83	87*
25	- 72	88*	
26	- 6	90*	
27	- 90	94*	
28	- 95	103*	
29	- 6	106*	
30	- 106	107*	146
31	- 107	110*	
32	- 112	113*	
33	- 116	119*	
34	- 106	124*	145
35	- 124	127*	
36	- 129	130*	
37	- 133	136*	
38	- 140	142*	
39	- 106	144*	
601	- 11WR	17WR	69WR 147*
602	- 18WR	70WR	148*
603	- 38WR	149*	
604	- 39WR	150*	
605	- 42WR	151*	
606	- 43WR	152*	
607	- 48WR	153*	
608	- 92WR	154*	
609	- 93WR	155*	

SUBROUTINE FIL15(N)

610	-	94WR	156*								
611	-	108WR	125WR	157*							
612	-	110WR	127WR	158*							
613	-	111WR	128WR	159*							
614	-	113WR	130WR	160*							
615	-	117WR	134WR	161*							
616	-	118WR	135WR	162*							
617	-	120WR	137WR	163*							
618	-	121WR	138WR	164*							
619	-	141WR	165*								
620	-	142WR	166*								
A	-	5CO	49=	63	85AG	96=					
A1	-	46=	48	49	51=						
A2	-	47=	49	50=							
A3	-	63=	65AG	66	67=						
ABS	-	48	92	93	111	128					
B	-	3CO	110	113	117	118	119	127	130	134	135
		136	141	142							
C1	-	3CO	110	111	127	128					
C2	-	3CO	42	43	88						
CDUN	-	2CO									
EK	-	4CO	14=	17	18	25	26	28	34AG	43	58
		59	61	65AG	98=						
ES	-	4CO									
ESEGPR	-	19	71	115	132						
ETAB	-	4CO	8=	11	18	25	26	28	34AG	58	59
		61	65AG	70	77	78	80	86AG	92WR	93WR	94
		97=									
ETH	-	4CO	11	17	42	69					
FIL15	-	1									
FLOAT	-	144									
I	-	7	8	9	13	14	15	20	25	26	28
		30	34AG	35	45	46	47	53	58	59	61
		65AG	66	72	77	78	80	82	86AG	87	88
		90	91	92WR	93	94	95	96	97	98	99
		100	101	102	103	112	113	116	117	118	119
		129	130	133	134	135	136	140	141	142	
INT	-	33=	34AG	85=	86AG						
J	-	23	25	26	32	33	56	58	59	75	77
		78	84	85							
JNT	-	3CO	33	39	85						
K	-	22=	24=	27=	30	33	34AG	55=	57=	60=	63
		65AG	74=	76=	79=	82	85	86AG			
L	-	21=	23	44=	45	54=	56	73=	75		
L1	-	3CO									
L2	-	3CO									
LG	-	2CO	106	114AG	131AG						
MAT	-	3CO									
MF	-	3CO									
MT	-	3CO	11	17	42	69	93	94	111	128	

SUBROUTINE FIL15(N)

N	-	1AG	6								
N1	-	3C0	32	39	84	107	109=	112	113	116	124
		126=	129	130	133	140	144				
N1X	-	3C0									
N2	-	3C0	7	10	13	16	21	28	37	44	54
		01	70	73	80	109	126	144			
N2X	-	3C0									
NBT	-	3C0	33	85							
NC	-	2C0									
ND	-	2C0									
NE	-	2C0	37=	38							
NI	-	2C0	41=	43	49	104=					
NK	-	2C0									
NP	-	2C0	16=	18	38						
NS	-	3C0									
NS1	-	2C0									
NTAB	-	2C0	10=	18	20	53	70	72	90		
Q	-	4C0	93	94	111	128					
RATIO	-	144=	145								
RECS	-	3C0									
RETURN	-	12	36	40	52	68	89	105	123	143	
SAV15	-	5C0									
SAVE	-	4C0									
STATE	-	114	131								
TERP1	-	34	65	86							
TP	-	119=	120	121	122=	136=	137	138	139=		
X	-	3C0	8	14	46	47	69	70	77	78	80
		06AG									
Y	-	3C0	9	15	46	47	82	86AG			
YCAL	-	4C0	35=	87=	91	92WR	100=				
YDIFF	-	91=	92								
YK	-	4C0	15=	30	34AG	102=					
YKTAB	-	4C0	30=	34AG	35	66	82=	86AG	87	88	101=
YTAB	-	4C0	9=	91	92WR	99=					
YTIL	-	4C0	66=	88=	93	94	103=				

SUBROUTINE ESEGPR(N)

1	SUBROUTINE ESEGPR(N)	ESG	1
2	COMMON/COUN/LG,NC,ND,NE,NI,NK,NP,NTAB,NS1	ESG	2
3	COMMON/RECS/MAT,MF,MT,C1,C2,L1,L2,N1,N2,NBT(100),JNT(100),X(2000),	ESG	3
	1 Y(2000),B(2000),N1X,N2X,NS	ESG	4
4	COMMON/ESEG/NPS,NESEGR(300),ESP(2000),EGP(2000),NPU(2000)	ESG	5
5	GO TO (1,2,6,10,14), N	ESG	6
	C	ESG	7
	C-----STORE 1 ES-EG PAIR FROM FILE 14.	ESG	8
	C	ESG	9
6	1 NESEGP(MT) = NESEGP(MT) + 1	ESG	10
7	NPS = NPS + 1	ESG	11
8	ESP(NPS) = C1	ESG	12
9	EGP(NPS) = C2	ESG	13
10	RETURN	ESG	14
	C	ESG	15
	C-----CHECK ES-EG PAIR FROM FILE 15.	ESG	16
	C OPTION 1	ESG	17
	C	ESG	18
11	2 IF (NESEGP(MT) .EQ. 0) GO TO 5	ESG	19
12	M = MT - 1	ESG	20
13	DO 3 I = 1, M	ESG	21
14	3 NTB = NTB + NESEGP(I)	ESG	22
15	I1 = NTB + 1	ESG	23
16	I2 = NTB + NESEGP(MT)	ESG	24
17	DO 4 I = I1, I2	ESG	25
18	4 IF (ESP(I).EQ.C1 .AND. EGP(I).EQ.C2) NPU(I) = 1	ESG	26
19	5 RETURN	ESG	27
	C	ESG	28
	C OPTION 2, LG = 1	ESG	29
	C	ESG	30
20	6 IF (NESEGP(MT) .EQ. 0) GO TO 9	ESG	31
21	M = MT - 1	ESG	32
22	DO 7 I = 1, M	ESG	33
23	7 NTB = NTB + NESEGP(I)	ESG	34
24	I1 = NTB + 1	ESG	35
25	I2 = NTB + NESEGP(MT)	ESG	36
26	DO 8 I = 1, N1, 2	ESG	37
27	DO 8 J = I1, I2	ESG	38
28	EG = C1 - B(I)	ESG	39
29	8 IF (ESP(J).EQ.C1 .AND. EGP(J).EQ.EG) NPU(I) = 1	ESG	40
30	9 RETURN	ESG	41
	C	ESG	42
	C OPTION 2, LG = 2	ESG	43
	C	ESG	44
31	10 IF (NESEGP(MT) .EQ. 0) GO TO 13	ESG	45
32	M = MT - 1	ESG	46
33	DO 11 I = 1, M	ESG	47
34	11 NTB = NTB + NESEGP(I)	ESG	48
35	I1 = NTB + 1	ESG	49
36	I2 = NTB + NESEGP(MT)	ESG	50

37	DO 12 I = 1, N1, 3	ESG 51
38	DO 12 J = 11, I2	ESG 52
39	EG = C1 = B(I)	ESG 53
40	12 IF (ESP(J).EQ.C1 .AND. EGP(J).EQ.EG) NPU(I) = .1	ESG 54
41	13 RETURN	ESG 55
	C	ESG 56
	C-----CHECK ALL ES=EG PAIRS USED.	ESG 57
	C	ESG 58
42	14 DO 17 I = 1, NPS	ESG 59
43	IF (NPU(I) .EQ. 1) GO TO 17	ESG 60
44	DO 15 J = 1, 300	ESG 61
45	K = J	ESG 62
46	NTB = NTB + NESEGP(I)	ESG 63
47	15 IF (NTB .GE. 1) GO TO 16	ESG 64
48	16 WRITE (6,601) K,ESP(I),EGP(I)	ESG 65
49	NTB = 0	ESG 66
50	17 CONTINUE	ESG 67
51	RETURN	ESG 68
52	601 FORMAT (15(1H*),41H THE FOLLOWING ES=EG PAIR, GIVEN IN MT = ,13,34	ESG 69
	1H , WAS NOT REFERENCED IN FILE 15. ,17(1H*)/15(1H*),6H ES = ,1PE12	ESG 70
	1.5,21X,6H EG = ,1PE12.5,21X,17(1H*))	ESG 71
53	END	ESG 72-

SUBROUTINE ESEGPR(N)

SYMBOL	REFERENCES
1	5 6*
2	5 11*
3	13 14*
4	17 18*
5	11 19*
6	5 20*
7	22 23*
8	26 27 29*
9	20 30*
10	5 31*
11	33 34*
12	37 38 40*
13	31 41*
14	5 42*
15	44 47*
16	47 48*
17	42 43 50*
601	48WR 52*
B	3CO 28 39
C1	3CO 8 18 28 29 39 40
C2	3CO 9 18
CDUN	2CO
EG	28= 29 39= 40
EGP	4CO 9= 18 29 40 48WR
ESEG	4CO
ESEGPR	1
ESP	4CO 8= 18 29 40 48WR
I	13 14 17 18 22 23 26 28 29 33 34 37 39 40 42 43 46 47 48WR
I1	15= 17 24= 27 35= 38
I2	16= 17 25= 27 36= 38
J	27 29 38 40 44 45
JNT	3CO
K	45= 48WR
L1	3CO
L2	3CO
LG	2CO
M	12= 13 21= 22 32= 33
MAT	3CO
MF	3CO
MT	3CO 6 11 12 16 20 21 25 31 32 36
N	1AG 5
N1	3CO 26 37
N1X	3CO
N2	3CO
N2X	3CO
NBT	3CO

SUBROUTINE ESEGPR(N)

NC	-	200									
ND	-	200									
NE	-	200									
NESEGP	-	400	6=	11	14	16	20	23	25	31	34
		36	46								
NI	-	200									
NK	-	200									
NP	-	200									
NPS	-	400	7=	8	9	42					
NPU	-	400	18=	29=	40=	43					
NS	-	300									
NS1	-	200									
NTAB	-	200									
NTB	-	14=	15	16	23=	24	25	34=	35	36	46=
		47	49=								
RECS	-	300									
RETURN	-	10	19	30	41	51					
X	-	300									
Y	-	300									

1	SUBROUTINE STATE(LG)	STA	1
2	COMMON/RECS/MAT,MF,MT,C1,C2,L1,L2,N1,N2,NBT(100),JNT(100),X(2000),	STA	2
	1 Y(2000),B(2000),N1X,N2X,NS	STA	3
3	COMMON/SAVE/ETH(300),E(300),ETAB(2000),YTAB(2000),YKTAB(2000),	STA	4
	1 YCAL(2000),YFIL(2000),EK(2000),YK(2000),ES(40)	STA	5
	C	STA	6
	C-----STORE ES.	STA	7
	C	STA	8
4	IF (MT.LE.4 .OR. (MT.GE.15 .AND. MT.LE.50) .OR. MT.GE.81) GO TO 3	STA	9
5	IF (MT.GE.5 .AND. MT.LE.14) NOST = MT - 4	STA	10
6	IF (MT.GE.51 .AND. MT.LE.80) NOST = MT - 40	STA	11
7	ES(NOST) = C1	STA	12
	C	STA	13
	C-----TEST ES.	STA	14
	C FOR LG = 1, N = 2.	STA	15
	C FOR LG = 2, N = 3.	STA	16
	C	STA	17
8	N = LG + 1	STA	18
9	DO 2 I = 1, N1, N	STA	19
10	DO 1 J = 1, NOST	STA	20
11	1 IF (B(I) .EQ. ES(J)) GO TO 2	STA	21
12	IF (B(I) .EQ. 0.0) GO TO 2	STA	22
13	WRITE (6,601) B(I)	STA	23
14	2 CONTINUE	STA	24
15	3 RETURN	STA	25
16	601 FORMAT (15(1H*),56H ESI MUST BE EQUAL TO ONE OF THE PREVIOUS STATE	STA	26
	1 LEVELS. ,39(1H*)/15(1H*),23H THE ESI IN QUESTION = ,1PE11.4,22X,3	STA	27
	19(1H*))	STA	28
17	END	STA	29-

SUBROUTINE STATE(LG)

SYMBOL	REFERENCES
1	10 11*
2	9 11 12 14*
3	4 15*
601	13WR 16*
B	2CO 11 12 13WR
C1	2CO 7
C2	2CO
EK	3CO
ES	3CO 7= 11
ETAB	3CO
ETH	3CO
I	9 11 12 13WR
J	10 11
JNT	2CO
L1	2CO
L2	2CO
LG	1AG 8
MAT	2CO
MF	2CO
MT	2CO 4 5 6
N	8= 9
N1	2CO 9
N1X	2CO
N2	2CO
N2X	2CO
NBT	2CO
NOST	5= 6= 7 10
NS	2CO
Q	3CO
RECS	2CO
RETURN	15
SAVE	3CO
STATE	1
X	2CO
Y	2CO
YCAL	3CO
YK	3CO
YKTAB	3CO
YTAB	3CO
YTIL	3CO

SUBROUTINE TEST2C(MT)

1	SUBROUTINE TEST2C(MT)	T2C	1
	C=====TEST REACTION TYPE, MT, FOR FILE 14=====	T2C	2
	C MT MUST BE IN THE RANGE 3-29, 51-80, 101-108, 110, 301-450	T2C	3
2	COMMON/TST2C/NIN,NOUT,NPUN,NT,MAT,MF,MM,NSEQ,LRD,LFI,LOD,LFP,ZA,AWT2C	T2C	4
	1R,MATP,MFP,MTP,NSEQP,NOPT,NSEQP1	T2C	5
3	NOUT = 6	T2C	6
4	NOPT = 0	T2C	7
5	10 IF(MT-3)150,20,20	T2C	8
6	20 IF(MT-29)170,170,30	T2C	9
7	30 IF(MT-51)150,40,40	T2C	10
8	40 IF(MT-80)170,170,50	T2C	11
9	50 IF(MT-101)150,60,60	T2C	12
10	60 IF(MT-108)170,170,70	T2C	13
11	70 IF(MT-110)150,170,80	T2C	14
12	80 IF(MT-301)150,90,90	T2C	15
13	90 IF(MT-450)170,170,150	T2C	16
14	150 IF(NOPT,EQ,0)GO TO 152	T2C	17
15	WRITE(NOUT,151)MT,NSEQP	T2C	18
16	151 FORMAT(37X,3HMT=14,29M INCORRECT SEQUENCE NUMBER,2X,16)	T2C	19
17	GO TO 170	T2C	20
18	152 WRITE(NOUT,153)MT	T2C	21
19	153 FORMAT(37X,3HMT=14,10M INCORRECT)	T2C	22
20	170 RETURN	T2C	23
21	END	T2C	24-

SUBROUTINE TEST2C(MT)

SYMBOL	REFERENCES
10	5*
20	5 6*
30	6 7*
40	7 8*
50	8 9*
60	9 10*
70	10 11*
80	11 12*
90	12 13*
150	5 7 9 11 12 13 14*
151	15WR 16*
152	14 18*
153	18WR 19*
170	6 8 10 11 13 17 20*
AWR	2C0
LDD	2C0
LFI	2C0
LFP	2C0
LRD	2C0
MAT	2C0
MATP	2C0
MF	2C0
MFP	2C0
MM	2C0
MT	1AG 5 6 7 8 9 10 11 12 13 15WR 18WR
MTP	2C0
NIN	2C0
NOPT	2C0 4= 14
NOUT	2C0 3= 15WR 18WR
NPUN	2C0
NSEQ	2C0
NSEQP	2C0 15WR
NSEQP1	2C0
NT	2C0
RETURN	20
TEST2C	1
TST2C	2C0
ZA	2C0

I N D E X
 END OF COMPUTATION.

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13. ABSTRACT Evaluations of neutron interaction and photon production cross sections for sodium, magnesium, chlorine, potassium, and calcium have been translated from a modified-UK format into ENDF/B format. The data have been reviewed and revised to a minor extent, and can be used by the LAPH code to generate multigroup photon production cross section matrices. All data sets have been transmitted to the University of California, Los Alamos Scientific Laboratory, to the National Neutron Cross Section Center at BNL, and to the Radiation Shielding Information Center at ORNL. Several "physics" checks have been proposed for the photon data, and a FORTRAN IV code, PHOX, has been written to incorporate some of these checks.			

14. KEY WORDS	LINK A		LINK B		LINK C	
	ROLE	WT	ROLE	WT	ROLE	WT
neutron interaction cross sections						
photon production cross sections						
sodium						
magnesium						
chlorine						
potassium						
calcium						
photon data checking code						
ENDF/B format						

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